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# Effective removal of bromate in nitrate-reducing anoxic zones during managed aquifer recharge for drinking water treatment

# Laboratoryscale simulations

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# Effective removal of bromate in nitrate-reducing anoxic zones during managed aquifer recharge for drinking water treatment: Laboratoryscale simulations



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#### ABSTRACT

The removal of bromate  $(BrO_3^-)$  as a by-product of ozonation in subsequent managed aquifer recharge (MAR) systems, specifically in anoxic nitrate  $(NO_3^-)$ -reducing zones, has so far gained little attention. In this study, batch reactors and columns were used to explore the influence of  $NO_3^-$  and increased assimilable organic carbon (AOC) due to ozonation pre-treatment on  $BrO_3^-$  removal in MAR systems. 8 m column experiments were carried out for 10 months to investigate  $BrO_3^-$  behavior in anoxic  $NO_3^-$ -reducing zones of MAR systems. Anoxic batch experiments showed that an increase of AOC promoted microbial activity and corresponding  $BrO_3^-$  removal. A drastic increase of  $BrO_3^-$  biodegradation was observed in the sudden absence of  $NO_3^-$  in both batch reactors and columns, indicating that  $BrO_3^-$  and  $NO_3^-$  competed for biodegradation by denitrifying bacteria and  $NO_3^-$  was preferred as an electron acceptor under the simultaneous presence of  $NO_3^-$  in  $NO_3^-$  reducing anoxic column,  $BrO_3^-$  removal gradually decreased, indicating that the presence of  $NO_3^-$  is a precondition for denitrifying bacteria to reduce  $BrO_3^-$  in  $NO_3^-$  reducing anoxic zones. In the 8 m anoxic column set-up (retention time 6 days), the  $BrO_3^-$  removal achieved levels as low as  $1.3 \ \mu g/L$ , starting at  $60 \ \mu g/L$  (98% removal). Taken together,  $BrO_3^-$  removal is likely to occur in vicinity of  $NO_3^-$ -reducing anoxic zones, so MAR systems following ozonation are potentially effective to remove  $BrO_3^-$ .

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### 1. Introduction

Managed aquifer recharge (MAR), such as artificial recharge and dune filtration, is a natural water treatment process that induces surface water to flow through the soil. After soil passage, the water is abstracted by vertical or horizontal wells (Bouwer, 2002; Tufenkji et al., 2002). In some European countries, water utilities use MAR as a robust and cost-effective water treatment process to supply drinking water without needing to use chlorination as a disinfection process because of its pathogen removal ability (Lekkerkerker, 2012; Maeng, 2010; Van der Hoek et al., 2014). Additionally, MAR

\* Corresponding author. E-mail addresses: wff1986@163.com, f.wang-2@tudelft.nl (F. Wang). has proven to be an effective barrier for multiple organic micropollutants (OMPs) present in surface waters during drinking water production due to filtration, sorption, ion-exchange, precipitation and biological degradation (Kim et al., 2015; Laws et al., 2011; Postigo and Barceló, 2015). However, some highly persistent trace organic compounds can still be detected in MAR filtrate (Drewes et al., 2003) and may reach the drinking water supply (Ternes et al., 2002).

Ozonation is a powerful process for the removal of many OMPs, and the combination of MAR with ozonation as a pre-treatment has been suggested as a comprehensive treatment system to effectively remove various OMPs during drinking water production (Lekkerkerker-Teunissen et al., 2012; Lekkerkerker et al., 2009; Oller et al., 2011). However, bromate  $(BrO_3^-)$ , a genotoxic





WATER RESEARCH carcinogen (Ahmad et al., 2013), may be formed when ozonation is applied in the treatment of bromide-containing water (Assuncao et al., 2011; Haag and Holgne, 1983; Kurokawa et al., 1990). WHO, USEPA, and the European Union have set drinking water regulations for the maximum allowable concentration of  $BrO_3^-$  at 10 µg/L (Carney, 1991; EU, 1998; Forum, 2005; WHO, 2011).

 $BrO_{\overline{3}}$  cannot be easily eliminated using conventional treatment technologies due to its high solubility and stability in water (Butler et al., 2005) and its weak sorption characteristics to common soil and sediment components. Several studies involving different chemical, physical and biological techniques have been conducted (Bhatnagar and Sillanpää, 2012; Hijnen et al., 1999; Jia et al., 2015; Wang et al., 2009; Xu et al., 2015a; Zhang et al., 2015). Microbial  $BrO_{\overline{3}}$  reduction may be an effective treatment strategy because microbiological reduction of BrO<sub>3</sub> has been observed in anaerobic activated sludge columns, biologically active carbon filters and denitrifying bioreactors (Hijnen et al., 1999; Kirisits et al., 2001; Van Ginkel et al., 2005). The study of Van Ginkel et al. (2005) showed that  $BrO_3^-$  reduction was detected only in the absence of  $O_2$  in a microbial culture from activated sludge. However, some other studies found that  $BrO_3^-$  reduction could also take place in the presence of O<sub>2</sub>. For example, a biological activated carbon (BAC) filter almost completely reduced 60  $\mu g/L\,BrO_3^-$  to  $Br^-$  at both 2 and 8 mg/L influent dissolved oxygen (DO) concentrations (Liu et al., 2012). Therefore, redox condition may be one of the important factors impacting BrO3 removal in MAR systems. Hijnen et al. (1995) isolated denitrifying organisms that were able to reduce  $BrO_3^-$  with ethanol as the electron donor and carbon source. Hijnen et al. (1999) showed that  $BrO_3^-$  was removed in a denitrifying bioreactor fed with methanol. However, they demonstrated that  $BrO_{\overline{3}}$  removal in a denitrifying bioreactor did not seem to be a realistic option in drinking water treatment due to the long contact times required for  $BrO_3^-$  removal and extensive post treatment necessary to remove excessive methanol and released biomass. The anoxic zone within MAR systems might be effective in reducing  $BrO_{\overline{3}}$ , as retention times in the subsurface are days to months. However, there has been only one study (Hübner et al., 2012) concerning the removal of BrO<sub>3</sub> in MAR systems since Hijnen et al. (1999) and Kruithof and Meijers (1995) mentioned that soil passage under anoxic conditions, such as artificial recharge and river bank filtration, may enable BrO<sub>3</sub><sup>-</sup> removal from ozonated water. Only recently, Hübner et al. (2016) studied BrO<sub>3</sub> removal in 1 m sand columns, with a focus on treatment of secondary effluent (wastewater) instead of drinking water treatment. They observed that  $BrO_3^-$  was effectively reduced under anoxic conditions instead of oxic conditions and that NO3 and BrO3 were consumed as electron acceptors simultaneously in small-scale columns. However, because microbial biodegradation in secondary effluent differs given high dissolved organic carbon (DOC) and  $NO_3^-$  concentrations, these findings cannot be directly translated to surface water infiltration sites for drinking water production. Water composition (e.g.  $NO_3^-$ ,  $SO_4^{2-}$ ,  $ClO_3^-$  and  $ClO_4^-$ ) is known to affect  $BrO_3^-$  reduction in reactors (Demirel et al., 2014; Fan et al., 2006; Kirisits et al., 2001; Xu et al., 2015b), so it is likely to affect biological  $BrO_3^-$  reduction during MAR as well.

Several microbial  $BrO_3^-$  conversion pathways have been described in literature.  $BrO_3^-$  was reduced to bromide by denitrifying and  $ClO_3^-$ -reducing enrichments, possibly via co-metabolic action of  $NO_3^-$  reductase and  $ClO_3^-$  reductase enzymes (Downing and Nerenberg, 2007). Other studies suggested the existence of a specific  $BrO_3^-$  reduction pathway (Davidson et al., 2011). Additionally, the aerobically expressed selenate reductase of *Enterobacter cloacae* is capable of low rates of  $BrO_3^-$  reduction (Ridley et al., 2006), indicating that oxic bacteria might also be capable of  $BrO_3^-$ 

reduction. Therefore, although different  $BrO_3^-$  removal pathways have been identified, it is unknown whether these pathways exist during MAR soil passage.

The objectives of this study were to explore the BrO<sub>3</sub><sup>-</sup> removal in NO<sub>3</sub><sup>-</sup>-reducing anoxic zones of MAR systems and the potential mechanisms behind this removal. Specifically, the influence of (a) increased assimilable organic carbon (AOC) concentrations (due to ozonation pre-treatment) and (b) NO<sub>3</sub><sup>-</sup> long-term presence, sudden absence and long-term absence and (c) BrO<sub>3</sub><sup>-</sup> removal performance with infiltration retention time in 8 m anoxic zones were investigated in order to evaluate the feasibility of BrO<sub>3</sub><sup>-</sup> removal by MAR systems.

#### 2. Materials and methods

#### 2.1. Water and sand

The water used in this study was collected every two weeks from the MAR site of Dunea, a drinking water company in the Netherlands. The composition of MAR influent water is shown in Table S1 in the supplemental information. The sand used in batch reactors and column reactors was collected from a 1 m depth from the MAR site of Dunea. Chemicals NaBrO<sub>3</sub>, NaNO<sub>3</sub>, CH<sub>3</sub>COONa, K<sub>2</sub>SO<sub>4</sub> and Purolite A520E resin were purchased from Sigma (St Louis, MO, United States). All chemicals were of AR grade. All solutions used in this study were prepared using water from a Millipore Milli-Q system.

#### 2.2. Batch experiments

To investigate the role of increased AOC from ozonation as a pretreatment for MAR and the influence of NO<sub>3</sub> on BrO<sub>3</sub> removal, batch experiments using 15 glass bottles with a volume of 500 mL were performed for approximately 3 months under anoxic conditions. The batch reactors were filled with 100 g sand and 400 mL MAR water. This ratio of MAR water and sand was chosen from previous literature that also focused on MAR studies (Wang et al., 2016). Anoxic conditions were provided by stripping the water with nitrogen gas for 15 min then sealing the bottles with rubber stoppers and plastic caps. All batch reactors were placed in a dark room with temperature control (11.5  $\pm$  0.5 °C). A 60 day acclimation period was necessary to stabilize the batch reactors with respect to DOC removal (fill-and-draw mode during the acclimation period, hydraulic retention time (HRT) 7 d). Next, the 15 bottles were divided into 5 groups with different DOC concentrations and different NO<sub>3</sub> concentrations as shown in Fig. 1a. Three batch reactors as reference (group 1) to distinguish  $BrO_3^-$  adsorption from biological BrO<sub>3</sub> removal in group 2 were autoclaved at 121 °C for 40 min to inactivate bacteria. Ozonation can oxidize a part of DOC into biodegradable DOC, so 1 mg/L of additional C-CH<sub>3</sub>COONa was dosed in group 3 to investigate the effect of ozonation pretreatment on  $BrO_3^-$  removal. The aim of groups 4 and 5 was to assess the effect of the sudden absence of  $NO_3^-$  on  $BrO_3^-$  removal. The microbial community may change in the absence of  $NO_{\overline{3}}$  after a certain time. To achieve  $BrO_3^-$  removal as early as possible before microbial community change, 4 mg/L C-CH<sub>3</sub>COONa was dosed into groups 4 and 5 to promote microbial activity. Also for groups 4 and 5, the concentration of  $NO_3^-$  initially present in the MAR water was measured daily until it fell below the detection limit, 0.89 mg/L. Then, 10 mg/L NO $_3^-$  was dosed to group 4 and not to group 5.60  $\mu$ g/L  $BrO_{\overline{3}}$  was dosed to all batch reactors after the acclimation period and the above described different treatments. BrO<sub>3</sub>, NO<sub>3</sub>, sulfate  $(SO_4^{2-})$ , adenosine triphosphate (ATP) and DOC samples were collected from groups 1-3 at day 7 and day 21. For groups 4 and 5, samples were collected after 2.7 h because of the high microbial a. Batch experiments



Fig. 1. Batch and column experimental designs.

activity in these groups caused by the 4 mg/L C-CH<sub>3</sub>COONa dose.

#### 2.3. Column experiments

All columns (L = 1 m, D = 36 mm) shown in Fig. 1b and c were constructed from PVC (L = 1 m, D = 36 mm). A peristaltic multichannel pump (205 S, Watson Marlow, The Netherlands) using Marprene<sup>®</sup> pump tubes (d = 0.63 mm, Watson Marlow, The Netherlands) was connected to the columns by dark polyamide tubing (d = 2.9 mm, Festo, The Netherlands) to feed both columns. The columns were operated in continuous up-flow mode at 11.5  $\pm$  0.5 °C, corresponding to the natural aquifer temperature, in a dark room to prevent algal growth.

To avoid the leaching of soil/sand grains, both the top and bottom of the column were fitted with perforated PVC plates (30 holes, d = 0.8 mm) that were covered with filter cloth (45  $\mu$ m, Top7even net & mesh, The Netherlands). The oxic column was fed from a 10 L open glass bottle with Dunea MAR influent water, and the anoxic columns were fed from 10 L sealed glass bottles with N<sub>2</sub> flushing as pre-treatment. Feed bottles were washed twice with acetone and flushed several times with demineralized water before refilling to avoid biofilm formation.

Before starting the  $BrO_3^-$  experiment, these columns had been acclimated for 3 months until steady state conditions were reached with respect to DOC removal and  $NO_3^-$  removal.

#### 2.3.1. 1 m oxic and anoxic sand columns

To investigate  $BrO_3^-$  biodegradation performance in oxic zones and anoxic  $NO_3^-$  reducing zones of MAR systems and to study the influence of  $NO_3^-$  on  $BrO_3^-$  removal, column experiments using a 1 m oxic sand column simulating oxic zones and a 1 m anoxic sand column simulating anoxic zones of MAR systems were carried out in the presence and absence of  $NO_3^-$ . The hydraulic retention time was 22 h for both columns, corresponding to a filtration velocity of 1 m/day.

The experiment lasted 13 months in total: a 3 months acclimation period followed by a 10 month period divided into two phases. In the first phase,  $NO_3^-$  was present in the influent water, while in the second phase,  $NO_3^-$  was absent. During the 13 months experiment, 150 µg/L C-CH<sub>3</sub>COONa was dosed to the influent water of both oxic and anoxic columns to simulate the increased AOC from ozonation since, in practice, the ozonation pre-treatment before MAR increases the AOC (Hammes et al., 2006; Orlandini et al., 1997; Sarathy et al., 2011; Van Der Hoek et al., 1998) and as reported by Hammes et al. (2006) 60-90% of the AOC consists of organic acid carbon. BrO<sub>3</sub><sup>-</sup> formation at concentrations ranging from <2 to 293 µg/L has been reported during ozonation of natural waters under normal drinking water treatment conditions (Amy et al., 2000; Glaze et al., 1993; Krasner et al., 1993; Van Der Hoek et al., 1998), but in 100 investigated drinking water utilities  $BrO_3^$ concentration was within the range of <2-60 µg/L after ozonation of water containing 2-429 µg/L Br<sup>-</sup> (Butler et al., 2005; Kirisits and Snoeyink, 1999). For this study it was decided to investigate the upper value of this range, so  $60 \,\mu g/L \, BrO_3^-$  was dosed to the influent of the oxic column and anoxic columns. A summary of  $BrO_3^-$  and AOC formed during ozonation based on existing literature (Agbaba et al., 2016; Escobar and Randall, 2001; Huang and Chen, 2004; Orlandini et al., 1997; Van Der Hoek et al., 1998) is presented in Table S2. The influent water of these columns was  $NO_3^-$  containing MAR water in phase 1, while in phase 2 the influent was  $NO_3^-$  free MAR water.  $NO_3^-$  free water was produced by using a strong base anion exchange resin Purolite A520E (ratio of water and resin: 2 L/ 20 g) to remove  $NO_3^-$  to below the detection limit (0.89 mg/L). The water was in contact with the resin were for a period of 12 h. The ion exchange resin, used to remove NO<sub>3</sub><sup>-</sup> from the MAR water, was pre-treated as follows. Firstly, A520E resin was soaked in both 1 M NaOH solution followed by 1 M HCl solution or one day each to remove impurities. Afterwards, the resin was washed several times using demineralized water until pH 7 was reached. Finally, the clean resin was dried in an oven at 80 °C for 24 h and kept in a desiccator until use. Since Purolite A520E resin removes not only  $NO_3^-$  but also a portion of  $SO_4^{2-}$ , 50 mg/L  $SO_4^{2-}$  was dosed back to the influent water in phase 2. Influent water samples and corresponding effluent water samples were collected every 1-2 weeks during each phase to measure  $BrO_3^-$ ,  $NO_3^-$  and  $SO_4^{2-}$  concentrations. DO concentrations in the influent and effluent of oxic and anoxic columns were measured to confirm oxic and anoxic conditions.

#### 2.3.2. 8 m anoxic columns

A long anoxic column set-up consisting of eight 1 m columns in series was used for 10 months to better simulate anoxic zones of MAR systems since the retention time, 6 days, was much longer than the above 1 m anoxic column in Section 2.3.1. The objective of the long anoxic column was to further investigate  $BrO_3^-$  biodegradation with respect to retention time in anoxic  $NO_3^-$ -reducing zones and to further assess the role of AOC formation, as a result of ozonation pre-treatment, on  $BrO_3^-$  biodegradation. The whole experiment consisted of a 4 months acclimation period followed by two phases with and without an extra 150  $\mu$ g/L C-CH3COONa in the influent water. Each phase was carried out for 3–4 months to establish a stable BrO<sub>3</sub> removal. Water samples were collected 4–7 times at depth 0 m, 1 m, 3 m and 8 m, that is retention time 0, 0.75, 2.25 and 6 days, during each phase to measure BrO<sub>3</sub>, NO<sub>3</sub> and SO<sub>4</sub><sup>2–</sup> concentrations. DO concentrations in the influent were measured to confirm anoxic conditions.

#### 2.4. Sample analysis

Dissolved oxygen (DO), temperature and pH were measured with a multimeter (SenTix<sup>®</sup> 940 IDS probe, Multi 340i, WTW, Germany) directly in the feed bottle or in a flow through cell connected to the influent or effluent tubes of the columns.

 $BrO_3^-$ ,  $NO_3^-$  and  $SO_4^{2-}$  samples were analysed by ion chromatography at Het Waterlaboratorium (Haarlem, The Netherlands). Following ion chromatography, BrO3 was also analysed by conductivity detection. 30 mL samples were pre-treated by filtration on barium and silver loaded on guard columns to remove sulfate and chloride respectively, followed by a H<sup>+</sup> column for the removal of  $Ag^+$  ions leaching from the  $Ag^+$  column. 2000  $\mu$ l of the sample was subsequently concentrated on a positively charged anion exchange column (Dionex IonPac AG9SC). The anions on the ion exchange column were eluted with 1.5 mL/min of a 0.7 mM NaHCO<sub>3</sub> solution and separated on an ion exchange analytical column (Dionex IonPac AS9SC). Detection was performed by using suppressed conductivity. The measured  $BrO_{3}^{-}$  concentration was confirmed using a two point calibrated UV absorption measurement at a wavelength of 200 nm. The  $BrO_{\overline{3}}$  detection limit was 0.5  $\mu$ g/L. NO<sub>3</sub> and SO<sub>4</sub><sup>2-</sup> were analysed with a ProfIC 15 - AnCat ion chromatograph (Metrohm 881 anion (suppressed) and 883 cation system) (Metrohm, Switzerland) after filtering through 0.45 µm filters (Whatman, Germany). A Supp 150/4.0 anion column was used with 3.2 mM Na<sub>2</sub>CO<sub>3</sub> and 1 mM NaHCO<sub>3</sub> eluent for the anions measurement. Regenerant for the suppressor was 50 mM H<sub>2</sub>SO<sub>4</sub>. Detection limits of  $NO_3^-$  and  $SO_4^{2-}$  were 0.89 mg/L and 0.5 mg/L, respectively. DOC was measured with a Shimadzu TOC analyser according to the protocols described in Wang et al. (2016).

#### 3. Results

#### 3.1. Batch reactor experiments

#### 3.1.1. Effect of increased AOC due to ozonation as pre-treatment

Fig. 2 presents BrO<sub>3</sub><sup>-</sup> concentrations over 7 days (Fig. 2a) and 21 days (Fig. 2b) in anoxic batch reactors with MAR water and acetate supplemented MAR water and autoclaved batch reactors with MAR water. In the reference experiments with autoclaved batch reactors, BrO<sub>3</sub><sup>-</sup> degradation over 7 days and 21 days was not observed, indicating BrO<sub>3</sub><sup>-</sup> adsorption did not occur. Therefore, the BrO<sub>3</sub><sup>-</sup> removal was caused by biodegradation instead of adsorption, which is in agreement with the studies of Xie and Shang (2006) and Weast (1986). Though differences were small, bromate removal was found not to be significant (p > 0.05) in MAR water, while removal was observed in acetate supplemented MAR water. Slightly more BrO<sub>3</sub><sup>-</sup> was removed in acetate supplemented MAR water after 21 days (9 µg/L, 16.9%) compared to 7 days (2.4 µg/L, 4.2%).

Fig. 3 presents NO<sub>3</sub><sup>-</sup> concentrations over 7 days (Fig. 3a) and 21 days (Fig. 3b) in anoxic batch reactors with MAR water (group 2) and acetate supplemented MAR water (group 3). NO<sub>3</sub><sup>-</sup> was not significantly biodegraded in MAR water (p > 0.05), while NO<sub>3</sub><sup>-</sup> was biodegraded in acetate supplemented MAR water over 7 days



Fig. 2.  $BrO_3^-$  removal in autoclaved and non-autoclaved batch reactors with MAR water and acetate supplemented MAR water over 7 days (a) and 21 days (b). An additional 1 mg/L AOC from CH<sub>3</sub>COONa solution was added to MAR water to create the acetate supplemented MAR water. All batch reactors were in anoxic conditions at 11.5 ± 0.5 °C (n = 3).



Fig. 3. NO<sub>3</sub> removal in anoxic batch reactors with MAR water and simulated ozonation-MAR water over 7 days (a) and 21 days (b). An additional 1 mg/L AOC from CH<sub>3</sub>COONa solution was added to MAR water to create the acetate supplemented MAR water.  $T = 11.5 \pm 0.5$  °C (n = 3).

(2.6 mg/L, 22.7%. p < 0.05), and at a greater magnitude after 21 days (17.8 mg/L, 87.8%. p < 0.05). These results demonstrate that the retention time as well as the availability of AOC is an important factor influencing BrO<sub>3</sub> and NO<sub>3</sub> biodegradation, with NO<sub>3</sub> degradation occurring faster than BrO<sub>3</sub> degradation.

#### 3.1.2. Presence of $NO_3^-$

The influence of NO<sub>3</sub><sup>-</sup> on BrO<sub>3</sub><sup>-</sup> removal was investigated in anoxic batch reactors containing acetate supplemented MAR water in the presence and sudden absence of NO<sub>3</sub><sup>-</sup> (Fig. 4). No BrO<sub>3</sub><sup>-</sup> biodegradation (p > 0.05) was observed in batch reactors with an initial NO<sub>3</sub><sup>-</sup> concentration of 6.1 mg/L, while a clear decrease of NO<sub>3</sub><sup>-</sup> (p < 0.05) from 6.1 mg/L to 3.8 mg/L was observed after 2.7 h. In case of a sudden absence of NO<sub>3</sub><sup>-</sup> in the batch reactors (lower than 0.89 mg/L), BrO<sub>3</sub><sup>-</sup> was reduced from 47 µg/L to 35 µg/L in 2.7 h (p < 0.05), indicating that NO<sub>3</sub><sup>-</sup> and BrO<sub>3</sub><sup>-</sup> compete for biodegradation.

#### 3.2. 1 m column experiments

## 3.2.1. Oxic and anoxic zones

The removal of  $BrO_3^-$ ,  $NO_3^-$  and  $SO_4^{2-}$  in 1 m oxic and anoxic



**Fig. 4.** BrO<sub>3</sub><sup>-</sup> and NO<sub>3</sub><sup>-</sup> removal in batch reactors with acetate supplemented MAR water in the presence and sudden absence of NO<sub>3</sub><sup>-</sup> within 2.7 h \* indicates measurements below the detection limit. T = 11.5  $\pm$  0.5 °C (n = 3).

columns (retention time 22 h) for 98 days are shown in Fig. 5. BrO<sub>3</sub><sup>-</sup> removal was slightly higher in the anoxic column (8%) than in the oxic column (5.7%), although the difference was not significant (p < 0.05). 10.7% NO<sub>3</sub><sup>-</sup> was removed in the anoxic column, indicating anoxic conditions were indeed reached. In the oxic column, NO<sub>3</sub><sup>-</sup> was not converted and passed through the column. No significant SO<sub>4</sub><sup>2-</sup> removal in both oxic and anoxic columns was observed, so neither columns reached SO<sub>4</sub><sup>2-</sup>-reducing conditions.

#### 3.2.2. Effect of $NO_3^-$

The 1 m columns were operated in two subsequent phases: during phase 1 (day 0–98),  $10.3 \pm 1.8 \text{ mg/L NO}_3^-$  was present in the influent, whereas during phase 2 (day 98–209),  $NO_3^-$  was extracted from the influent until the concentration was lower than 0.89 mg/L. Fig. 6 presents  $BrO_3^-$  removal in the oxic and anoxic columns with long-term presence and absence of NO<sub>3</sub>. During phase 1, the  $BrO_3$ removal in the oxic column (1.3-11.2%) and anoxic column (3.9–11.7%), with a 22 h retention time, was not highly effective. However, during phase 2, the sudden absence of  $NO_3^-$  in the influent water at day 98 resulted in sharp initial increases of  $BrO_{\overline{3}}$ reduction (82.5% in anoxic column and 13.6% in oxic column), after which BrO<sub>3</sub><sup>-</sup> removal decreased to 61.4% in the anoxic column and 0.32% in the oxic column in day 98-99.5. After that, the oxic column had a very limited  $BrO_3^-$  removal of 0–3.3% lower than that in the presence of  $NO_3^-$ , whereas the  $BrO_3^-$  removal in the anoxic column gradually decreased and finally returned to a steady 5.5-12.9% during 99.5-209 days.

#### 3.3. 8 m column experiments

#### 3.3.1. Effect of infiltration retention time

In order to investigate the effect of infiltration retention time during MAR, a series of columns (8 m total, 6 days retention time) was operated with MAR influent water for several months. Fig. 7 presents the continuous BrO<sub>3</sub> removal during the final 2 months for 1, 3 and 8 m infiltration depth. In the first 1 m (corresponding to a retention time of 0.75 day), no clear BrO<sub>3</sub> and NO<sub>3</sub> removal was observed. After 3 m infiltration (corresponding to a retention time of 2.25 days), BrO<sub>3</sub> and NO<sub>3</sub> remaining concentrations were clearly lower than the influent concentrations with 20.4% BrO<sub>3</sub> and 15.8% NO<sub>3</sub> removal. After 8 m of soil passage, 48.2% BrO<sub>3</sub> and 30.2% NO<sub>3</sub>



**Fig. 5.** BrO<sub>3</sub><sup>-</sup>, NO<sub>3</sub><sup>-</sup> and SO<sub>4</sub><sup>2-</sup> removal in oxic and anoxic columns with acetate supplemented MAR water as the influent. 150  $\mu$ g/L AOC from CH<sub>3</sub>COONa solution was added to MAR water to compose the acetate supplemented MAR water. The concentrations of BrO<sub>3</sub>, NO<sub>3</sub><sup>-</sup> and SO<sub>4</sub><sup>2-</sup> were 58.9  $\pm$  3.1  $\mu$ g/L, 10.3  $\pm$  1.8 mg/L and 51.9  $\pm$  10.1 mg/L respectively. T = 11.5  $\pm$  0.5 °C. n = 5.



**Fig. 6.** BrO<sub>3</sub><sup>-</sup> removal in the 1 m oxic and anoxic columns containing acetate supplemented MAR water as influent with  $10.3 \pm 1.8 \text{ mg/L} \text{ NO}_3^-$  (phase 1: 0–98 days) and acetate supplemented MAR water as influent with NO<sub>3</sub><sup>-</sup> below than detection limit (0.89 mg/L) (phase 2: 98–209 days). 150 µg/L AOC from a CH<sub>3</sub>COONa solution was added to the MAR water to compose acetate supplemented MAR water. The dashed line at day 98 separates phase 1 and phase 2. Influent BrO<sub>3</sub><sup>-</sup> was 56.6 ± 6.45 µg/L. Influent DO in the oxic column and anoxic column was 8.52–10.74 mg/L and below 0.6 mg/L respectively. T = 11.5 ± 0.5 °C.



**Fig. 7.** BrO<sub>3</sub><sup>-</sup> removal and normalized concentrations of BrO<sub>3</sub><sup>-</sup> and NO<sub>3</sub><sup>-</sup> in the 8 m anoxic column set-up containing MAR water as the influent. BrO<sub>3</sub><sup>-</sup> and NO<sub>3</sub><sup>-</sup> in the influent were 63 ± 4 µg/L and 13 ± 3.8 mg/L respectively. Influent DO was below 0.6 mg/L, T = 11.5 ± 0.5 °C.

were removed and the. Final  $BrO_3^-$  concentration reached with a retention time of 6 days was 29.6  $\mu$ g/L.

#### 3.3.2. Effect of increased AOC due to ozonation pre-treatment

Fig. 8 presents concentrations of BrO<sub>3</sub>, NO<sub>3</sub> and SO<sub>4</sub><sup>-</sup> along the column height of the 8 m anoxic columns in series containing acetate supplemented MAR water (phase 1, Fig. 8a) and MAR water (phase 2, Fig. 8b), respectively. Fig. 8a shows that BrO<sub>3</sub> was removed by 8%, 59% and 98%, at a depth of 1 m, 3 m and 8 m, respectively. NO<sub>3</sub> was removed by 8%, 51% and 80% at a depth of 1 m, 3 m and 8 m, respectively. NO<sub>3</sub> was removed by 8%, 51% and 80% at a depth of 1 m, 3 m and 8 m, respectively. Consequently, at the end of the 8 m column, corresponding to an infiltration retention time of 6 days, the BrO<sub>3</sub> concentration was as low as 1.3 µg/L and the NO<sub>3</sub> concentration was 1.1 mg/L. No SO<sub>4</sub><sup>-</sup> removal was observed in this column set-up with and without the increased AOC concentration as a result of ozonation pre-treatment, indicating no SO<sub>4</sub><sup>2</sup><sup>-</sup> reducing conditions were reached. Comparison of the NO<sub>3</sub> and



**Fig. 8.** Average concentrations (n = 5–8) of BrO<sub>3</sub>, NO<sub>3</sub> and SO<sub>4</sub><sup>2</sup> with depth in the 8 m anoxic column during phase 1 with acetate supplemented MAR water (a) and during phase 2 with only MAR water (b). 150  $\mu$ g/L AOC from CH<sub>3</sub>COONa solution was added to MAR water to compose the acetate supplemented MAR water. BrO<sub>3</sub>, NO<sub>3</sub> and SO<sub>4</sub><sup>2</sup> concentrations in the influent water were 61.83 ± 5.18  $\mu$ g/L, 10.7 ± 6 mg/L and 52.5 ± 8.5 mg/L. Mostly, influent DO was below 0.6 mg/L. T = 11.5 ± 0.5 °C.

 $BrO_3^-$  removal efficiencies of the two phases consistently shows better  $BrO_3^-$  and  $NO_3^-$  removal over the height of the column, indicating that the addition of 150  $\mu g/L$  C-CH3COONa resulted in substantially higher  $BrO_3^-$  and  $NO_3^-$  removals.

#### 4. Discussion

#### 4.1. Role of $NO_3^-$ in $BrO_3^-$ removal

As stated in the introduction, it has been reported by other authors that biological  $BrO_3^-$  reduction is a side reaction of the  $NO_3^$ reduction pathway (Butler et al., 2005; Korom, 1992), and  $BrO_3^-$  can be biodegraded by several other anoxic bacteria instead of denitrifying bacteria (Davidson et al., 2011). Both anoxic batch reactors and 1 m anoxic column experiments showed that  $BrO_{\overline{3}}$  removal in the presence of  $NO_3^-$  was low and  $NO_3^-$  biodegradation was higher, indicating that  $BrO_{\overline{3}}$  biodegradation can occur in the presence of NO<sub>3</sub>. BrO<sub>3</sub> removal suddenly increased due to the sudden absence of NO<sub>3</sub>, indicating that  $BrO_3$  and NO<sub>3</sub> in MAR systems may compete for biodegradation by denitrifying bacteria, and denitrifying bacteria prefer  $NO_{\overline{3}}$  over  $BrO_{\overline{3}}$  although the biodegradation of  $NO_3^-$  and  $BrO_3^-$  occur simultaneously in anoxic  $NO_3^-$ -reducing zones. In Fig. 8, the  $BrO_3^-$  biodegradation rate may initially appear higher than  $NO_3^-$  biodegradation rate in 1–8 m, but actually the mass of  $NO_3^-$  reduction (phase 1: 2.02 mg/L/m in 1–8 m, phase 2: 0.63 mg/L/m in 1–8 m) was much higher than the mass of  $BrO_3^$ biodegradation (phase 1: 20.59  $\mu$ g/L/m, phase 2: 10.27  $\mu$ g/L/m in 1-8 m).

Some studies demonstrated the potential role of  $NO_3^-$  reductase in BrO<sub>3</sub><sup>-</sup> reduction (Davidson et al., 2011; Hijnen et al., 1995). It can be observed from Fig. 8 that both  $NO_3^-$  and  $BrO_3^-$  biodegradation rates in the first 1 m column passage were lower than from 1 to 3 m. One potential explanation for this result is that even if the anoxic condition were achieved in the first 1 m, DO became lower with increasing retention time and resulted in more active  $NO_3^-$  reductase (Bell et al., 1990; Cavigelli and Robertson, 2000), and correspondingly more  $NO_3^-$  and  $BrO_3^-$  biodegradation.  $NO_3^-$  and  $BrO_3^-$  biodegradation NO\_3^- and BrO\_3^- biodegradation rates reduced in 3–8 m soil passage than higher up in the column, which can be potentially explained by AOC becoming insufficient as retention time increased and therefore lowered the level of microbial activity.

In the 1 m anoxic column, a rapid decrease of BrO<sub>3</sub><sup>-</sup> removal was observed in 1.5 days (running time 98-99.5 days) following an increase due to the sudden absence of NO<sub>3</sub>. Subsequently, a gradual decrease of  $BrO_3^-$  biodegradation within 2.5 months (phase 2 in Fig. 6) was observed. This study is the first documentation of  $BrO_3^$ removal in the long-term absence of NO<sub>3</sub>. Korner and Zumft (1989) concluded that the presence of nitrogen oxides was a prerequisite to promote the synthesis and the activity of denitrification enzymes. Several other studies (Cove, 1966; Saleh-Lakha et al., 2009; Sun et al., 2016) reported that  $NO_3^-$  absence or limited  $NO_3^-$  leads to a decrease of denitrification functional genes, and NO<sub>3</sub> reductase activity decay or denitrification rate decrease in several hours in pure microbial species and mixed microbial strains. Therefore, the rapid decrease of  $BrO_{\overline{3}}$  removal in the 8 m column from 82.5% to 61.4% in 1.5 days (running time 98–99.5 days) can potentially be explained by the limitation of NO<sub>3</sub><sup>-</sup> reductase activity of denitrifying bacteria by a  $NO_3^-$  concentration below detection limit (0.89 mg/L). The gradual decrease of BrO<sub>3</sub> biodegradation fits the first-order kinetic model with the first-order decay constant 0.034/day (Fig. S1 in the supplemental information). The decay of heterotrophic bacteria due to a lack of substrate is a relatively slow process, particularly under anoxic conditions. Lin (2008) showed that when  $NO_{\overline{3}}$  or glucose were limited in a moving-fixed bed biofilm reactor, denitrifying bacterial biomass decayed from 100% to 51.5% in 11 days with a first-order kinetic coefficient of 0.061/day. Although the decay rate of denitrifying bacteria reported in the previous study (Lin, 2008) is faster (double) than the observed  $BrO_3^-$  removal decrease, given that these experiments were performed under different conditions (including higher temperatures; 20–25 °C vs 11 °C), the results of Lin (2008) indicate the hypothesized relationship between denitrifying bacteria biomass and  $BrO_3^-$  removal.

#### 4.2. Ozonation as MAR pre-treatment

Figs. 2, 3 and 7 show that in both the batch experiments and the 8 m column experiment, the addition of extra C-CH<sub>3</sub>COONa, simulating formation of AOC during ozonation pre-treatment, resulted in slight but significantly higher NO<sub>3</sub> and BrO<sub>3</sub> reductions. This observation is similar to the results of Kirisits et al. (2001) who showed that the increase of DOC as an external electron donor resulted in the increase of BrO<sub>3</sub> reduction in a BAC filter. The addition of extra carbon stimulated microbial growth, which was monitored with ATP measurements. Biomass in the batch reactors with 1 mg/L C-CH<sub>3</sub>COONa addition was approximately two times as high as in the reference reactors (3.3 ng/mL and 1.5 ng/mL respectively; Fig. S2). This result suggests that an increase of AOC as a result of the ozonation pre-treatment can promote microbial activity and therefore BrO<sub>3</sub> removal in subsequent MAR systems.

Inevitably, the ozonation pre-treatment not only affects the AOC concentration but also causes high concentrations of dissolved oxygen (DO) in the MAR influent water. In the column studies,  $BrO_3^$ reduction was much higher in the anoxic column than in the oxic column, indicating that biological reduction of  $BrO_{3}$  predominantly occurs in anoxic zones instead of oxic zones in MAR systems. This result is in agreement with previous studies (Hübner et al., 2016; Kirisits et al., 2001; Liu et al., 2012). Hijnen et al. (1995) found that  $BrO_3^-$  reduction was inhibited by oxygen. Controlled column studies simulating MAR revealed inefficient BrO3 removal under oxic conditions in the study of Hübner et al. (2012). This observation can be potentially explained by DO being preferred over  $BrO_3^-$ (and  $NO_3^-$ ) as a competing electron acceptor. It is therefore recommended to design ozonation-MAR systems in such a way that anoxic zones develop, which can generally be achieved by extending the subsurface retention time. Depending on sitespecific water quality and hydrogeological conditions, oxic zones are usually found in the first several meters with a retention time of a couple of hours to days (Bertelkamp et al., 2016). Therefore, the ozonation effluent with high oxygen concentrations is not likely to limit biological  $BrO_{\overline{3}}$  reduction in most MAR systems.

#### 4.3. Redox conditions in MAR

Fig. S3 in the supplemental information shows redox conditions in MAR systems and the theoretical sequence of terminal electron acceptor processes. The initial infiltration phase in MAR systems are usually oxic, followed first by NO<sub>3</sub><sup>-</sup>-reducing and then Fe/Mnreducing zones (Bertelkamp et al., 2016; Lekkerkerker-Teunissen et al., 2012; Maeng et al., 2010; Schmidt et al., 2011). This study only focused on BrO<sub>3</sub><sup>-</sup> removal in oxic and NO<sub>3</sub><sup>-</sup>-reducing anoxic zones.

In the oxic column, the observed slight  $BrO_3^-$  reduction (Fig. 6) is an indication that minor  $BrO_3^-$  reduction by oxic bacteria in MAR systems can also take place. Based on the absence of  $NO_3^-$  removal in the oxic column, it can be concluded that no denitrifying bacteria or anoxic microniches were present in this column. Therefore,  $BrO_3^$ reduction by denitrifying bacteria in this oxic column can be excluded.

In the current study, the retention time in the 8 m anoxic column was 6 days.  $60 \ \mu g/L \ BrO_3^-$  was biodegraded to  $1.3 \ \mu g/L$  and 29.6  $\ \mu g/L$  in this long anoxic column set-up with and without increased AOC, respectively. In practice, travel times (weeks, months or even years) for MAR systems are much longer than those used in this study (Baumgarten et al., 2011; Grünheid et al., 2005; Stauder et al., 2012). With a greater retention time of the anoxic  $NO_3^-$ -reducing zones in MAR systems, more  $BrO_3^-$  than in the 8 m anoxic column with 6 days retention time may be biodegraded, as the travel time is longer and thus the reaction time is also longer. In addition, the concentration of  $NO_{\overline{3}}$  as a competitor of  $BrO_{\overline{3}}$ reduction by denitrifying bacteria becomes lower and lower. Therefore,  $BrO_3^-$  biodegradation should be more efficient with greater retention time in anoxic zones, especially in the zone immediately after  $NO_{\overline{3}}$  depletion, i.e. at the interface of the anoxic denitrification zone and the Fe/Mn oxide reduction zone. Additional evidence of this inference is illustrated by the study of Hübner et al. (2016), in which it was observed that  $BrO_{\overline{3}}$  removal in the presence of low  $NO_{\overline{3}}$  concentrations was significantly higher than in the presence of high  $NO_3^-$  concentrations.

#### 5. Conclusions

This study focused on the effect of  $NO_3^-$  and the role of increased AOC concentrations on the removal of  $BrO_3^-$  in  $NO_3^-$ -reducing anoxic zones of MAR systems. The following conclusions can be drawn:

- BrO<sub>3</sub> and NO<sub>3</sub> compete for reduction by denitrifying bacteria, but BrO<sub>3</sub> reduction and NO<sub>3</sub> reduction can occur simultaneously even if denitrifying bacteria prefer NO<sub>3</sub> to BrO<sub>3</sub> as an electron acceptor.
- The presence of NO<sub>3</sub> is a precondition for denitrifying bacteria to reduce BrO<sub>3</sub> in NO<sub>3</sub>-reducing anoxic zones of MAR systems.
- An increase of AOC as a result of ozonation pre-treatment promotes microbial activity and therefore BrO<sub>3</sub><sup>-</sup> removal in subsequent MAR systems.
- In the 8 m long anoxic column (retention time 6 days) simulating anoxic NO<sub>3</sub><sup>-</sup>-reducing zones of MAR systems, BrO<sub>3</sub><sup>-</sup> biodegraded to a concentration of 1.3 μg/L, indicating that BrO<sub>3</sub><sup>-</sup> biodegradation by denitrifying bacteria can happen in anoxic NO<sub>3</sub><sup>-</sup>-reducing zones of MAR systems.
- MAR systems following ozonation are potentially effective to biodegrade BrO<sub>3</sub>, provided that anoxic NO<sub>3</sub> reducing conditions are reached in MAR systems.

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#### Appendix A. Supplementary data

Supplementary data related to this article can be found at https://doi.org/10.1016/j.watres.2017.11.052.

#### References

- Agbaba, J., Jazić, J.M., Tubić, A., Watson, M., Maletić, S., Isakovski, M.K., Dalmacija, B., 2016. Oxidation of natural organic matter with processes involving O<sub>3</sub>, H<sub>2</sub>O<sub>2</sub> and UV light: formation of oxidation and disinfection by-products. RSC Adv. 6 (89), 86212–86219.
- Ahmad, M.K., Zubair, H., Mahmood, R., 2013. DNA damage and DNA-protein crosslinking induced in rat intestine by the water disinfection by-product potassium bromate. Chemosphere 91 (8), 1221–1224.

- Amy, G., Bull, R., Craun, G.F., Pegram, R., Siddiqui, M., Organization, W.H., 2000. Disinfectants and Disinfectant By-products.
- Assuncao, A., Martins, M., Silva, G., Lucas, H., Coelho, M.R., Costa, M.C., 2011. Bromate removal by anaerobic bacterial community: mechanism and phylogenetic characterization. J. Hazard Mater. 197, 237–243.
- Baumgarten, B., Jährig, J., Reemtsma, T., Jekel, M., 2011. Long term laboratory column experiments to simulate bank filtration: factors controlling removal of sulfamethoxazole. Water Res. 45 (1), 211–220.
- Bell, L.C., Richardson, D.J., Ferguson, S.J., 1990. Periplasmic and membrane-bound respiratory nitrate reductases in Thiosphaera pantotropha. The periplasmic enzyme catalyzes the first step in aerobic denitrification. FEBS Lett. 265 (1–2), 85–87.
- Bertelkamp, C., Verliefde, A.R.D., Schoutteten, K., Vanhaecke, L., Vanden Bussche, J., Singhal, N., van der Hoek, J.P., 2016. The effect of redox conditions and adaptation time on organic micropollutant removal during river bank filtration: a laboratory-scale column study. Sci. Total Environ. 544, 309–318.
- Bhatnagar, A., Sillanpää, M., 2012. Sorption studies of bromate removal from water by Nano-Al<sub>2</sub>O<sub>3</sub>. Sep. Sci. Technol. 47 (1), 89–95.
- Bouwer, H., 2002. Artificial recharge of groundwater: hydrogeology and engineering. Hydrogeol. J. 10 (1), 121–142.
- Butler, R., Godley, A., Lytton, L., Cartmell, E., 2005. Bromate environmental contamination: review of impact and possible treatment. Crit. Rev. Environ. Sci. Technol. 35 (3), 193–217.
- Carney, M., 1991. European drinking water standards. J. Am. Water Works Assoc. 48-55.
- Cavigelli, M.A., Robertson, G.P., 2000. The functional significance of denitrifier community composition in a terrestrial ecosystem. Ecology 81 (5), 1402–1414.
- Cove, D.J., 1966. The induction and repression of nitrate reductase in the fungus Aspergillus nidulans. Biochim. Biophys. Acta 113 (1), 51–56.Davidson, A.N., Chee-Sanford, J., Lai, H.Y.M., Ho, C.H., Klenzendorf, J.B., Kirisits, M.J.,
- Davidson, A.N., Chee-Sanford, J., Lai, H.Y.M., Ho, C.H., Klenzendorf, J.B., Kirisits, M.J., 2011. Characterization of bromate-reducing bacterial isolates and their potential for drinking water treatment. Water Res. 45 (18), 6051–6062.
- Demirel, S., Uyanik, I., Yurtsever, A., çelikten, H., Uçar, D., 2014. Simultaneous bromate and nitrate reduction in water using sulfur-utilizing autotrophic and mixotrophic denitrification processes in a fixed bed column reactor. Clean. -Soil, Air, Water 42 (9), 1185–1189.
- Downing, L.S., Nerenberg, R., 2007. Kinetics of microbial bromate reduction in a hydrogen-oxidizing, denitrifying biofilm reactor. Biotechnol. Bioeng. 98 (3), 543–550.
- Drewes, J.E., Heberer, T., Rauch, T., Reddersen, K., 2003. Fate of pharmaceuticals during ground water recharge. Ground Water Monit. Remed. 23 (3), 64–72.
- Escobar, I.C., Randall, A.A., 2001. Assimilable organic carbon (AOC) and biodegradable dissolved organic carbon (BDOC): complementary measurements. Water Res. 35 (18), 4444–4454.
- EU, 1998. Councial directive 98/83/EC of 3 November 1998 on the quality of water intended for human consumption. L330/54. In: Official Journal of the European Communities, vol. 5, p. L330.
- Fan, C., Chan, C.H., Xie, L., Shang, C., 2006. Factors Affecting Bromate Removal Capacity of Zerovalent Iron Packed Columns, vol. 6, pp. 119–130.
- Forum, U.S.E.P.A.R.A., 2005. Guidelines for Carcinogen Risk Assessment. Risk Assessment Forum, United states.
- Glaze, W.H., Weinberg, H.S., Cavanagh, J.E., 1993. Evaluating the formation of brominated DBPs during ozonation. J. Am. Water Works Assoc. 85 (1), 96–103.
- Grünheid, S., Amy, G., Jekel, M., 2005. Removal of bulk dissolved organic carbon (DOC) and trace organic compounds by bank filtration and artificial recharge. Water Res. 39 (14), 3219–3228.
- Haag, W.R., Holgne, J., 1983. Ozonation of bromide-containing waters: kinetics of formation of hypobromous acid and bromate. Environ. Sci. Technol. 17 (5), 261–267.
- Hammes, F., Salhi, E., Köster, O., Kaiser, H.P., Egli, T., von Gunten, U., 2006. Mechanistic and kinetic evaluation of organic disinfection by-product and assimilable organic carbon (AOC) formation during the ozonation of drinking water. Water Res. 40 (12), 2275–2286.
- Hijnen, W.A.M., Jong, R., Van Der Kooij, D., 1999. Bromate removal in a denitrifying bioreactor used in water treatment. Water Res. 33 (4), 1049–1053.
- Hijnen, W.A.M., Voogt, R., Veenendaal, H.R., Van der Jagt, H., Van der Kooij, D., 1995. Bromate reduction by denitrifying bacteria. Appl. Environ. Microbiol. 61 (1), 239–244.
- Huang, W.J., Chen, L.Y., 2004. Assessing the effectiveness of ozonation followed by GAC filtration in removing bromate and assimilable organic carbon. Environ. Technol. 25 (4), 403–412.
- Hübner, U., Kuhnt, S., Jekel, M., Drewes, J.E., 2016. Fate of bulk organic carbon and bromate during indirect water reuse involving ozone and subsequent aquifer recharge. J. Water Reuse Desalination 6 (3), 413–420.
- Hübner, U., Miehe, U., Jekel, M., 2012. Optimized removal of dissolved organic carbon and trace organic contaminants during combined ozonation and artificial groundwater recharge. Water Res. 46 (18), 6059–6068.
- Jia, A., Wu, C., Hu, W., Hu, C., 2015. Bromate adsorption on three variable charge soils: kinetics and thermodynamics. Clean. - Soil, Air, Water 43 (7), 1072–1077.
- Kim, H.C., Noh, J.H., Chae, S.R., Choi, J., Lee, Y., Maeng, S.K., 2015. A multi-parametric approach assessing microbial viability and organic matter characteristics during managed aquifer recharge. Sci. Total Environ. 524–525, 290–299.
- Kirisits, M.J., Snoeyink, V.L., 1999. Reduction of bromate in a BAC filter. J. Am. Water Works Assoc. 91 (8), 74–84.
- Kirisits, M.J., Snoeyink, V.L., Inan, H., Chee-sanford, J.C., Raskin, L., Brown, J.C., 2001.

Water quality factors affecting bromate reduction in biologically active carbon filters. Water Res. 35 (4), 891–900.

- Korner, H., Zumft, W.G., 1989. Expression of denitrification enzymes in response to the dissolved oxygen levels and respiratory substrate in continuous culture of Pseudomonas stutzeri. Appl. Environ. Microbiol. 55 (7), 1670–1676.
- Korom, S.F., 1992. Natural denitrification in the saturated zone: a review. Water Resour. Res. 28 (6), 1657–1668.
- Krasner, S.W., Glaze, W.H., Weinberg, H.S., Daniel, P.A., Najm, I.N., 1993. Formation and control of bromate during ozonation of waters containing bromide. J. Am. Water Works Assoc. 85 (1), 73–81.
- Kruithof, J.C., Meijers, R.T., 1995. Bromate formation by ozonation and advanced oxidation and potential options in drinking water treatment. Water Supply 13 (2), 93–103.
- Kurokawa, Y., Maekawa, A., Takahashi, M., Hayashi, Y., 1990. Toxicity and carcinogenicity of potassium bromate - a new renal carcinogen. Environ. Health Perspect. 87, 309–335.
- Laws, B.V., Dickenson, E.R.V., Johnson, T.A., Snyder, S.A., Drewes, J.E., 2011. Attenuation of contaminants of emerging concern during surface-spreading aquifer recharge. Sci. Total Environ. 409 (6), 1087–1094.
  Lekkerkerker-Teunissen, K., Chekol, E.T., Maeng, S.K., Ghebremichael, K.,
- Lekkerkerker-Teunissen, K., Chekol, E.T., Maeng, S.K., Ghebremichael, K., Houtman, C.J., Verliefde, A.R.D., Verberk, J.Q.J.C., Amy, G.L., Van Dijk, J.C., 2012. Pharmaceutical removal during managed aquifer recharge with pretreatment by advanced oxidation. Water Sci. Technol. Water Supply 12, 755–767.
- Lekkerkerker, K., 2012. Advanced Oxidation and Managed Aquifer Recharge. PhD thesis. Delft University of Technology. Lekkerkerker, K., Scheideler, J., Maeng, S.K., Ried, A., Verberk, J.Q.J.C., Knol, A.H.,
- Lekkerkerker, K., Scheideler, J., Maeng, S.K., Ried, A., Verberk, J.Q.J.C., Knol, A.H., Amy, G., Van Dijk, J.C., 2009. Advanced oxidation and artificial recharge: a synergistic hybrid system for removal of organic micropollutants. Water Sci. Technol. Water Supply 9, 643–651.
- Lin, Y.H., 2008. Kinetics of nitrogen and carbon removal in a moving-fixed bed biofilm reactor. Appl. Math. Model. 32 (11), 2360–2377.
- Liu, J., Yu, J., Li, D., Zhang, Y., Yang, M., 2012. Reduction of bromate in a biological activated carbon filter under high bulk dissolved oxygen conditions and characterization of bromate-reducing isolates. Biochem. Eng. J. 65 (0), 44–50.
- Maeng, S.K, 2010. Multiple Objective Treatment Aspects of Bank Filtration. PhD thesis. Delft University of Technology, Delft.
- Maeng, S.K., Sharma, S.K., Lekkerkerker-Teunissen, K., Amy, G.L., 2010. Occurrence and fate of bulk organic matter and pharmaceutically active compounds in managed aquifer recharge: a review. Water Res. 45 (10), 3015–3033.
- Oller, I., Malato, S., Sánchez-Pérez, J.A., 2011. Combination of Advanced Oxidation Processes and biological treatments for wastewater decontamination-A review. Sci. Total Environ. 409 (20), 4141–4166.
- Orlandini, E., Kruithof, J.C., Van der Hoek, J.P., Siebel, M.A., Schippers, J.C., 1997. Impact of ozonation on disinfection and formation of biodegradable organic matter and bromate. Aqua 46 (1), 20–30.
- Postigo, C., Barceló, D., 2015. Synthetic organic compounds and their transformation products in groundwater: occurrence, fate and mitigation. Sci. Total Environ. 503–504, 32–47.
- Ridley, H., Watts, C.A., Richardson, D.J., Butler, C.S., 2006. Resolution of distinct membrane-bound enzymes from Enterobacter cloacae SLD1a-1 that are responsible for selective reduction of nitrate and selenate oxyanions. Appl. Environ. Microbiol. 72 (8), 5173–5180.
- Saleh-Lakha, S., Shannon, K.E., Henderson, S.L., Zebarth, B.J., Burton, D.L., Goyer, C., Trevors, J.T., 2009. Effect of nitrate and acetylene on nirS, cnorB, and nosZ expression and denitrification activity in Pseudomonas mandelii. Appl. Environ. Microbiol. 75 (15), 5082–5087.
- Sarathy, S.R., Stefan, M.I., Royce, A., Mohseni, M., 2011. Pilot-scale UV/H<sub>2</sub>O<sub>2</sub> advanced oxidation process for surface water treatment and downstream biological treatment: effects on natural organic matter characteristics and DBP formation potential. Environ. Technol. 32 (15), 1709–1718.
- Schmidt, C.M., Fisher, A.T., Racz, A.J., Lockwood, B.S., Huertos, M.L., 2011. Linking denitrification and infiltration rates during managed groundwater recharge. Environ. Sci. Technol. 45 (22), 9634–9640.
- Stauder, S., Stevanovic, Z., Richter, C., Milanovic, S., Tucovic, A., Petrovic, B., 2012. Evaluating bank filtration as an alternative to the current water supply from deeper aquifer: a case study from the Pannonian basin, Serbia. Water Resour. Manag. 26 (2), 581–594.
- Sun, Y., De Vos, P., Heylen, K., 2016. Nitrous oxide emission by the non-denitrifying, nitrate ammonifier Bacillus licheniformis. BMC Genom. 17 (1).
- Ternes, T.A., Meisenheimer, M., McDowell, D., Sacher, F., Brauch, H.J., Haist-Gulde, B., Preuss, G., Wilme, U., Zulei-Seibert, N., 2002. Removal of pharmaceuticals during drinking water treatment. Environ. Sci. Technol. 36 (17), 3855–3863.
- Tufenkji, N., Ryan, J.N., Elimelech, M., 2002. The promis of bank filtration. Environ. Sci. Technol. 36 (21), 422A–428A.
- Van der Hoek, J.P., Bertelkamp, C., Verliefde Bertelkamp, A.R.D., Singhal, N., 2014. Drinking water treatment technologies in Europe: state of the art - challenges -Research needs. J. Water Supply Res. Technol. - Aqua 63 (2), 124–130.
- Van Der Hoek, J.P., Rijnbende, D.O., Lokin, C.J.A., Bonné, P.A.C., Loonen, M.T., Hofman, J.A.M.H., 1998. Electrodialysis as an alternative for reverse osmosis in an integrated membrane system. Desalination 117 (1–3), 159–172.
- Van Ginkel, C.G., Van Haperen, A.M., Van Der Togt, B., 2005. Reduction of bromate to bromide coupled to acetate oxidation by anaerobic mixed microbial cultures. Water Res. 39 (1), 59–64.
- Wang, F., van Halem, D., van der Hoek, J.P., 2016. The fate of H<sub>2</sub>O<sub>2</sub> during managed aquifer recharge: a residual from advanced oxidation processes for drinking

water production. Chemosphere 148, 263-269.

- Wang, Q., Snyder, S., Kim, J., Choi, H., 2009. Aqueous ethanol modified nanoscale zerovalent iron in Bromate reduction: synthesis, characterization, and reactivity. Environ. Sci. Technol. 43 (9), 3292-3299.
- Weast, R., 1986. 87 CRC Handbook of Chemistry and Physics 67th Ed. CRC press, Boca Raton FI.
- WHO, G., 2011. Guidelines for drinking-water quality, vol. 216, 303-4. Xie, L., Shang, C., 2006. A Review on Bromate Occurrence and Removal Strategies in Water Supply, vol. 6, pp. 131–136. Xu, J.H., Gao, N.Y., Zhao, D.Y., Yin, D.Q., Zhang, H., Gao, Y.Q., Shi, W., 2015.

Comparative study of nano-iron hydroxide impregnated granular activated carbon (Fe-GAC) for bromate or perchlorate removal. Sep. Purif. Technol. 147, 9-16.

- Xu, J.H., Gao, N.Y., Zhao, D.Y., Zhang, W.X., Xu, Q.K., Xiao, A.H., 2015b. Efficient reduction of bromate in water by nano-iron hydroxide impregnated granular activated carbon (Fe-GAC). Chem. Eng. J. 275, 189–197.
- Zhang, Y.Q., Wu, Q.P., Zhang, J.M., Yang, X.H., 2015. Removal of bromide and bromate from drinking water using granular activated carbon. J. Water Health 13 (1), 73–78.