



**THE INFLUENCE OF
FRICTION COEFFICIENT
AND WHEEL/RAIL
PROFILES ON ENERGY
DISSIPATION IN THE
WHEEL/RAIL CONTACT**

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The influence of friction coefficient and wheel/rail profiles on energy dissipation in the wheel/rail contact

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INTRODUCTION

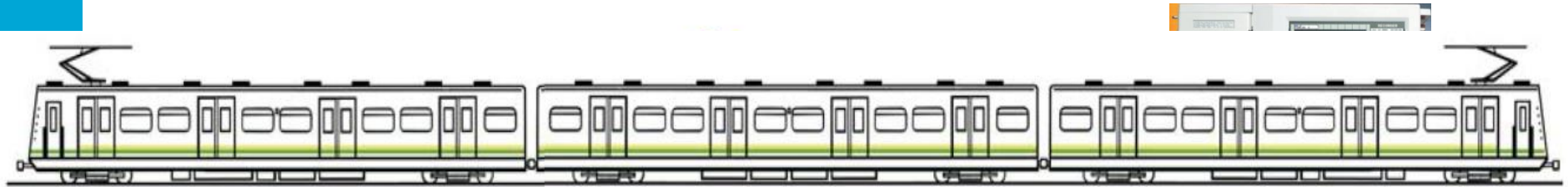
This work gives a further explanation of the effect of the friction coefficient in the energy dissipation in the wheel/rail contact. To such an end, several simulations were performed using a multibody model, including the torque of the wheels, and varying the friction coefficient from 0.2 to 0.7.

Previous work:

	Post – Lubricated Condition	Lubricated Condition
Power Measurements Reduction – Field [KW]	9.4%	15.3%
Power Calculations Reduction - Multibody [KW]	21.0%	35.0%
Calculated wear reduction [$\mu\text{g}/(\text{m mm}^2)$]	19.8%	36.1%

G. Idarraga et.al. 2015

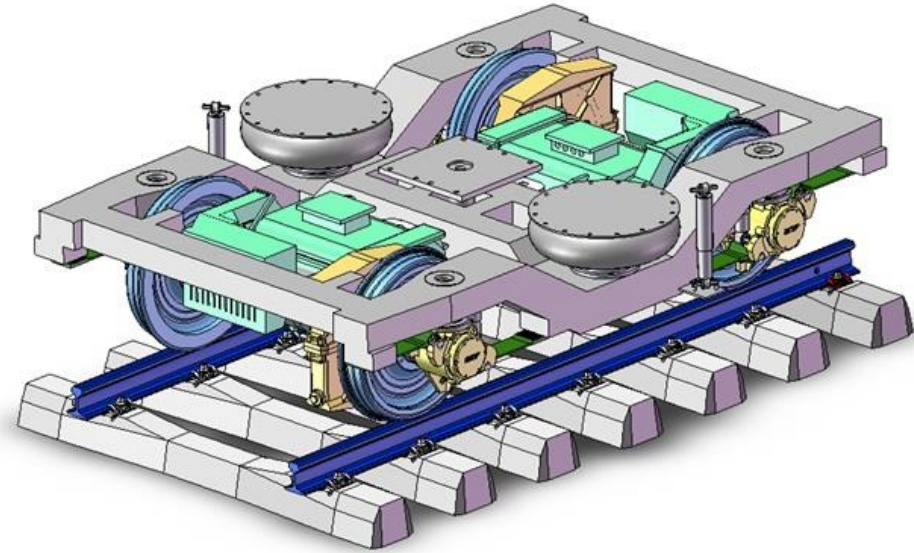
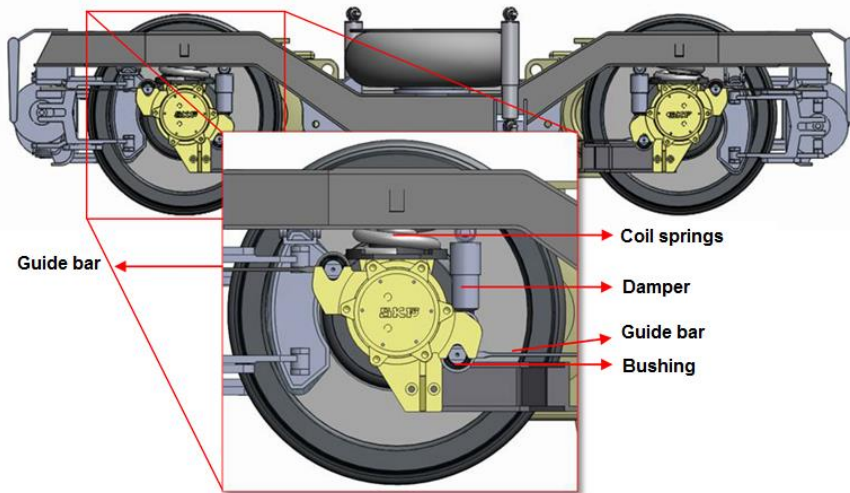
THE VEHICLE MODEL:



A

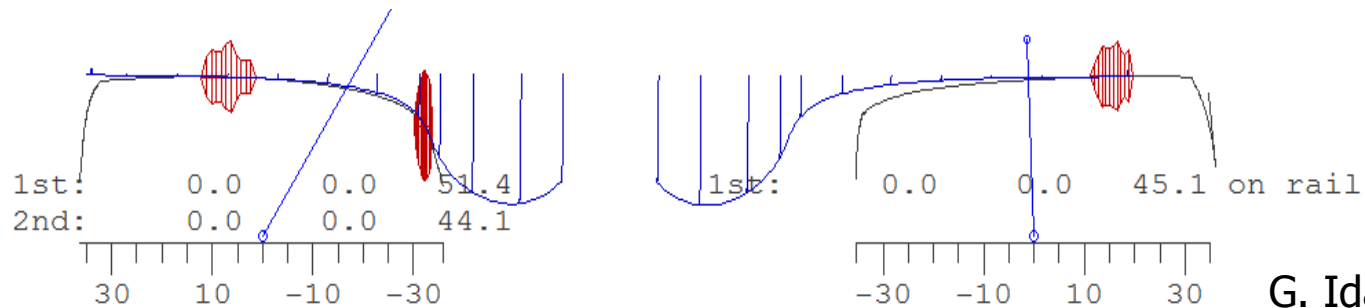
R

B



A. R. Martinez 2010, $a(t)$: vehicle acceleration, L. Castañeda et al. 2010

TRACK MODEL:



G. Idarraga et. al. 2015

ENERGY AND WEAR CALCULATIONS:

$$P_{frict} = (T_x\gamma_x + T_y\gamma_y)V$$

Where V is the velocity of the vehicle, T the tangential force, and γ the creepage (normalized slip). When the contribution of spin is included it becomes:

$$P_{frict} = (T_x\gamma_x + T_y\gamma_y + M\varphi)V$$

Where M is the spin moment and φ is the spin creepage.

$$Wear_{Rate} = KT\gamma/A$$

Where, K is a wear coefficient and A is the contact area.

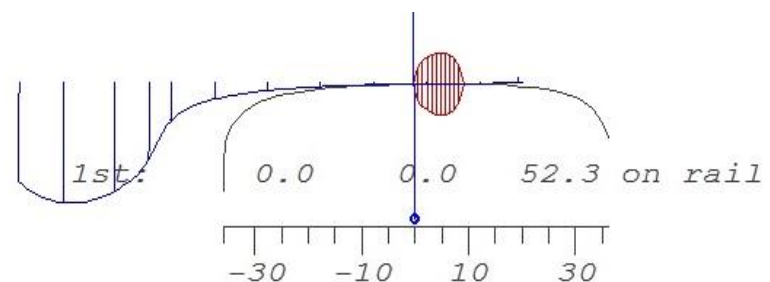
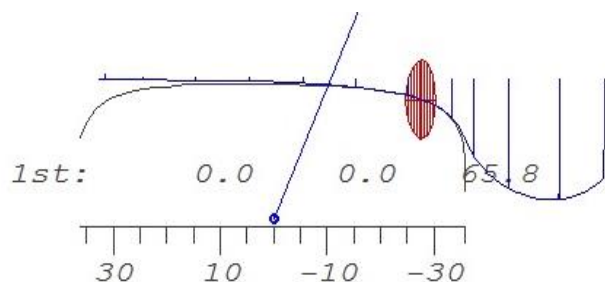
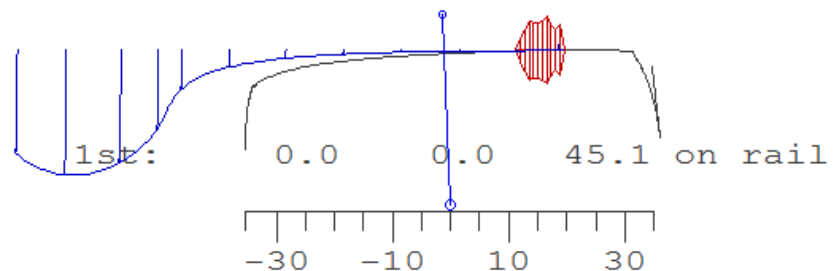
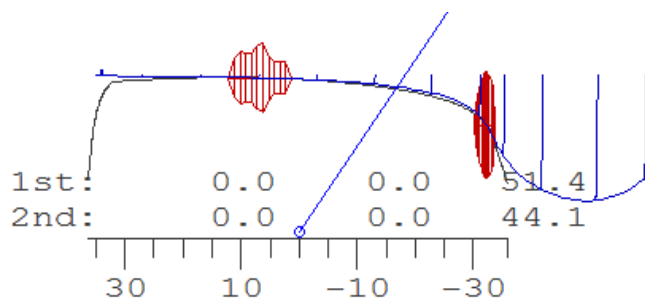
$$Wear_{Rate} = \begin{cases} 5.3I_w & I_w < 10.4 \\ 55.0 & 10.4 \leq I_w \leq 77.2 \\ 61.9I_w & I_w > 77.2 \end{cases}$$

Where I_w is the wear index.

R. Lewis and R. S. Dwyer-Joyce 2004

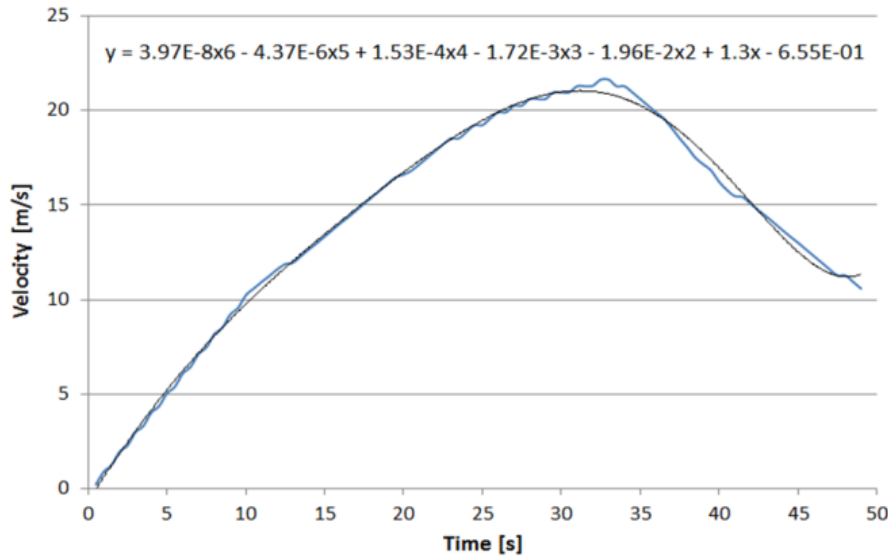
EFFECT OF PROFILES ON THE ENERGY DISSIPATION AND WEAR RATES

Couple	Rail profiles	Wheel profiles	Designation
1	Worm CPC-HRC	New Ore S1002	Measured Profiles
2	New UIC 60	New Ore S1002	Standard Profiles



TRACTION MOMENT ON THE WHEELS

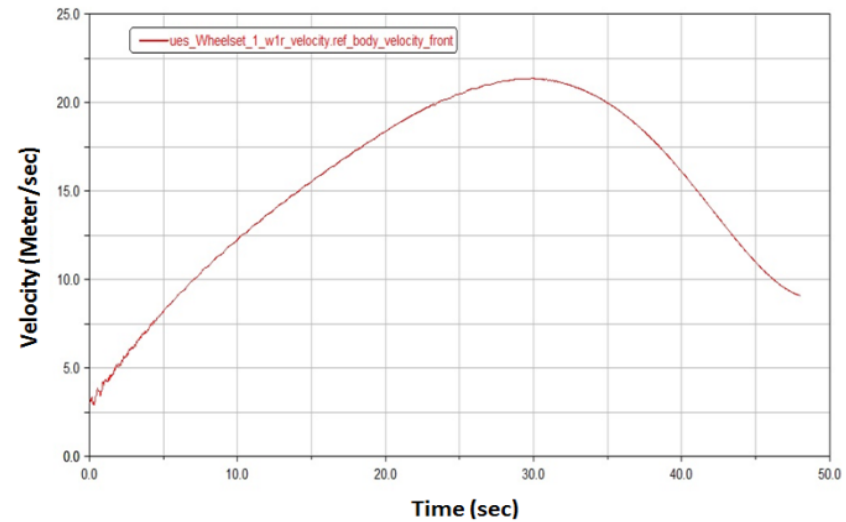
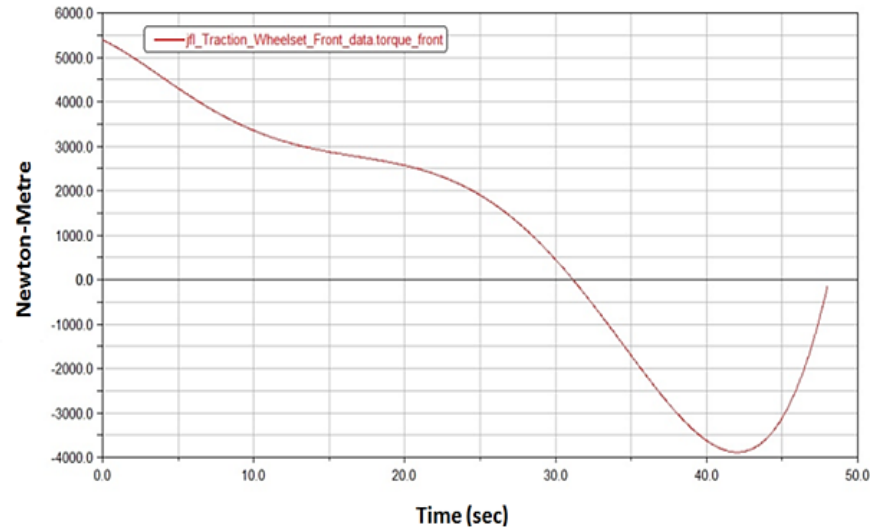
Vehicle velocity curve



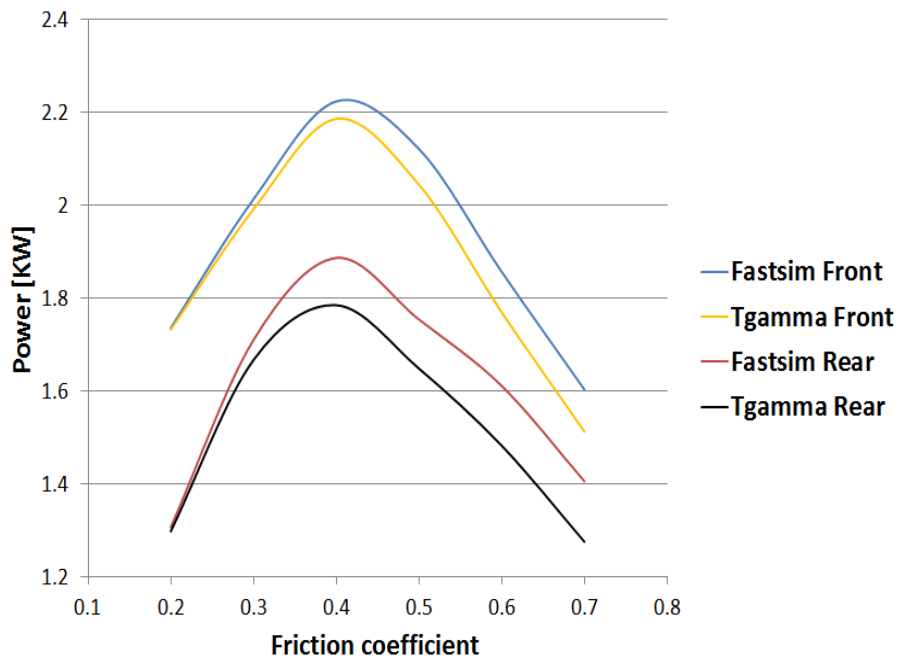
$$M = \frac{ma(t)R}{16}$$

m : Vehicle mass R : Wheel radius

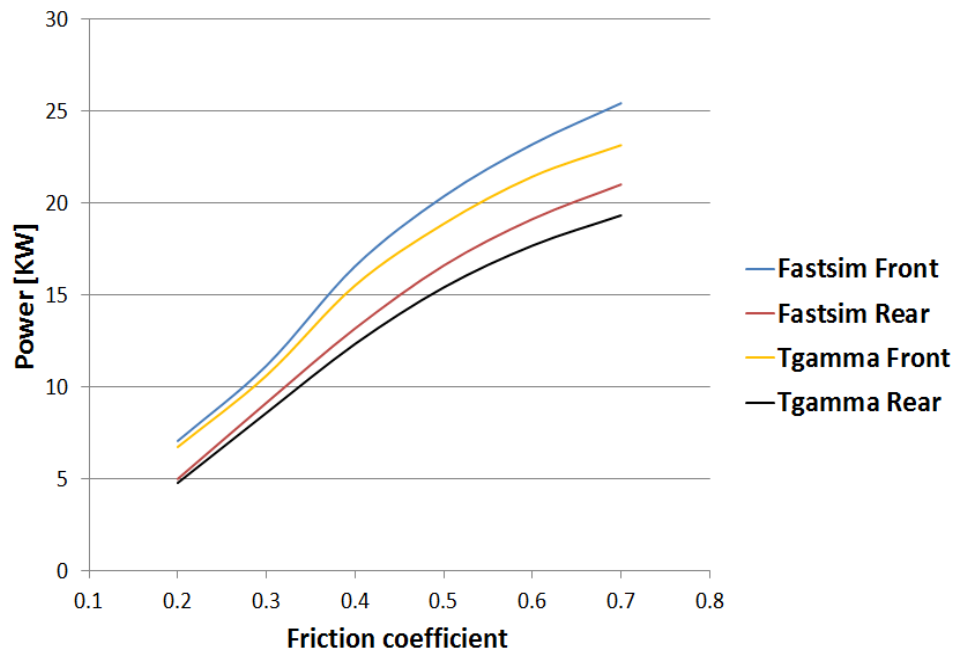
$a(t)$: vehicle acceleration



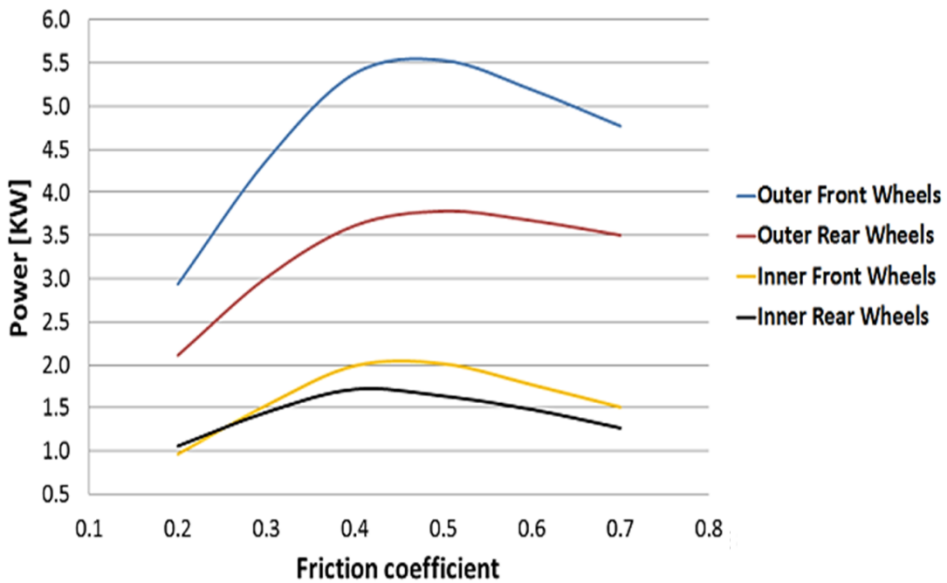
Inner Wheels



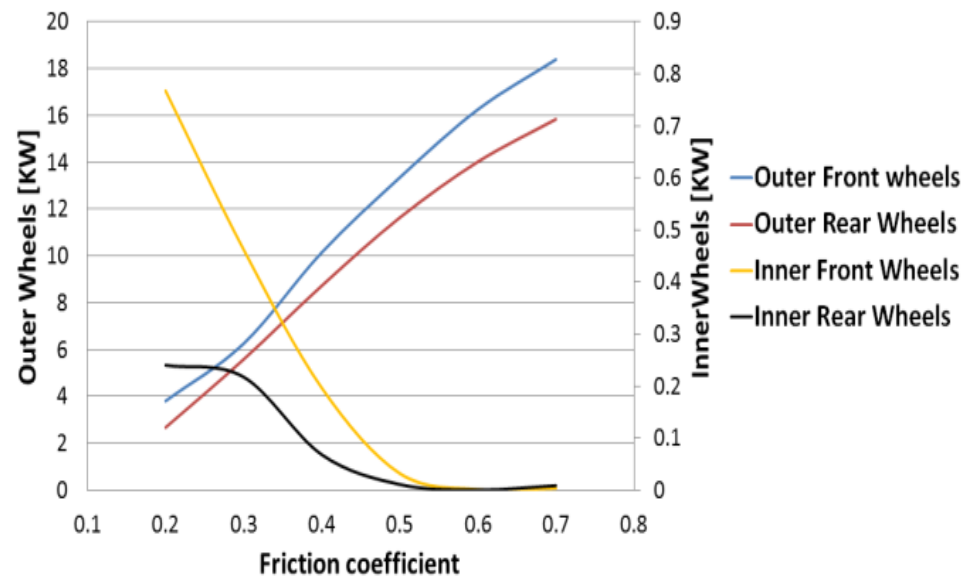
Outer Wheels



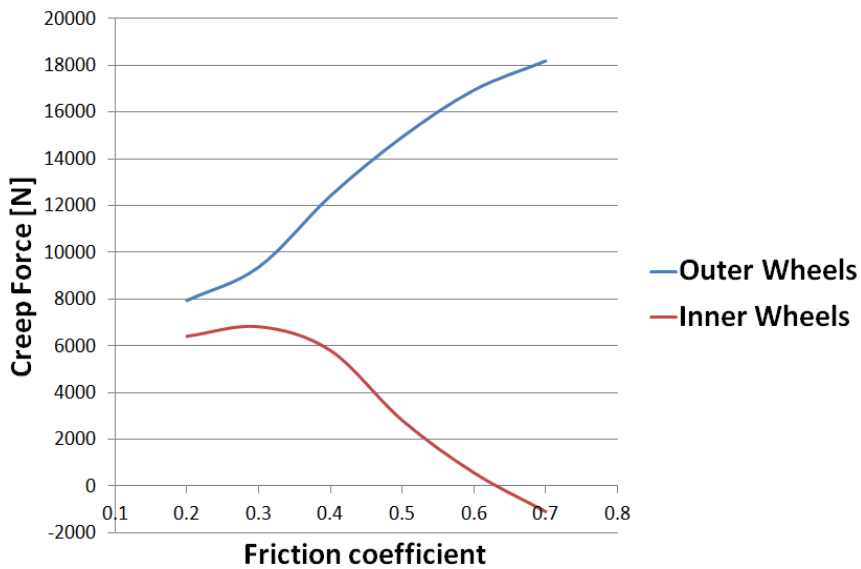
Lateral Power Consumption



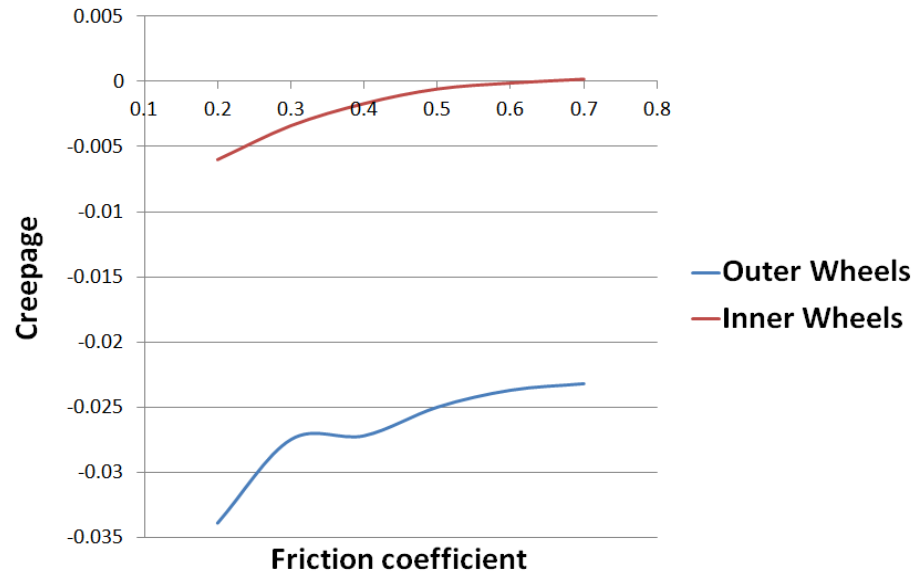
Longitudinal Power Consumption



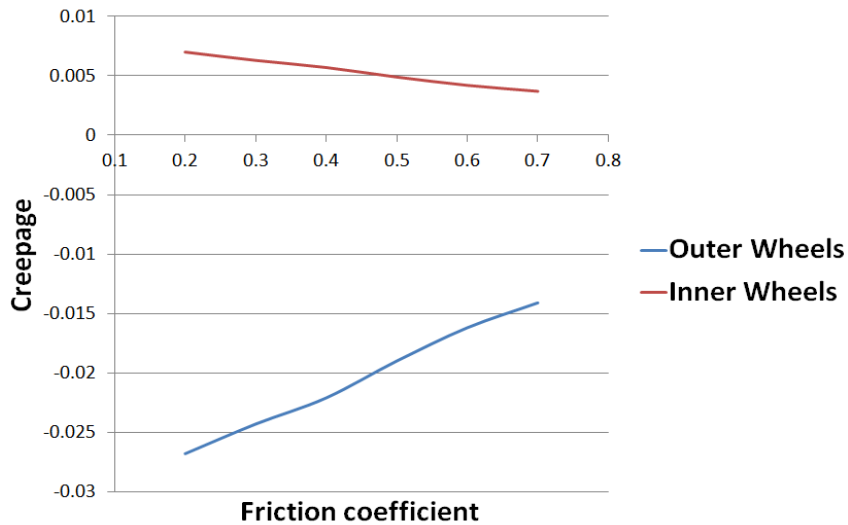
Creep Force - Longitudinal



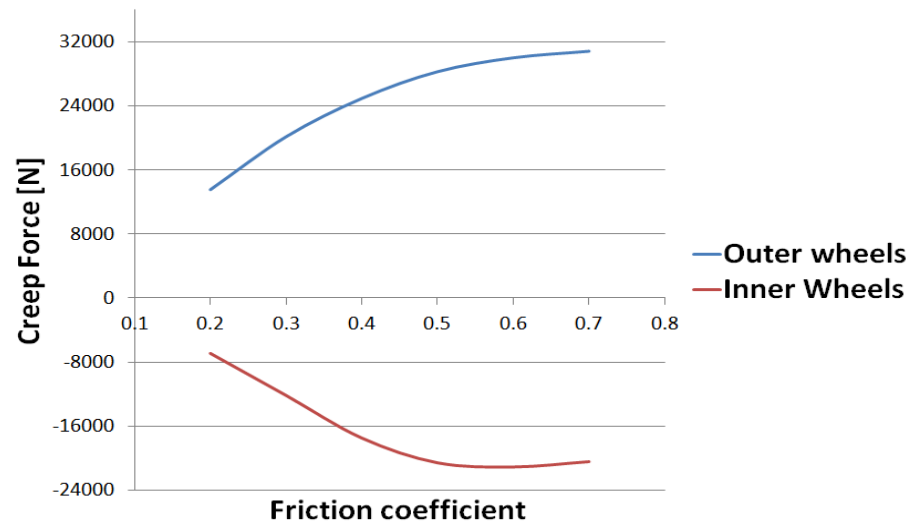
Longitudinal Creepage



Lateral Creepage



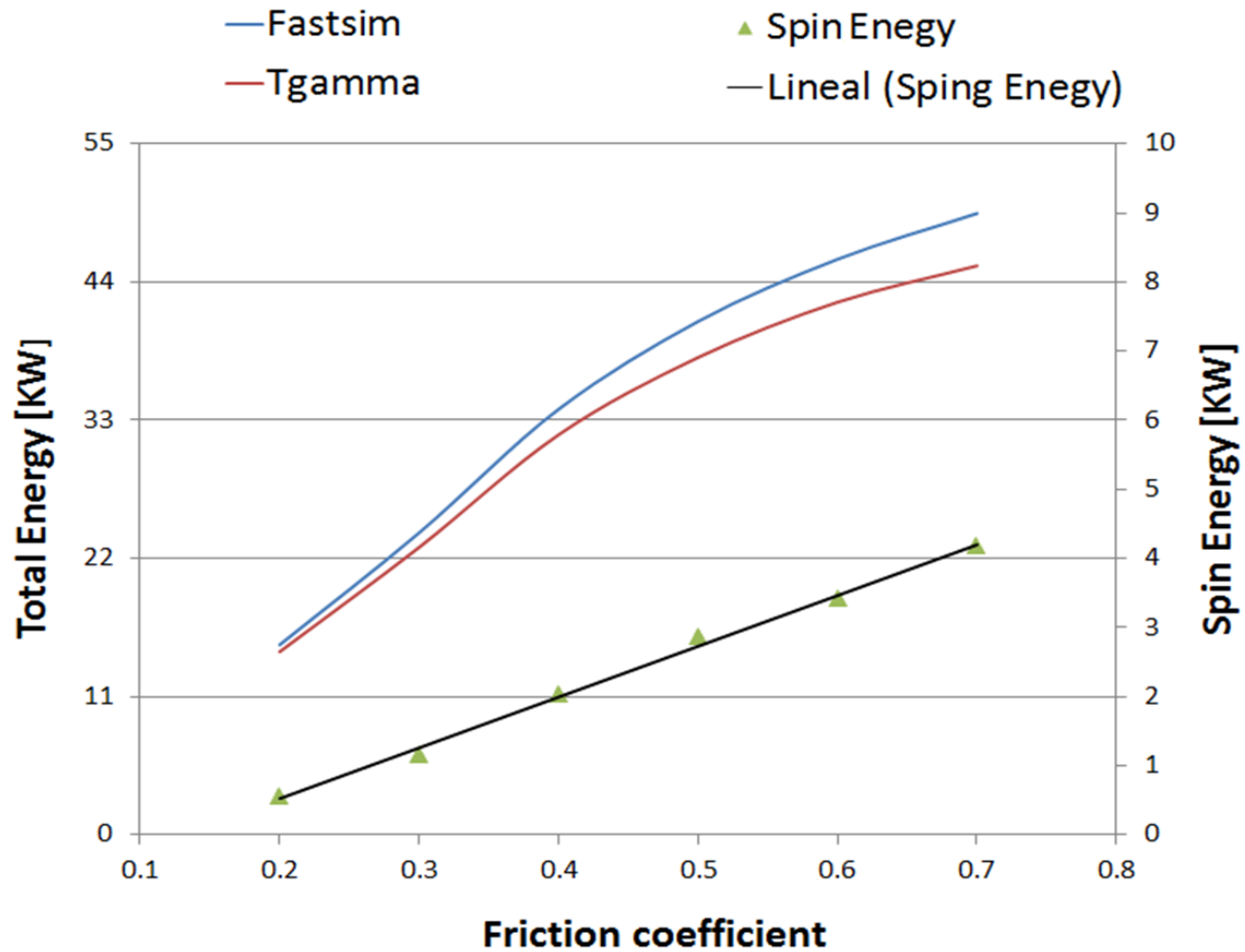
Creep Force - Lateral



$$v_y = -\alpha$$

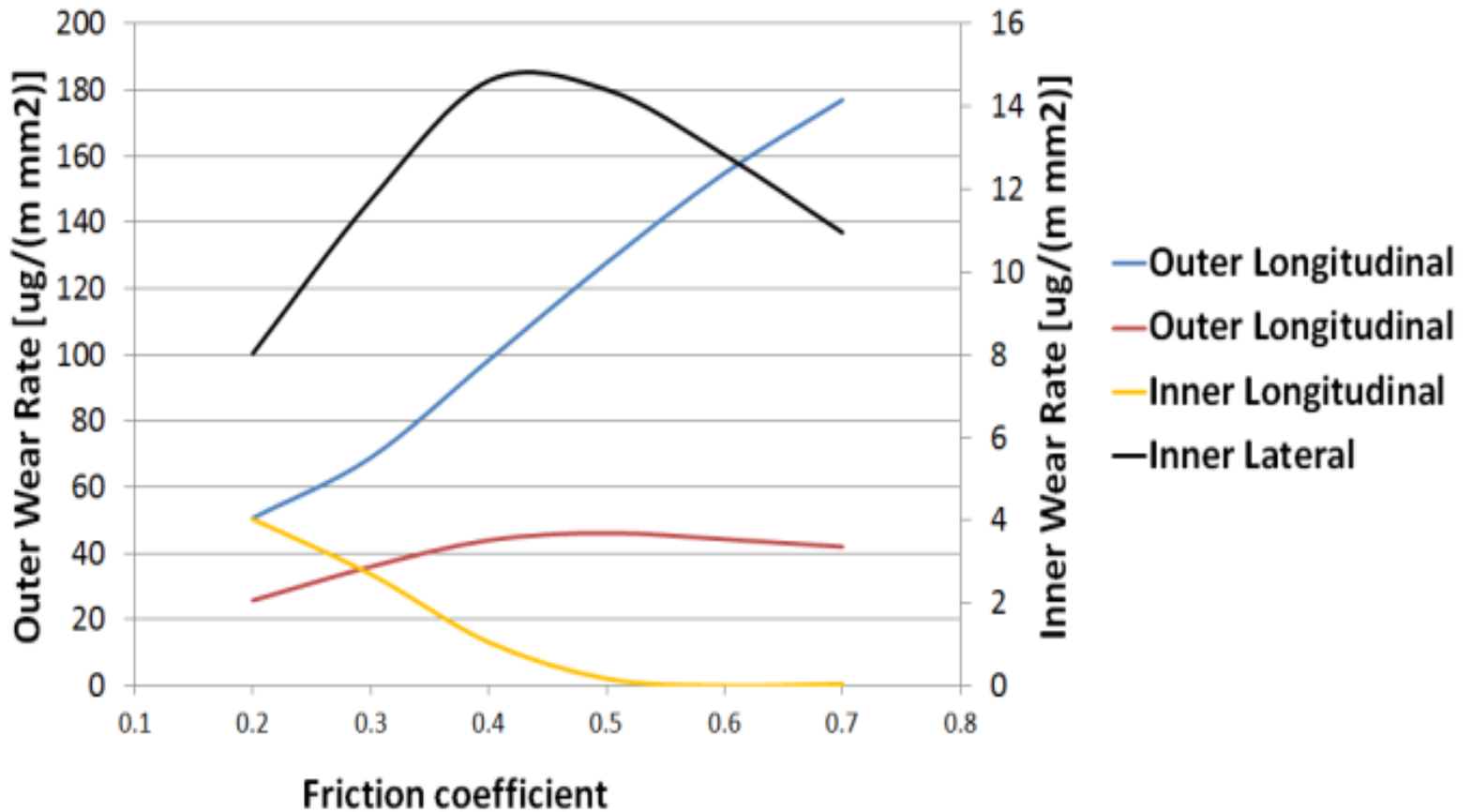
$$P_{frict} = (T_x \gamma_x + T_y \gamma_y) V$$

POWER CALCULATIONS:

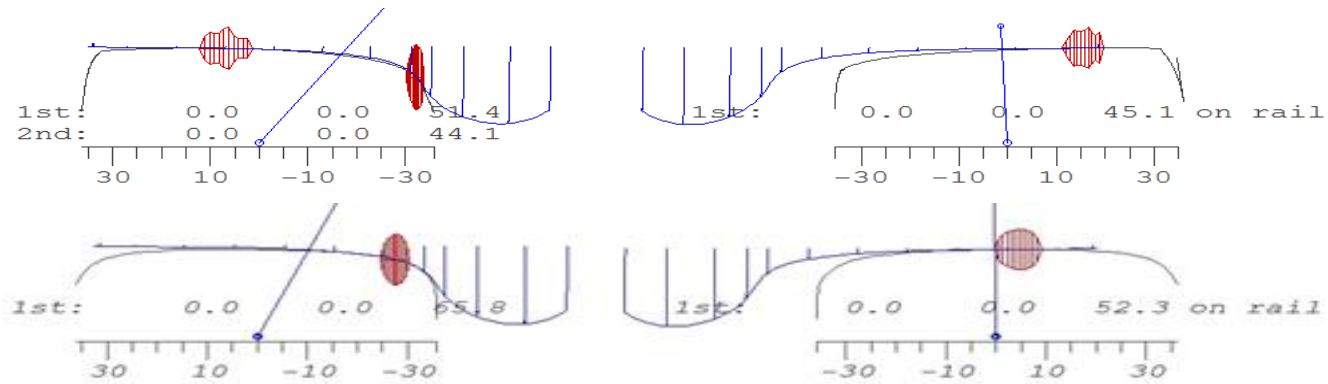


WEAR CALCULATIONS:

Wear Rate Outer and Inner Wheels

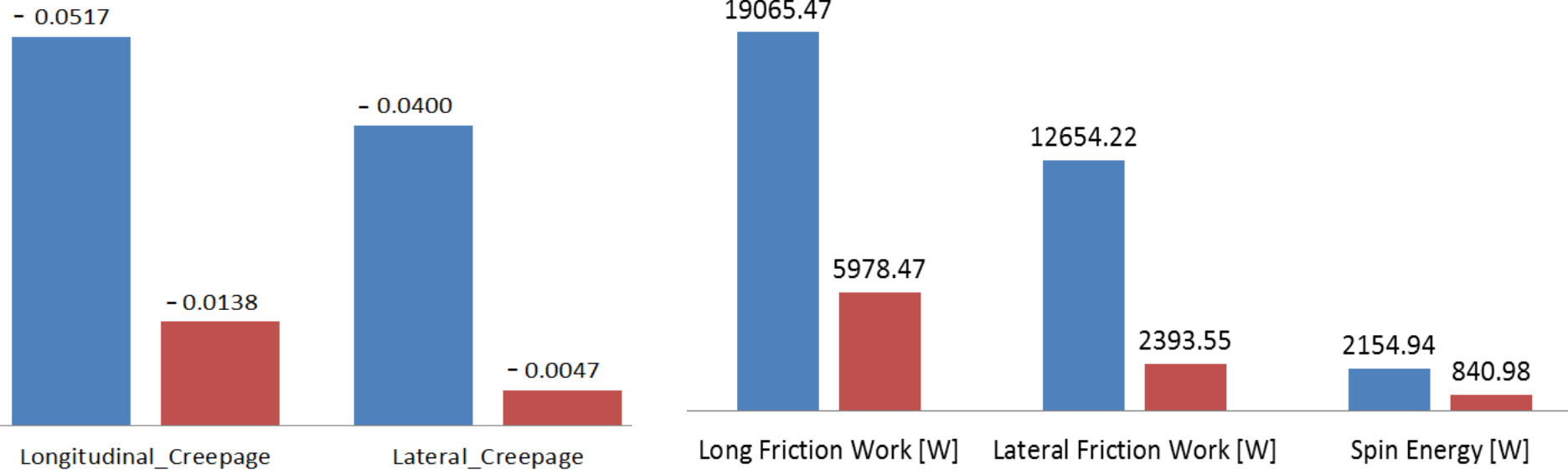


EFFECT OF THE PROFILES ON THE ENERGY DISSIPATION AND WEAR RATES



■ Measured Profiles ■ Standard Profiles

■ Measured Profiles ■ Standard Profiles



EFFECT OF THE PROFILES ON THE ENERGY DISSIPATION AND WEAR RATES

Wheel/rail profiles effect in the total energy dissipation of the first bogie.

	Measured profiles	Standard Profiles
Total Energy [KW]	33.9	9.2

Wheel/rail profiles effect in the wear rates of the first bogie.

	Measured profiles	Standard Profiles
Wear Rate [$\mu\text{g}/(\text{m mm}^2)$]	158.1	30.6

CONCLUSIONS AND RECOMMENDATIONS

- The energy dissipation generated by spin increases as the friction coefficient grows.
- It is only recommended to neglect the effect of the spin moment in the energy calculations for low friction coefficient conditions
- As the friction coefficient increases, the inner wheel loses traction while the outer wheel increases it, this condition produces a rotational moment of the wheelset in clockwise direction, reducing the yaw angle of the wheelset.
- The energy consumption increases linearly as the friction coefficient grows
- The results of simulations with different profiles are important since they show the necessity for optimizing profiles and re-profiling procedures. An optimized wheel/rail profile combination greatly reduces the energy dissipation and the wear rates.

ACKNOWLEDGMENTS

