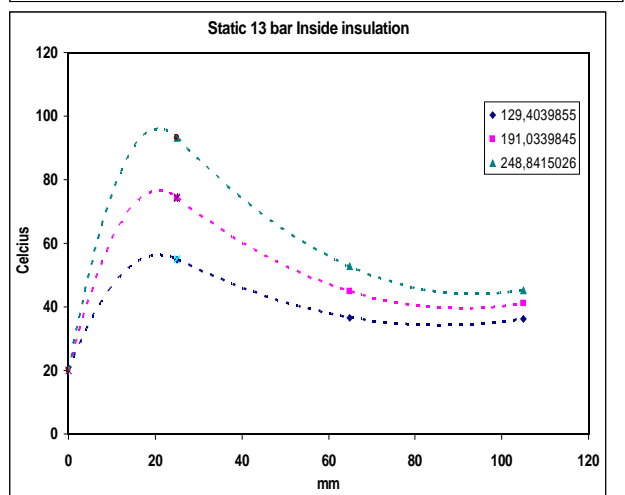
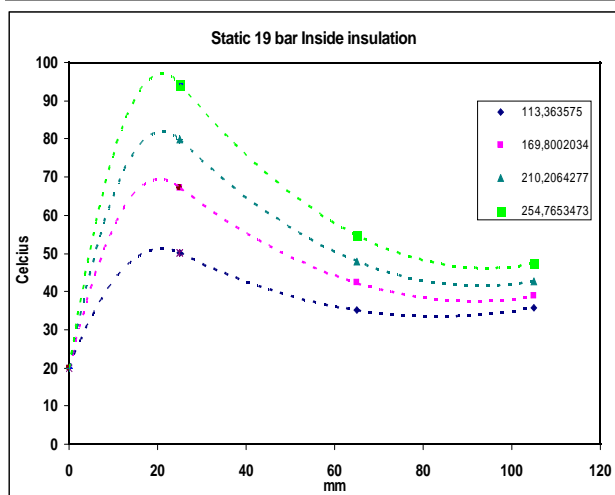
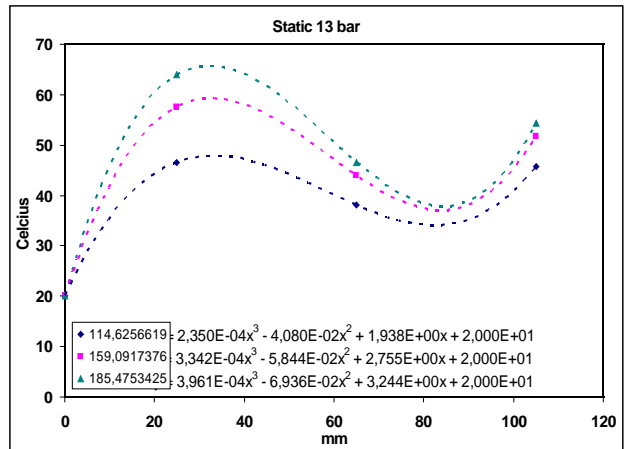
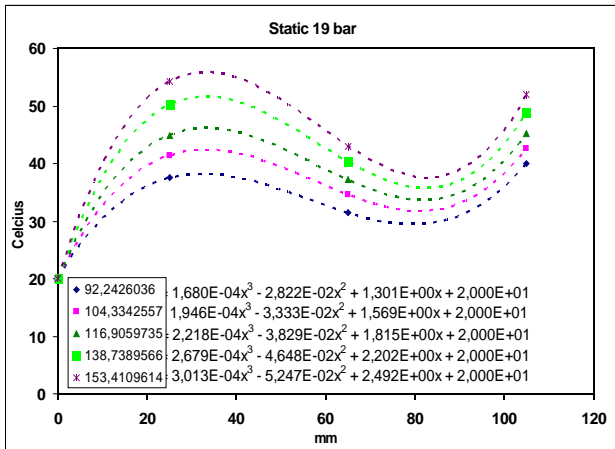
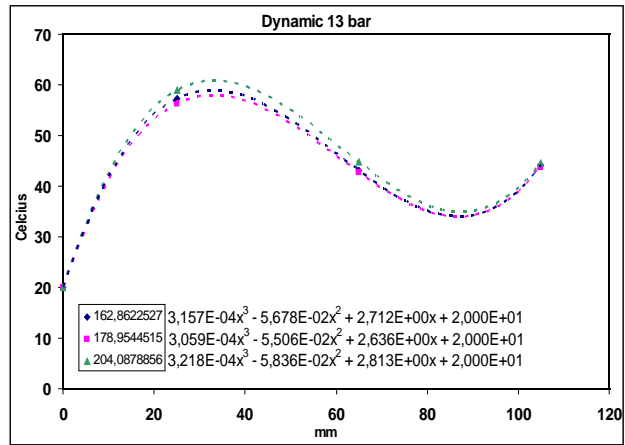
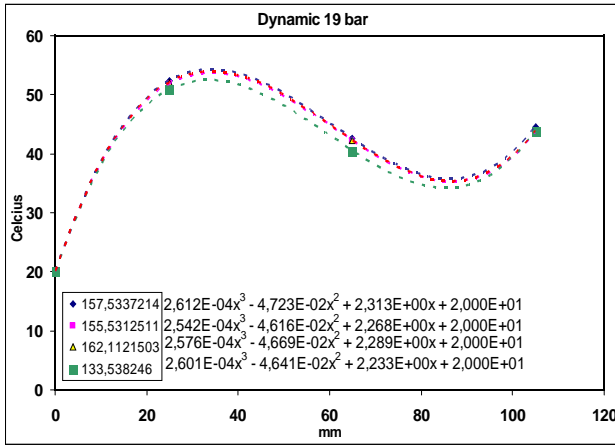
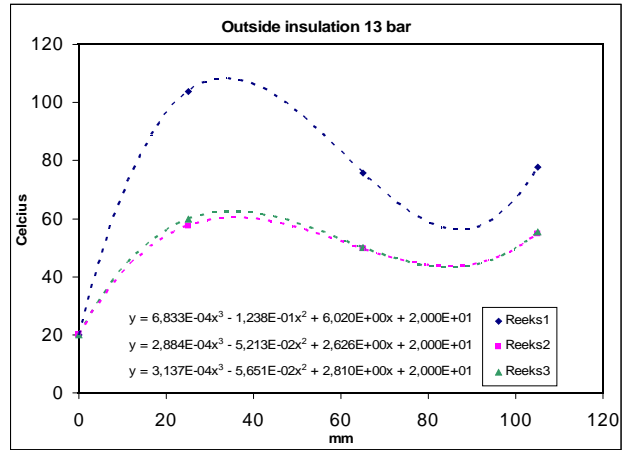
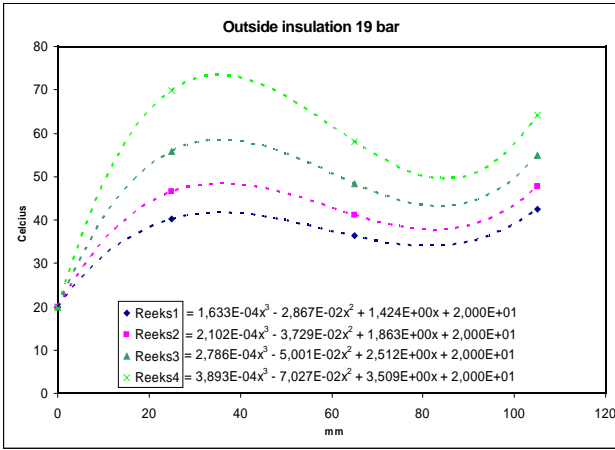
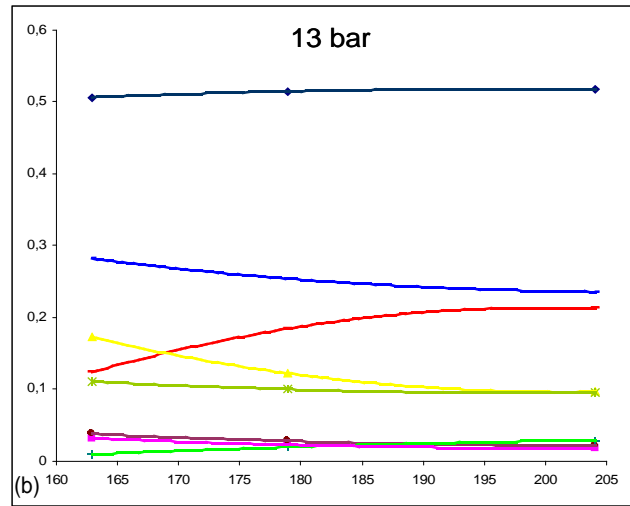
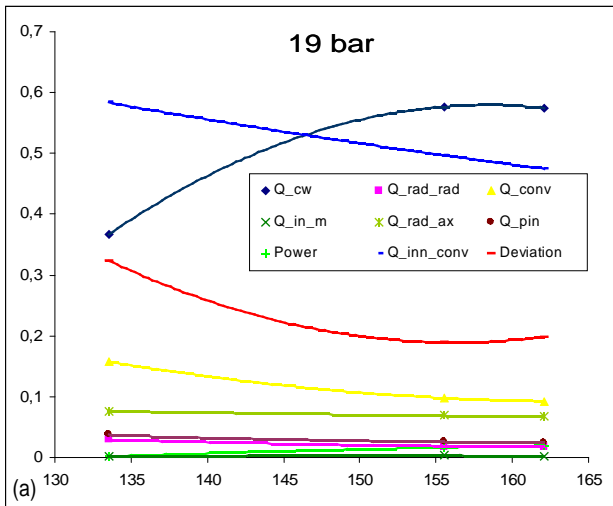


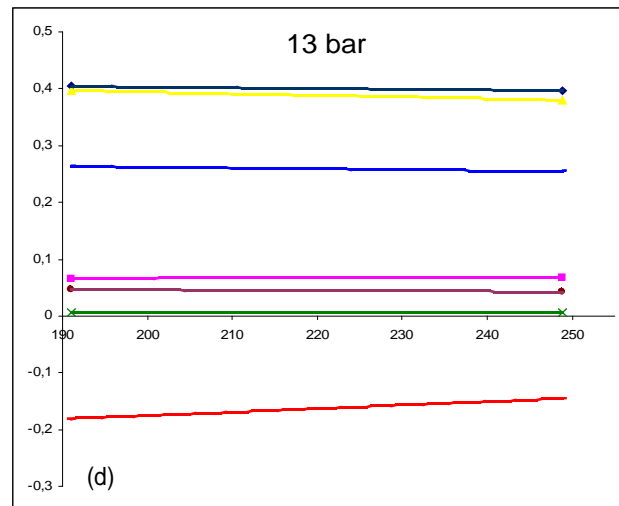
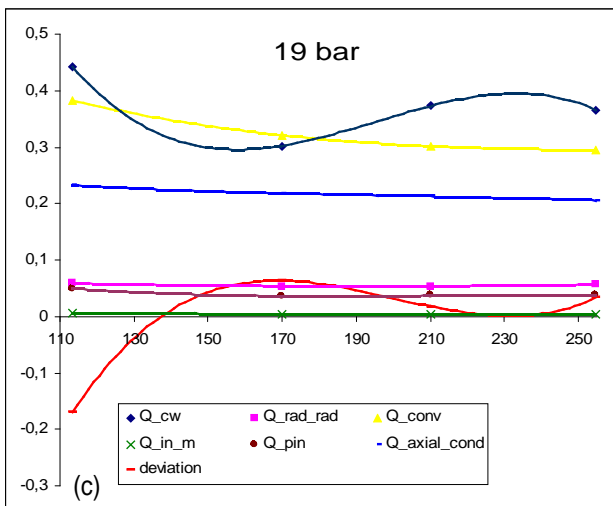
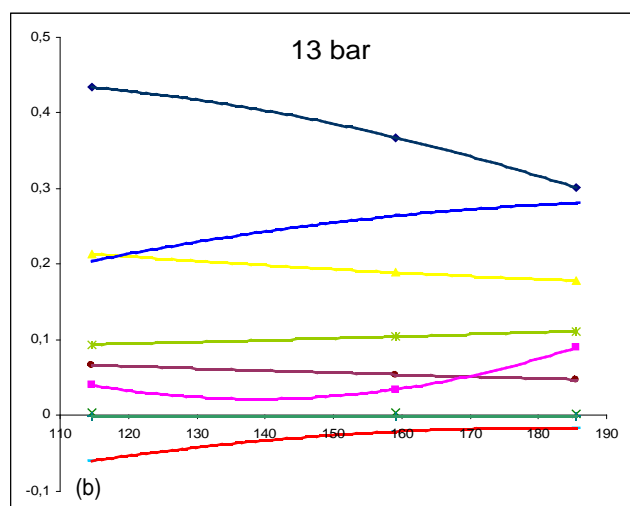
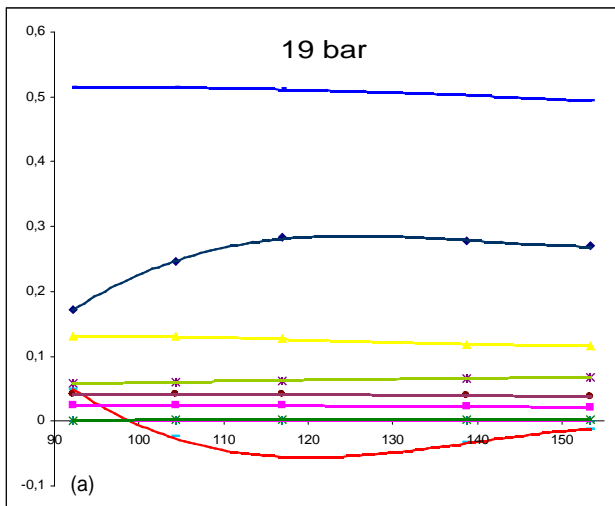
Appendix A1: Temperature profiles single stage



Appendix A2: Heat losses



Dynamic state



Static State (a-b) Inside insulation (c-d) no insulation

Figure A2 On the x axis is the hot regenerator temperature in °C. On the y-axis is the fraction of the heat input

Appendix B The DeltaEC Program

At the university of Los Alamos, New Mexico in the United States of America a software tool was developed in order to predict the behavior of thermoacoustic systems, this software is called DeltaEC.

The program is quite extensive, for this reason the only modules described in this chapter are those used in the simulation of the experimental setup that will be described in chapter 4.

Model Backgrounds

DeltaEC is designed to numerically integrate the wave equation, and other equations in one spatial dimension. It assumes, low amplitudes or low mach numbers and a time dependence of:

$$\alpha(t) = \alpha_0 + \alpha_a e^{i\omega t} \quad (3.1)$$

DeltaEC consists of different modules, they can be standardized parts, or user defined equations. Standardized parts have inputs, such as the dimensions of a geometrical shape. These inputs are presented on the left side of the screen, and use a small letter. Outputs are presented at the right side with a capital. In this way, user defined functions (RPN-blocks) can call these values, use them for calculations, and produce values as inputs for other blocks.

All conservation laws (mass, momentum, Temperature, and energy) apply at all times at all connections between elements. Friction, and other conversion processes are programmed for the segments, and will be stated in this appendix.

Calculation is done by numerical methods. This enables the user to calculate more values at the same time. There is no limit to number of values that can be calculated simultaneously. The user needs to define a guess and a target in order to start the calculation. When the target is met by the correct value of the guess the calculation ends. The user can define multiple guesses as long as the number of targets is equal to the number of guesses, while the calculation decreases in stability as the number of guesses increases. It could also be that the solution is not singular when there are too many guesses defined. Because of the instability of the calculation method, it is important to input guess values in close approximation to their actual values. This can be done by building up the model gradually, and inserting new elements with initial zero length or work, then adjusting the guess values gradually or precalculated by hand a result in more simple geometries in order to establish an initial equilibrium.

When a new calculation is started first of all the program tries to alter the frequency of the acoustic wave to meet the boundary and preset conditions, this is done with the shooting method, start conditions, and frequency variations. When the acoustic equation meets the preset boundaries temperatures are calculated with the shooting method, and so on. Communication between different modules goes through temperature, acoustic energy, gas temperature, phase, pressure, pressure amplitude, and direct current velocity.

There is also a 'begin' module, and 'hardends'. In 'hardends' boundary conditions, such as energy transport, and velocity can be stated. In the begin module general properties for gas, and additional conditions for calculation are inputs. In other modules the material of the solid is an input, although this doesn't have far more consequences than the conductivity. It would be adequate to state all inputs are geometries, material types, and externally connected properties (such as temperature). The boundary condition for solid hardends are no volumetric flow through the wall (real value equals zero) and no volumetric flow along the wall due to friction (imaginary value equals zero) will go through to the next element. The condition is described as a target. This can only happen

when the right frequency, and pressure amplitude occur in the entire geometry. Because these values are correlated, the pressure amplitude and frequency are set as guesses.

Duct, and cone

The duct is the most basic form of element. It is a volume with surface friction and dynamic phase delay. The relation between these is determined by the geometry.

$$\frac{dp_a}{dx} = -\frac{i\omega p_m}{(1-f_v)A} U_a$$

$$\frac{dU_a}{dx} = -\frac{iA\omega}{\rho_m a^2} \left(1 + \frac{\gamma-1}{1+\varepsilon_s} f_T\right) p_a \quad (B2)$$

Where a is the speed of sound in m/s

$$r_0 = 2A/\Pi \quad (B3)$$

The Rott functions B3b are f_T the thermal relaxation dissipation and the f_v viscous dissipation given: if: $r_0/\delta < 25$ (B3a)

$$f_T = \frac{2J_1((i-1)r_0/\delta_T)}{(i-1)(r_0/\delta_T)J_0((i-1)r_0/\delta_T)}$$

$$f_v = \frac{2J_1((i-1)r_0/\delta_v)}{(i-1)(r_0/\delta_v)J_0((i-1)r_0/\delta_v)} \quad (B3b)$$

if: $r_0/\delta > 30$, boundary layer opproximation;

$$f_T = (1-i)\Pi\delta_T/2A, \quad f_v = (1-i)\Pi\delta_v/2A \quad (B3c)$$

Where Π is the perimeter.

There also is an approximation of the Moody diagram for intermediate values.

The ratio between heat transport through the working fluid, and the wall:

$$\varepsilon_s = \left(\frac{k\rho_m c_p}{k_s \rho_s c_s}\right)^{1/2} \quad (B4)$$

For a cone are two additional functions stated for perimeters, and areas

$$\Pi(x) = \Pi_1 + (\Pi_2 - \Pi_1) \frac{x - x_0}{\Delta x}$$

$$A(x) = \left(\sqrt{A_1} + (\sqrt{A_2} - \sqrt{A_1}) \frac{x - x_0}{\Delta x}\right)^2 \quad (B5)$$

A_1 start area, A_2 final area, Π_1 start perimeter, Π_2 final perimeter, and Δx the length are inputs.

Turbulence can be chosen from two options called pessimistic and optimistic turbulence, this is done in the begin module. In optimistic turbulence solely the formulas stated above are valid, there are viscous losses independent on the roughness of the surface. In the case of pessimistic turbulence the turbulent velocity and velocity from the cycle are added to be calculated together in order to increase friction according to the roughness.

When there is pessimistic turbulence, the resistive component of the pressure that could be described by pressure multiplication factor G , and hence the viscous power dissipation is increased.

$$G = \frac{\delta_v^2 N_R f_M - (1 - 9\pi/32) Rn \, d f_M / d Rn}{24\pi r_h^2 \operatorname{Re}(i/(1-f_v))} \quad (B6)$$

Where Rn is the Reynolds number, and f_M the Moody friction factor:

$$\frac{1}{f_M} = 1.74 - 2 \log_{10} \left(2\epsilon + \frac{18.7}{Rn\sqrt{f_M}}\right) \quad (B7)$$

ϵ being the roughness of the surface, which is an input.

More information on the subject of turbulence, and direct current addition and Doppler effects can

be found in the DeltaEC manual chapter 10.1.1. This is left out, because the membranes in our setup eliminate direct currents.

Surface

At the surface acoustic power is dissipated, by thermo-viscous effects Temperature and pressure amplitude are assumed constant, but the volume flow is changed according to the theory of thermal-hysteresis, equation 3.8.

$$U_{a,out} = U_{a,in} - \frac{\omega p_a}{\rho_m a^2} \frac{\gamma - 1}{1 + \varepsilon_s} A_s \frac{\delta_T}{2}, \text{ equation 3.4 applies} \quad (\text{B8})$$

A_s is the surface area, which is an input.

Impedance

In the impedance volumetric flow rate and temperature are constant. The pressure amplitude is:

$$p_{a,out} = p_{a,in} - ZU_a \quad (\text{B9})$$

This comes from the analogy with alternating currents, where Z is the resistance in oscillation. Z is an input, which consists of a real part (due to friction losses), and an imaginary part as the electrical impedance does.

Minor (user defined additional friction) losses

Additional friction can be added by using a minor loss element. Because of sharp angles in the flow, like hard turns, sudden expansion, and geometrical disturbances.

$$\Delta p = -\frac{1}{2} K u^2 \quad (\text{B10})$$

The friction constant K is an input.

Regenerator = Stkscreen

Regenerators can be modeled with a STK segment where a temperature gradient is present.

$$\dot{H}_{total} = \dot{H}_{2,k} + Nm w_m \quad (\text{B11})$$

$$\dot{H}_{2,k} = \frac{1}{2} \text{Re} \left[p_a \tilde{U}_a \left(1 - \frac{T_m \beta (f_T - \tilde{f}_v)}{(1 + \varepsilon_s)(1 + \sigma)(1 - \tilde{f}_v)} \right) \right] + \frac{\rho_m c_p}{2 A_{cs,fluid} \omega (1 + \sigma)(1 - \tilde{f}_v)^2} \frac{T_m U_a^2 Y - (A_{cs,fluid} k_{fluid} + A_{cs,solid} k_{solid}) \frac{dT_m}{dx}}{dx} \quad (\text{B12})$$

$$Y = \text{Im} \left[\tilde{f}_v + \frac{(f_T - \tilde{f}_v)(1 + \varepsilon_s f_v / f_T)}{(1 + \varepsilon_s)(1 + \sigma)} \right]$$

The velocity is changed indirectly through the temperature gradient. For pressure gradients two formulas apply.

$$\frac{dp_{2,0}}{dx} = -\frac{\mu G N_{2,0}}{8 r_h^2 A_{cs} B} \left(c_1(B) + c_2(B) Rn_{2,0} \left(1 + \frac{1}{2 \varepsilon_{2,0}^2} + \frac{|p_a| \cos B}{p_m \varepsilon_{2,0}} \right) \right), \text{ for } |\varepsilon_{2,0}| \geq 1 \quad (\text{B13})$$

B being the input volume porosity, and:

$$\frac{dp_{2,0}}{dx} = -\frac{\mu G N_{2,0}}{8 r_h^2 A_{cs} B} \left(c_1(B) + \frac{c_2(B) Rn_{2,0}}{\pi \varepsilon_{s,2,0}^2} \left[\left(1 + 2 \varepsilon_{s,2,0}^2 + 2 \varepsilon_{2,0} \frac{|p_a| \cos B}{p_m} \right) \sin^{-1} |\varepsilon_{2,0}| + \frac{\varepsilon_{2,0}}{|\varepsilon_{2,0}|} \left(3 \varepsilon_{2,0} + \frac{2(2 + \varepsilon_{2,0}^2) |p_a| \cos B}{3 p_m} \right) \right] \sqrt{1 - \varepsilon_{2,0}^2} \right) \quad (\text{B14})$$

for $|\varepsilon_{2,0}| \geq 1$

$$Rn = \frac{G |N_{2,0}| 4 r_h}{A_{cs} B \mu}$$

Where r_h is the hydraulic diameter, which is an input, which should be chosen as $\frac{1}{4} D_{wire} B / (1 - B)$, D_{wire} is the wire diameter, $N_{2,0}$ is the molar flux at the end of the segment, and:

$$\varepsilon_{2,0} = G N_{2,0} / \rho_m |U_a| \quad (\text{B15})$$

Thermal Buffer Tube = Stkduct

In a thermal buffer tube the same wave-function applies as in a normal tube, however here thermoacoustics are not negligible, and a temperature gradient is added.

The thermal buffer tube acts like a stack with a single channel. Consequently a heating effect takes place along the wall.

$$\frac{dp_a}{dx} = -\frac{i\omega p_m}{(1-f_v)A} U_a$$

$$\frac{dU_a}{dx} = -\frac{iA\omega}{\rho_m a^2} \left(1 + \frac{\gamma-1}{1+\varepsilon_s} f_k\right) p_a + \frac{\beta(f_T - f_v)}{(1-f_v)(1-\sigma)(1+\varepsilon_s)} \frac{dT_m}{dx} U_a \quad (\text{B16})$$

$$\frac{dT_m}{dx} = \frac{\dot{H}_{2,k} - \frac{1}{2} \text{Re} \left[p_a \tilde{U}_a \left(1 - \frac{T_m \beta (f_T - \tilde{f}_v)}{(1+\varepsilon_s)(1+\sigma)(1-\tilde{f}_v)}\right) \right]}{\frac{\rho_m c_p}{2A_{cs,fluid} \omega (1+\sigma)(1-\tilde{f}_v)^2} \text{Im} \left[\tilde{f}_v + \frac{(f_T - \tilde{f}_v)(1+\varepsilon_s f_v/f_T)}{(1+\varepsilon_s)(1+\sigma)} \right] - (A_{cs,fluid} k_{fluid} + A_{cs,solid} k_{solid})} \quad (\text{B17})$$

Here formula 3.3c and 3.16 apply

$$\varepsilon_s = \left(\frac{k \rho_m c_p}{k_s \rho_s c_s} \right)^{1/2} \frac{1}{\tanh((1+i)l/\delta_s)} \quad (\text{B18})$$

where: $l = A_{cs,wall} / \Pi_{wall}$

HX, and TX (heat exchangers)

Heat exchangers HX have parallel plates, while TX have a shell and tube geometry. Equations 3.2, 3.3, and 3.4 also apply.

if: $25 < r_0 / \delta < 30$

$$f_T = \frac{\tanh((1+i)y_0/\delta_T)}{(1+i)y_0/\delta_T}, \quad f_v = \frac{\tanh((1+i)y_0/\delta_v)}{(1+i)y_0/\delta_v} \quad (\text{B19})$$

$$\frac{dT_m}{dx} = 0 \quad (\text{B20})$$

$$T_{solid} = T_m + \frac{\dot{Q}}{hA_{cs,gas} x_{eff} / r}$$

Appendix B 1 Predictions by DeltaEC

The program has been proven to effectively find simple optimum geometries. This is used, so both the series, and parallel configurations are optimized for the resonator dimensions of the laboratory setup.

The effect of deviation from this optimum, and the possibility of improvement on the resonator dimension will also be done in DeltaEC. After the experiments the DeltaEC model is compared with the results.

Optimization in Series.

In DeltaEC it is easy to optimize the setup. In this section two hypothetical dimensions are changed, and two real dimensions are changed. Dimensions are called hypothetical when the shell that is provided for these experiments doesn't allow free manipulation of these dimensions. Real dimensions can be changed without the need of new components for the setup.

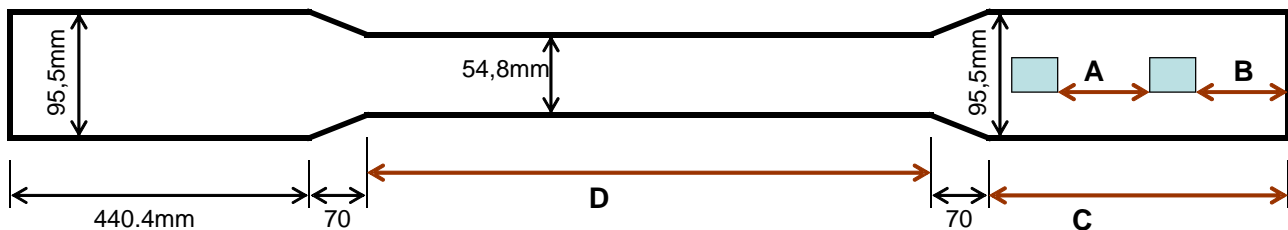


Figure 3.1 Dimension Analyzes

The most important issue is optimization of the distance between the regenerator blocks was found to peak at no distance between the blocks. However the difference between 0 mm and 75 mm (75 being the geometrical maximum when not placing the generator inside the cone) was less than 0,05% of 11,55% thermal efficiency. One may argue that this doesn't represent a serial multistage setup, because one connection between the compliance, and impedance is missing. On the other hand thermal buffer tubes can be shortened to overcome this issue, or the issue could simply be ignored considering the lower thermal power would be the only point of interest. When series are compared to parallel it is preferable the series is a real series configuration, besides no spacing would mean a high power input to the second stage, and a high difference in operating conditions of both stages.

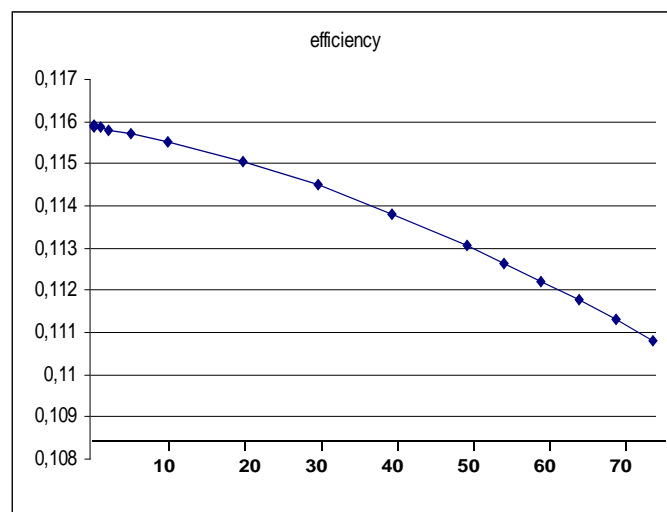


Figure B2.1 Efficiency as a function of the distance between generator 1, and the thermal buffer tube of generator 2. of the overall thermoacoustic system in series from deltaE simulation. The value A on the x-axis goes from 0 to 75mm. The first compliance was 120mm (value B) the first regenerator 130mm, and the second regenerator was 100mm.

When the thermal efficiency is plotted against the distance between the first stage/generator, and the wall the correlation is alarmingly high. The thermal efficiency could drop 9 % from the total of 12 % when the first stage is placed incorrectly (figure B2.2). Since there is a lot of space used by cooling pipes, and signal lines, and electrical wires for the heater it would be best to place the first stage just over 120 mm from the wall.

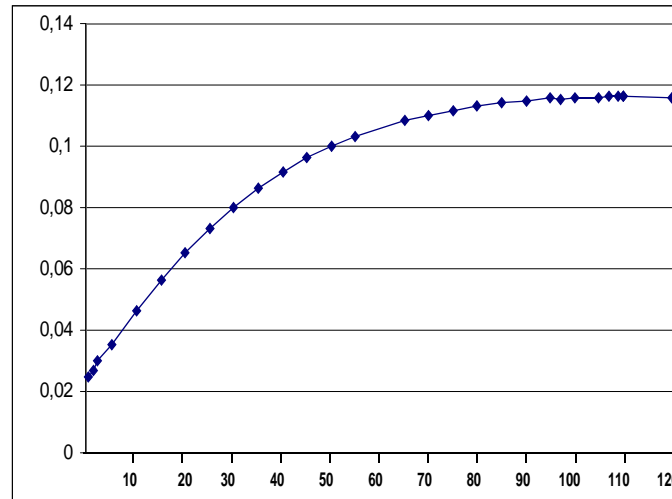


Figure B2.2 Efficiency as a function of distance between outer regenerator, and end seal of the overall thermoacoustic system in series from deltaE simulation. The x-axis goes from 0 to 120mm spacing between the first generator, and the compliance wall. The distance between the two generators was 1mm. The first regenerator was 130mm, and the second regenerator was 100mm.

Optimization of the values for C and D is removed from this report, because the resonator in which the experiments are conducted was already built and can not easily undergo changes in geometry.

The DeltaEC code was made by ECN and only needed adjustments for geometry and data retrieval.

Appendix B2: Parallel configuration

```

1 C:\Users\CHRIS\Documents\Parrespet\masterfile_parallel Two stage engine (symmetric
  located on either ends)
2 Two engines in a half wavelength resonator. We call this parallel
3 arrangement in contrast with series multi stage engine. This exercise helps
4 us examine the merits and demerits of series or parallel config. The main
5 objective is to look for configurations that offer low temperature driven
6 systems.
7 0 BEGIN
8 1.9000E+06 a Mean P Pa
9 Gues 71.318 b Freq Hz
10 300.00 c TBeg K
11 Gues 1.0317E+05 d |p| Pa
12 0.0000 e Ph(p) deg
13 0.0000 f |U| m^3/s
14 0.0000 g Ph(U) deg
15 Optional Parameters
16 nitrogen Gas type
17 1 RPN Drive ratio 5.4298E-02 A ChngMe
18 0.0000 a G or T
19 0d 0a /
20 2 DUCT compliance
21 7.1630E-03 a Area m^2 Mstr 1.0210E+05 A |p| Pa
22 0.30002 b Perim m 2a 1.1297E-03 B Ph(p) deg
23 0.1130 c Length m 1.4027E-02 C |U| m^3/s
24 2.0000E-03 d Srough -90.034 D Ph(U) deg
25 Master-Slave Links 0.0000 E Htot W
26 Optional Parameters -0.44484 F Edot W
27 ideal Solid type
28 3 TBRANCH Change Me
29 Gues -5.8580E+05 a Re(Zb) Pa-s/m^3 1.0210E+05 A |p| Pa
30 Gues 6.9314E+06 b Im(Zb) Pa-s/m^3 1.1297E-03 B Ph(p) deg
31 Master-Slave Links 1.4678E-02 C |U| m^3/s
32 -94.83 D Ph(U) deg
33 Optional Parameters -63.107 E HtotBr W
34 -63.107 F EdotBr W
35 62.662 G EdotTr W
36 4 DUCT Change Me
37 4.4660E-03 a Area m^2 9.6750E+04 A |p| Pa
38 0.48412 b Perim m 0.2134 B Ph(p) deg
39 0.1280 c Length m 2.4269E-02 C |U| m^3/s
40 2.0000E-03 d Srough -92.913 D Ph(U) deg
41 Master-Slave Links -63.107 E Htot W
42 Optional Parameters -64.039 F Edot W
43 ideal Solid type
44 5 SOFTEND Change Me
45 9.6750E+04 A |p| Pa
46 0.2134 B Ph(p) deg
47 2.4269E-02 C |U| m^3/s
48 -92.913 D Ph(U) deg
49 -63.107 E Htot W
50 Possible targets -64.039 F Edot W
51 -0.12889 G Re(z)
52 2.3594 H Im(z)
53 300.00 I T K
54 6 DUCT Change Me
55 2.5072E-03 a Area m^2 Mstr 1.0212E+05 A |p| Pa
56 0.1775 b Perim m 6a -2.5210E-02 B Ph(p) deg
57 1.0000E-02 c Length m 1.2382E-03 C |U| m^3/s

```

59	Master-Slave Links					63.107	E	Htot	W
60	Optional Parameters					62.639	F	Edot	W
61	ideal	Solid type							
62	7 MINOR	Change Me							
63	Same	6a	2.5072E-03	a Area	m^2	1.0211E+05	A	p	Pa
64			4.0000	b K+		-2.5882E-02	B	Ph(p)	deg
65			4.0000	c K-		1.2382E-03	C	U	m^3/s
66						7.7581	D	Ph(U)	deg
67						63.107	E	Htot	W
68						62.634	F	Edot	W
69	8 TX	Change Me							
70	Same	6a	2.5072E-03	a Area	m^2	1.0211E+05	A	p	Pa
71			0.3460	b GasA/A		-0.14673	B	Ph(p)	deg
72			1.5000E-02	c Length	m	1.2219E-03	C	U	m^3/s
73			1.0000E-03	d radius	m	-2.9641	D	Ph(U)	deg
74	Gues		-160.26	e HeatIn	W	-97.157	E	Htot	W
75	Master-Slave Links					62.306	F	Edot	W
76	Possible targets					300.00	G	GasT	K
77	ideal	Solid type				259.53	H	SolidT	K
78	9 STKSCREEN	Change Me							
79			2.3578E-03	a Area	m^2	9.7673E+04	A	p	Pa
80			0.7866	b VolPor		0.62041	B	Ph(p)	deg
81			1.4500E-02	c Length	m	2.8998E-03	C	U	m^3/s
82			2.7650E-05	d rh	m	-24.343	D	Ph(U)	deg
83			0.2000	e ksFrac		-97.157	E	Htot	W
84	Master-Slave Links					128.38	F	Edot	W
85						300.00	G	TBeg	K
86	stainless	Solid type				677.93	H	TEnd	K
87	10 HX	Change Me							
88	Same	6a	2.5072E-03	a Area	m^2	9.7648E+04	A	p	Pa
89			0.3800	b GasA/A		0.5950	B	Ph(p)	deg
90			3.6000E-03	c Length	m	2.9232E-03	C	U	m^3/s
91			9.0000E-04	d y0	m	-25.394	D	Ph(U)	deg
92	OPlt		250.00	e HeatIn	W	152.84	E	Htot	W
93	Master-Slave Links					128.29	F	Edot	W
94	Possible targets					677.93	G	GasT	K
95	ideal	Solid type				879.22	H	SolidT	K
96	11 RPN	ChangeMe							
97			393.97	a G or T		677.93	A	ChngeMe	
98	10G								
99	12 STKDUCT	Change Me							
100	Same	6a	2.5072E-03	a Area	m^2	9.7025E+04	A	p	Pa
101			0.1775	b Perim	m	0.29234	B	Ph(p)	deg
102			8.1400E-02	c Length	m	5.3147E-03	C	U	m^3/s
103			2.9500E-04	d WallA	m^2	-59.928	D	Ph(U)	deg
104	Master-Slave Links					152.84	E	Htot	W
105						128.05	F	Edot	W
106						677.93	G	TBeg	K
107	stainless	Solid type				308.00	H	TEnd	K
108	13 RPN	ChangeMe							
109			0.0000	a G or T		-24.94	A	ChngeMe	
110	14F 12E -								
111	14 TX	Change Me							
112	Same	6a	2.5072E-03	a Area	m^2	9.6750E+04	A	p	Pa
113			0.3460	b GasA/A		0.2134	B	Ph(p)	deg
114			5.0000E-03	c Length	m	5.3771E-03	C	U	m^3/s
115			1.0000E-03	d radius	m	-60.333	D	Ph(U)	deg
116	Same	13A	-24.94	e HeatIn	W	127.90	E	Htot	W

117	Targ	300.00	f	SolidT	K			127.90	F	Edot	W
118	Master-Slave Links							308.00	G	GasT	K
119	ideal	Solid type						300.00	H	SolidT	K
120	15 UNION	Change Me									
121	5 a	SegNum						9.6750E+04	A	p	Pa
122	TargSame 5A	9.6750E+04	b	p Sft	Pa			0.2134	B	Ph(p)	deg
123	TargSame 5B	0.2134	c	Ph(p)S	deg			2.8945E-02	C	U	m^3/s
124	Possible targets							-87.172	D	Ph(U)	deg
125								64.796	E	Htot	W
126								63.864	F	Edot	W
127								308.00	G	T	K
128	16 DUCT	Change Me									
129		7.1630E-03	a	Area	m^2	Mstr		9.1702E+04	A	p	Pa
130		0.30002	b	Perim	m	16a		0.10013	B	Ph(p)	deg
131		0.1100	c	Length	m			4.1470E-02	C	U	m^3/s
132		2.0000E-03	d	Srough				-87.99	D	Ph(U)	deg
133	Master-Slave Links							64.796	E	Htot	W
134	Optional Parameters							63.376	F	Edot	W
135	ideal	Solid type									
136	17 DUCT	Change Me									
137		7.1630E-03	a	Area	m^2	Mstr		8.6932E+04	A	p	Pa
138		0.30002	b	Perim	m	17a		1.0348E-02	B	Ph(p)	deg
139		8.0000E-02	c	Length	m			5.0101E-02	C	U	m^3/s
140		2.0000E-03	d	Srough				-88.333	D	Ph(U)	deg
141	Master-Slave Links							64.796	E	Htot	W
142	Optional Parameters							62.938	F	Edot	W
143	ideal	Solid type									
144	18 CONE	Change Me									
145		7.1630E-03	a	AreaI	m^2	Mstr		8.2053E+04	A	p	Pa
146		0.30002	b	PerimI	m	18a		-7.0489E-02	B	Ph(p)	deg
147		4.5000E-02	c	Length	m			5.3215E-02	C	U	m^3/s
148		2.8000E-03	d	AreaF	m^2	Mstr		-88.437	D	Ph(U)	deg
149		0.18758	e	PerimF	m	18d		64.796	E	Htot	W
150		2.0000E-03	f	Srough				62.232	F	Edot	W
151	Master-Slave Links										
152	Optional Parameters										
153	ideal	Solid type									
154	19 MINOR	Change Me									
155	Same 20a	2.8000E-03	a	Area	m^2			8.2023E+04	A	p	Pa
156		0.5000	b	K+				1.0423	B	Ph(p)	deg
157		0.5000	c	K-				5.3215E-02	C	U	m^3/s
158								-88.437	D	Ph(U)	deg
159								64.796	E	Htot	W
160								19.832	F	Edot	W
161	20 DUCT	Change Me									
162	Same 18d	2.8000E-03	a	Area	m^2	Mstr		6.6940E-10	A	p	Pa
163		0.18758	b	Perim	m	20a		-179.64	B	Ph(p)	deg
164		0.4200	c	Length	m			6.1562E-02	C	U	m^3/s
165	Same 18f	2.0000E-03	d	Srough				-88.539	D	Ph(U)	deg
166	Master-Slave Links							64.796	E	Htot	W
167	Optional Parameters							-3.9762E-13	F	Edot	W
168	ideal	Solid type									
169	21 RPN	dr									
170		0.0000	a	G or T				29.482	A	ChngMe	
171						P		5.4298	B	ChngMe	
172	0d 0a / 100 * 21A 21A *										
173	22 RPN	phase difference between pressure and velocity									
174		180.00	a	G or T				-91.106	A	ChngMe	

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175 20B 20D -
176 23 SOFTEND Change Me
177 Targ 0.0000 a Re(z) 6.6940E-10 A |p| Pa
178 Targ 0.0000 b Im(z) -179.64 B Ph(p) deg
179 6.1562E-02 C |U| m^3/s
180 -88.539 D Ph(U) deg
181 64.796 E Htot W
182 Possible targets -3.9762E-13 F Edot W
183 -7.9007E-17 G Re(z)
184 -4.0934E-15 H Im(z)
185 308.00 I T K
186 24 RPN Eta Carnot
187 0.0000 a G or T P 0.25546 A Eta
188 0.55747 B Eta Car
189 1 9G 9H / - 15F 10e /
190 25 RPN Etar
191 0.0000 a G or T P 0.45824 A ChngeMe
192 24A 24B /

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Appendix B3 Serial configuration

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1 C:\Users\CHRIS\Documents\Parrespet\masterfile_series Two stage engine in series (
  stage)
2 Minor losses are made zero to compare with parallel configuration
3 0 BEGIN 0
4 1.9000E+06 a Mean P Pa
5 Gues 72.223 b Freq Hz
6 300.00 c TBeg K
7 Gues 1.1128E+05 d |p| Pa
8 0.0000 e Ph(p) deg
9 0.0000 f |U| m^3/s
10 0.0000 g Ph(U) deg
11 Optional Parameters
12 nitrogen Gas type
13 1 SURFACE Closed end
14 Same 2a 7.1630E-03 a Area m^2 1.1128E+05 A |p| Pa
15 0.0000 B Ph(p) deg
16 1.9627E-06 C |U| m^3/s
17 180.00 D Ph(U) deg
18 0.0000 E Htot W
19 ideal Solid type -0.10921 F Edot W
20 2 DUCT tube
21 7.1630E-03 a Area m^2 1.1011E+05 A |p| Pa
22 0.3000 b Perim m 1.3071E-03 B Ph(p) deg
23 0.1130 c Length m 1.5321E-02 C |U| m^3/s
24 2.0000E-03 d Srough -90.041 D Ph(U) deg
25 Master-Slave Links 0.0000 E Htot W
26 Optional Parameters -0.63012 F Edot W
27 ideal Solid type
28 3 TBRANCH split
29 Gues -6.1395E+05 a Re(Zb) Pa-s/m^3 1.1011E+05 A |p| Pa
30 Gues 6.8468E+06 b Im(Zb) Pa-s/m^3 1.3071E-03 B Ph(p) deg
31 Master-Slave Links 1.6017E-02 C |U| m^3/s
32 -95.123 D Ph(U) deg
33 Optional Parameters -78.754 E HtotBr W
34 -78.754 F EdotBr W
35 78.124 G EdotTr W
36 4 RPN Larea
37 Same 4A 4.6558E-03 a G or T 4.6558E-03 A ChngMe
38 2a 9a -
39 5 DUCT Change Me
40 4.4660E-03 a Area m^2 1.0419E+05 A |p| Pa
41 0.48412 b Perim m 0.23158 B Ph(p) deg
42 0.1280 c Length m 2.6481E-02 C |U| m^3/s
43 2.0000E-03 d Srough -93.087 D Ph(U) deg
44 Master-Slave Links -78.754 E Htot W
45 Optional Parameters -79.857 F Edot W
46 stainless Solid type
47 6 SOFTEND Change Me
48 1.0419E+05 A |p| Pa
49 0.23158 B Ph(p) deg
50 2.6481E-02 C |U| m^3/s
51 -93.087 D Ph(U) deg
52 -78.754 E Htot W
53 Possible targets -79.857 F Edot W
54 -0.13499 G Re(z)
55 2.3281 H Im(z)
56 300.00 I T K
57 7 DUCT dummy duct

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59          1.0000 b Perim m          1.3071E-03 B Ph(p) deg
60          0.0000 c Length m        1.5533E-03 C |U| m^3/s
61          0.0000 d Srough          23.998 D Ph(U) deg
62 Master-Slave Links                78.754 E Htot W
63 Optional Parameters                78.124 F Edot W
64 ideal Solid type
65      8 BEGIN
66      Same 0a 1.9000E+06 a Mean P Pa
67      Same 0b 72.223 b Freq Hz
68          300.00 c TBeg K
69      Same 7A 1.1011E+05 d |p| Pa
70      Same 7B 1.3071E-03 e Ph(p) deg
71      Same 7C 1.5533E-03 f |U| m^3/s
72      Same 7D 23.998 g Ph(U) deg
73 Optional Parameters
74 Sameas 0 nitrogen Gas type
75      9 DUCT 10
76          2.5072E-03 a Area m^2 Mstr 1.1012E+05 A |p| Pa
77          0.17749 b Perim m 9a -2.7289E-02 B Ph(p) deg
78          1.0000E-02 c Length m 1.4275E-03 C |U| m^3/s
79          3.0000E-04 d Srough 6.4470 D Ph(U) deg
80 Master-Slave Links                78.124 E Htot W
81 Optional Parameters                78.098 F Edot W
82 stainless Solid type
83      10 MINOR Change Me
84      Same 9a 2.5072E-03 a Area m^2 1.1012E+05 A |p| Pa
85          4.0000 b K+ -2.7633E-02 B Ph(p) deg
86          0.0000 c K- 1.4275E-03 C |U| m^3/s
87          6.4470 D Ph(U) deg
88          78.124 E Htot W
89          78.094 F Edot W
90      11 TX Rhx1 9
91      Same 9a 2.5072E-03 a Area m^2 1.1011E+05 A |p| Pa
92          0.3460 b GasA/A -0.15867 B Ph(p) deg
93          1.5000E-02 c Length m 1.4142E-03 C |U| m^3/s
94          1.0000E-03 d radius m -3.6968 D Ph(U) deg
95 Gues -164.7 e HeatIn W -86.579 E Htot W
96 Master-Slave Links                77.709 F Edot W
97 Possible targets                    300.00 G GasT K
98 stainless Solid type                263.77 H SolidT K
99      12 STKSCREEN regen 1
100          2.3578E-03 a Area m^2 1.0520E+05 A |p| Pa
101          0.7866 b VolPor 0.64047 B Ph(p) deg
102          1.5000E-02 c Length m 3.0477E-03 C |U| m^3/s
103          2.7650E-05 d rh m -25.152 D Ph(U) deg
104          0.2000 e ksFrac -86.579 E Htot W
105 Master-Slave Links                144.34 F Edot W
106          300.00 G TBeg K
107          610.49 H TEnd K
108      13 RPN ChangeMe
109          0.0000 a G or T 18.663 A ChngMe
110 16e 11e + 11F + 12F -
111      14 RPN Tc-Reg
112          297.70 a G or T 300.00 A FreeT
113 12G
114      15 RPN temp.R1
115          400.00 a G or T 610.49 A FreeT
116 12H

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117	16 HX	hhx1								
118	Same	9a	2.5072E-03	a Area	m ²	1.0518E+05	A p	Pa		
119			0.3800	b GasA/A		0.61287	B Ph(p)	deg		
120			3.6000E-03	c Length	m	3.0741E-03	C U	m ³ /s		
121			9.0000E-04	d y0	m	-26.23	D Ph(U)	deg		
122			250.00	e HeatIn	W	163.42	E Htot	W		
123	Master-Slave Links						144.24	F Edot	W	
124	Possible targets						610.49	G GasT	K	
125	stainless	Solid type					807.92	H SolidT	K	
126	17 STKDUCT	Change Me								
127	Same	9a	2.5072E-03	a Area	m ²	1.0449E+05	A p	Pa		
128	Same	9b	0.17749	b Perim	m	0.30954	B Ph(p)	deg		
129	Same	18A	7.9400E-02	c Length	m	5.6523E-03	C U	m ³ /s		
130			2.9500E-04	d WallA	m ²	-60.509	D Ph(U)	deg		
131	Master-Slave Links						163.42	E Htot	W	
132						143.99	F Edot	W		
133						610.49	G TBeg	K		
134	stainless	Solid type					321.31	H TEnd	K	
135	18 RPN	cal. L-tbz								
136			2.5000E-02	a G or T		7.9400E-02	A ChngMe			
137	5c 9c - 11c - 12c - 16c - 19c -									
138	19 TX	Rhx1								
139			2.3758E-03	a Area	m ²	1.0419E+05	A p	Pa		
140			0.3460	b GasA/A		0.23158	B Ph(p)	deg		
141			5.0000E-03	c Length	m	5.7172E-03	C U	m ³ /s		
142			1.0000E-03	d radius	m	-60.897	D Ph(U)	deg		
143			-63.029	e HeatIn	W	100.39	E Htot	W		
144	Targ		300.00	f SolidT	K	143.81	F Edot	W		
145	Master-Slave Links						321.31	G GasT	K	
146	stainless	Solid type					300.00	H SolidT	K	
147	20 UNION	Rejoin								
148	6 a	SegNum								
149	TargSame	5A	1.0419E+05	b p Sft	Pa	0.23158	B Ph(p)	deg		
150	TargSame	5B	0.23158	c Ph(p)S	deg	3.1467E-02	C U	m ³ /s		
151	Possible targets						-87.533	D Ph(U)	deg	
152						21.638	E Htot	W		
153						63.954	F Edot	W		
154						321.31	G T	K		
155	21 RPN	power output								
156			5.0000	a G or T		63.954	A FreeT			
157	20F									
158	22 RPN	COP1								
159			0.1000	a G or T		0.10476	A ChngMe			
160	20F 16G /									
161	23 DUCT	Room temp duct								
162	Same	5a	4.4660E-03	a Area	m ²	1.0355E+05	A p	Pa		
163	Same	5b	0.48412	b Perim	m	0.21936	B Ph(p)	deg		
164			1.0000E-02	c Length	m	3.2260E-02	C U	m ³ /s		
165			2.0000E-03	d Srough		-87.591	D Ph(U)	deg		
166	Master-Slave Links						21.638	E Htot	W	
167	Optional Parameters						63.825	F Edot	W	
168	ideal	Solid type								
169	24 TBRANCH	split								
170	Gues		-7.1457E+04	a Re(Zb)	Pa-s/m ³	1.0355E+05	A p	Pa		
171	Gues		3.1581E+06	b Im(Zb)	Pa-s/m ³	0.21936	B Ph(p)	deg		
172	Master-Slave Links						3.2778E-02	C U	m ³ /s	
173						-91.077	D Ph(U)	deg		
174	Optional Parameters						-38.388	E HtotBr	W	

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175                                     -38.388 F EdotBr W
176                                     102.21 G EdotTr W
177      25 RPN          Byp2-L
178          0.1000 a G or T          0.1890 A ChngMe
179 0.44 2c - 5c - 23c -
180      26 RPN          Larea2
181          4.3800E-03 a G or T      4.6558E-03 A ChngMe
182 2a 31a -
183      27 DUCT          Change Me
184      Same 26A 4.6558E-03 a Area m^2 Mstr 9.6374E+04 A |p| Pa
185          0.50883 b Perim m      27a 0.32115 B Ph(p) deg
186          0.1000 c Length m      4.0740E-02 C |U| m^3/s
187          3.0000E-04 d Srough      -90.833 D Ph(U) deg
188 Master-Slave Links          -38.388 E Htot W
189 Optional Parameters          -39.537 F Edot W
190 stainless Solid type
191      28 SOFTEND      Change Me
192                                     9.6374E+04 A |p| Pa
193                                     0.32115 B Ph(p) deg
194                                     4.0740E-02 C |U| m^3/s
195                                     -90.833 D Ph(U) deg
196                                     -38.388 E Htot W
197 Possible targets          -39.537 F Edot W
198                                     -3.0465E-02 G Re(z)
199                                     1.5124 H Im(z)
200                                     321.31 I T K
201      29 DUCT          dummy duct used to get input properties 23
202          1.0000 a Area m^2          1.0355E+05 A |p| Pa
203          1.0000 b Perim m          0.21936 B Ph(p) deg
204          0.0000 c Length m          2.0452E-03 C |U| m^3/s
205          0.0000 d Srough          15.351 D Ph(U) deg
206 Master-Slave Links          60.026 E Htot W
207 Optional Parameters          102.21 F Edot W
208 ideal Solid type
209      30 BEGIN
210      Same 0a 1.9000E+06 a Mean P Pa
211      Same 0b 72.223 b Freq Hz
212          300.00 c TBeg K
213      Same 29A 1.0355E+05 d |p| Pa
214      Same 29B 0.21936 e Ph(p) deg
215      Same 29C 2.0452E-03 f |U| m^3/s
216      Same 29D 15.351 g Ph(U) deg
217 Optional Parameters
218 Sameas 0 nitrogen Gas type
219      31 DUCT          10
220      Same 9a 2.5072E-03 a Area m^2 Mstr 1.0356E+05 A |p| Pa
221          0.17752 b Perim m      31a 0.17706 B Ph(p) deg
222          1.0000E-02 c Length m      1.9757E-03 C |U| m^3/s
223          3.0000E-04 d Srough      2.8448 D Ph(U) deg
224 Master-Slave Links          102.21 E Htot W
225 Optional Parameters          102.19 F Edot W
226 stainless Solid type
227      32 MINOR      Change Me
228      Same 9a 2.5072E-03 a Area m^2          1.0353E+05 A |p| Pa
229          4.0000 b K+          0.17648 B Ph(p) deg
230          4.0000 c K-          1.9757E-03 C |U| m^3/s
231                                     2.8448 D Ph(U) deg
232                                     102.21 E Htot W

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233									102.17	F	Edot	W
234	33 TX	Rhx1										9
235	Same 31a	2.5072E-03	a	Area	m ²				1.0351E+05	A	p	Pa
236	Same 11b	0.3460	b	GasA/A					-1.7146E-02	B	Ph(p)	deg
237	Same 11c	1.5000E-02	c	Length	m				1.9721E-03	C	U	m ³ /s
238	Same 11d	1.0000E-03	d	radius	m				-4.0237	D	Ph(U)	deg
239	Gues	-233.38	e	HeatIn	W				-131.17	E	Htot	W
240	Master-Slave Links								101.82	F	Edot	W
241	Possible targets								300.00	G	GasT	K
242	stainless	Solid type							263.05	H	SolidT	K
243	34 STKSCREEN	regen 2										
244		2.3578E-03	a	Area	m ²				9.6966E+04	A	p	Pa
245	Same 12b	0.7866	b	VolPor					0.79601	B	Ph(p)	deg
246		1.3200E-02	c	Length	m				4.0874E-03	C	U	m ³ /s
247	Same 12d	2.7650E-05	d	rh	m				-17.726	D	Ph(U)	deg
248	Same 12e	0.2000	e	ksFrac					-131.17	E	Htot	W
249	Master-Slave Links								187.90	F	Edot	W
250									300.00	G	TBeg	K
251	stainless	Solid type							610.49	H	TEnd	K
252	35 RPN	ChangeMe										
253		0.0000	a	G or T					29.113	A	ChngMe	
254	39e 33e + 33F + 34F -											
255	36 RPN	Tc-reg2										
256		301.40	a	G or T					300.00	A	FreeT	
257	34G											
258	37 RPN	temp.R2										
259	TargSame 15A	610.49	a	G or T					610.49	A	FreeT	
260	34H											
261	38 RPN	ChangeMe										
262		0.0000	a	G or T					348.58	A	ChngMe	
263	39e											
264	39 HX	hhx1										
265	Same 31a	2.5072E-03	a	Area	m ²				9.6936E+04	A	p	Pa
266	Same 16b	0.3800	b	GasA/A					0.75328	B	Ph(p)	deg
267	Same 16c	3.6000E-03	c	Length	m				4.1047E-03	C	U	m ³ /s
268	Same 16d	9.0000E-04	d	y0	m				-18.507	D	Ph(U)	deg
269	Gues	348.58	e	HeatIn	W				217.41	E	Htot	W
270	Master-Slave Links								187.81	F	Edot	W
271	Possible targets								610.49	G	GasT	K
272	stainless	Solid type							885.78	H	SolidT	K
273	40 STKDUCT	Change Me										
274	Same 31a	2.5072E-03	a	Area	m ²				9.6586E+04	A	p	Pa
275	Same 31b	0.17752	b	Perim	m				0.44177	B	Ph(p)	deg
276	Same 41A	5.3200E-02	c	Length	m				5.2489E-03	C	U	m ³ /s
277		2.9500E-04	d	WallA	m ²				-41.833	D	Ph(U)	deg
278	Master-Slave Links								217.41	E	Htot	W
279									187.56	F	Edot	W
280									610.49	G	TBeg	K
281	stainless	Solid type							320.18	H	TEnd	K
282	41 RPN	calc.of tbz length										
283		5.0000E-02	a	G or T					5.3200E-02	A	ChngMe	
284	27c 31c - 33c - 34c - 39c - 42c -											
285	42 TX	Rhx1										
286	Same 31a	2.5072E-03	a	Area	m ²				9.6374E+04	A	p	Pa
287		0.3460	b	GasA/A					0.32115	B	Ph(p)	deg
288		5.0000E-03	c	Length	m				5.2971E-03	C	U	m ³ /s
289		1.0000E-03	d	radius	m				-42.437	D	Ph(U)	deg
290		-63.029	e	HeatIn	W				154.39	E	Htot	W

291	Targ	300.00	f	SolidT	K	187.41	F	Edot	W
292	Master-Slave Links					320.18	G	GasT	K
293	stainless	Solid type				300.00	H	SolidT	K
294	43 RPN	ChangeMe							
295		0.0000	a	G or T		0.0000	A	ChngeMe	
296	0.212 rho * 42C * 41a / 41a / 43a *								
297	44 IMPEDANCE	minor loss							
298	Same 43A	0.0000	a	Re(Zs)	Pa-s/m^3	9.6374E+04	A	p	Pa
299		0.0000	b	Im(Zs)	Pa-s/m^3	0.32115	B	Ph(p)	deg
300	Master-Slave Links					5.2971E-03	C	U	m^3/s
301						-42.437	D	Ph(U)	deg
302						154.39	E	Htot	W
303						187.41	F	Edot	W
304	45 UNION	Rejoin							
305	28 a	SegNum				9.6374E+04	A	p	Pa
306	TargSame 27A	9.6374E+04	b	p Sft	Pa	0.32115	B	Ph(p)	deg
307	TargSame 27B	0.32115	c	Ph(p)S	deg	4.4434E-02	C	U	m^3/s
308	Possible targets					-85.719	D	Ph(U)	deg
309						116.00	E	Htot	W
310						147.87	F	Edot	W
311						320.18	G	T	K
312	46 DUCT	tube							
313		7.1630E-03	a	Area	m^2	9.1406E+04	A	p	Pa
314		0.3000	b	Perim	m	0.13149	B	Ph(p)	deg
315		8.0000E-02	c	Length	m	5.3608E-02	C	U	m^3/s
316		2.0000E-03	d	Srough		-86.42	D	Ph(U)	deg
317	Master-Slave Links					116.00	E	Htot	W
318	Optional Parameters					147.35	F	Edot	W
319	ideal	Solid type							
320	47 CONE	cone							
321		7.1630E-03	a	AreaI	m^2	8.6328E+04	A	p	Pa
322		0.3000	b	PerimI	m	-4.9885E-02	B	Ph(p)	deg
323		4.5000E-02	c	Length	m	5.6920E-02	C	U	m^3/s
324		2.8000E-03	d	AreaF	m^2	-86.63	D	Ph(U)	deg
325		0.1720	e	PerimF	m	116.00	E	Htot	W
326		2.0000E-03	f	Srough		146.56	F	Edot	W
327	Master-Slave Links								
328	Optional Parameters								
329	stainless	Solid type							
330	48 MINOR	Change Me							
331	Same 47d	2.8000E-03	a	Area	m^2	8.6241E+04	A	p	Pa
332		0.5000	b	K+		1.1132	B	Ph(p)	deg
333		0.5000	c	K-		5.6920E-02	C	U	m^3/s
334						-86.63	D	Ph(U)	deg
335						116.00	E	Htot	W
336						96.651	F	Edot	W
337	49 DUCT	resonat.							
338	Same 47d	2.8000E-03	a	Area	m^2	6.2068E+04	A	p	Pa
339	Same 47e	0.1720	b	Perim	m	0.43482	B	Ph(p)	deg
340		0.1260	c	Length	m	6.1403E-02	C	U	m^3/s
341	Same 47f	2.0000E-03	d	Srough		-86.83	D	Ph(U)	deg
342	Master-Slave Links					116.00	E	Htot	W
343	Optional Parameters					90.942	F	Edot	W
344	stainless	Solid type							
345	50 DUCT	resonat.							
346	Same 49a	2.8000E-03	a	Area	m^2	2.1728E+04	A	p	Pa
347	Same 49b	0.1720	b	Perim	m	-3.5983	B	Ph(p)	deg
348		0.1960	c	Length	m	6.5348E-02	C	U	m^3/s

349	Same 47f	<i>2.0000E-03</i>	d	Srough		<i>-87.071</i>	D	Ph(U)	deg
350	Master-Slave Links					<i>116.00</i>	E	Htot	W
351	Optional Parameters					<i>80.702</i>	F	Edot	W
352	stainless			Solid type					
353	51 DUCT			resonat.					
354	Same 49a	<i>2.8000E-03</i>	a	Area	m ²	<i>2.0220E+04</i>	A	p	Pa
355	Same 49b	<i>0.1720</i>	b	Perim	m	<i>-171.2</i>	B	Ph(p)	deg
356		<i>0.1960</i>	c	Length	m	<i>6.5417E-02</i>	C	U	m ³ /s
357	Same 47f	<i>2.0000E-03</i>	d	Srough		<i>-87.259</i>	D	Ph(U)	deg
358	Master-Slave Links					<i>116.00</i>	E	Htot	W
359	Optional Parameters					<i>69.794</i>	F	Edot	W
360	stainless			Solid type					
361	52 DUCT			resonat.					
362	Same 49a	<i>2.8000E-03</i>	a	Area	m ²	<i>8.4915E+04</i>	A	p	Pa
363	Same 49b	<i>0.1720</i>	b	Perim	m	<i>-176.25</i>	B	Ph(p)	deg
364		<i>0.3220</i>	c	Length	m	<i>5.7203E-02</i>	C	U	m ³ /s
365	Same 47f	<i>2.0000E-03</i>	d	Srough		<i>-87.513</i>	D	Ph(U)	deg
366	Master-Slave Links					<i>116.00</i>	E	Htot	W
367	Optional Parameters					<i>53.757</i>	F	Edot	W
368	stainless			Solid type					
369	53 MINOR			Change Me					
370	Same 47d	<i>2.8000E-03</i>	a	Area	m ²	<i>8.4894E+04</i>	A	p	Pa
371		<i>0.5000</i>	b	K+		<i>-177.44</i>	B	Ph(p)	deg
372		<i>0.5000</i>	c	K-		<i>5.7203E-02</i>	C	U	m ³ /s
373						<i>-87.513</i>	D	Ph(U)	deg
374						<i>116.00</i>	E	Htot	W
375						<i>3.0982</i>	F	Edot	W
376	54 CONE			cone					
377	Same 47d	<i>2.8000E-03</i>	a	AreaI	m ²	<i>9.0007E+04</i>	A	p	Pa
378	Same 47e	<i>0.1720</i>	b	PerimI	m	<i>-177.46</i>	B	Ph(p)	deg
379		<i>4.5000E-02</i>	c	Length	m	<i>5.3937E-02</i>	C	U	m ³ /s
380	Same 2a	<i>7.1630E-03</i>	d	AreaF	m ²	<i>-87.512</i>	D	Ph(U)	deg
381	Same 2b	<i>0.3000</i>	e	PerimF	m	<i>116.00</i>	E	Htot	W
382	Same 47f	<i>2.0000E-03</i>	f	Srough		<i>2.3031</i>	F	Edot	W
383	Master-Slave Links								
384	Optional Parameters								
385	stainless			Solid type					
386	55 DUCT			Change Me					
387	Same 58a	<i>7.1630E-03</i>	a	Area	m ²	<i>1.0073E+05</i>	A	p	Pa
388		<i>0.3000</i>	b	Perim	m	<i>-177.47</i>	B	Ph(p)	deg
389		<i>0.1990</i>	c	Length	m	<i>3.0610E-02</i>	C	U	m ³ /s
390		<i>2.0000E-03</i>	d	Srough		<i>-87.517</i>	D	Ph(U)	deg
391	Master-Slave Links					<i>116.00</i>	E	Htot	W
392	Optional Parameters					<i>1.1862</i>	F	Edot	W
393	ideal			Solid type					
394	56 RPN			ChangeMe					
395		<i>0.0000</i>	a	G or T		<i>0.2410</i>	A	ChngeMe	
396	0.44 55c -								
397	57 DUCT			Change Me					
398	Same 58a	<i>7.1630E-03</i>	a	Area	m ²	<i>1.0440E+05</i>	A	p	Pa
399	Same 58b	<i>0.3000</i>	b	Perim	m	<i>-177.48</i>	B	Ph(p)	deg
400		<i>0.1280</i>	c	Length	m	<i>1.4522E-02</i>	C	U	m ³ /s
401		<i>2.0000E-03</i>	d	Srough		<i>-87.522</i>	D	Ph(U)	deg
402	Master-Slave Links					<i>116.00</i>	E	Htot	W
403	Optional Parameters					<i>0.59871</i>	F	Edot	W
404	ideal			Solid type					
405	58 DUCT			tube					
406	Same 2a	<i>7.1630E-03</i>	a	Area	m ²	<i>1.0545E+05</i>	A	p	Pa

407	Same	2b	0.3000	b Perim	m	-177.48	B Ph(p)	deg	
408			0.1130	c Length	m	1.9689E-06	C U	m^3/s	
409	Same	47f	2.0000E-03	d Srough		-177.48	D Ph(U)	deg	
410	Master-Slave Links						116.00	E Htot	W
411	Optional Parameters						0.10381	F Edot	W
412	ideal	Solid type							
413	59	SURFACE	Change Me						
414	Same	2a	7.1630E-03	a Area	m^2	1.0545E+05	A p	Pa	
415						-177.48	B Ph(p)	deg	
416						1.2949E-15	C U	m^3/s	
417						91.065	D Ph(U)	deg	
418						116.00	E Htot	W	
419	ideal	Solid type				-1.7354E-12	F Edot	W	
420	60	HARDEND	Change Me						
421	Targ		0.0000	a R(1/z)		1.0545E+05	A p	Pa	
422	Targ		0.0000	b I(1/z)		-177.48	B Ph(p)	deg	
423						1.2949E-15	C U	m^3/s	
424						91.065	D Ph(U)	deg	
425	Possible targets						116.00	E Htot	W
426						-1.7354E-12	F Edot	W	
427						-3.1785E-16	G R(1/z)		
428						-1.2500E-14	H I(1/z)		
429	61	RPN	Acoustic Polwer						
430			0.0000	a G or T		152.72	A ChngeMe		
431	34F 33F - 12F + 11F -								
432	62	RPN	Eta & Carnot						
433			0.0000	a G or T		0.24704	A ChngeMe		
434						0.50859	B ChngeMe		
435	1 34G 34H / - 45F 16e 39e + /								
436	63	RPN	Eta_r						
437			0.0000	a G or T		0.48573	A ChngeMe		
438	62A 62B /								
439	64	RPN	Dr						
440			0.0000	a G or T		30.800	A ChngeMe		
441						5.5498	B ChngeMe		
442	60A 0a / 100 * 64A 64A *								
443	65	RPN	Dr Engine side						
444			0.0000	a G or T		34.303	A ChngeMe		
445						5.8569	B ChngeMe		
446	0d 0a / 100 * 65A 65A *								
447	66	RPN	ChangeMe						
448			0.0000	a G or T		83.918	A ChngeMe		
449	45F 20F -								
450	67	RPN	Eta engines						
451			0.0000	a G or T		0.25582	A ChngeMe		
452						0.24074	B ChngeMe		
453	66A 39e / 20F 16e /								

Appendix B4: Serial configuration with load

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1  F:\series_load Two stage engine in series (multi stage) with external load
2  Minor losses are made zero to compare with parallel configuration
3  0 BEGIN 0
4  1.9000E+06 a Mean P Pa
5  Gues 64.839 b Freq Hz
6  300.00 c TBeg K
7  4.3700E+04 d |p| Pa
8  0.0000 e Ph(p) deg
9  0.0000 f |U| m^3/s
10 0.0000 g Ph(U) deg
11 Optional Parameters
12 nitrogen Gas type
13 1 SURFACE Closed end
14 Same 2a 7.1630E-03 a Area m^2 4.3700E+04 A |p| Pa
15 0.0000 B Ph(p) deg
16 7.3030E-07 C |U| m^3/s
17 180.00 D Ph(U) deg
18 0.0000 E Htot W
19 ideal Solid type -1.5957E-02 F Edot W
20 2 DUCT tube
21 7.1630E-03 a Area m^2 4.3328E+04 A |p| Pa
22 0.3000 b Perim m 1.1105E-03 B Ph(p) deg
23 0.1130 c Length m 5.4055E-03 C |U| m^3/s
24 2.0000E-03 d Srough -90.044 D Ph(U) deg
25 Master-Slave Links 0.0000 E Htot W
26 Optional Parameters -9.1957E-02 F Edot W
27 ideal Solid type
28 3 TBRANCH split
29 Gues -9.2184E+05 a Re(Zb) Pa-s/m^3 4.3328E+04 A |p| Pa
30 Gues 7.8153E+06 b Im(Zb) Pa-s/m^3 1.1105E-03 B Ph(p) deg
31 Master-Slave Links 5.5058E-03 C |U| m^3/s
32 -96.726 D Ph(U) deg
33 Optional Parameters -13.972 E HtotBr W
34 -13.972 F EdotBr W
35 13.880 G EdotTr W
36 4 RPN Larea
37 Same 4A 4.6023E-03 a G or T 4.6023E-03 A ChngeMe
38 2a 9a -
39 5 DUCT Change Me
40 Same 4A 4.6023E-03 a Area m^2 4.1533E+04 A |p| Pa
41 0.4404 b Perim m 0.22475 B Ph(p) deg
42 0.1280 c Length m 9.3310E-03 C |U| m^3/s
43 2.0000E-03 d Srough -93.952 D Ph(U) deg
44 Master-Slave Links -13.972 E Htot W
45 Optional Parameters -14.112 F Edot W
46 stainless Solid type
47 6 SOFTEND Change Me
48 4.1533E+04 A |p| Pa
49 0.22475 B Ph(p) deg
50 9.3310E-03 C |U| m^3/s
51 -93.952 D Ph(U) deg
52 -13.972 E Htot W
53 Possible targets -14.112 F Edot W
54 -0.198 G Re(z)
55 2.7115 H Im(z)
56 300.00 I T K
57 7 DUCT dummy duct
58 1.0000 a Area m^2 4.3328E+04 A |p| Pa

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59          1.0000 b Perim m          1.1105E-03 B Ph(p) deg
60          0.0000 c Length m        6.4375E-04 C |U| m^3/s
61          0.0000 d Srough          5.5683 D Ph(U) deg
62 Master-Slave Links                13.972 E Htot W
63 Optional Parameters                13.880 F Edot W
64 ideal Solid type
65      8 BEGIN
66          2.0000E+06 a Mean P Pa
67      Same 0b 64.839 b Freq Hz
68          300.00 c TBeg K
69      Same 7A 4.3328E+04 d |p| Pa
70      Same 7B 1.1105E-03 e Ph(p) deg
71      Same 7C 6.4375E-04 f |U| m^3/s
72      Same 7D 5.5683 g Ph(U) deg
73 Optional Parameters
74 Sameas 0 nitrogen Gas type
75      9 DUCT 10
76          2.5607E-03 a Area m^2 Mstr 4.3328E+04 A |p| Pa
77          0.17937 b Perim m 9a -2.9234E-02 B Ph(p) deg
78          1.0000E-02 c Length m 6.4813E-04 C |U| m^3/s
79          3.0000E-04 d Srough -8.7982 D Ph(U) deg
80 Master-Slave Links                13.880 E Htot W
81 Optional Parameters                13.877 F Edot W
82 stainless Solid type
83      10 RPN minor loss
84          0.0000 a G or T          0.0000 A ChngMe
85 0.212 rho * 9C * 9a / 9a / 10a *
86      11 IMPEDANCE Change Me
87      Same 10A 0.0000 a Re(Zs) Pa-s/m^3 4.3328E+04 A |p| Pa
88          0.0000 b Im(Zs) Pa-s/m^3 -2.9234E-02 B Ph(p) deg
89 Master-Slave Links                6.4813E-04 C |U| m^3/s
90          -8.7982 D Ph(U) deg
91          13.880 E Htot W
92          13.877 F Edot W
93      12 TX Rhx1 9
94      Same 9a 2.5607E-03 a Area m^2 4.3297E+04 A |p| Pa
95          0.3460 b GasA/A -0.16655 B Ph(p) deg
96          1.5000E-02 c Length m 6.6435E-04 C |U| m^3/s
97          1.0000E-03 d radius m -16.201 D Ph(U) deg
98 Gues -38.564 e HeatIn W -24.683 E Htot W
99 Master-Slave Links                13.823 F Edot W
100 Possible targets                300.00 G GasT K
101 stainless Solid type                283.04 H SolidT K
102      13 STKSCREEN regen 1
103      Same 9a 2.5607E-03 a Area m^2 4.2043E+04 A |p| Pa
104          0.7866 b VolPor 0.64786 B Ph(p) deg
105          1.5000E-02 c Length m 1.0694E-03 C |U| m^3/s
106          2.7650E-05 d rh m -34.679 D Ph(U) deg
107          0.2000 e ksFrac -24.683 E Htot W
108 Master-Slave Links                18.341 F Edot W
109          300.00 G TBeg K
110 stainless Solid type                436.62 H TEnd K
111      14 RPN Tc-Reg
112          297.70 a G or T          300.00 A FreeT
113 13G
114      15 RPN temp.R1
115          627.93 a G or T          436.62 A FreeT
116 13H

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117	16 HX	hhx1							
118	Same	9a	2.5607E-03	a Area	m ²	4.2027E+04	A p	Pa	
119			0.3800	b GasA/A		0.61992	B Ph(p)	deg	
120			3.6000E-03	c Length	m	1.0818E-03	C U	m ³ /s	
121			9.0000E-04	d y0	m	-35.641	D Ph(U)	deg	
122	Gues		55.120	e HeatIn	W	30.437	E Htot	W	
123	Master-Slave Links					18.330	F Edot	W	
124	Possible targets					436.62	G GasT	K	
125	stainless	Solid type				478.67	H SolidT	K	
126	17 STKDUCT	Change Me							
127	Same	9a	2.5607E-03	a Area	m ²	4.1675E+04	A p	Pa	
128	Same	9b	0.17937	b Perim	m	0.30383	B Ph(p)	deg	
129	Same	18A	7.9400E-02	c Length	m	2.0695E-03	C U	m ³ /s	
130			2.9500E-04	d WallA	m ²	-64.573	D Ph(U)	deg	
131	Master-Slave Links					30.437	E Htot	W	
132						18.308	F Edot	W	
133						436.62	G TBeg	K	
134	stainless	Solid type				222.18	H TEnd	K	
135	18 RPN	cal. L-tbz							
136			2.5000E-02	a G or T		7.9400E-02	A ChngMe		
137	5c 9c - 12c - 13c - 16c - 19c -								
138	19 TX	Rhx1							
139	Same	9a	2.5607E-03	a Area	m ²	4.1533E+04	A p	Pa	
140			0.3460	b GasA/A		0.22475	B Ph(p)	deg	
141			5.0000E-03	c Length	m	2.0941E-03	C U	m ³ /s	
142			1.0000E-03	d radius	m	-64.907	D Ph(U)	deg	
143	Gues		252.53	e HeatIn	W	282.97	E Htot	W	
144	Targ		300.00	f SolidT	K	18.288	F Edot	W	
145	Master-Slave Links					222.18	G GasT	K	
146	stainless	Solid type				300.00	H SolidT	K	
147	20 RPN	ChangeMe							
148			0.0000	a G or T		0.0000	A ChngMe		
149	0.212 rho * 19C * 19a / 19a / 20a *								
150	21 IMPEDANCE	minor loss							
151	Same	20A	0.0000	a Re(Zs)	Pa-s/m ³	4.1533E+04	A p	Pa	
152			0.0000	b Im(Zs)	Pa-s/m ³	0.22475	B Ph(p)	deg	
153	Master-Slave Links					2.0941E-03	C U	m ³ /s	
154						-64.907	D Ph(U)	deg	
155						282.97	E Htot	W	
156						18.288	F Edot	W	
157	22 UNION	Rejoin							
158	6 a	SegNum				4.1533E+04	A p	Pa	
159	Targ		1.0471E+05	b p Sft	Pa	0.22475	B Ph(p)	deg	
160	Targ		0.5499	c Ph(p)S	deg	1.1208E-02	C U	m ³ /s	
161	Possible targets					-88.747	D Ph(U)	deg	
162						269.00	E Htot	W	
163						4.1756	F Edot	W	
164						222.18	G T	K	
165	23 RPN	power output							
166			5.0000	a G or T		4.1756	A FreeT		
167	22F								
168	24 RPN	COP1							
169			0.1000	a G or T		9.5636E-03	A ChngMe		
170	22F 16G /								
171	25 DUCT	Room temp duct							
172			7.1630E-03	a Area	m ²	4.1336E+04	A p	Pa	
173	Same	2b	0.3000	b Perim	m	0.22022	B Ph(p)	deg	
174			1.0000E-02	c Length	m	1.1640E-02	C U	m ³ /s	

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175          2.0000E-03 d Srough          -88.787 D Ph(U) deg
176 Master-Slave Links          269.00 E Htot W
177 Optional Parameters          4.1702 F Edot W
178 ideal          Solid type
179      26 TBRANCH          split
180 Gues          -4.0886E+05 a Re(Zb) Pa-s/m^3          4.1336E+04 A |p| Pa
181 Gues          3.5585E+06 b Im(Zb) Pa-s/m^3          0.22022 B Ph(p) deg
182 Master-Slave Links          1.1540E-02 C |U| m^3/s
183          -96.334 D Ph(U) deg
184 Optional Parameters          -27.225 E HtotBr W
185          -27.225 F EdotBr W
186          31.395 G EdotTr W
187      27 RPN          Byp2-L
188          0.1000 a G or T          0.1890 A ChngMe
189 0.44 2c - 5c - 25c -
190      28 RPN          Larea2
191          4.3800E-03 a G or T          4.6023E-03 A ChngMe
192 2a 33a -
193      29 DUCT          Change Me
194 Same 28A 4.6023E-03 a Area m^2          3.7889E+04 A |p| Pa
195          0.5059 b Perim m          0.76966 B Ph(p) deg
196          0.1000 c Length m          1.4185E-02 C |U| m^3/s
197          2.0000E-03 d Srough          -95.072 D Ph(U) deg
198 Master-Slave Links          -27.225 E Htot W
199 Optional Parameters          -27.351 F Edot W
200 stainless          Solid type
201      30 SOFTEND          Change Me
202          3.7889E+04 A |p| Pa
203          0.76966 B Ph(p) deg
204          1.4185E-02 C |U| m^3/s
205          -95.072 D Ph(U) deg
206          -27.225 E Htot W
207 Possible targets          -27.351 F Edot W
208          -0.13576 G Re(z)
209          1.3269 H Im(z)
210          222.18 I T K
211      31 DUCT          dummy duct used to get input properties 23
212          1.0000 a Area m^2          4.1336E+04 A |p| Pa
213          1.0000 b Perim m          0.22022 B Ph(p) deg
214          0.0000 c Length m          1.5289E-03 C |U| m^3/s
215          0.0000 d Srough          -6.2927 D Ph(U) deg
216 Master-Slave Links          296.22 E Htot W
217 Optional Parameters          31.395 F Edot W
218 ideal          Solid type
219      32 BEGIN
220 Same 0a 1.9000E+06 a Mean P Pa
221 Same 0b 64.839 b Freq Hz
222          300.00 c TBeg K
223 Same 31A 4.1336E+04 d |p| Pa
224 Same 31B 0.22022 e Ph(p) deg
225 Same 31C 1.5289E-03 f |U| m^3/s
226 Same 31D -6.2927 g Ph(U) deg
227 Optional Parameters
228 Sameas 0 nitrogen Gas type
229      33 DUCT          10
230          2.5607E-03 a Area m^2 Mstr          4.1327E+04 A |p| Pa
231          0.1794 b Perim m 33a          0.14858 B Ph(p) deg
232          1.0000E-02 c Length m          1.5554E-03 C |U| m^3/s

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233		3.0000E-04	d	Srough		-12.244	D	Ph(U)	deg
234	Master-Slave Links					31.395	E	Htot	W
235	Optional Parameters					31.392	F	Edot	W
236	stainless			Solid type					
237	34 RPN			minor loss					
238		0.0000	a	G or T		0.0000	A	ChngMe	
239	0.212 rho * 33C * 33a / 33a / 34a *								
240	35 IMPEDANCE			Change Me					
241	Same 34A	0.0000	a	Re(Zs) Pa-s/m^3		4.1327E+04	A	p	Pa
242		0.0000	b	Im(Zs) Pa-s/m^3		0.14858	B	Ph(p)	deg
243	Master-Slave Links					1.5554E-03	C	U	m^3/s
244						-12.244	D	Ph(U)	deg
245						31.395	E	Htot	W
246						31.392	F	Edot	W
247	36 TX			Rhx1	9				
248	Same 33a	2.5607E-03	a	Area m^2		4.1253E+04	A	p	Pa
249	Same 12b	0.3460	b	GasA/A		-0.17625	B	Ph(p)	deg
250	Same 12c	1.5000E-02	c	Length m		1.5737E-03	C	U	m^3/s
251	Same 12d	1.0000E-03	d	radius m		-15.345	D	Ph(U)	deg
252	Gues	-79.317	e	HeatIn W		-47.921	E	Htot	W
253	Master-Slave Links					31.328	F	Edot	W
254	Possible targets					300.00	G	GasT	K
255	stainless			Solid type		284.99	H	SolidT	K
256	37 STKSCREEN			regen 2					
257	Same 33a	2.5607E-03	a	Area m^2		3.8151E+04	A	p	Pa
258	Same 13b	0.7866	b	VolPor		1.3650	B	Ph(p)	deg
259		1.3200E-02	c	Length m		2.3473E-03	C	U	m^3/s
260	Same 13d	2.7650E-05	d	rh m		-23.208	D	Ph(U)	deg
261	Same 13e	0.2000	e	ksFrac		-47.921	E	Htot	W
262	Master-Slave Links					40.720	F	Edot	W
263						300.00	G	TBeg	K
264	stainless			Solid type		436.62	H	TEnd	K
265	38 RPN			Tc-reg2					
266		301.40	a	G or T		300.00	A	FreeT	
267	37G								
268	39 RPN			temp.R2					
269	TargSame 15A	436.62	a	G or T		436.62	A	FreeT	
270	37H								
271	40 HX			hhx1					
272	Same 33a	2.5607E-03	a	Area m^2		3.8125E+04	A	p	Pa
273	Same 16b	0.3800	b	GasA/A		1.2924	B	Ph(p)	deg
274	Same 16c	3.6000E-03	c	Length m		2.3556E-03	C	U	m^3/s
275	Same 16d	9.0000E-04	d	y0 m		-23.676	D	Ph(U)	deg
276	Gues	99.847	e	HeatIn W		51.926	E	Htot	W
277	Master-Slave Links					40.708	F	Edot	W
278	Possible targets					436.62	G	GasT	K
279	stainless			Solid type		514.77	H	SolidT	K
280	41 STKDUCT			Change Me					
281	Same 33a	2.5607E-03	a	Area m^2		3.7889E+04	A	p	Pa
282	Same 33b	0.1794	b	Perim m		0.76882	B	Ph(p)	deg
283	Same 42A	5.8200E-02	c	Length m		2.8287E-03	C	U	m^3/s
284		2.9500E-04	d	WallA m^2		-39.85	D	Ph(U)	deg
285	Master-Slave Links					51.926	E	Htot	W
286						40.676	F	Edot	W
287						436.62	G	TBeg	K
288	stainless			Solid type		300.00	H	TEnd	K
289	42 RPN			calc.of tbz length					
290		5.0000E-02	a	G or T		5.8200E-02	A	ChngMe	

291	29c 33c - 36c - 37c - 40c - 0.0 -							
292	43 RPN	ChangeMe						
293	Targ	300.00	a G or T		300.00	A	ChngeMe	
294	41H							
295	44 IMPEDANCE	minor loss						
296	Same 43A	300.00	a Re(Zs)	Pa-s/m ³	3.7889E+04	A	p	Pa
297		0.0000	b Im(Zs)	Pa-s/m ³	0.76966	B	Ph(p)	deg
298	Master-Slave Links				2.8287E-03	C	U	m ³ /s
299					-39.85	D	Ph(U)	deg
300					51.926	E	Htot	W
301					40.675	F	Edot	W
302	45 UNION	Rejoin						
303	30 a	SegNum			3.7889E+04	A	p	Pa
304	Targ	9.8327E+04	b p Sft	Pa	0.76966	B	Ph(p)	deg
305	Targ	0.7405	c Ph(p)S	deg	1.5968E-02	C	U	m ³ /s
306	Possible targets				-86.706	D	Ph(U)	deg
307				P	24.701	E	Htot	W
308					13.324	F	Edot	W
309					300.00	G	T	K
310	46 DUCT	tube						
311		7.1630E-03	a Area	m ²	3.6178E+04	A	p	Pa
312		0.3000	b Perim	m	0.66532	B	Ph(p)	deg
313		8.0000E-02	c Length	m	1.9220E-02	C	U	m ³ /s
314		2.0000E-03	d Srough		-87.148	D	Ph(U)	deg
315	Master-Slave Links				24.701	E	Htot	W
316	Optional Parameters				13.265	F	Edot	W
317	ideal	Solid type						
318	47 CONE	cone						
319		7.1630E-03	a AreaI	m ²	3.4273E+04	A	p	Pa
320		0.3000	b PerimI	m	0.55557	B	Ph(p)	deg
321		4.5000E-02	c Length	m	2.0334E-02	C	U	m ³ /s
322		2.3543E-03	d AreaF	m ²	-87.272	D	Ph(U)	deg
323		0.1720	e PerimF	m	24.701	E	Htot	W
324		2.0000E-03	f Srough		13.206	F	Edot	W
325	Master-Slave Links							
326	Optional Parameters							
327	stainless	Solid type						
328	48 DUCT	resonat.						
329	Same 47d	2.3543E-03	a Area	m ²	2.4725E+04	A	p	Pa
330	Same 47e	0.1720	b Perim	m	-0.16288	B	Ph(p)	deg
331		0.1230	c Length	m	2.1645E-02	C	U	m ³ /s
332	Same 47f	2.0000E-03	d Srough		-87.429	D	Ph(U)	deg
333	Master-Slave Links				24.701	E	Htot	W
334	Optional Parameters				12.763	F	Edot	W
335	stainless	Solid type						
336	49 DUCT	resonat.						
337	Same 48a	2.3543E-03	a Area	m ²	8260.1	A	p	Pa
338	Same 48b	0.1720	b Perim	m	-4.9192	B	Ph(p)	deg
339		0.2000	c Length	m	2.2839E-02	C	U	m ³ /s
340	Same 47f	2.0000E-03	d Srough		-87.641	D	Ph(U)	deg
341	Master-Slave Links				24.701	E	Htot	W
342	Optional Parameters				11.951	F	Edot	W
343	stainless	Solid type						
344	50 DUCT	resonat.						
345	Same 48a	2.3543E-03	a Area	m ²	8798.6	A	p	Pa
346	Same 48b	0.1720	b Perim	m	-171.48	B	Ph(p)	deg
347		0.2000	c Length	m	2.2819E-02	C	U	m ³ /s
348	Same 47f	2.0000E-03	d Srough		-87.822	D	Ph(U)	deg

349	Master-Slave Links					24.701	E	Htot	W
350	Optional Parameters					11.094	F	Edot	W
351	stainless	Solid type							
352	51 DUCT	resonat.							
353	Same 48a	2.3543E-03	a	Area	m^2	3.4305E+04	A	p	Pa
354	Same 48b	0.1720	b	Perim	m	-176.48	B	Ph(p)	deg
355		0.3170	c	Length	m	2.0326E-02	C	U	m^3/s
356	Same 47f	2.0000E-03	d	Srough		-88.098	D	Ph(U)	deg
357	Master-Slave Links					24.701	E	Htot	W
358	Optional Parameters					9.8652	F	Edot	W
359	stainless	Solid type							
360	52 CONE	cone							
361	Same 47d	2.3543E-03	a	AreaI	m^2	3.6209E+04	A	p	Pa
362	Same 47e	0.1720	b	PerimI	m	-176.57	B	Ph(p)	deg
363		4.5000E-02	c	Length	m	1.9211E-02	C	U	m^3/s
364	Same 2a	7.1630E-03	d	AreaF	m^2	-88.185	D	Ph(U)	deg
365	Same 2b	0.3000	e	PerimF	m	24.701	E	Htot	W
366	Same 47f	2.0000E-03	f	Srough		9.8060	F	Edot	W
367	Master-Slave Links								
368	Optional Parameters								
369	stainless	Solid type							
370	53 RPN	ChangeMe							
371		0.0000	a	G or T		0.1130	A	ChngMe	
372	0.44 55c - 54c -								
373	54 DUCT	Change Me							
374	Same 2a	7.1630E-03	a	Area	m^2	3.9861E+04	A	p	Pa
375		0.3000	b	Perim	m	-176.76	B	Ph(p)	deg
376		0.1990	c	Length	m	1.0871E-02	C	U	m^3/s
377		2.0000E-03	d	Srough		-89.32	D	Ph(U)	deg
378	Master-Slave Links					24.701	E	Htot	W
379	Optional Parameters					9.6659	F	Edot	W
380	ideal	Solid type							
381	55 DUCT	Change Me							
382	Same 2a	7.1630E-03	a	Area	m^2	4.1110E+04	A	p	Pa
383	Same 2b	0.3000	b	Perim	m	-176.87	B	Ph(p)	deg
384		0.1280	c	Length	m	5.1826E-03	C	U	m^3/s
385		2.0000E-03	d	Srough		-92.032	D	Ph(U)	deg
386	Master-Slave Links					24.701	E	Htot	W
387	Optional Parameters					9.5851	F	Edot	W
388	ideal	Solid type							
389	56 RPN	ChangeMe							
390		0.0000	a	G or T	P	8.0795E-02	A	ChngMe	
391	54F 55F -								
392	57 DUCT	tube							
393	Same 2a	7.1630E-03	a	Area	m^2	4.1467E+04	A	p	Pa
394	Same 2b	0.3000	b	Perim	m	-176.96	B	Ph(p)	deg
395	Same 53A	0.1130	c	Length	m	4.6020E-04	C	U	m^3/s
396	Same 47f	2.0000E-03	d	Srough		-172.81	D	Ph(U)	deg
397	Master-Slave Links					24.701	E	Htot	W
398	Optional Parameters					9.5166	F	Edot	W
399	ideal	Solid type							
400	58 SURFACE	Change Me							
401	Same 2a	7.1630E-03	a	Area	m^2	4.1467E+04	A	p	Pa
402						-176.96	B	Ph(p)	deg
403						4.5951E-04	C	U	m^3/s
404						-172.81	D	Ph(U)	deg
405						24.701	E	Htot	W
406	ideal	Solid type				9.5023	F	Edot	W

```

407      59 IMPEDANCE Change Me
408      OP1t      9.0000E+07 a Re(Zs) Pa-s/m^3      3000.2 A |p| Pa
409      0.0000 b Im(Zs) Pa-s/m^3      97.241 B Ph(p) deg
410      Master-Slave Links      4.5951E-04 C |U| m^3/s
411      -172.81 D Ph(U) deg
412      24.701 E Htot W
413      5.9852E-04 F Edot W
414      60 COMPLIANCE Change Me
415      5.7000E-02 a SurfAr m^2      3000.2 A |p| Pa
416      1.0000E-03 b Volume m^3      97.241 B Ph(p) deg
417      Master-Slave Links      3.2018E-14 C |U| m^3/s
418      -24.788 D Ph(U) deg
419      24.701 E Htot W
420      ideal      Solid type      -2.5473E-11 F Edot W
421      61 HARDEND Change Me
422      Targ      0.0000 a R(1/z) P      3000.2 A |p| Pa
423      Targ      0.0000 b I(1/z) P      97.241 B Ph(p) deg
424      3.2018E-14 C |U| m^3/s
425      -24.788 D Ph(U) deg
426      Possible targets      24.701 E Htot W
427      -2.5473E-11 F Edot W
428      -5.9536E-12 G R(1/z)
429      -9.5171E-12 H I(1/z)
430      62 RPN      Carnot
431      0.0000 a G or T      8.5979E-02 A ChngeMe
432      0.3129 B ChngeMe
433      1 13G 13H / - 45F 16e 40e + /
434      63 RPN      ChangeMe
435      0.0000 a G or T      8.5979E-02 A ChngeMe
436      0.3129 B ChngeMe
437      1 37G 37H / - 45F 16e 40e + /
438      64 RPN      ChangeMe
439      0.0000 a G or T      0.27478 A ChngeMe
440      63A 63B /
441      65 RPN      Drive Ratio
442      Targ      2.3000E-02 a G or T      2.3000E-02 A ChngeMe
443      0d 0a /
444      66 RPN      ChangeMe
445      0.0000 a G or T      9.1483 A ChngeMe
446      45F 22F -
447      67 RPN      ChangeMe
448      0.0000 a G or T      7.5755E-02 A ChngeMe
449      9.1623E-02 B ChngeMe
450      66A 40e / 22F 16e /

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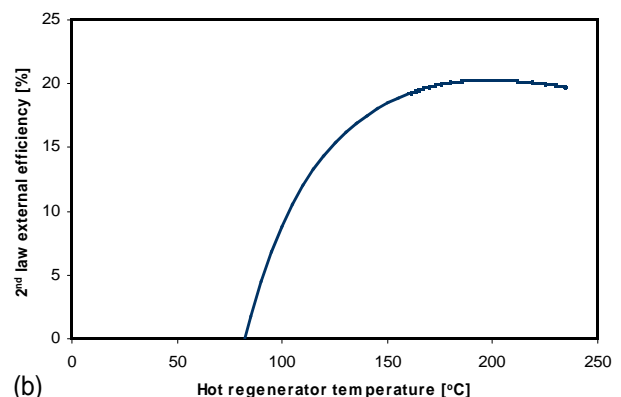
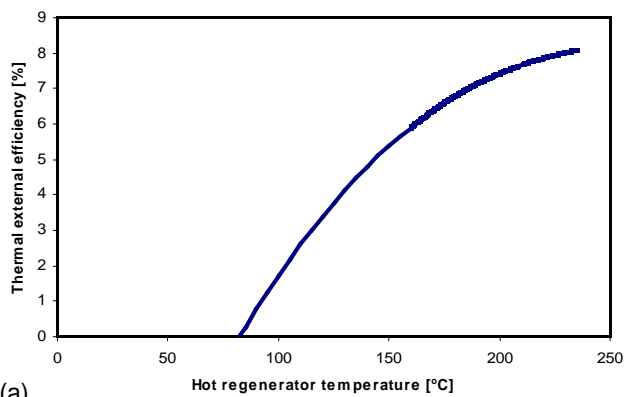


Figure B1 (a) Thermal and (b) second law efficiency of the load power in the DeltaEC simulation of the serial configuration.

Appendix C: Apparatuses dictionary

Driver

Generation of sound is done by a heat driven engine, mechanical pistons, or a speaker. The heat driven engine also can create a temperature gradient from acoustic energy and will be discussed in S2.2.2. In order to optimize the driver different components are added to the system.

Linear motor

Acoustic waves can be created by acoustic power in speakers, or by piston displacement. Pistons have a better efficiency in converting electricity into mechanical acoustic power, which gives this technology currently the upper edge in thermoacoustic cooling or heating with electricity.

Driver/Load

Stack

The stack is an effective surface area for the transformation of acoustic energy into thermal energy, and vice versa. The stack can be a prime mover, or a heat pump/refrigerator. All stacks are permeable in the axial direction. The word stack is used for interactions with a standing wave.

A mathematical determination can be made whether a stack is a motor or a consumer of acoustic energy by observing the critical temperature gradient. When the temperature gradient within the stack or regenerator is higher than the critical gradient then acoustic power is produced. Acoustic power can be transferred into a temperature gradient until it reaches the critical value.

There is a theoretical critical temperature for a hypothetical system without viscous losses, when the heat introduced by the pressure wave equals the heat extracted by the same wave. The critical temperature determines whether the system is an acoustic driver, or an absorber of acoustic energy. In reality there are viscous losses, which results in two critical temperatures with a comparable deviation from this critical temperature. When the temperature is between these values, the acoustic effect is ineffective, and acoustic energy is used to transport heat from the hot to the cold side.

Swift (1988) derived a critical temperature gradient.

$$\frac{\partial T}{\partial x_{crit}} = \frac{T_m \beta \omega p_a}{\rho_m c_p x_a} \quad (C1)$$

Where T_m is the average temperature of the stack, x_a the length of the stack, all constants taken from the working fluid.

Swift (1988) further derived a relationship between design choices, and the attainable heat flux.

$$\dot{Q} \sim \Pi \delta_T T_m \beta p_a u_a \left(\frac{\Delta T}{\Delta T_c} - 1 \right) \quad (C2)$$

With Π the perimeter of the cross section of the stack.

Regenerator

The regenerator is explained in detail in chapter 2, it is an apparatus similar to the stack. The regenerator transfers heat into acoustic energy, or visa versa. The acoustic energy being in this case a traveling wave.

Because the regenerator has favorable conditions, concerning the equal phase of pressure, and volumetric flow, it can constantly exchange heat with the medium. The ratio between viscous, and thermal boundary layer is not important anymore.

What is important is the thermal penetration depth. The pressure drop within the regenerator must be as low as possible while the surface area remains high. Ideally the hydraulic diameter shouldn't

exceed twice the thermal penetration depth.

$$\delta_{T,penetration} = \sqrt{\frac{2k_{regen}}{\rho_{regen} c_{p,regen} \omega}} \quad (C3)$$

Jet Pump

Section 2.3.1 states why direct current in the traveling wave loop is unfavorable. The torus is asymmetrical, and so is the friction and the time-delay in different ends of the torus. This would result in a direct current beside the alternating current to compensate the friction and time delay effects. A Jet pump could be introduced to prevent this. The most simple jet pump can be a narrow cone geometry. The cone shape introduces a pressure loss, which is in theory equally asymmetric in the opposite direction of the torus, Backhaus and Swift (2000) concluded the theoretical required pressure drop in the jet pump can be expressed by:

$$\Delta \bar{p}_{jetpump} = \frac{R}{2\rho_m} \text{Re}(\rho_a \bar{U}_a) \quad (C4)$$

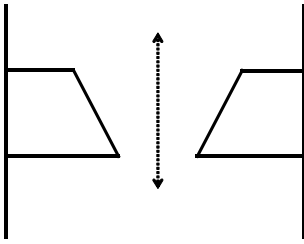


Figure C1 Jet pump

They designed a jet pump with a different flow loss in different directions, this principle can be expressed:

$$\Delta \bar{p}_{jetpump} = \frac{\rho_m (U_{a,jetpump})^2}{8A^2} \left(K_{s,expansion} - K_{s,compression} + \left(\frac{A_s}{A_b} \right)^2 (K_{b,compression} - K_{b,expansion}) \right) \quad (C5)$$

Where K is the friction constant while b and s represent the wide, and the small side.

Membrane

The jet pump operates by the introduction of unwanted pressure losses, and would in theory only completely block Gedeon streaming (section 2.3.1) at one specific condition, which is often slightly different in reality than in practice. A membrane can transfer impulse while it is impenetrable for the working fluid. The inelastic losses are small and the heat conduction through the membrane is also small.

Heat exchangers

In literature heat exchangers are explained, and tested extensively. What is important in the thermoacoustic system is the temperature difference, and temperature gradient over the stack/regenerator $\Delta T = (T_h - T_c)$, and $\partial T / \partial x_a$.

Piezoelectric elements

A piezoelectric element can convert acoustic energy into electricity. In the test setup a load is applied to the acoustic resonator, which causes the same damping as a piezoelectric element would. If a setup is used for the production of electrical power the load power is very important.

Distribution

Resonator

Acoustic waves travel in the radial direction of a spherical coordinate system. This would lead to the dispersion of energy, and a reduction of the energy density in an acoustic wave. In order to prevent a reduction of energy density the sound wave is contained within a tube of impermeable material.

The resonator can only operate a standing wave due to the boundary conditions, nevertheless this could be useful in dominating the frequency of the system. The resonator is also the shell that determines the system boundary. It should always be structurally stronger than the medium that transports acoustic waves.

Extensions

Because the standing wave has unfavorable conditions for energy transfer, the regenerator is not placed within the oscillator, but in an extension where no borders dictate a standing wave. Such a configuration can have many shapes. Most commonly known are the torus, and the axial configuration. In the experiments we will use a coaxial configurations. Toruses have proven to generate better efficiencies. This is mostly due to the impracticality of thermal insulation in a coaxial configuration.

Feedback channel as a control for system impedance

The feedback channel is a small connection of the medium to different sides of the regenerator. This creates a loop in the system that corrupts the boundary layers that cause standing waves, thus creating a traveling wave. Because of the analogy between electrical and acoustical systems, the acoustic impedance is often represented as a coil.

In an electrical circuit the impedance is expressed as Z , in ohm, being the resistance in a circuit that is in operation under an alternating current. The resistance consists of a real, and an imaginary part. The real part is caused by viscous friction and the imaginary part by phase effects.

Compliance/ Capacitance

The compliance is a volume that can accumulate energy (pressure times volume). A volume in an acoustic wave will behave similarly to a capacitor in an electrical circuit with alternating current.

Sound Transport Medium

The acoustic wave needs to be transported through the system, This happens by a medium also called the working fluid. The medium could be a solid, liquid or gas; in this sense the term fluid is not correct. Nevertheless it is common to use gases and liquids. It undergoes the process of compression and expansion, thus it transports the heat.

From acoustics the relation between specific compressibility γ , and the speed of sound a is given by:

$$\gamma - 1 = \frac{T_m \beta^2 a^2}{c_p} \quad (C6)$$

β is the isentropic expansion coefficient and T_m is the average temperature of the medium.

Flow straightener

In order to reduce the Rayleigh streaming, a friction barrier is placed at the exit of the thermal buffer tube. This will reduce the flow of highly buoyant hot fluids leaving, and cold fluids entering the thermal buffer tube.

Appendix C1: Two microphone method

The acoustic power is the power contents of an acoustic wave. As stated earlier the 2 microphone method predicts the acoustic energy transported through a cross sectional area. The velocity, the mean pressure, and the pressure difference could be derived from just two pressure sensors, as long as pressure amplitude, phase, and overall pressure can be separated.

The determination of acoustic energy in this matter was developed by Fusco et al. (1992). It is based upon the principle that the volume flow is a result of the pressure difference between two points.

Two general equations were used by Fusco et al. concerning viscous losses and the complex wave number which is the coefficient of p'' and was assigned Y .

$$i\omega\rho u = -\frac{dp'}{dx} + \mu \frac{1}{r} \frac{\partial}{\partial r} \left(r \frac{\partial u}{\partial r} \right) \quad (C7)$$

$$Y^2 = \frac{\omega}{a^2} \left(\frac{1 + (\gamma - 1)f_T}{1 - f_v} \right)$$

Then he used the statements for the derivative of pressure in an acoustic wave to determine

$$p' \left(\frac{-\Delta x}{2} \right) = p'_A = Ae^{-ik\Delta x/2} + Be^{ik\Delta x/2}$$

$$p' \left(\frac{\Delta x}{2} \right) = p'_B = Ae^{ik\Delta x/2} + Be^{-ik\Delta x/2}$$

$$p'(x=0) = A + B + (p'_A + p'_B) \frac{\sin(k\Delta x/2)}{\sin(k\Delta x)} \quad (C8)$$

$$\frac{dp'(x=0)}{dx} = ik(A - B) = k(p'_A - p'_B) \frac{\cos(k\Delta x/2)}{\sin(k\Delta x)}$$

$$\dot{W}_{2mic} = \frac{-\pi r}{2\omega\rho_m} \operatorname{Im} \left((p'_A + p'_B) \frac{\sin(k\Delta x/2)}{\sin(k\Delta x)} k(p'_A - p'_B) \frac{\cos(k\Delta x/2)}{\sin(k\Delta x)} (1 - f_v) \right)$$

$$k \approx \frac{\omega}{C_m} \left(1 + \frac{(\gamma - 1)f_T}{2} + \frac{f_v}{2} \right) \approx \frac{\omega}{C_m} \left(1 + \frac{(1 - i)}{2} \left(1 + \frac{\gamma - 1}{\sqrt{\operatorname{Pr}}} \right) \frac{\delta_v}{r} \right)$$

$$\dot{W}_{2mic} = \frac{-\pi r}{2\rho_m C_m \sin(\omega\Delta x / C_m)} \left(\operatorname{Im}(p'_A p'_B) - \frac{\delta_v}{2r} \left(\operatorname{Im}(p'_A p'_B) \left(1 - \frac{\gamma - 1}{\sqrt{\operatorname{Pr}}} + \left(1 + \frac{\gamma - 1}{\sqrt{\operatorname{Pr}}} \right) \frac{\omega\Delta x}{C_m} \frac{\cos\left(\frac{\omega\Delta x}{C_m}\right)}{\sin\left(\frac{\omega\Delta x}{C_m}\right)} \right) \right) \right. \\ \left. + \frac{1}{2} (p'^2_A - p'^2_B) \left(1 - \frac{\gamma - 1}{\sqrt{\operatorname{Pr}}} + \left(1 + \frac{\gamma - 1}{\sqrt{\operatorname{Pr}}} \right) \frac{\omega\Delta x}{C_m} \frac{1}{\sin\left(\frac{\omega\Delta x}{C_m}\right)} \right) \right)$$

$\operatorname{Re}()$ is the real part of $()$, and $\operatorname{Im}()$ is the imaginary part of $()$

$$\frac{\omega\Delta x}{C_m} \frac{\cos\left(\frac{\omega\Delta x}{C_m}\right)}{\sin\left(\frac{\omega\Delta x}{C_m}\right)} \approx 1, \text{ and } \frac{\omega\Delta x}{C_m \sin\left(\frac{\omega\Delta x}{C_m}\right)} \approx 1$$

So equation C8 could be rewritten as

$$\dot{W}_{2mic} = \frac{-\pi r}{2\rho_m C_m \sin(\omega\Delta x / C_m)} \left(\text{Im}(p'_A p'_B) \left(1 - \frac{\delta_v}{r} \right) + \frac{\delta_v}{2r} (p'^2_A - p'^2_B) \right)$$

$$\dot{W}_{2mic} = \frac{-\pi r}{2\rho_m C_m \sin(\omega\Delta x / C_m)} \left((|p'_A| |p'_B| \sin \phi) \left(1 - \frac{\delta_v}{r} \right) + \frac{\delta_v}{2r} (p'^2_A - p'^2_B) \right)$$
(C9)

A more simple approach is used for a non viscous medium:

$$\dot{W} = \overline{p(t)U(t)} = \text{Re}(\overline{p_a U_a}) / 2$$

$$i\omega\rho U = -\frac{dp}{dx}$$

$$p = \frac{p_1 + p_2}{2}$$
(C10)

$$\frac{dp}{dx} = \frac{p_1 - p_2}{\Delta x}$$

$$\frac{\dot{W}_{2mic}}{A_{cs}} = \text{Re} \left(\frac{i}{\omega\rho} \frac{p_1 - p_2}{\Delta x} \frac{\overline{p_1 + p_2}}{2} \right) \frac{1}{2} = \frac{1}{4\omega\rho\Delta x} \text{Im}(\overline{p_1 + p_2})(p_1 - p_2) = \frac{|p_1| |p_2| \sin \phi}{2\omega\Delta x}$$

$$\dot{W}_{2mic} = \frac{A_{cs} |p_1| |p_2| \sin \phi}{2\omega\Delta x}$$

For a viscous medium the derived equation 3.6 of Fusco et al. 1992 was further simplified by Backhaus and Swift (2002)

$$i\omega\rho u(x, y) = -\frac{dp}{dx} + \mu \frac{\partial^2 u(x, y)}{\partial y^2}$$

For $r \gg \delta_v$ it holds that:

$$u = \frac{i}{\omega\rho} \left(1 - e^{(-1+i)\frac{y}{\delta_v}} \right) \frac{dp}{dx}$$
(C11)

The volumetric velocity is the average flow speed over the cross sectional area

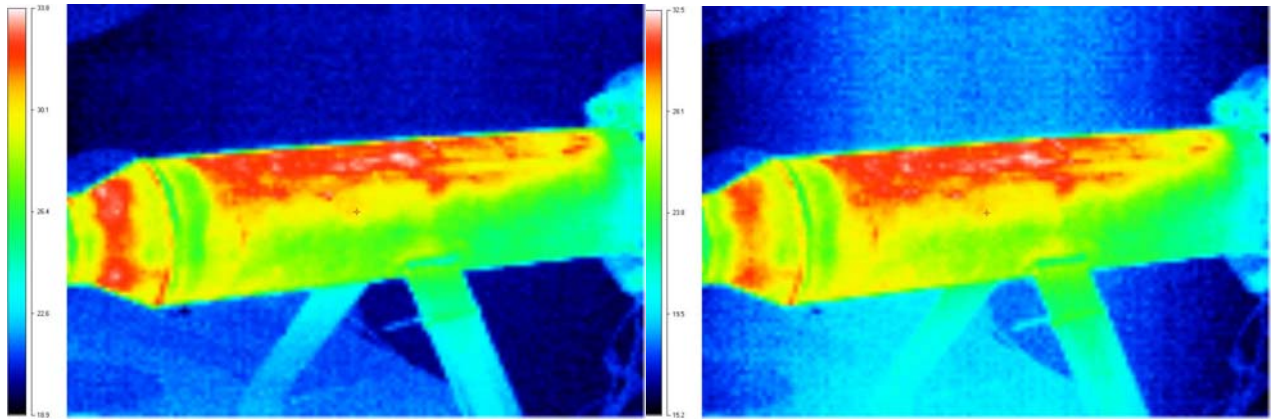
$$U = \frac{iA}{\omega\rho} \left(1 - (1-i)\frac{\delta_v}{2r} \right) \frac{dp}{dx}$$

$$p \cong \frac{(p_2 + p_3)}{2}, \quad \frac{dp}{dx} \cong \frac{(p_2 - p_3)}{\Delta x}$$

$$\dot{W}_{2mic} = \frac{A_{cs}}{2\omega\Delta x} \left(1 - \frac{\delta_v}{r} \right) |p_1| |p_2| \sin \phi + \frac{\delta_v}{2r} (|p_1|^2 - |p_2|^2)$$

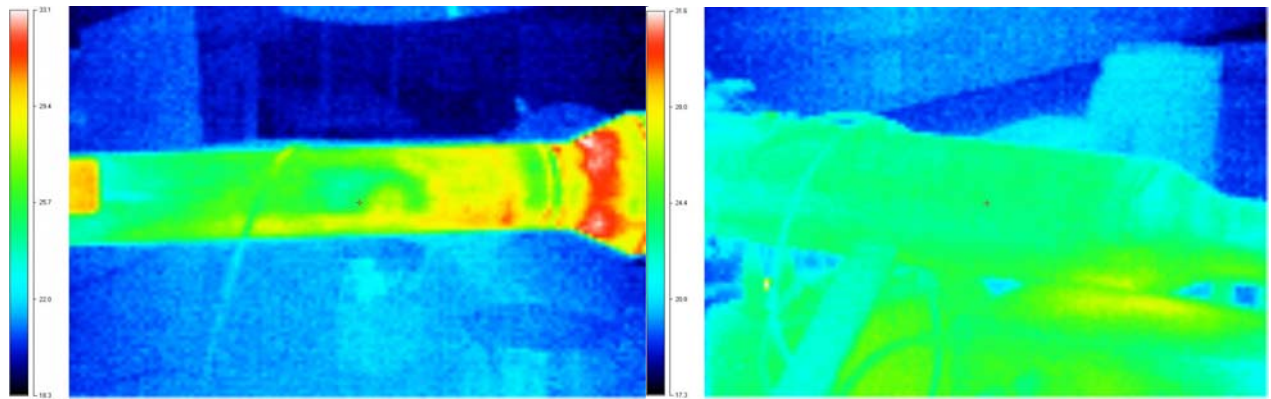
Where A_{cs} is the cross sectional area, and Δx is the distance between the two microphones, ρ is the density of the medium, and ω is the frequency of the acoustic wave, r is the radius of the cross sectional area, while δ_v is the viscous penetration depth, and Φ is the phase difference between p_1 , and p_2 .

Appendix D1 Heat Images Serial configuration.



D1

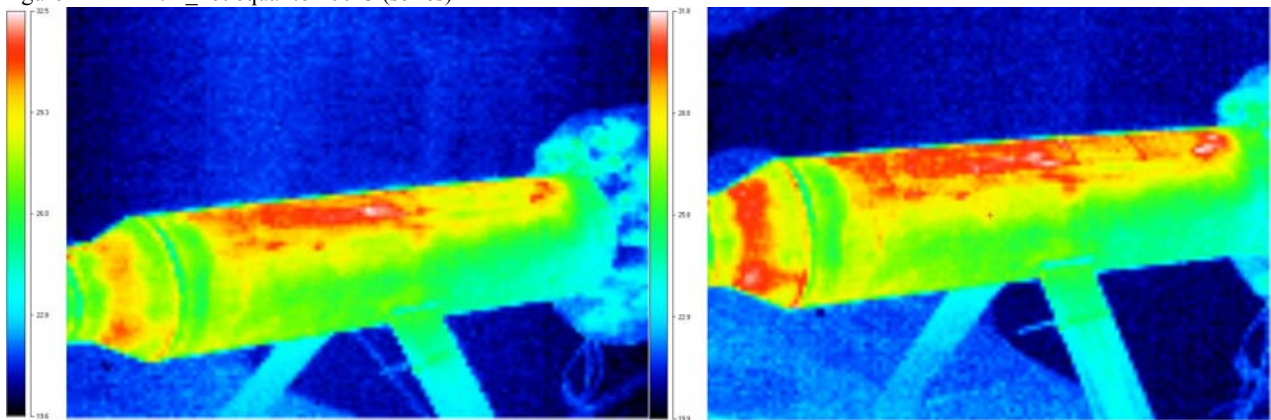
D2



D3

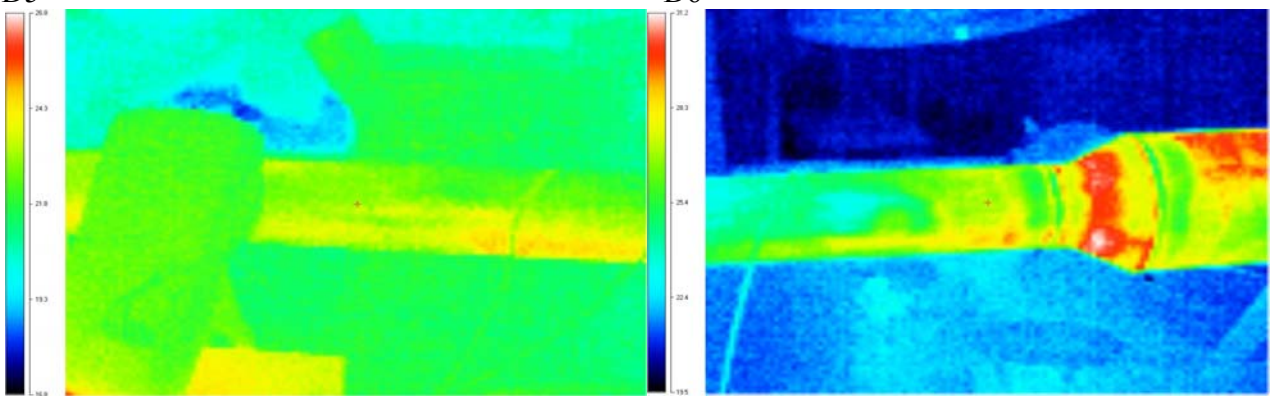
D4

Figure D1-D4 At T_{hot} equal to 200°C (series)



D5

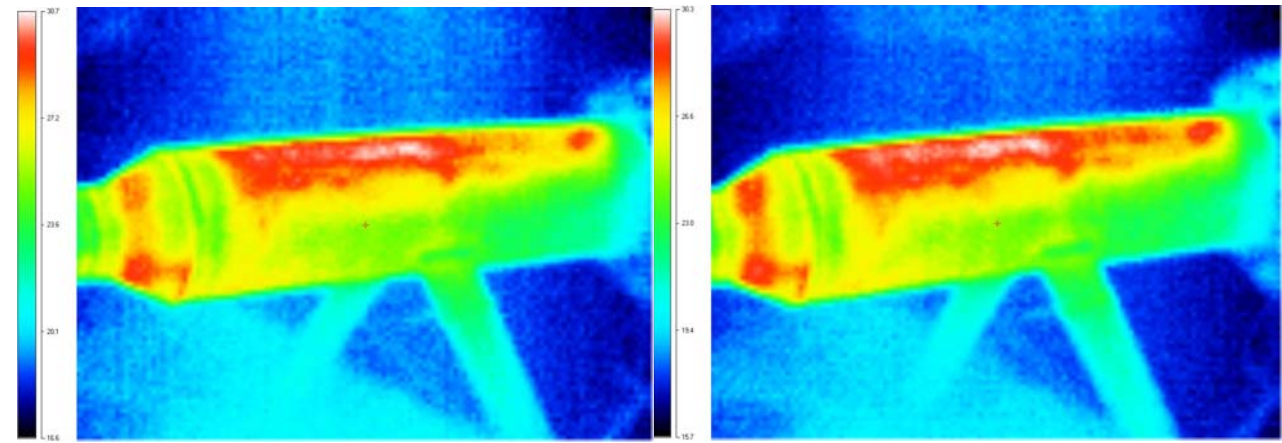
D6



D7

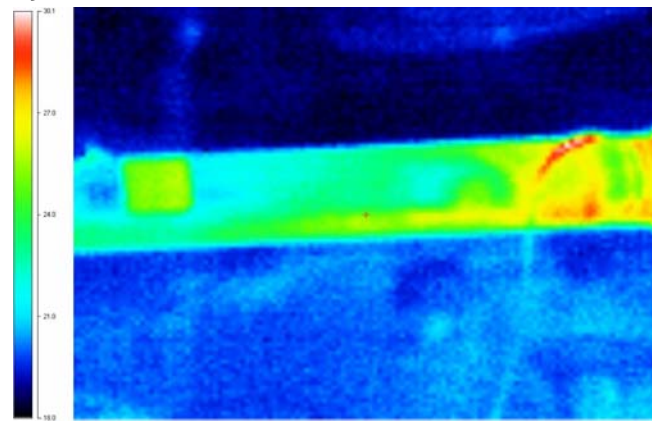
D8

Figure D5-D8 At T_{hot} equal to 160°C (series)



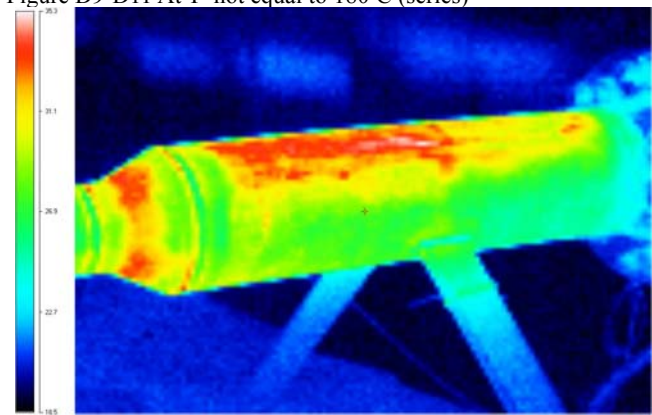
D9

D10

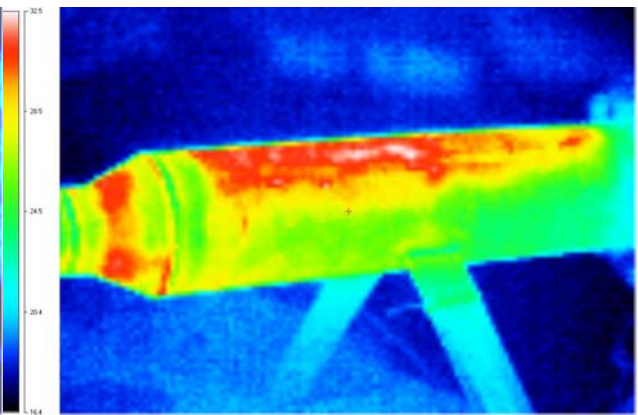


D11

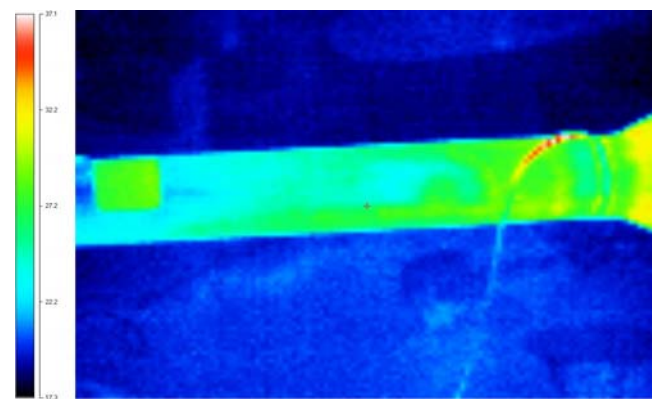
Figure D9-D11 At T_{hot} equal to 180°C (series)



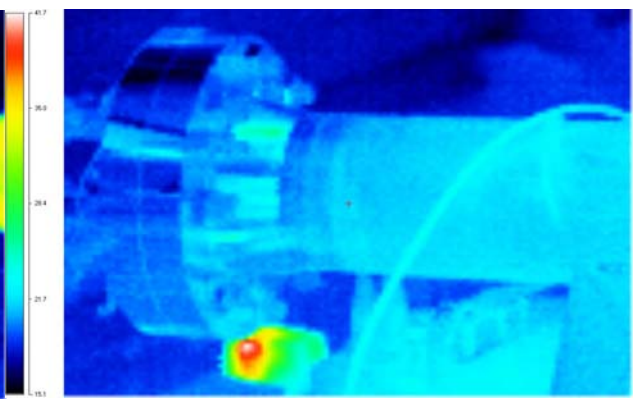
D12



D13



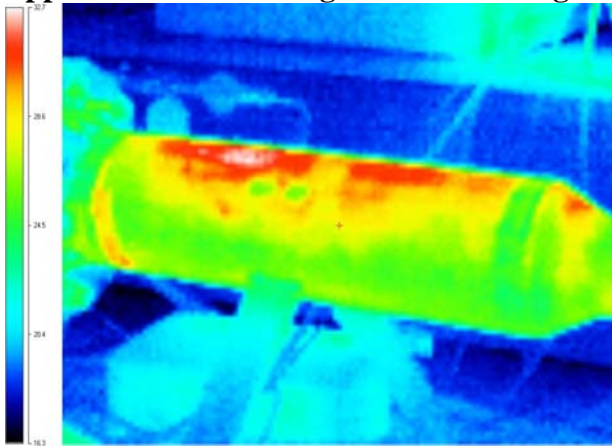
D14



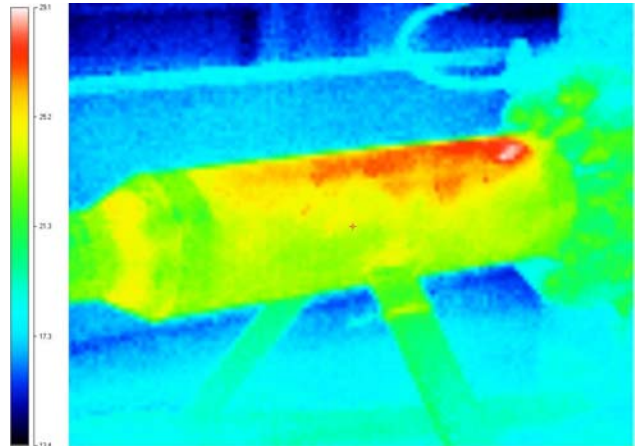
D15

Figure D12-D15 At T_{hot} equal to 220°C (series)

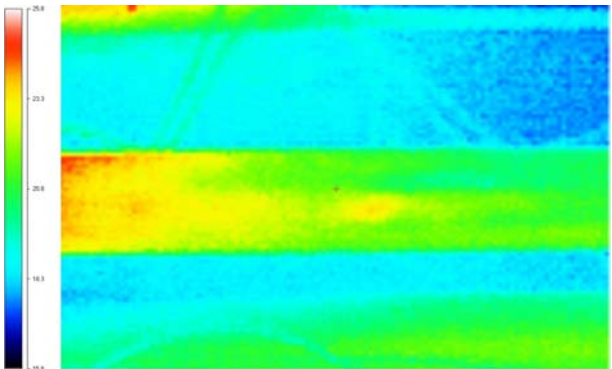
Appendix D2 Heat Images Parallel configuration.



D16

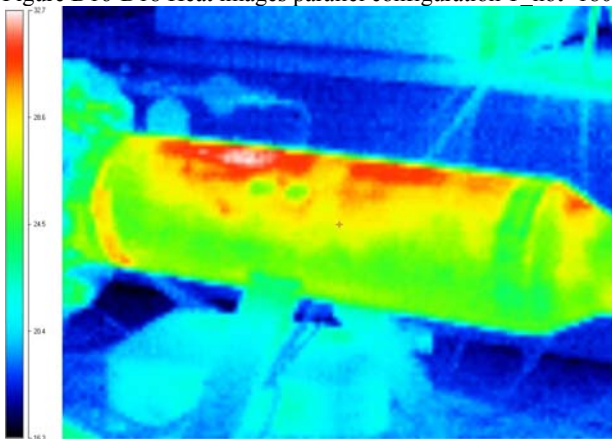


D17

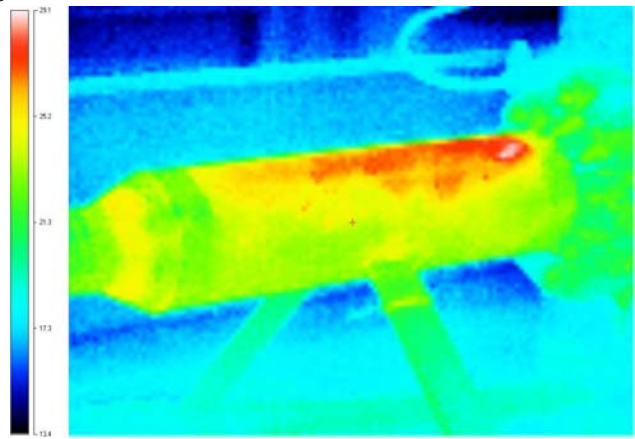


D18

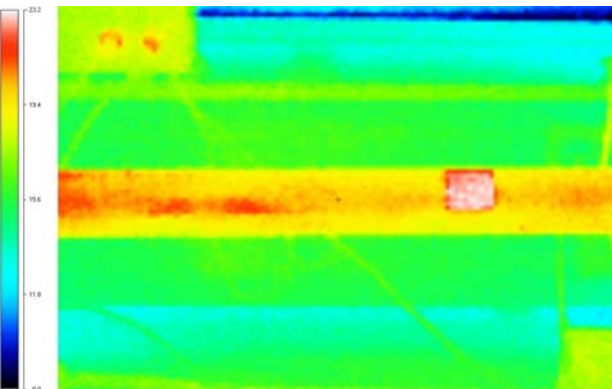
Figure D16-D18 Heat images parallel configuration $T_{hot}=180^{\circ}\text{C}$



D19

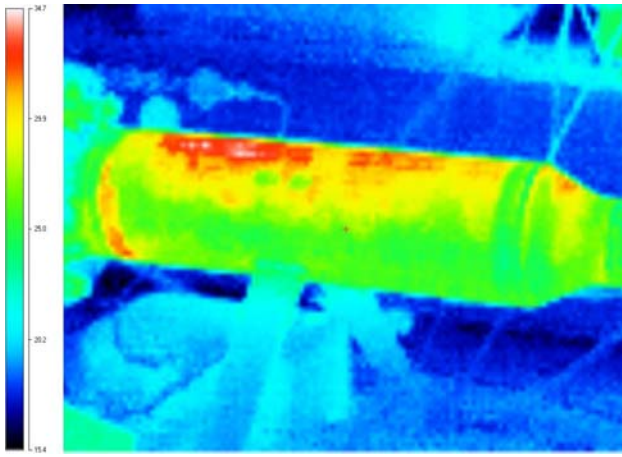


D20

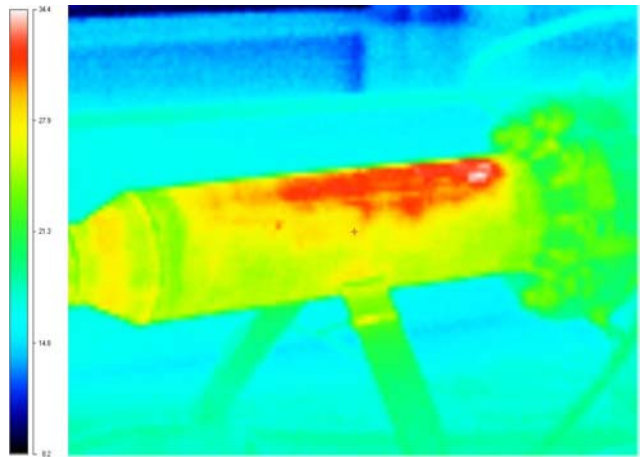


D21

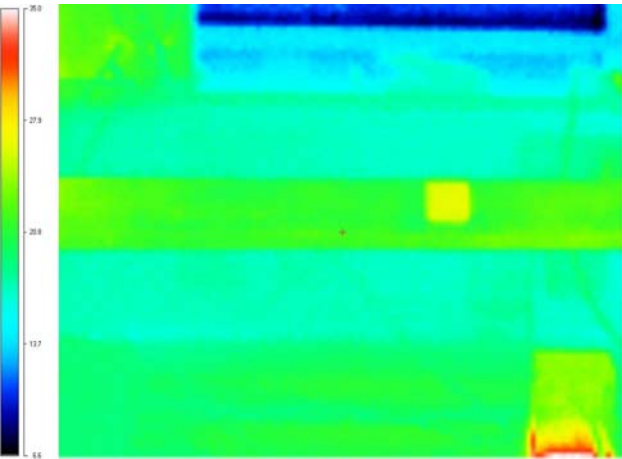
Figure D19-D21 Heat images parallel configuration $T_{hot}=200^{\circ}\text{C}$



D22



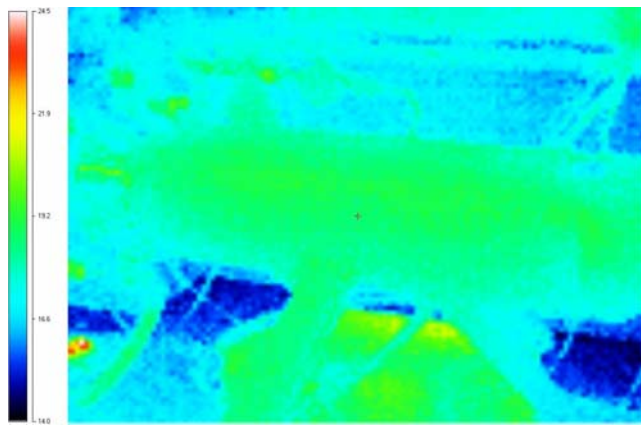
D23



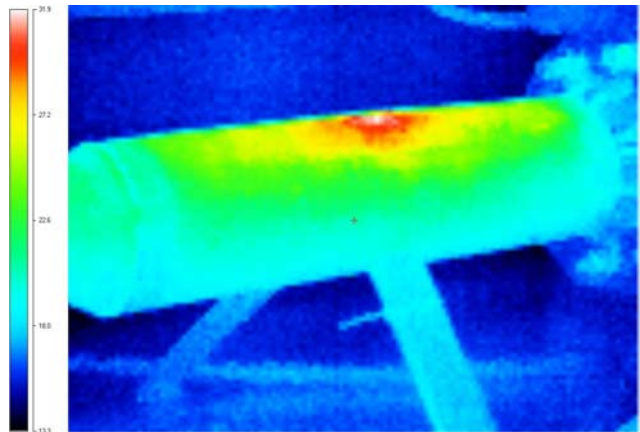
D24

Figure D22-D24 Heat images parallel configuration $T_{hot}=220^{\circ}\text{C}$

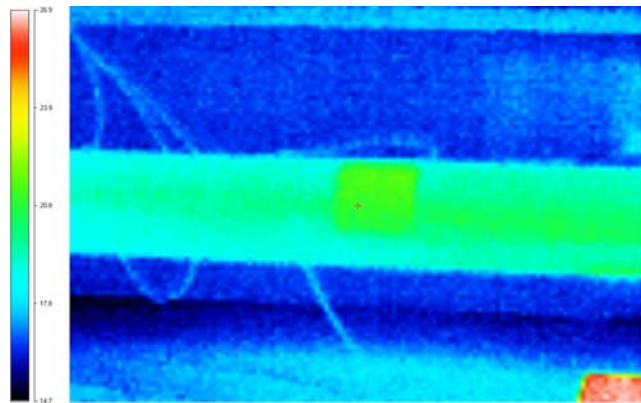
D3 Validation static Heat Images



D25

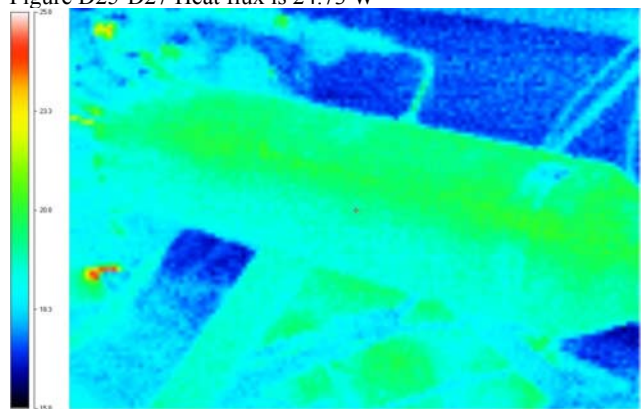


D26

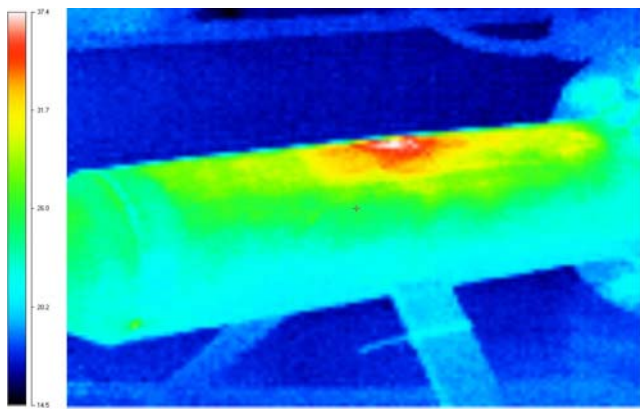


D27

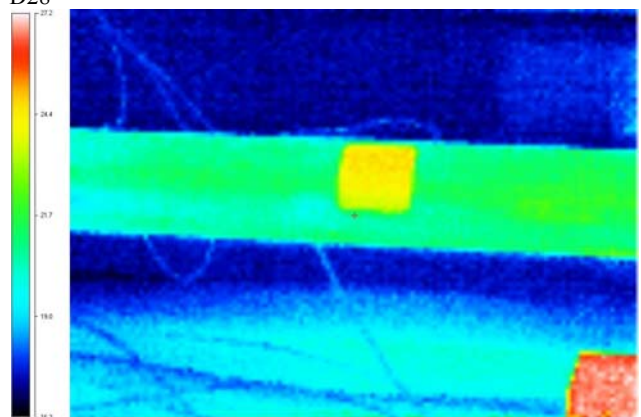
Figure D25-D27 Heat flux is 24.73 W



D28



D29



D30

Figure D28-D30 Heat Flux is 31.15 W