



P5 Presentation

The transparent facade of the future
Design strategies for maximizing transparency with self-supporting glass facade systems

Katerina Doulkari

RESEARCH DEFINITION



CONCLUSION

/// RESEARCH DEFINITION ///



Zamora Offices - Alberto Campo Baeza



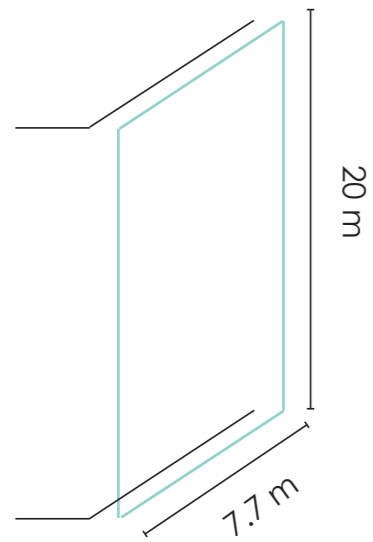
Rainbow Panorama - Olafur Eliasson

OMA

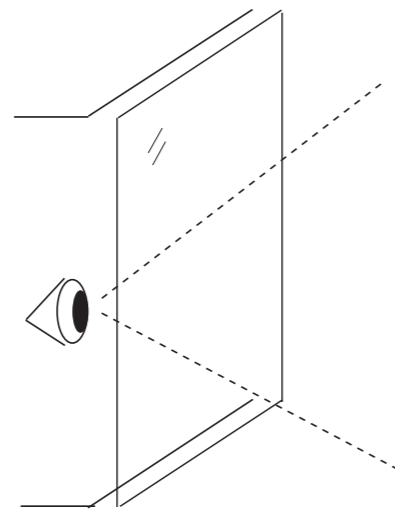
ABT

TU Delft

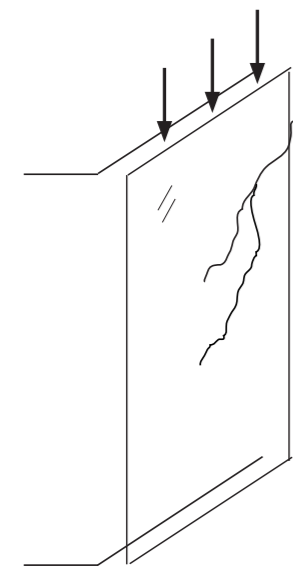
SCHELDEBOUW



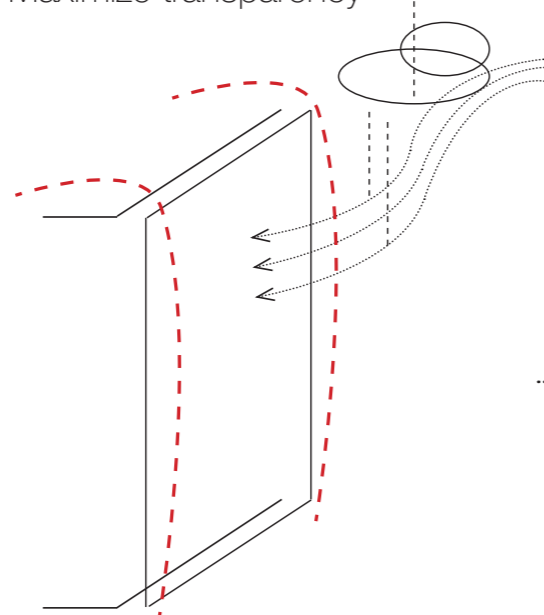
Size



Maximize transparency

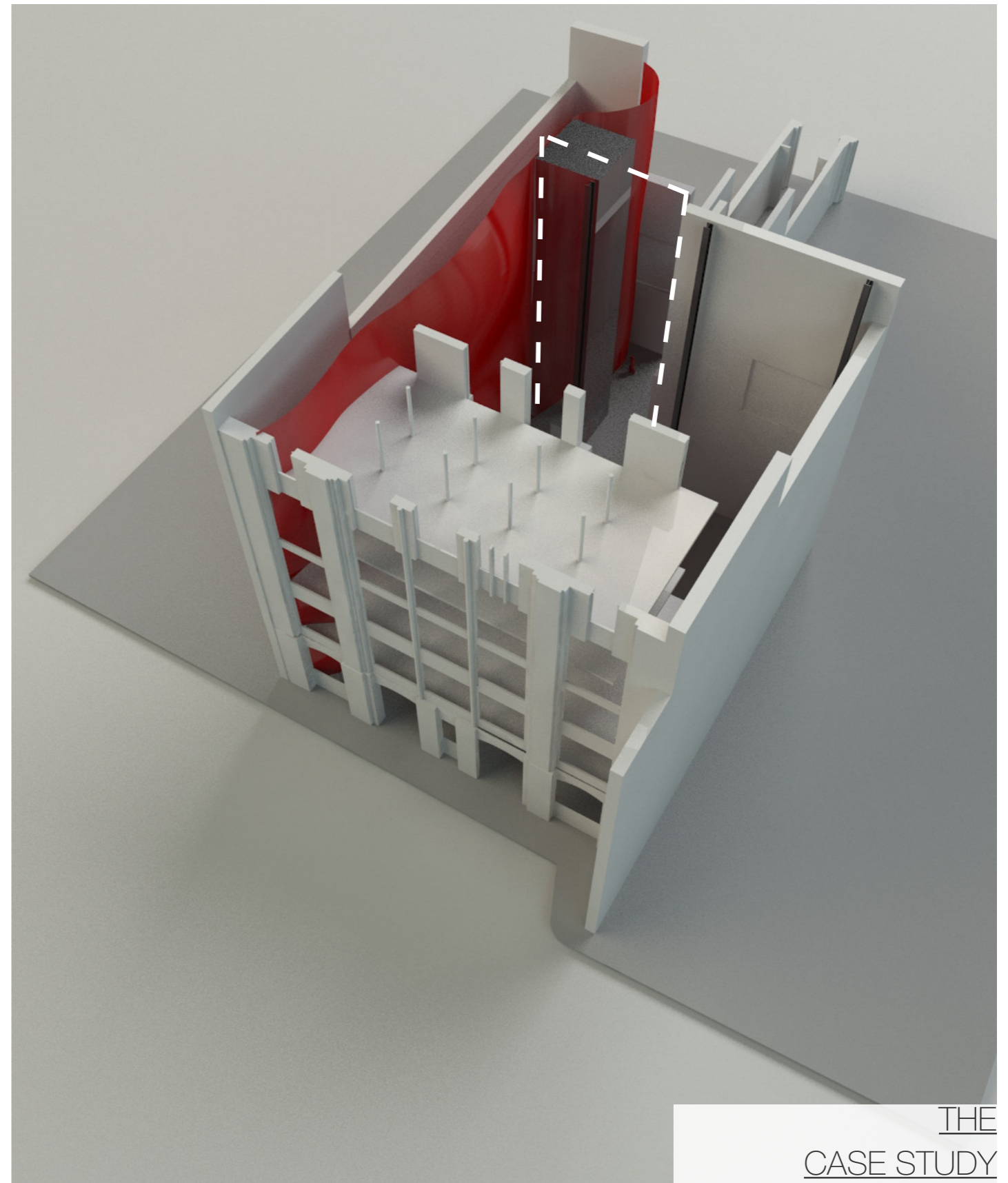


Fail - safe concept



Weatherproofing

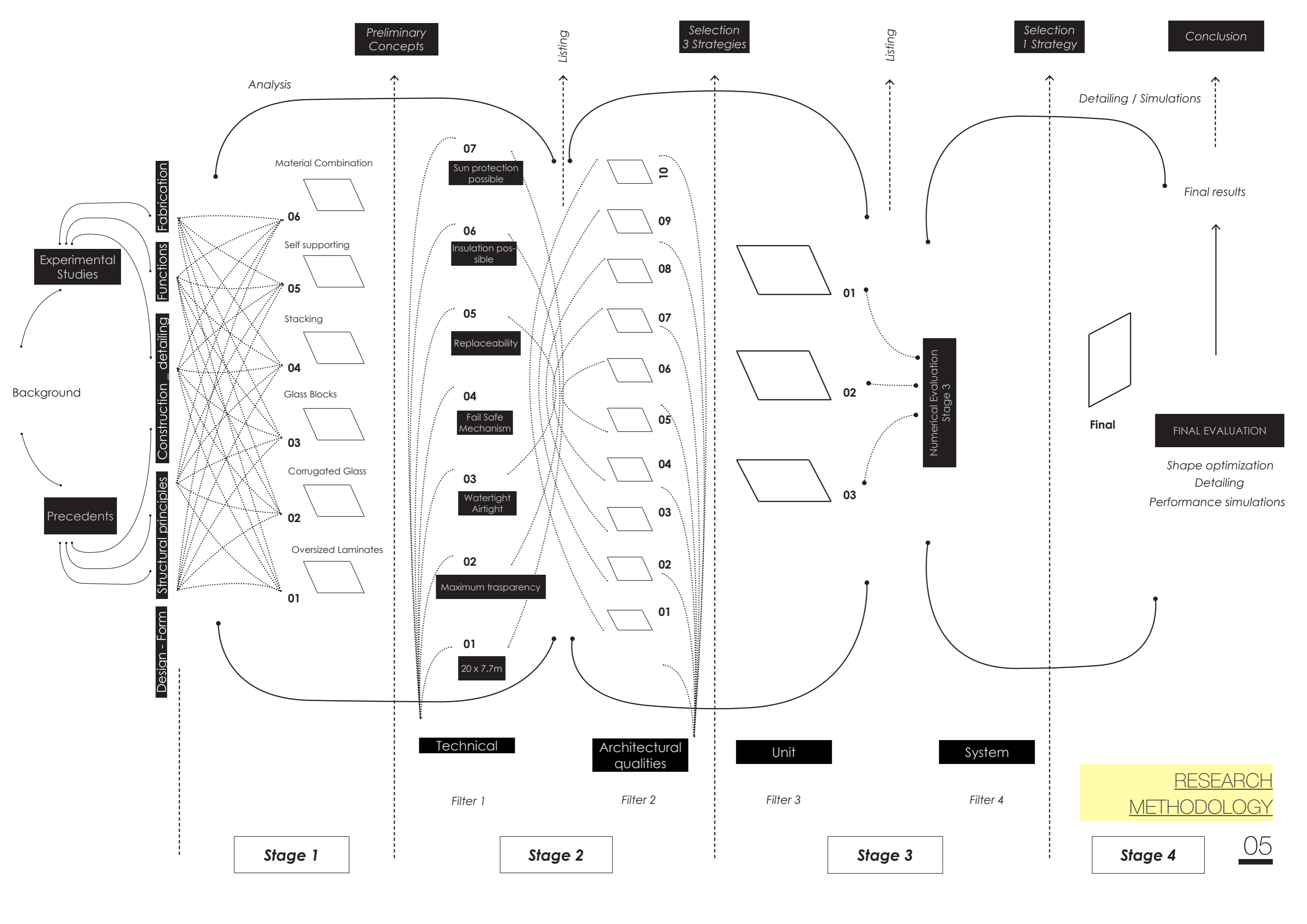
Interesting design + Structural feasibility



THE CASE STUDY

“What are the design strategies that one can employ in order to maximize transparency in glass facades and which strategy is the most appropriate to follow for the structural design for a transparent facade of the future that will be applied in ‘La Fayette Modern’?”

- 1 | What is the optimal geometry of glass components to be used for the construction of the facade?
- 2 | What are the criteria to evaluate an optimal structural design strategy for the glass facade?
- 3 | Which parameters can influence the performance of a glass component?
- 4 | How can manufacturing availability and processes influence the structural design with glass?
- 5 | What are the ways, in which we can enhance the safety of the glass facade?
- 6 | How should a structural joint between glass components be designed in order to increase transparency?



/// **STAGE 1**_ ANALYSIS OF GLASS TECHNOLOGY ///

Form - typologies

01 Linear 1D
 Column, Rods & Bars, Mullion, Beam

02 Surfaces 2D
 Plates, Slabs

03 Shells & Solids 3D
 Shell, Folded Plate, Cells - Unit, Massive block

Are components whose dimensions are small in 2 directions and large in a 3rd direction - lengthwise.

Flat sheet geometry where the dimensions are large in the two directions and small in the third (thickness).

Generally subjected to **axial loads**. In frames and girders ties and struts are respectively subjected to **tension** and **compression**. In columns we can have depending on the joining method (articulated or fixed) respectively pure **vertical compressive axial load** or axial load combined with bending stresses.

Generally correspond to the geometry of the linear elements but they are also subjected to bending and shear forces. **Transverse bending**, **Longitudinal bending**, **shear stresses**, **axial stresses**. Eccentric load can cause **torsion**.

Are subjected to **axial forces** exclusively that act in the plane of the element itself. They can be prone to local buckling. **Tension** transferred by point fixings in friction. **Compression** transferred by point fixings in contact. In both cases laminated glass for residual stability reasons is employed.

Subjected to forces acting perpendicular to their plane. Distinguished from the plates subjected to the different direction of the loading. They can be prone to local buckling.

Shells are formations subjected to **in-plane stresses** and we distinguish them in two categories: the curved elements and the curved surfaces consisted of flat elements (faceted surfaces).

Because of their geometry and width-height ratio they possess a greater stability and resistance to bending stresses and torsion than flat sheets or linear elements.

Columns & Bars, Beams & Fins, Plates, Slabs, Shells, Solids

One-piece cross-section
 Strips of float glass have maximum thickness up to 25mm. The maximum slenderness ratio of 1/50 results in a maximum height of 1m for a compression member. Therefore glass tubes or solid cast glass struts are more suitable as compression elements.

Plane Beams - Fins
 Bending stresses around the major axis which places the stress concentration around the edges. Increasing depth can help reducing tensile bending forces. Lamination of 3 pieces toughened glass. Carrying dead and wind loads. Outer edge subjected to compression.

2 directional spanning
1 directional spanning
4 point support

Composite cross-section
 Compared to one-piece elements the combination of multiple cross sections joined together can create interesting and stronger compression elements. **Gluing glass to glass**, **gluing glass strips to metal connecting sections**, **Joining strips via individual fixings**.

Composite cross-section
 Composing an extremely efficient cross section by composing individual monolithic elements. Creating shapes that can optimally handle the bending stresses. (ex. I-shape). Higher torsional rigidity. Higher bending strength. Contact or friction fixing points via elastic intermediate pad.

Multi-ply slabs
 Consist of multiple layers of single slabs loosely stacked and bonded with adhesive. Shear stiff interlayer good for bending stiffness. Non beneficial in safety if one of the glass breaks. In that case a more viscoelastic layer is preferred. Residual stability after the failure of a single pane.

Faceted shells
 Faceted surfaces are consisted of elements with radius of curvature very large compared to their size. They are usually undergoing very high compressive stresses, which means that the stability has to be ensured.

Multi-ply with edge seats
 Creates a sort of hollow box that is sensitive to deformations of the structure that cause twist. The air cavity acts structurally. Benefit or disadvantage related to temperature and hence pressure conditions.

Combination with materials
 Limited use of glass in ties and struts because of the limited sizes of the product and sudden failure behaviour. Combining glass with other materials can allow overcoming these hindrance. **plastic**, **metal**, **timber**. Product of this method is the concentric prestressed monolithic glass tube.

Material combination
 Lending glass a ductile behaviour by combining it with a ductile material. Therefore now it can exhibit apart from high compressive strength on tensile strength in order to carry the safety loads for a certain amount of time after it fails.

Slabs with ribs & stiffeners
 Combination of slabs with ribs can allow for larger spans and more efficient structure. **Reducing stresses and deformations**. Uninterrupted spans. Additive assembly. Multi-leaf insulating sections.

Membranes
 Very interesting from engineering and architectural point of view. Elements are subjected exclusively to high tensile axial forces uni-directional or bi-directional. Transferring the forces to neighbouring elements is up to now feasible only by clamping or individual fixings. Causes local stress concentration. Residual load bearing capacity is not yet adequate in tensile stresses.

Fixed slabs
 The glass plane here carries the compressive loads and the truss in one or two axes the tensile loads. Truss connected via props or webs.

Form - typologies

01 Flat Glass

02 Curved
 Single curved, Double curved

03 Solid

Primary process - flat glass

Step 1 - Production of flat glass
 Floating / pouring still liquid glass on a bed of molten tin. This allowed the production of a glass panel with two perfectly flat surfaces. One is resulting from the perfectly flat surface of the molten tin and the other, upper one, from the gravity that flattens the surface of the molten glass. By cooling the slowly moving ribbon of the molten glass it can solidify and basically allow for a continuous process with the ribbon cut in different panels. Effects of the process.

Step 2 - Production of curved glass
Hot Bending
 Curved or faceted glass is manufactured by slowly heating flat glass up to the softening temperature. When the flat panel starts slumping by gravity, it is taking its curved shape on the customized mold. Once the geometry is achieved a slow cooling process follows known as "annealing". Curved glass can be also produced tempered and heat strengthened.

Cold Bending
 During the cold-bending process, several sheets of tempered glass are combined to make a laminated safety glass sandwich and then shaped as a glass/film laminate in an autoclave to become a single unit, two processes.

Cold-bending with shape-enhancing lamination
 By using shear-compliant film (PVB film) sheets of glass are mechanically anchored to a shape-fixing substructure, in order to lend permanence to their shape.

Cold-bending with shape-fixing lamination
 By using shear-resistant film (SG film by DuPont) shapes are maintained solely on the strength of the film's shear resistance.

Hybrid forming
 The skin could be created using single-curvature hot-bent glass according to a limited number of families but is preferred to use "ad hoc" panels produced using variable mould machines. The glasses are, then, successively cold-bent, before lamination or on-site, in order to adapt its curvature to the all different non-circular supporting lines.

Cast glass
 Glass casting is the process in which glass objects are cast by directing molten glass into a mould where it solidifies. Modern cast forming methods are: Sand casting and kiln casting.

Sand casting
 Pale de verre means glass paste. Crushed glass mixed with binders. The paste is applied in the inner surface of a negative mould as a coating. After the coating is fired at the appropriate temperature the glass is fused and creates a hollow unit that can have thick or thin walls.

Kiln casting
 Pale de verre means glass paste. Crushed glass mixed with binders. The paste is applied in the inner surface of a negative mould as a coating. After the coating is fired at the appropriate temperature the glass is fused and creates a hollow unit that can have thick or thin walls.

Forming processes

Curved forming

Hot bending
Cold bending

Type of connection

01 Non-positive
 In non-positive connections the joint is held together by applying a force that presses the individual elements together.

02 Positive
 Positive connections are connecting individual components together based solely on interlocking of geometries.

03 Material Bonding
 Forces can be transmitted through the adhesion connective forces developed in a molecular or atomic level.

Form of force transfer

Friction connection
 In this type of connections the forces occurring in the glass element are transferred via friction to the joint. Here the mechanical interlocking between the microscopic surface imperfections of the two material faces in contact. The forces therefore are transferred via axial/shear force from the glass to the joint.

Contact connection
 In contact connections the compressive force acting perpendicular to the contact faces provides the force-transfer mechanism.

Clamp Fixings

Linear clamp fixing
 01. Without safety
 02. With safety

Point clamp fixing
 Resistance of facades against wind suction can be achieved by ways of individual clamping.

Combination clamp fixing

Types of movability
 01. Rigid fixing
 02. Hinged fixing

Form of disc
 The disc point fixings are made of stainless steel and are in contact with two sides of the glass pane. Their diameter is according to the drilled hole and it should be at least 50mm.

Form of hole
 Cylindrical
 Cylindrical-conical
 Cylindrical-conical with undercut

Drilled Fixings

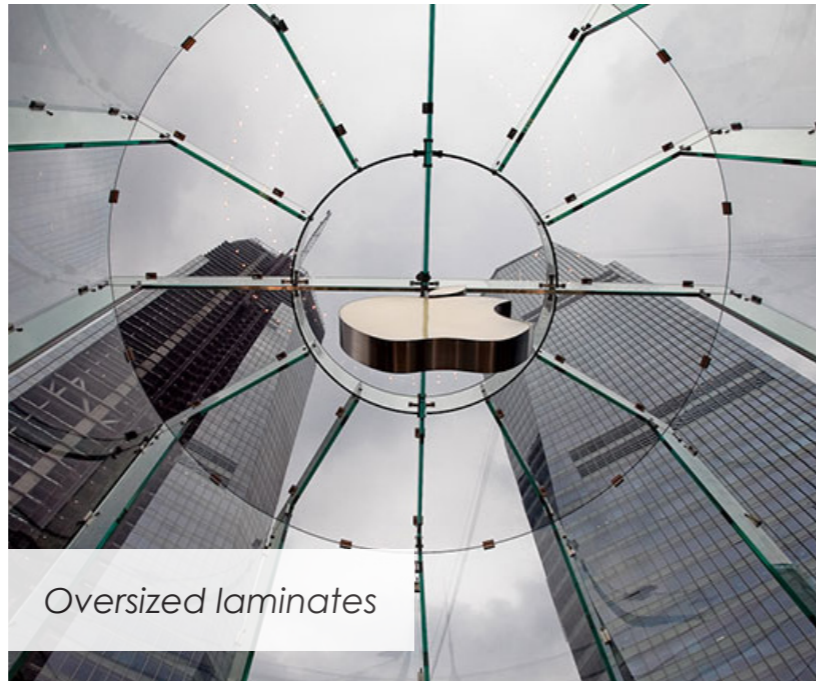
Force transfer on supports

Glues
 Gluing is the most common way of adhesive bonding. Adhesive can be applied: **Linearly**, **Discrete points**.

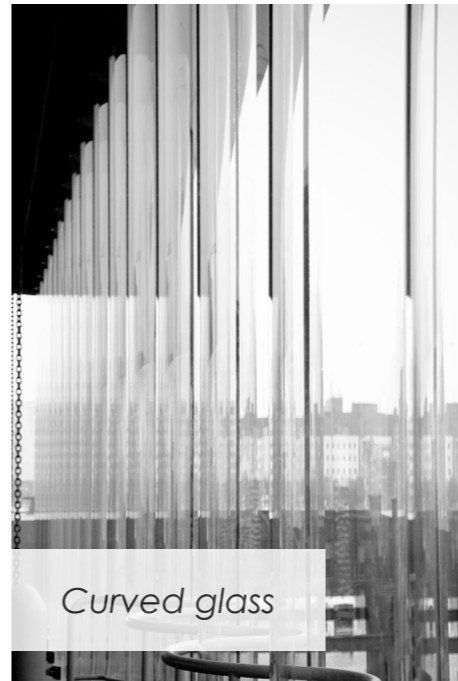
Silicones
 Is a type of facade construction in which the glass is permanently connected to an adapter frame via a loadbearing water-proof silicone joint.

01. Black
 Black silicon is made from polymer base plus chalk, silicic acid and soot fillers.

02. Transparent
 Transparent silicones are possible, but require more expensive polymers such as resins. This is why they are not established in facades yet.



Oversized laminates



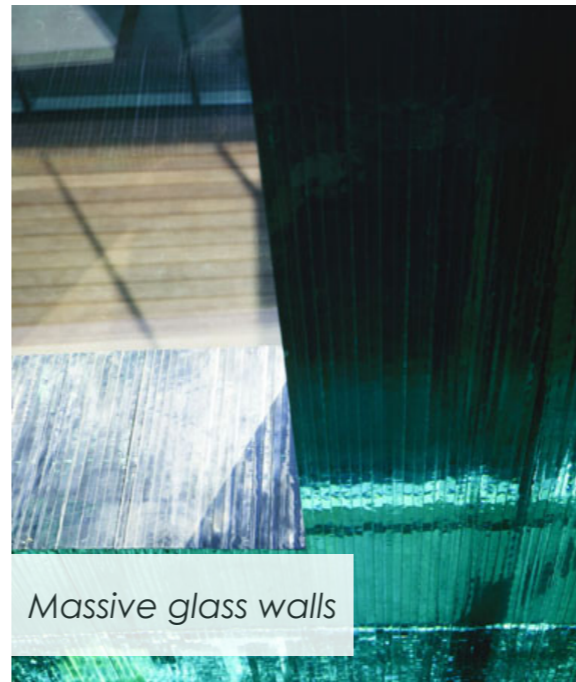
Curved glass



*Tubular
glass columns*



I glass profiles



Massive glass walls



Glass bricks

Transparency

Form

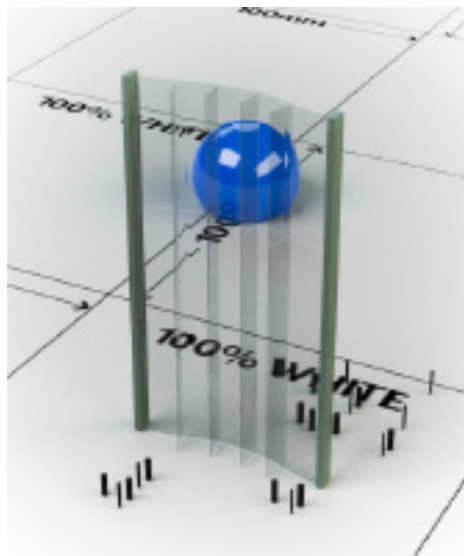
Structure

Construction

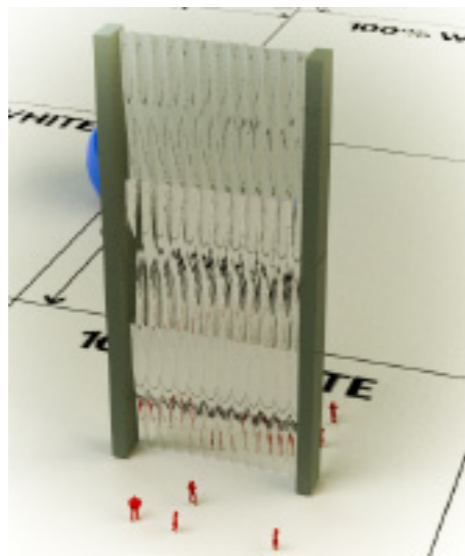
Fabrication

Connections

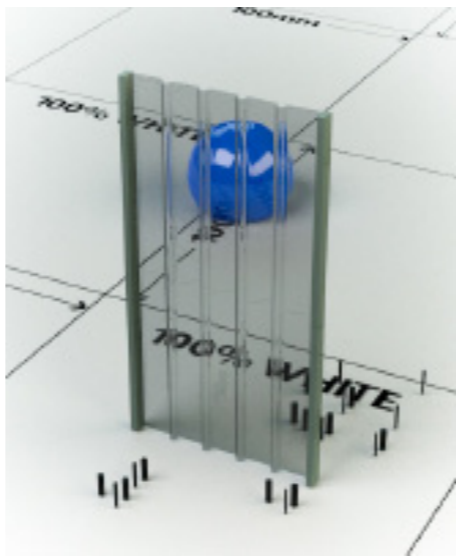
/// **STAGE 2**_PRELIMINARY CONCEPTS GENERATION ///



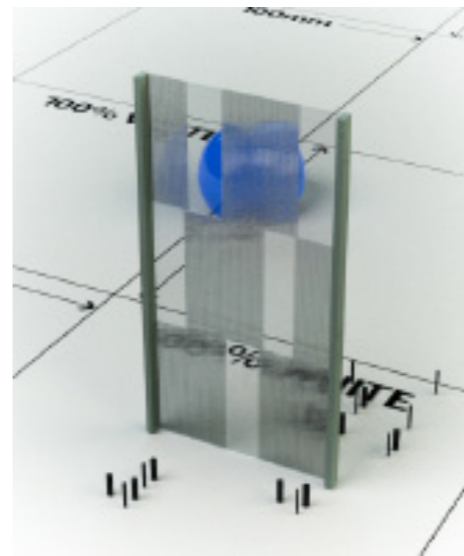
Glass Fin + Glass Plate



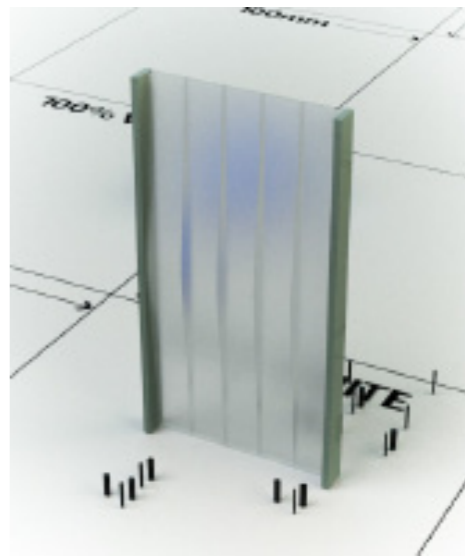
Corrugated shell



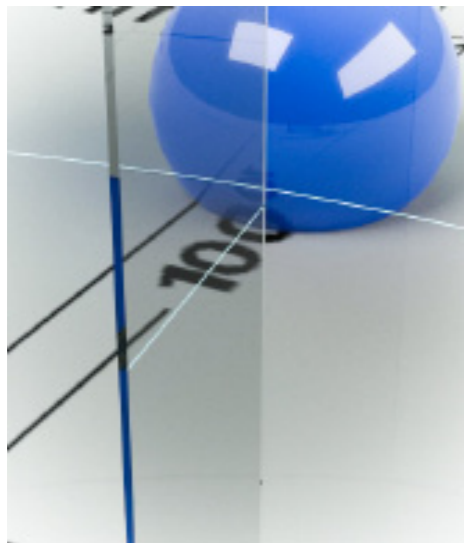
Bended + Glass Plate



Glass tubes



Integrated fins (I - profile)



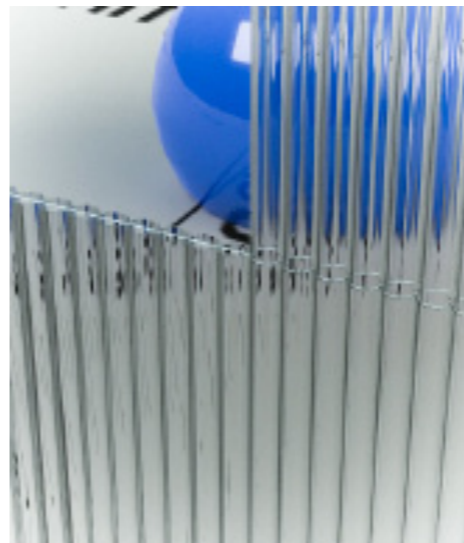
01



02



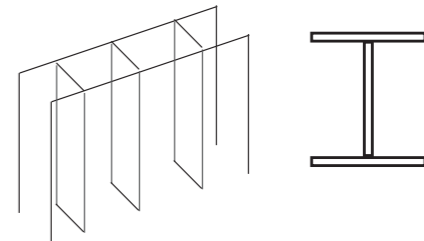
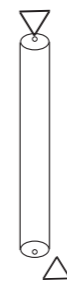
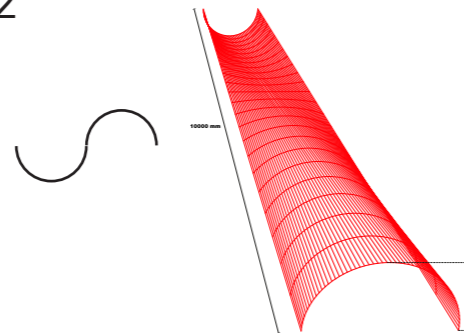
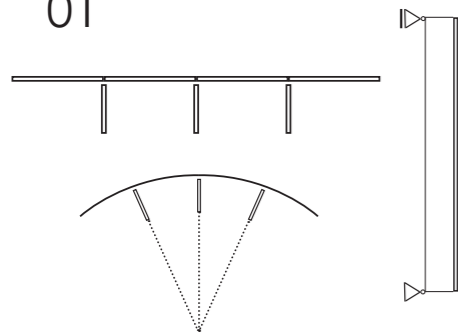
03



04

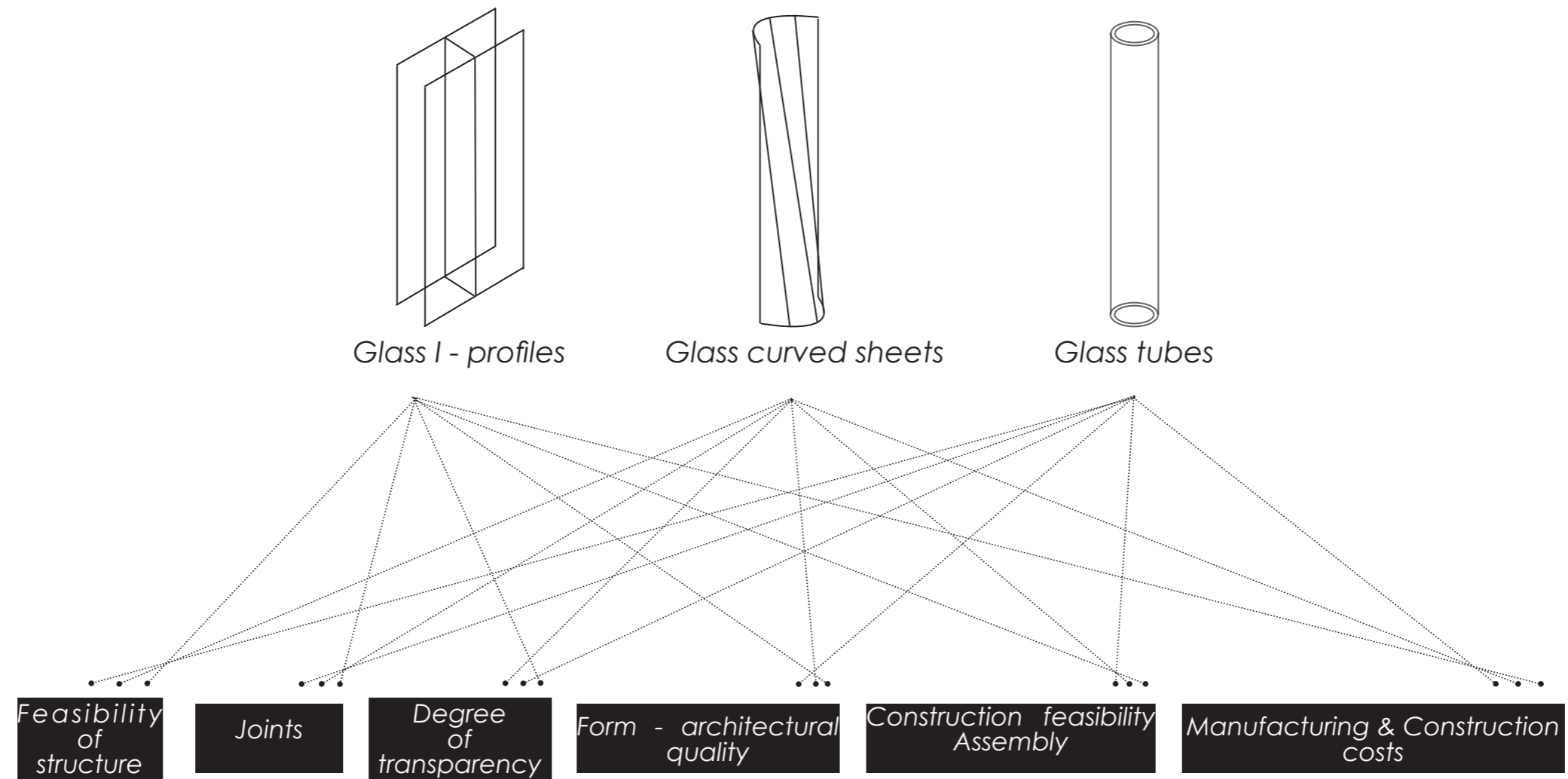


05



NEW Design methodology based on

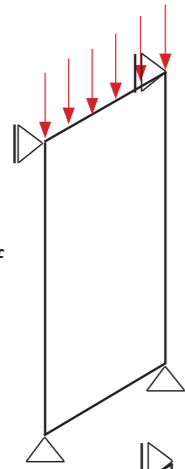
Glass Component type



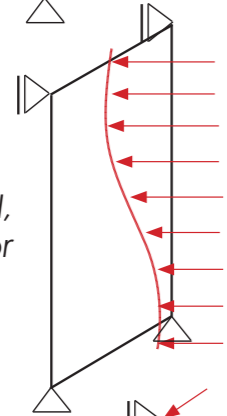
/// **STAGE 3**_DESIGN RESEARCH - 3 STRATEGIES ///

Load Actions

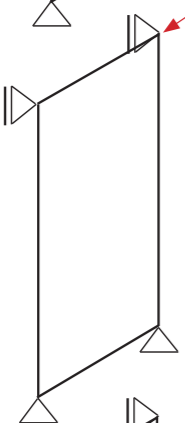
01
Dead load, self weight



02
Wind load, pressure or suction



03
Horizontal in-plane load

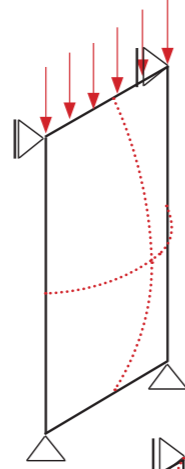


04
Impact loads

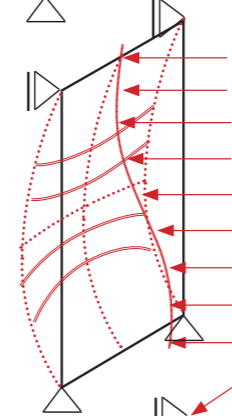


Resulting Condition

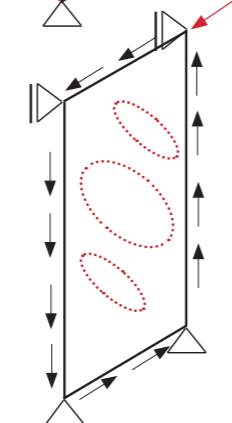
Local Buckling



Bending Stresses

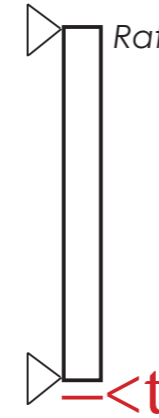


Shear Buckling



Stiffening Methods

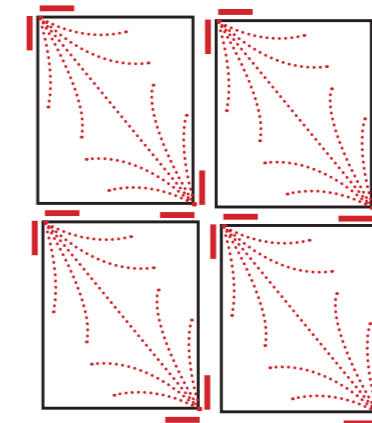
01 Ratio thickness - span



02 Use effective cross sections



01 Transfer the load as bracing



01 **Self supporting skin /**
No secondary support

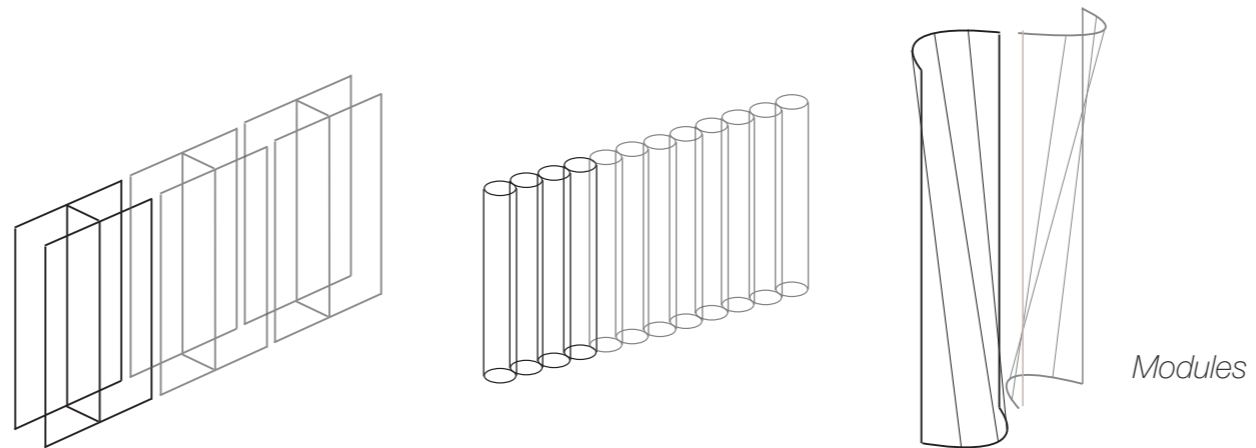
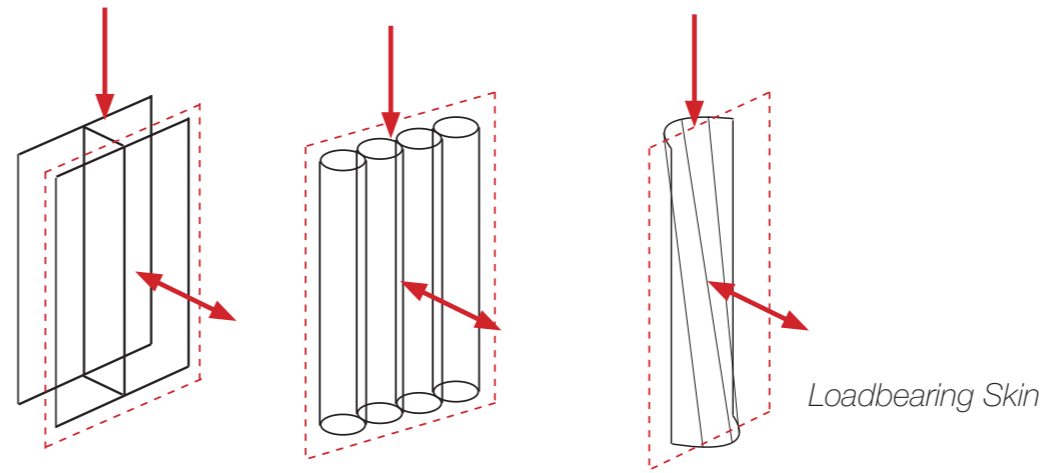
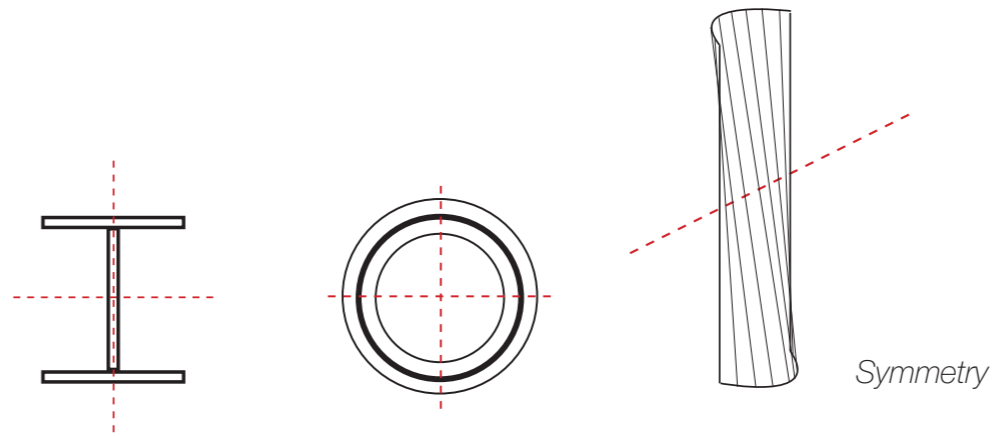
02 **Symmetry /**
at least along one axis

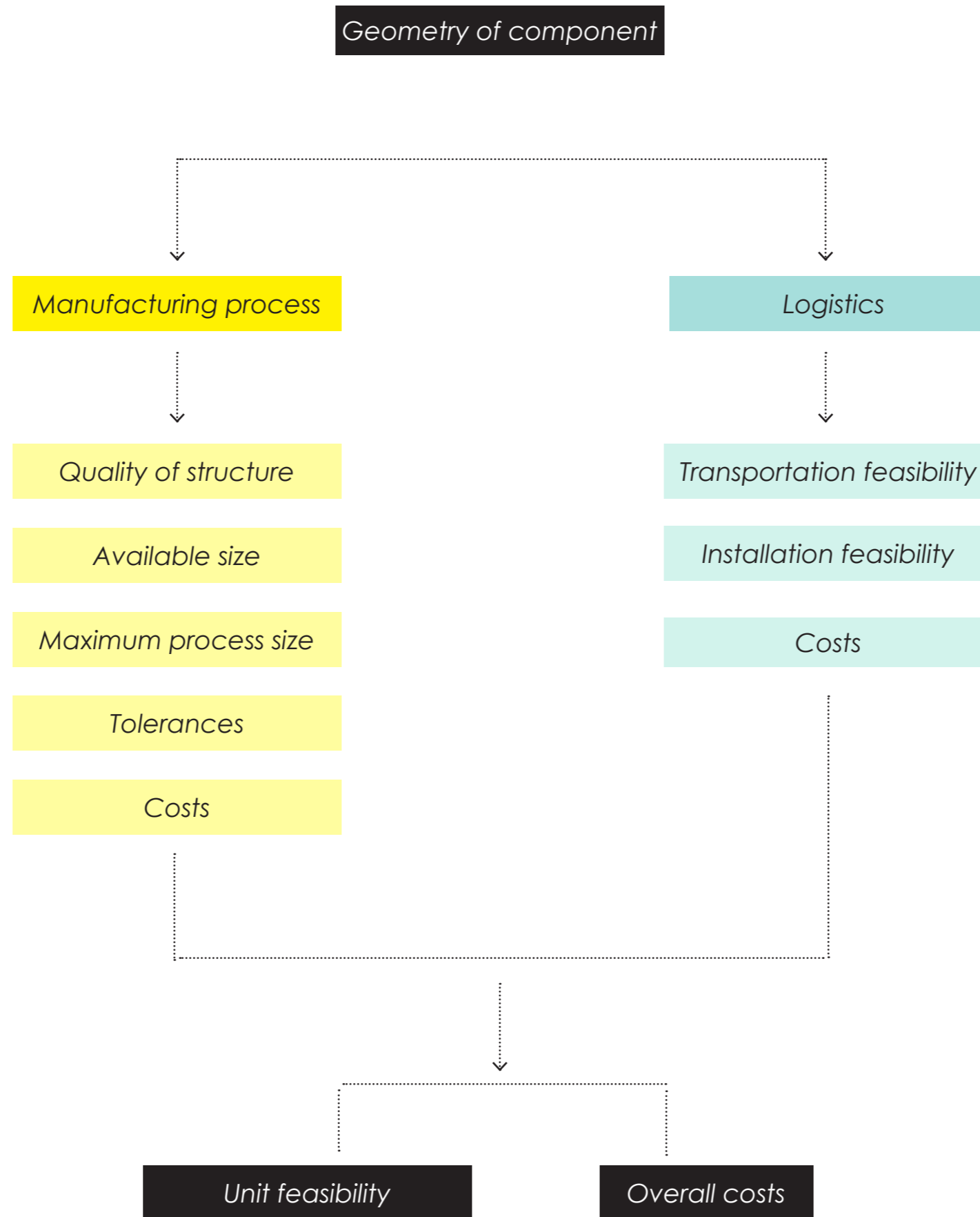
03 **Homogeneous appearance /**
Same from exterior and interior

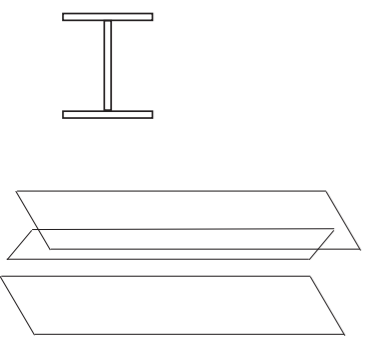
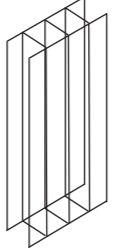
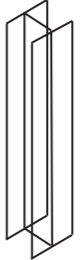
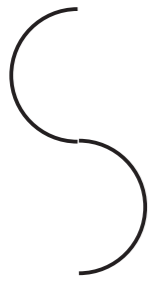
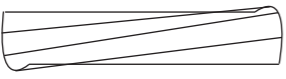


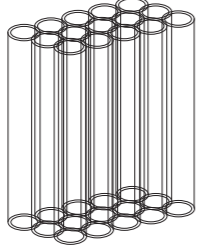
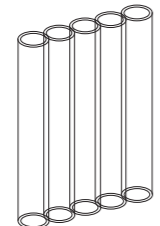
04 **Transparent or frameless joints /**

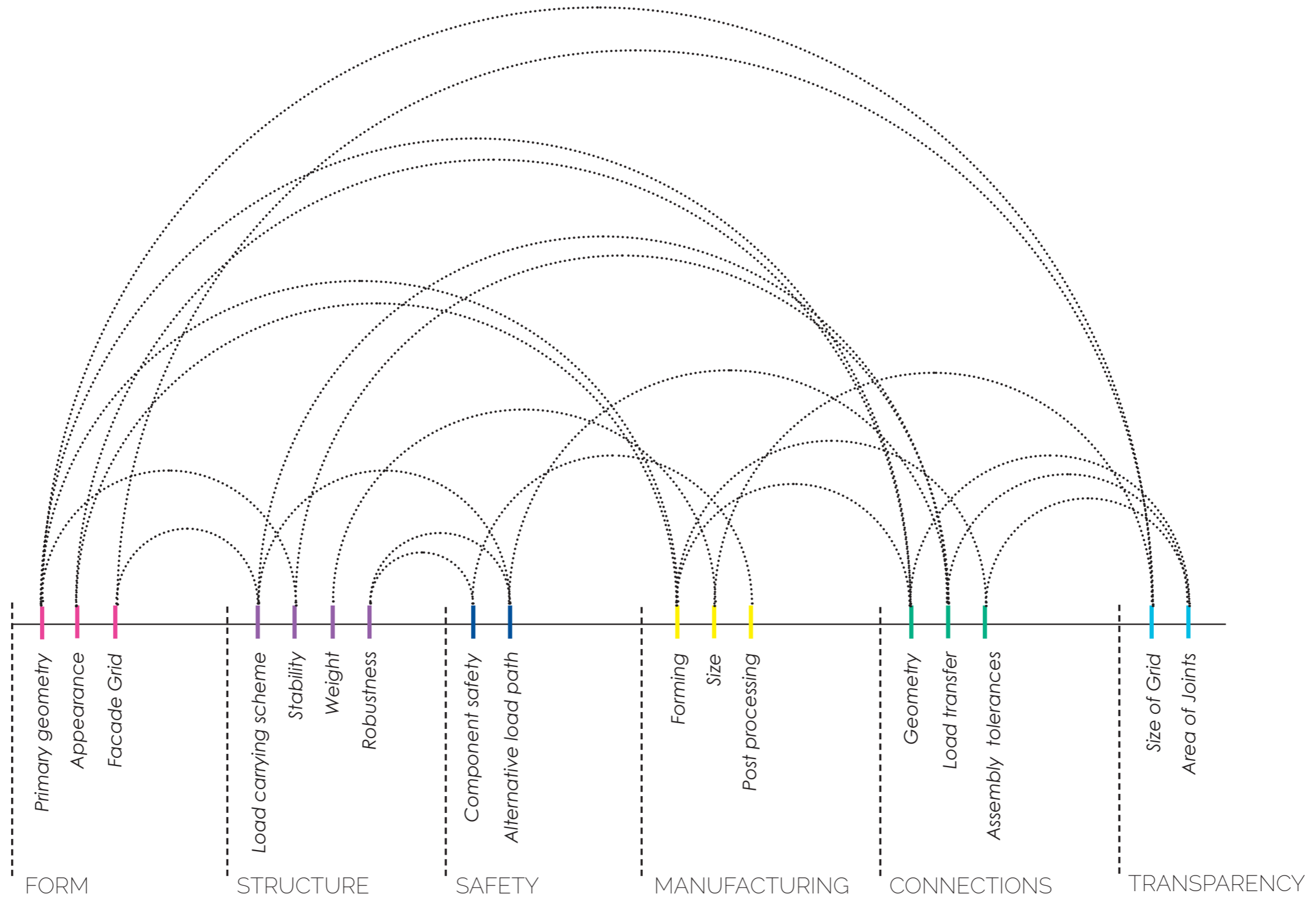
05 **Design versatility /**
Many form potential

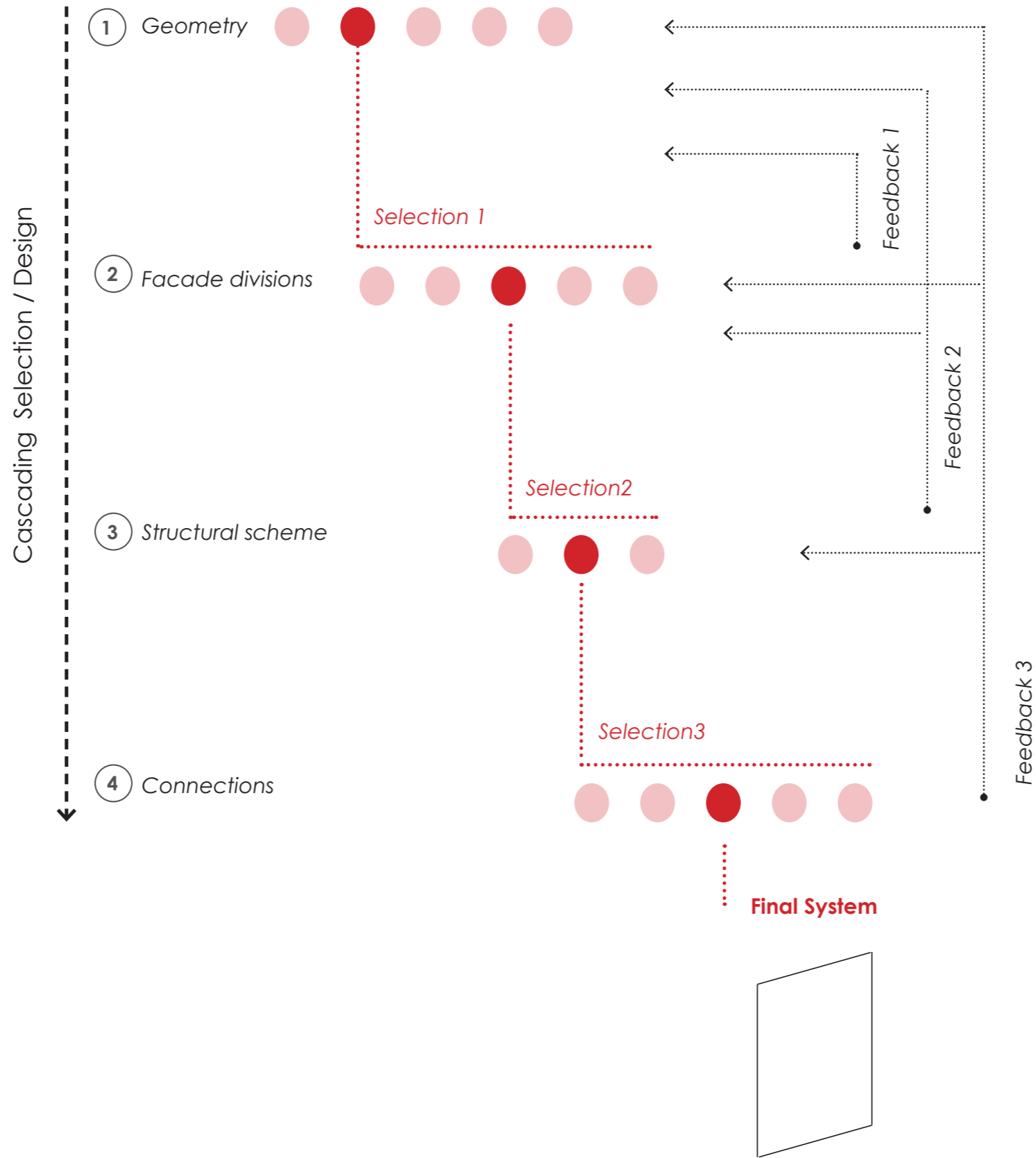
06 **Modules /**
Possibility of assembly in units





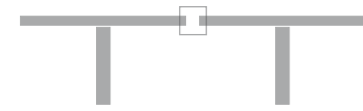
Geometry		Manufacturing							Logistics		Safety		
Primary shape	Unit scheme	Process	Max. Raw size	Min. Radius /Diameter	Max. Processing size	Max. lamination size	Max. Realized size	Tolerances	Costs	Feasibility	Costs	Lamination	Tempering
 Flat sheet	 Ribbed plate	Float glass	approx. 25000 mm		8000mm in Europe	15000mm in glass industry	14000m	++ for oversized (+ - 1 mm / m)	++ (for oversized)	++ (for oversized)	++ (depending on producer)	++	++
	 I-profile				15000mm in China	23500mm in aircraft autoclave							
 Bended surface	 Double curved	Cold Bending	size of flat panel depending on radius	-	+	every size produced		+	+	+	- (for pre-bent)	++	++
	 Single curved	Hot Bending	6000mm length	++	6000mm length	every size produced	5600m length	- (+2mm) (depends on the complexity and size)	-- custom mould + adjustable mould	+	--	+	++
 Hollow tubes	 Bundle	Centrifuging process	standard 1500mm SCHOT -10000 mm	420mm	+	1500mm	not specified	-- (-+5 mm)	--	+	+	+	+ (size limitation)
	 Single row	Daner process	--							+	+	+	



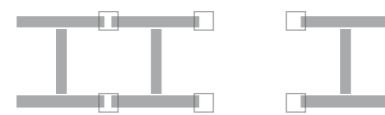




01 Thick plate



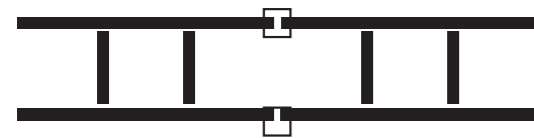
02 T- shape



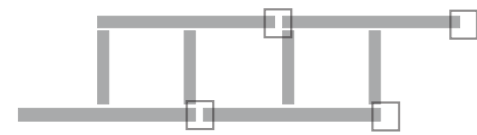
03 I - profile



04 Wide I - profile

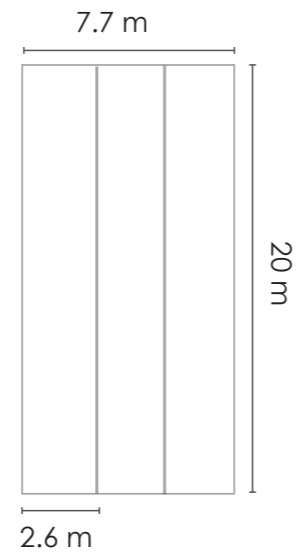


05 Ribbed plate

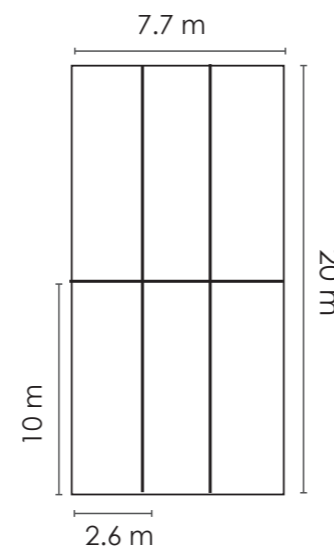


06 Ribbed plate 2 open edges

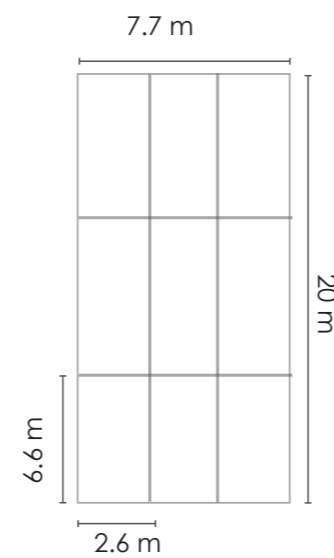
01 Extreme



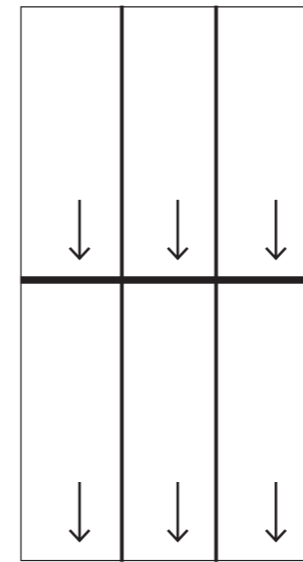
02 Oversized -transportable



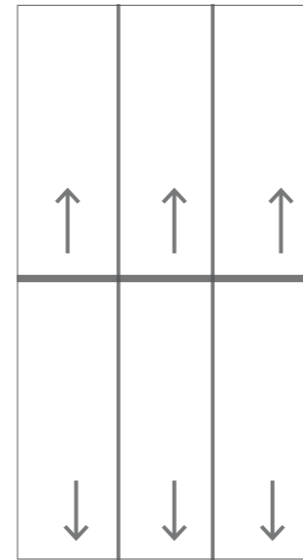
03 Smaller - economic



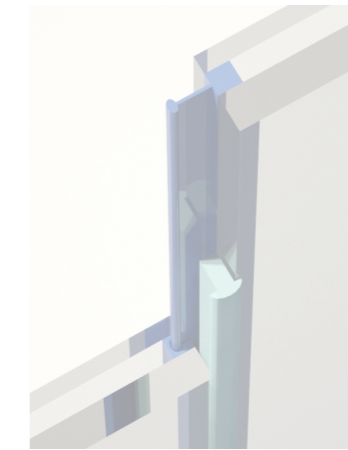
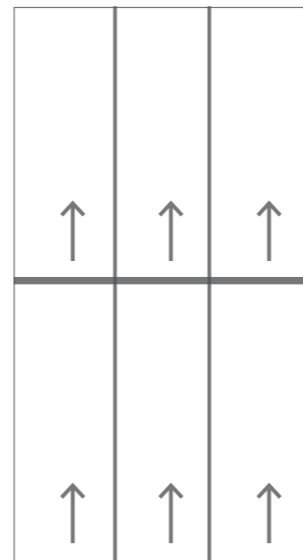
01 Stacking



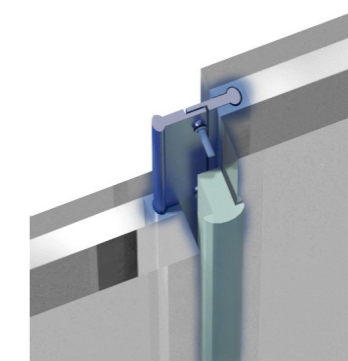
02 Half hanging Half standing



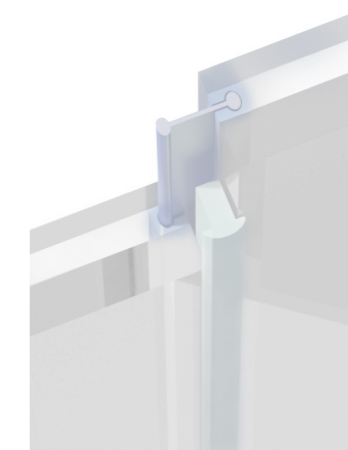
03 Hanging



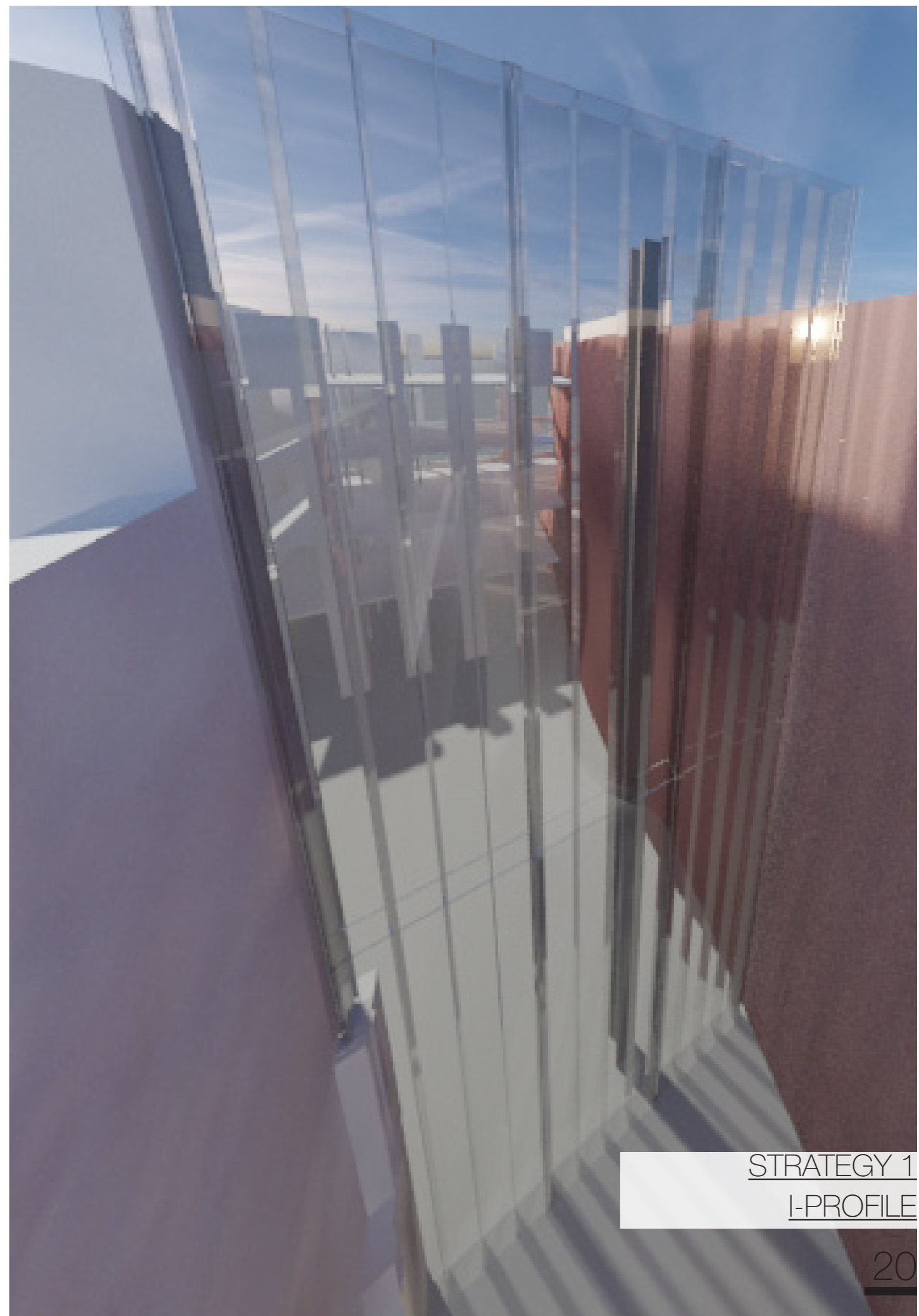
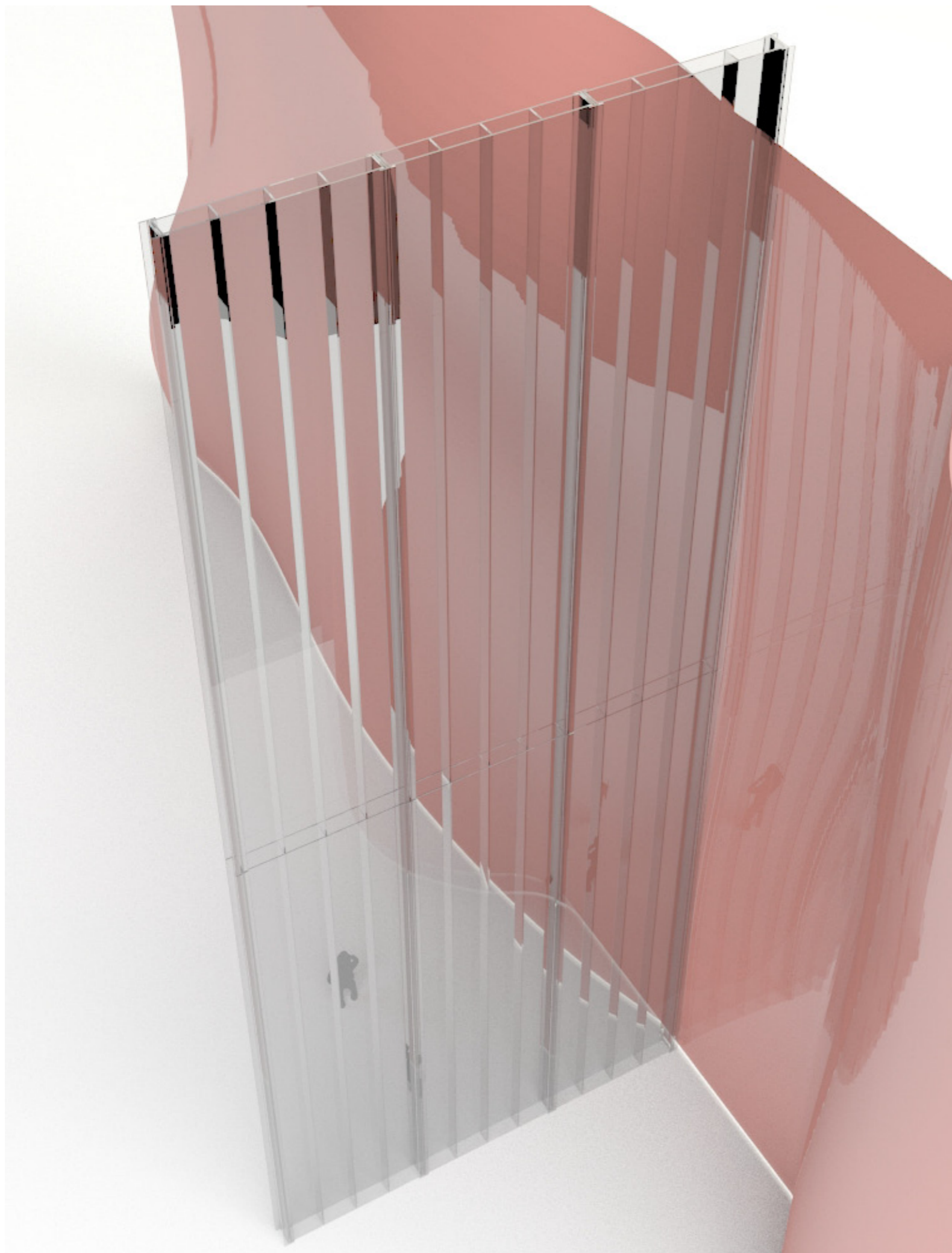
01 Sliding asymmetrical profiles



02 Intermediate adjustable member



03 Intermediate sliding section



STRATEGY 1
I-PROFILE



01 Twisted curve 1



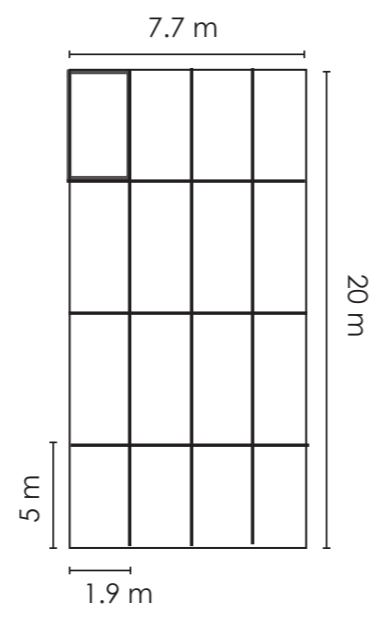
02 Alternative 2



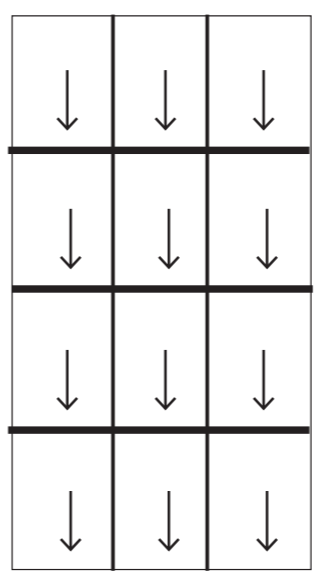
03 Twisted curve 2



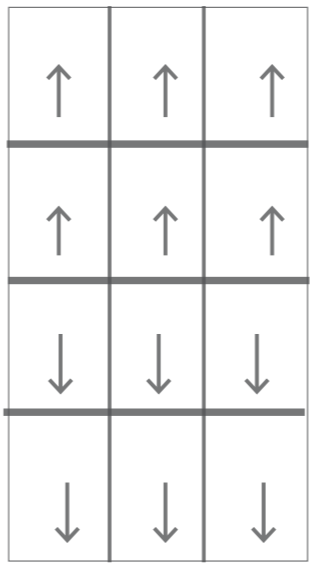
04 Glass curtain



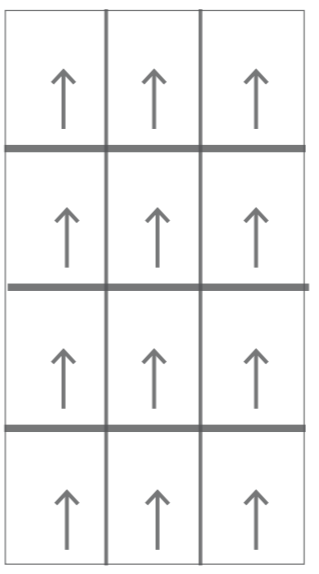
01 Even Grid 4 x 4



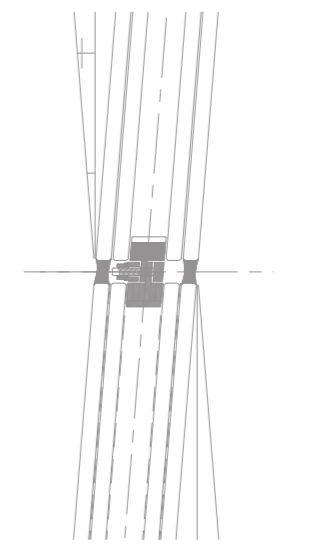
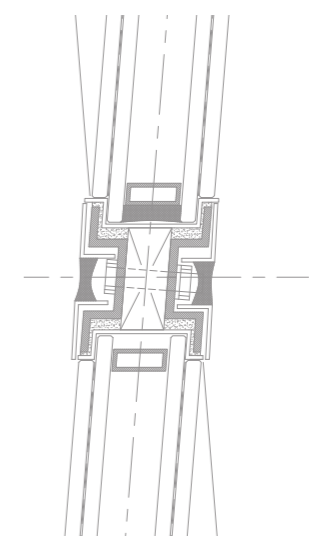
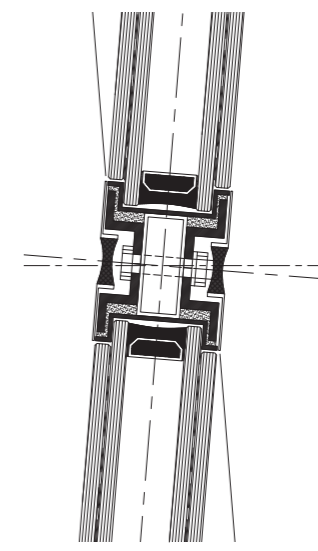
01 Standing

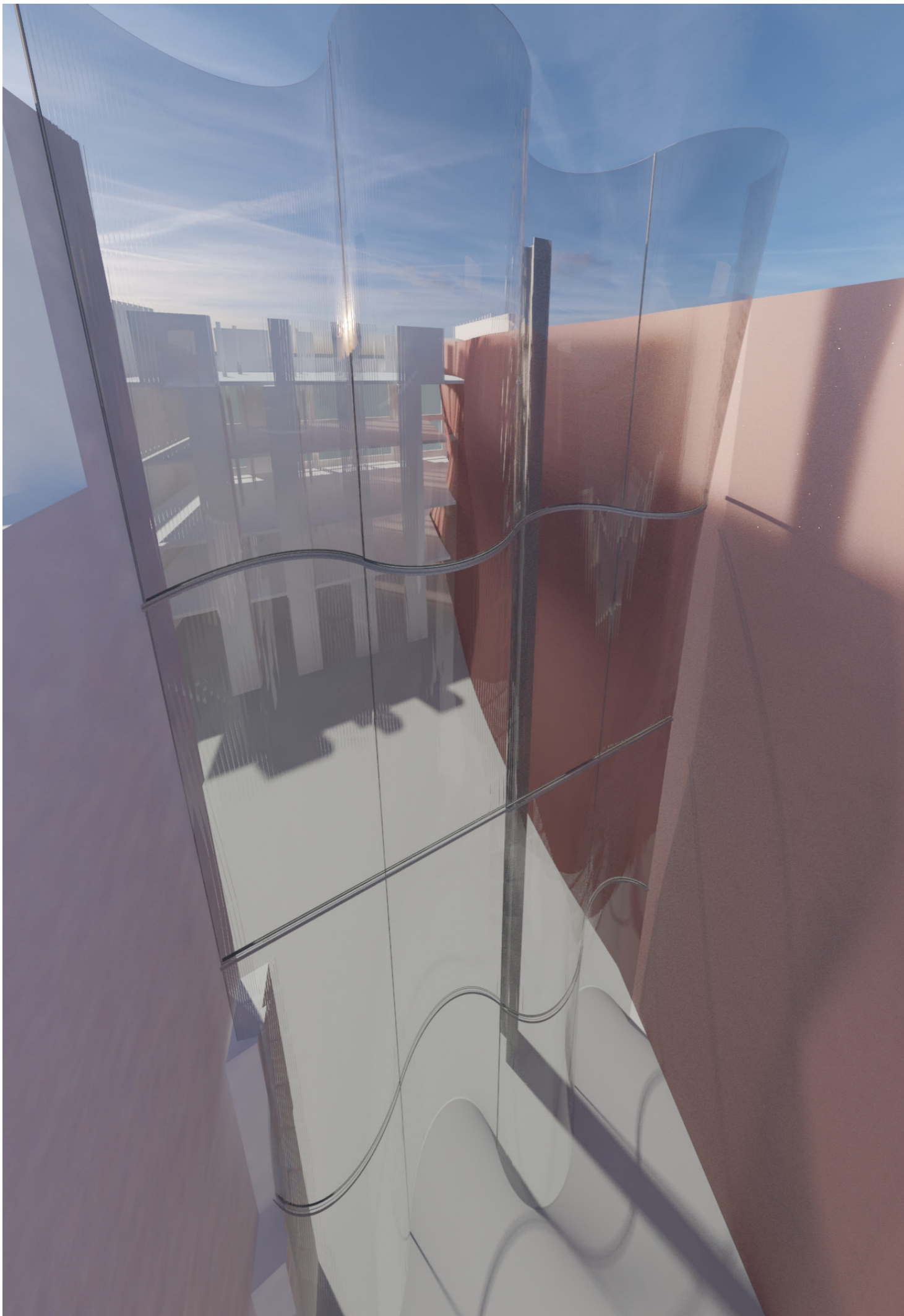


02 Half hanging - Half standing

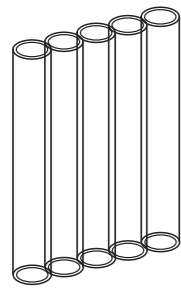


03 All hanging

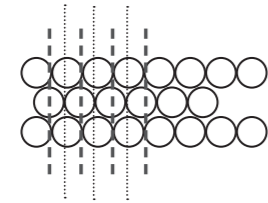
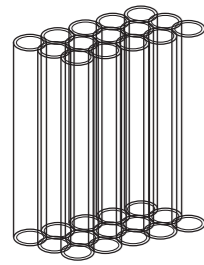




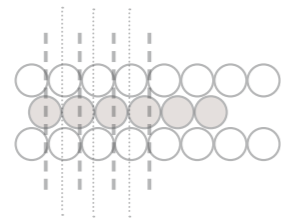
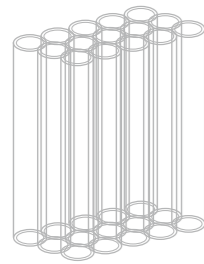
STRATEGY 2
GLASS CURTAIN



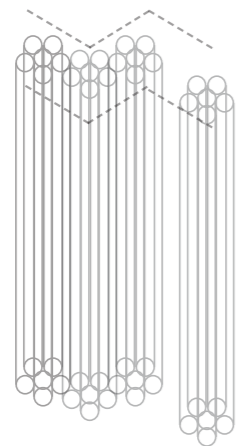
01 Single row hollow tubes



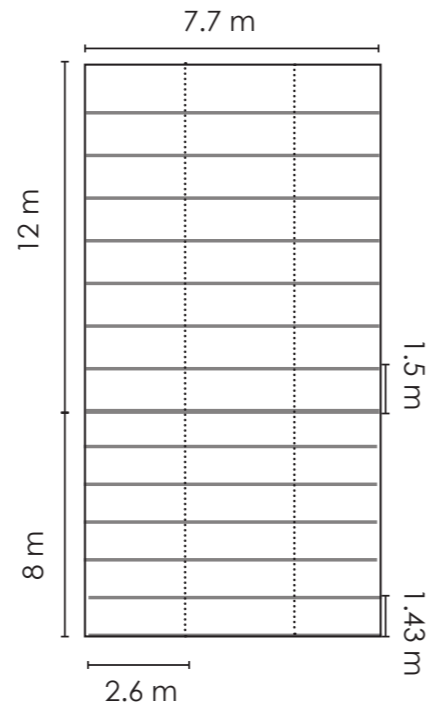
02 Multiple rows hollow tubes



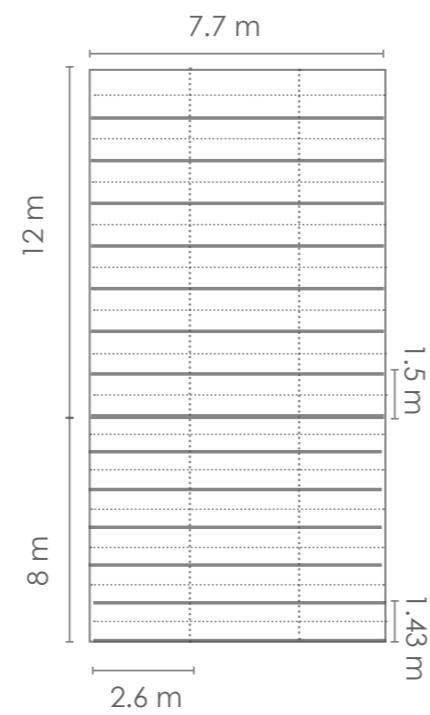
03 Hollow out massive core



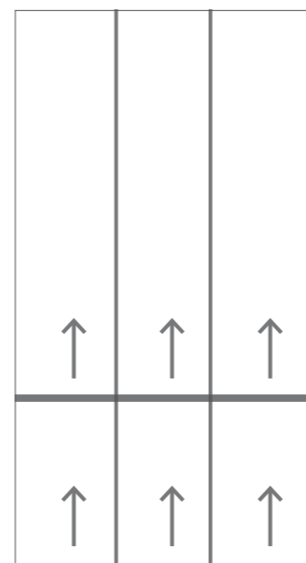
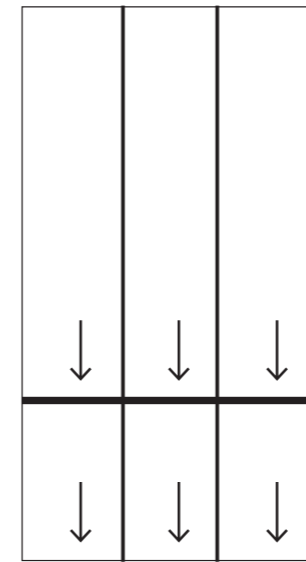
04 Massive bundles



01 Normal grid

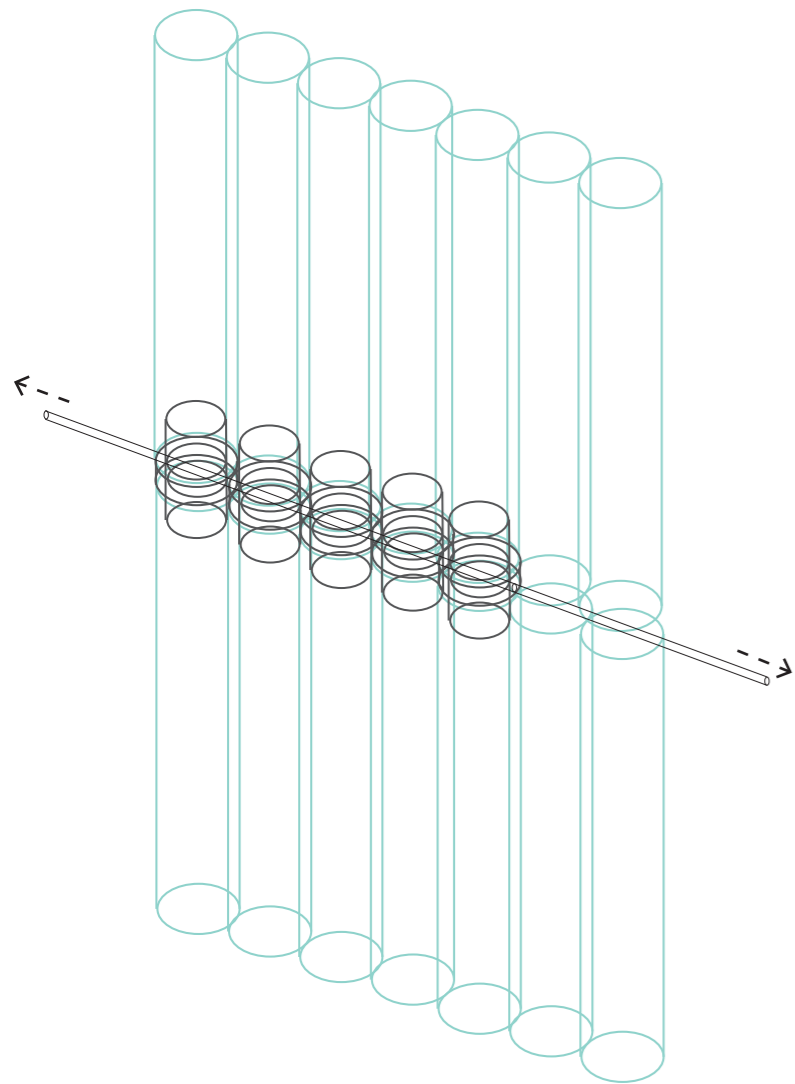


02 Overlapping grid



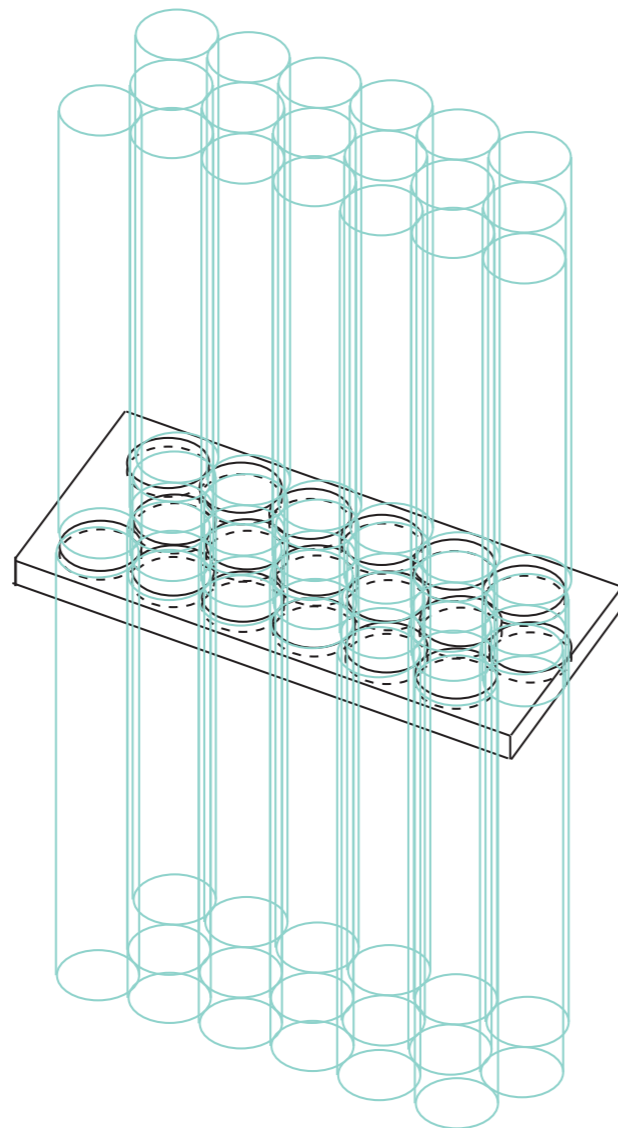
01 Intermediate transparent sleeve

CONCEPT 1
Single row units

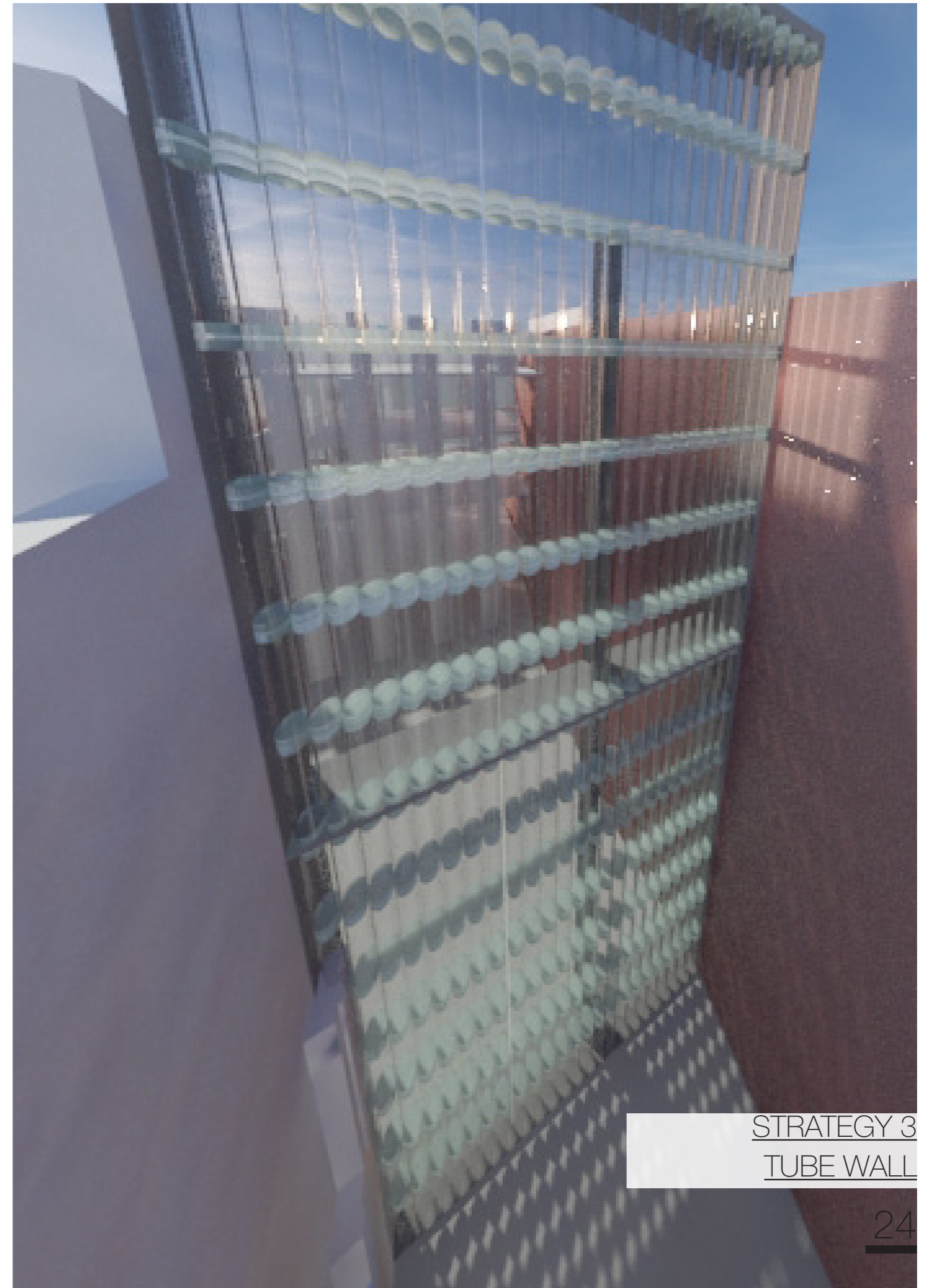


01 Single row hollow tubes with intermediate transparent sleeve joint. Stabilized by post tensioned rods.

CONCEPT 2
Multiple row units



02 Multiple row of tubes. Intermediate support. Tubes fixed in a special dish profile with resin added at the bottom.



	Units			System				Overall Feasibility
	Size	Costs	Form potential	Structure Feasibility	Form / Appearance	Joints	Transparency	
Strategy 1 / I-profile	++	+	-	++	-	+	++	++
Strategy 2 / Curved	+	+	++	+	++	-	+	+
Strategy 3 / Tubes	--	--	+	-	++	--	-	+

	Units			System				Overall Feasibility
	Size	Costs	Form potential	Structure Feasibility	Form / Appearance	Joints	Transparency	
Strategy 1 / I-profile	++	+	-	++	-	+	++	++
Strategy 2 / Curved	+	+	++	+	++	-	+	+
Strategy 3 / Tubes	--	--	+	-	++	--	-	+

1 | Transparency

2 | Structural performance

3 | Size

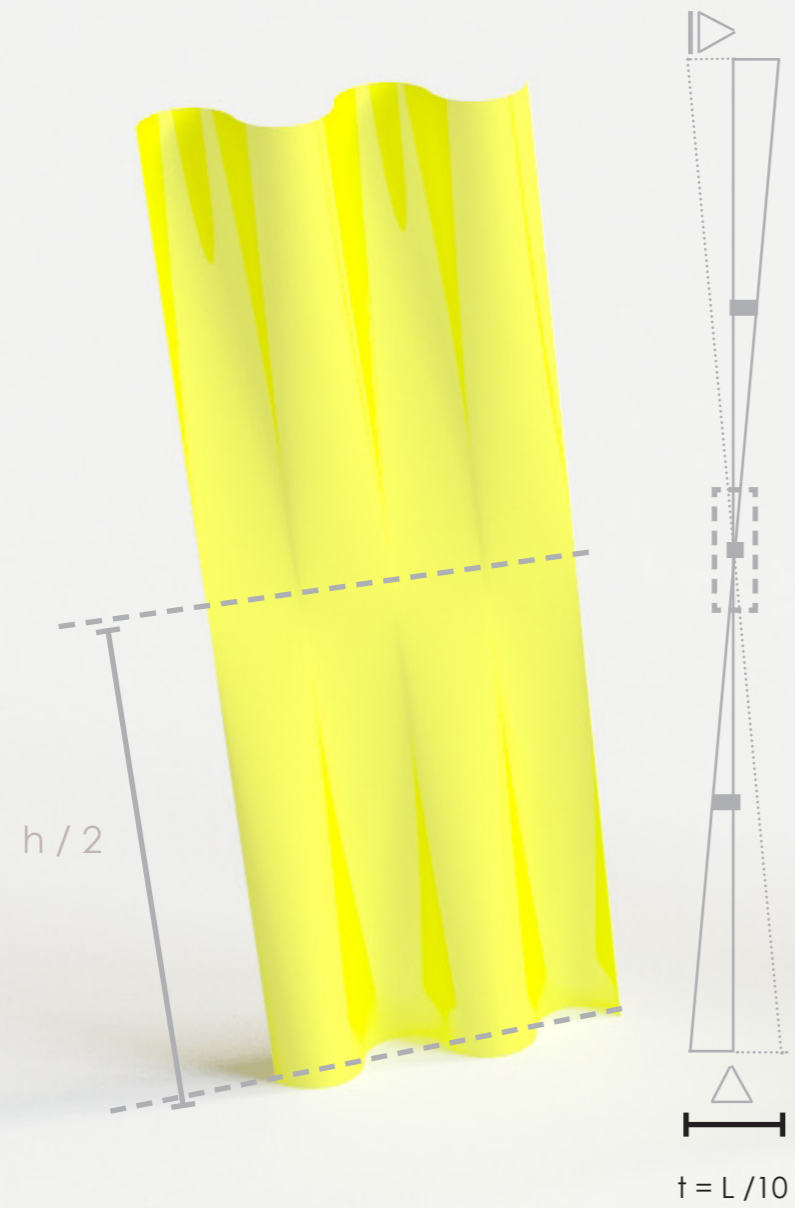
4 | Design Versatility

5 | Processing

6 | Information availability

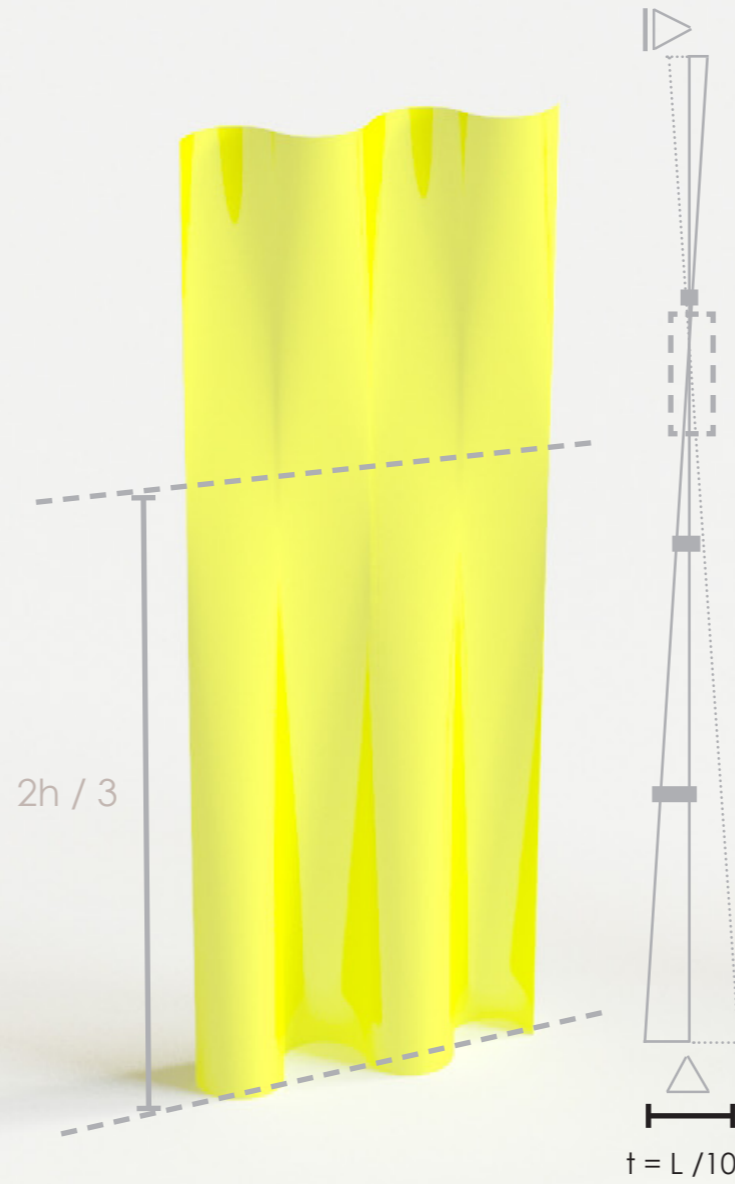
7 | Architects' preference

/// **STAGE 4**_FINAL DESIGN DEVELOPMENT ///



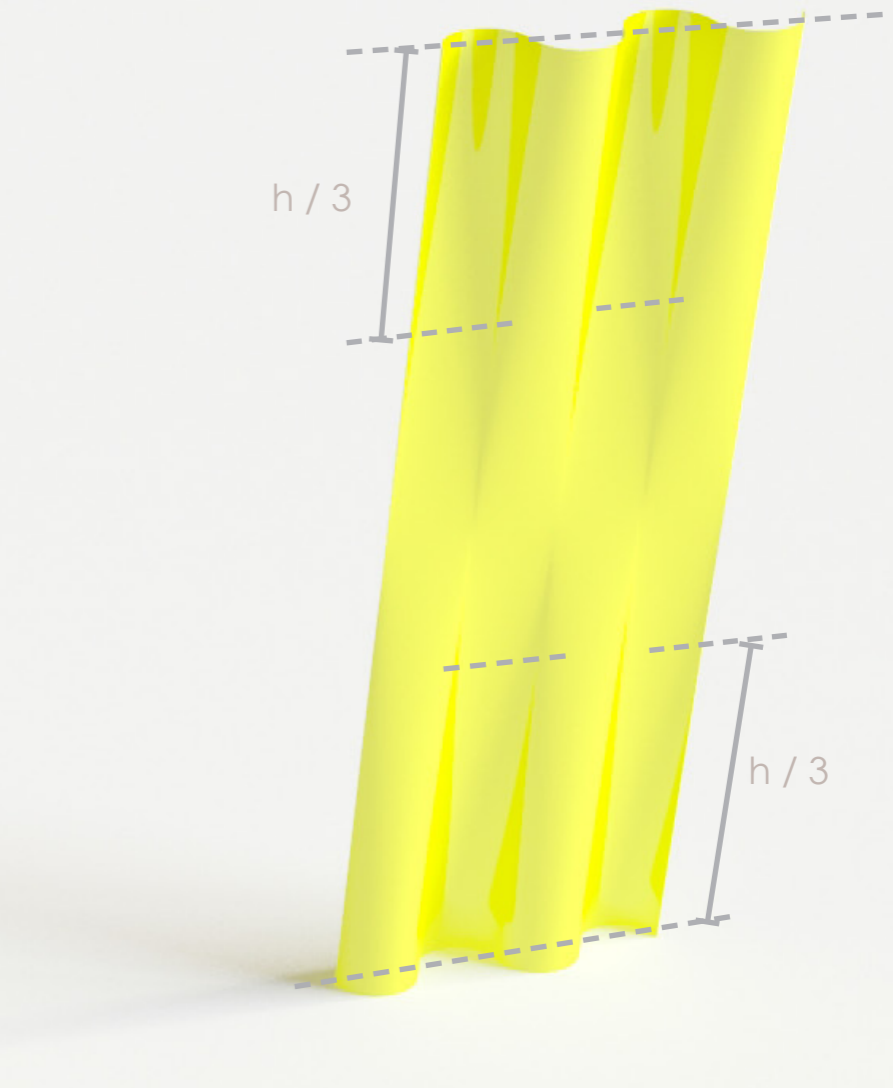
01

- _Common symmetry axis
- _Middle weak point



02

- _Common symmetry axis
- _Elevating the twist axis higher ($2h/3$)
- _Avoid weak central connection

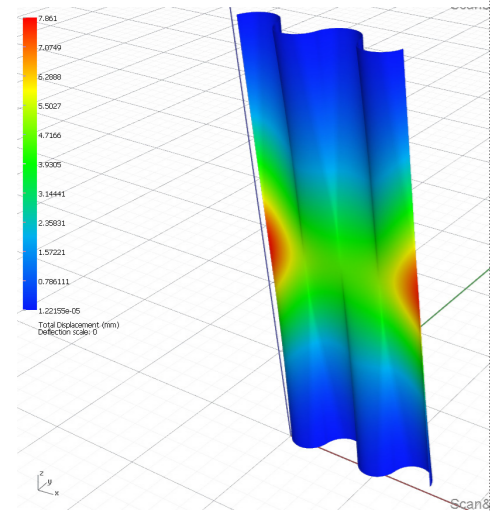


03

- _ Not common symmetry axis
- _ Alternating for each panel
- _ Avoid weak central connection
- _ Complicated surface
- _ Uneven load distribution

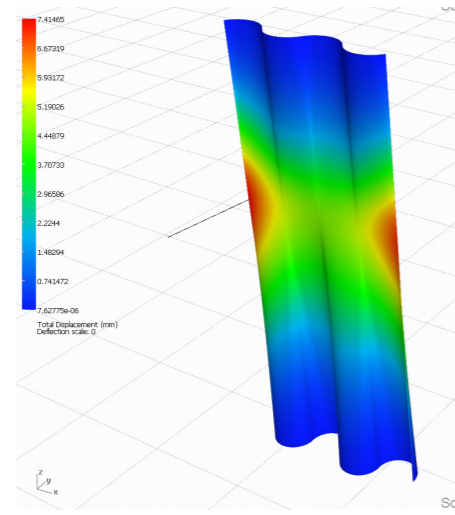
DESIGN
IMPROVEMENTS

01



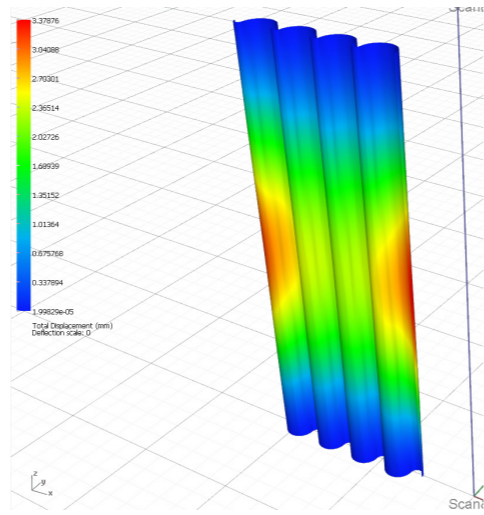
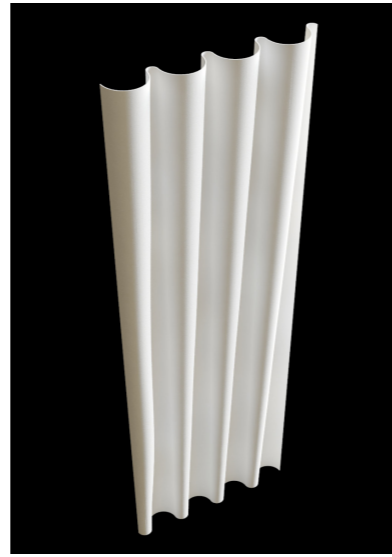
Maximum displacement
7.86mm

02



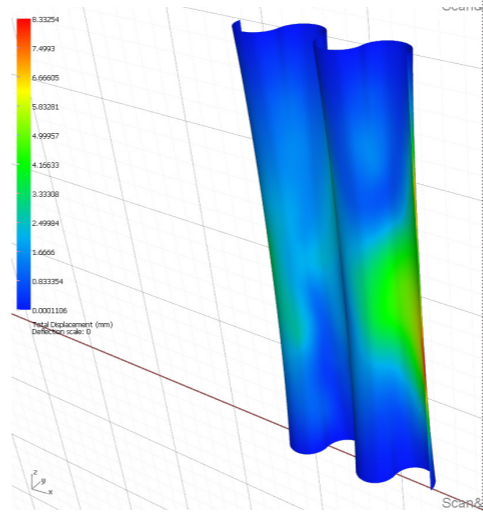
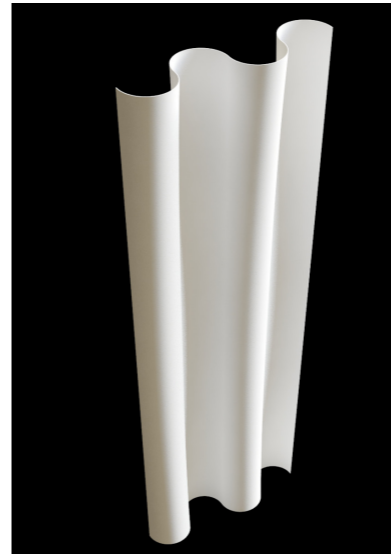
Maximum displacement
7.41mm

03



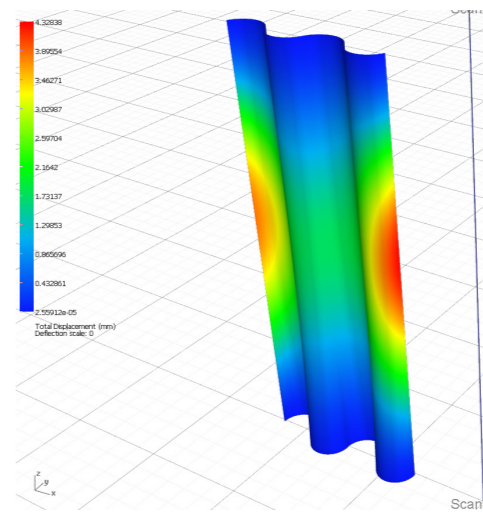
Maximum displacement
3.33mm

04



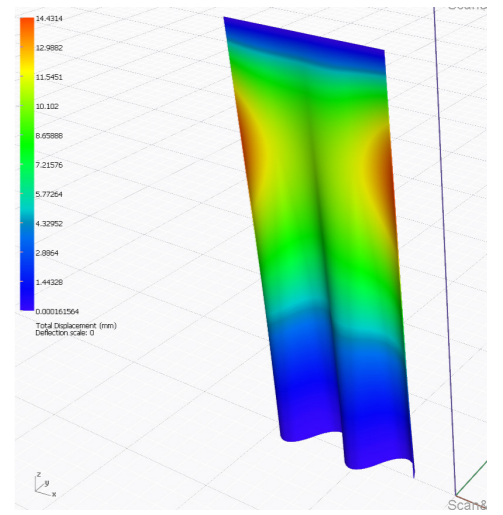
Maximum displacement
8.33mm

05



Maximum displacement
4.32mm

06



Maximum displacement
14.12mm

01 Geometry & Material

The calculation can be done only for monolithic solid element. Not an option to model separate materials. The surface has to be only out of one material.

02 Boundary conditions

Non accurately modeled. They are presented as fixed, instead of hinge at the bottom and roller at the top.

03 Safety factor

The partial factor of safety to enhance reliability of the structure is not applied.

04 Maximum stresses

Not an option to evaluate the stresses in plane of the facade. We can only check for displacements and global stresses.

01 Design Value

The most interesting of the designs. Resembles a glass curtain hanging from the ceiling.

02 Structural shape

Stiff double-curved sinus shaped shell reducing towards the top to a flat edge. The pyramidoid scheme provides greater stability by lowering the center of gravity.

03 Transparency

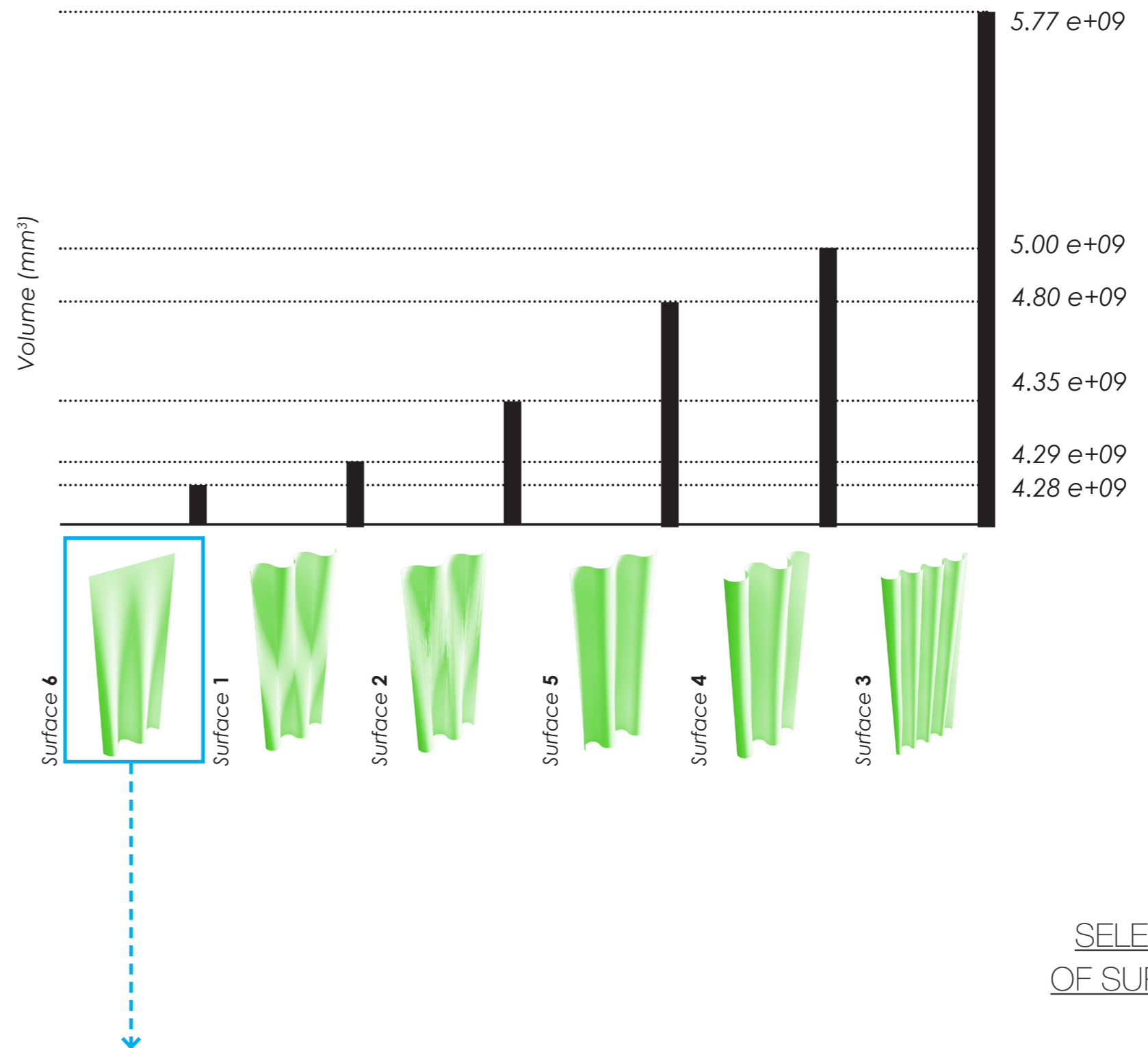
The deflections are transferred at the top part of the element. No need for additional supports behind the surface like in the twisted panel.

04 Manufacturing

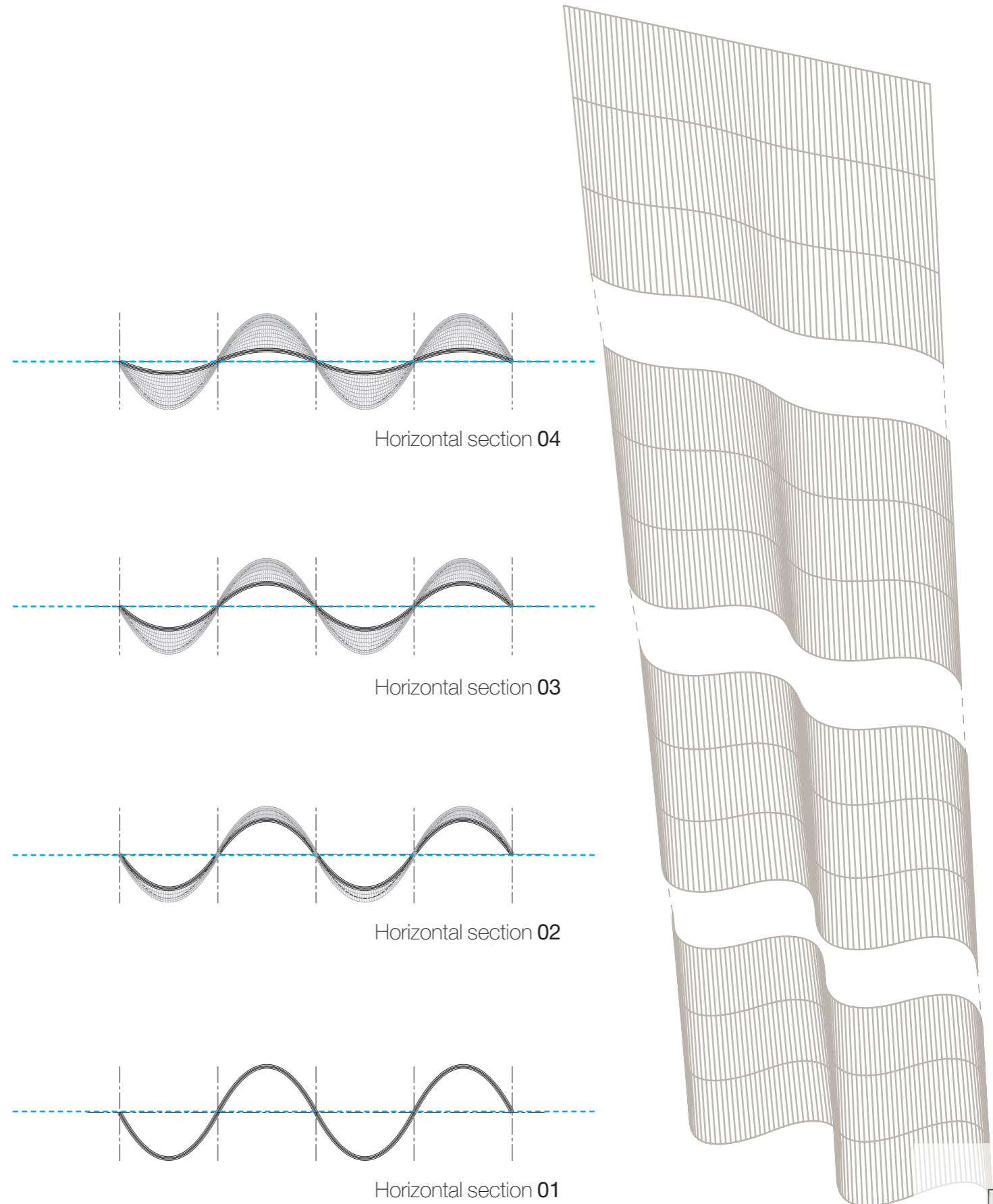
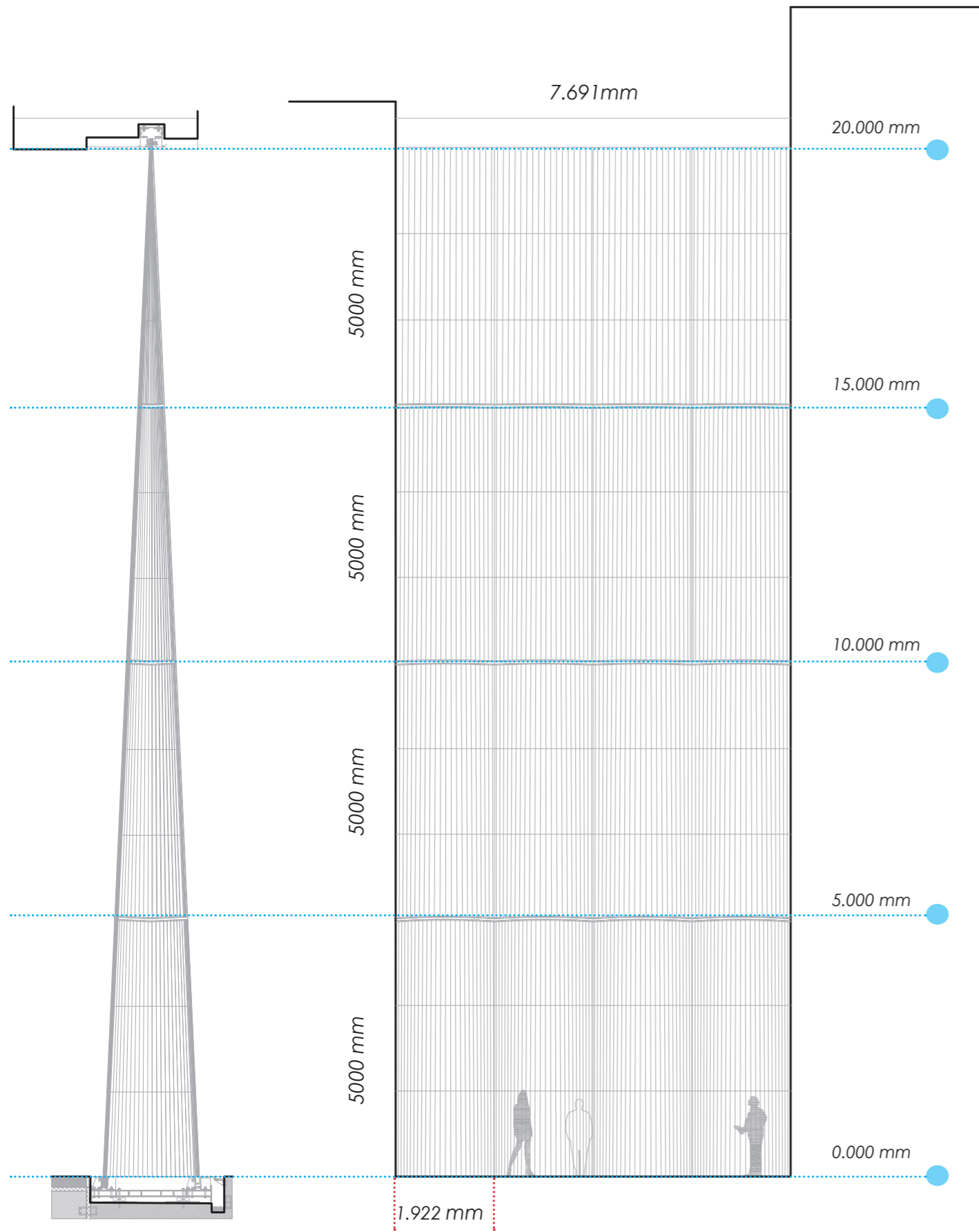
Because the curvature is reduced towards the top edge, the overall complexity and intensity of radii is less than in the other facade shapes.

05 Cost

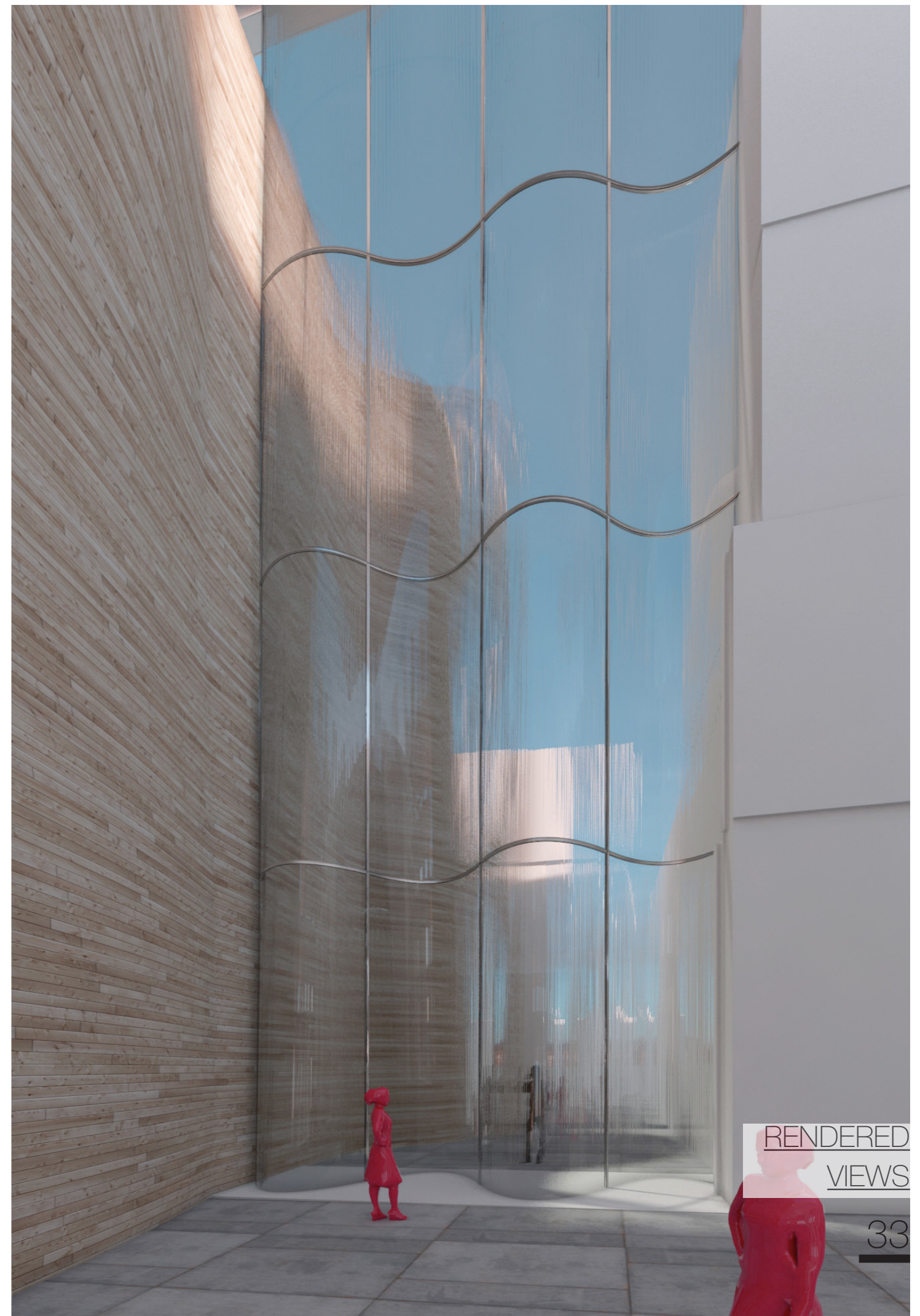
The most effective shape as the use of material is less. Calculated volume **4.28e+09 mm³**.

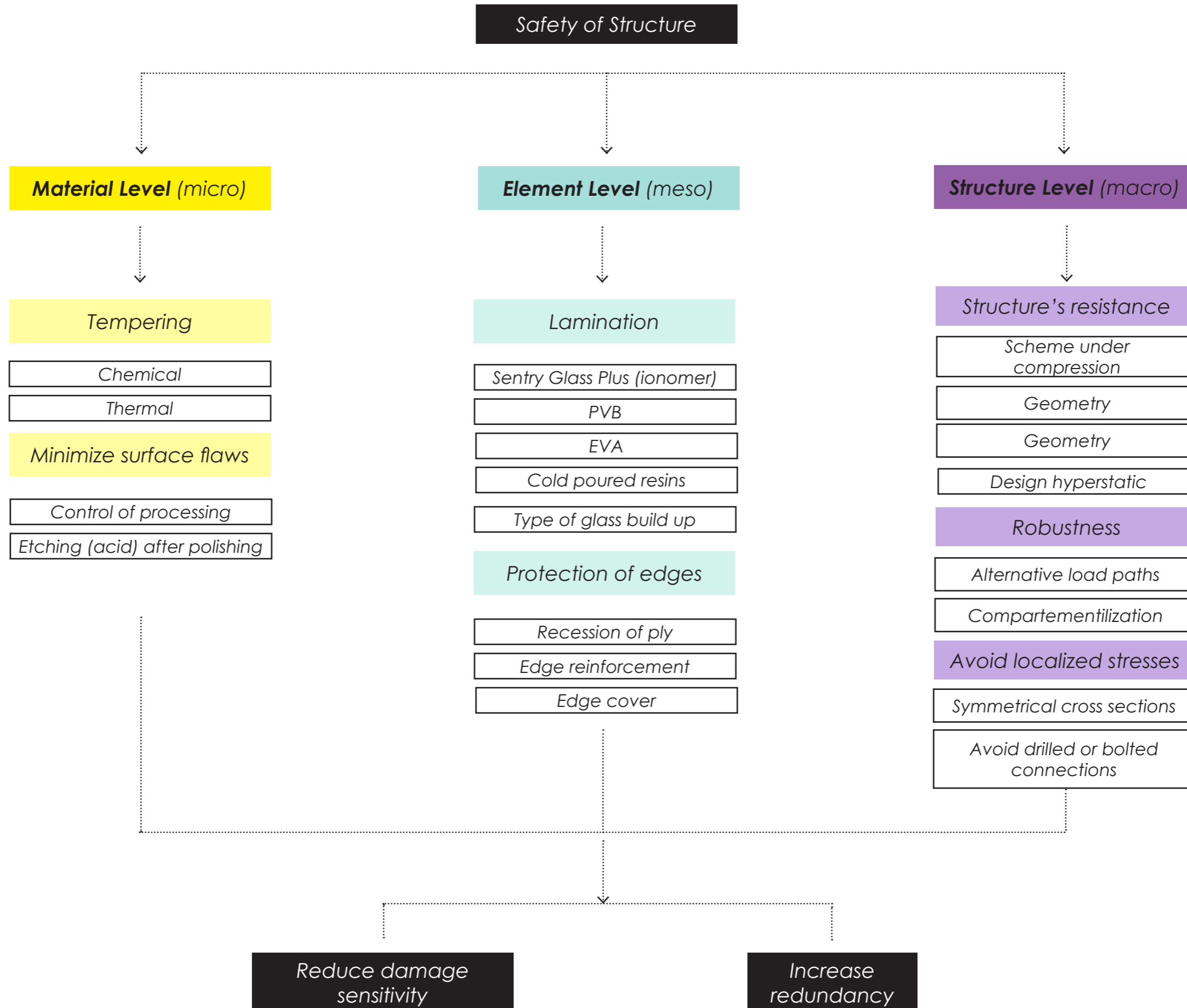


SELECTION
OF SURFACE



FINAL
DESIGN

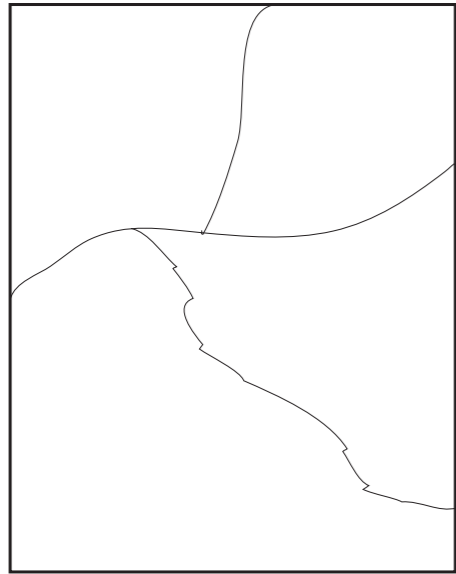




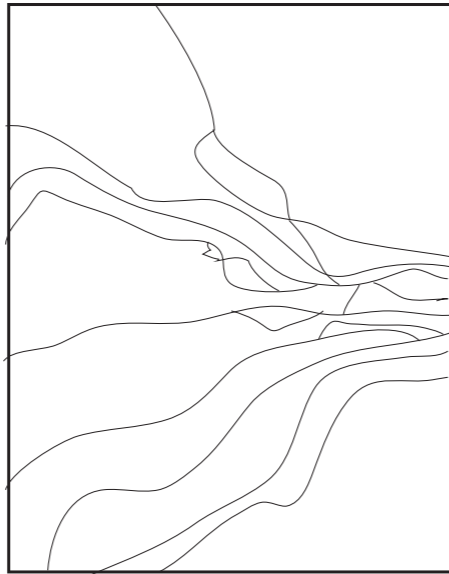
NO PRE-STRESS

PRE-STRESS

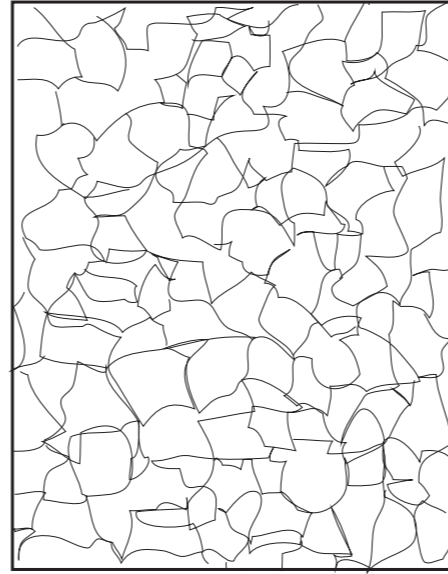
Annealed glass



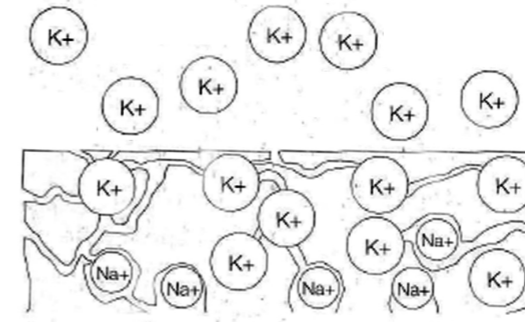
Heat strengthened glass



Fully tempered glass

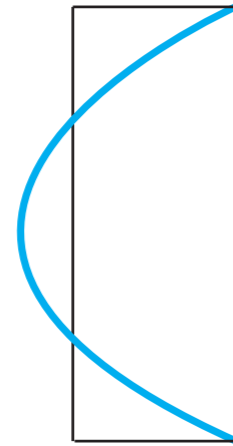


Chemically strengthened

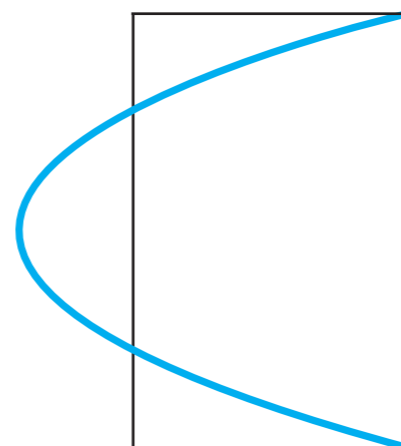


Maximum Tensile strength

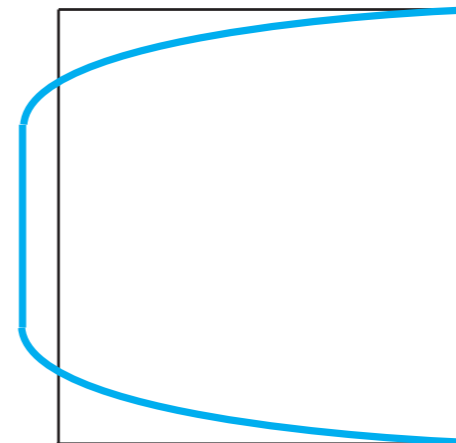
45 N / mm²



70 N / mm²



120 N / mm²



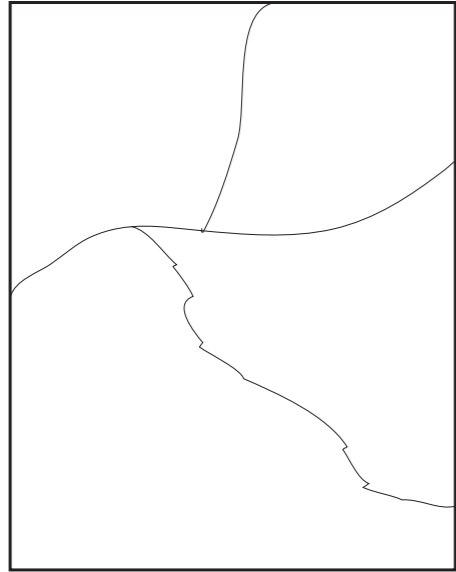
- _Lower damage sensitivity
- _Long term stress resistance
- _Thermal stress resistant
- _Impact resistant
- _Scratch resistant

- _Soft body impact resistant
- _Thermal stress resistant
- _Long term load resistant
- _Prone to hardbody impact
- _Prone to deep scratches
- _Chipping
- _Nickel sulfide inclusions

- _Cutting or drilling remains possible
- _Thin layer of compression
- _Prone to self-fatigue
- _For complicated geometries
- _Expensive process
- _Rare in structural application

MATERIAL
LEVEL (MICRO)

Annealed glass



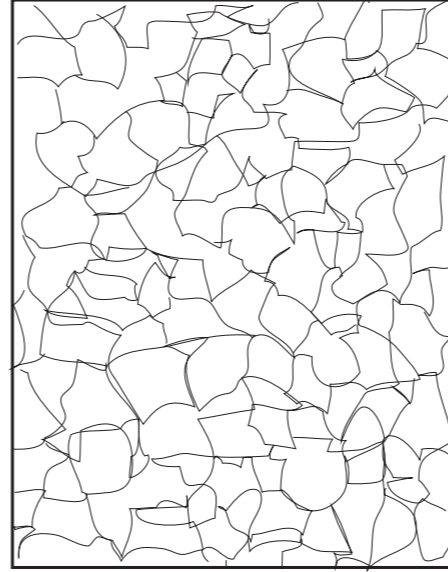
45 N / mm²

Heat strengthened glass



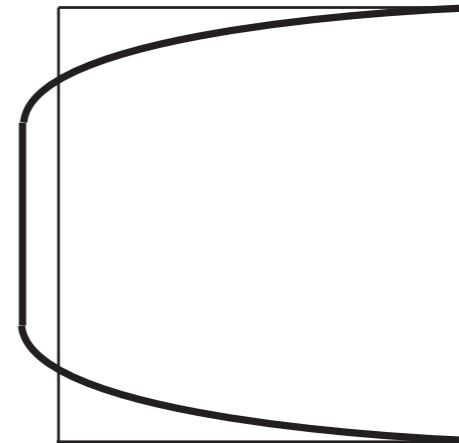
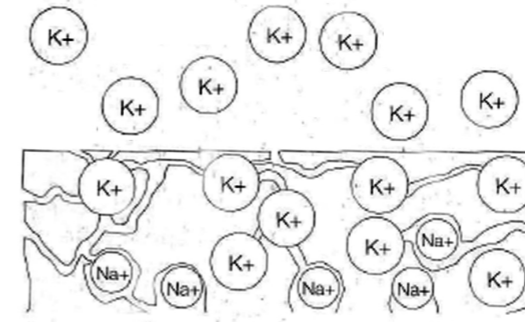
70 N / mm²

Fully tempered glass



120 N / mm²

Chemically strengthened



LAMINATION OF FACADE PANELS

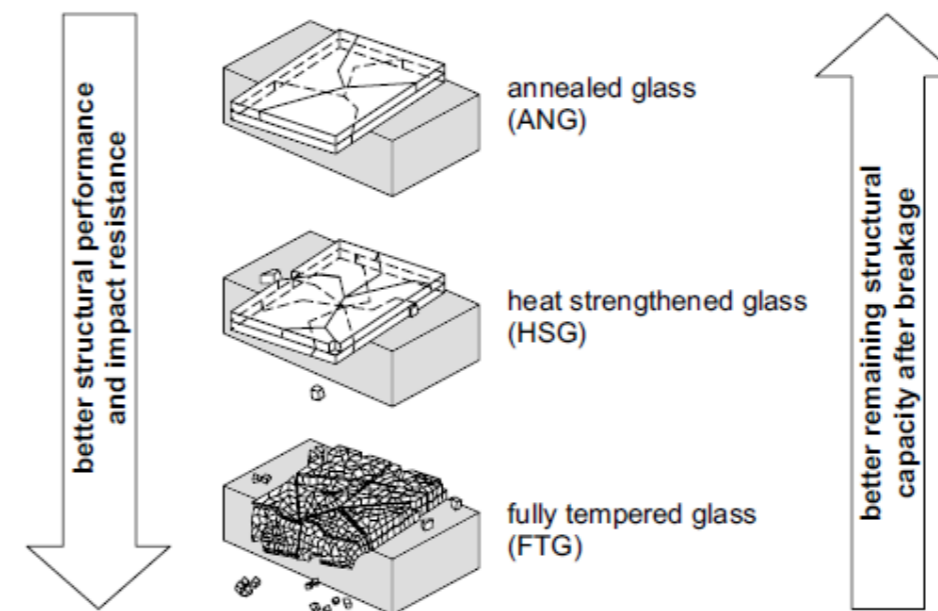


Polyvinyl Butyral **PVB**

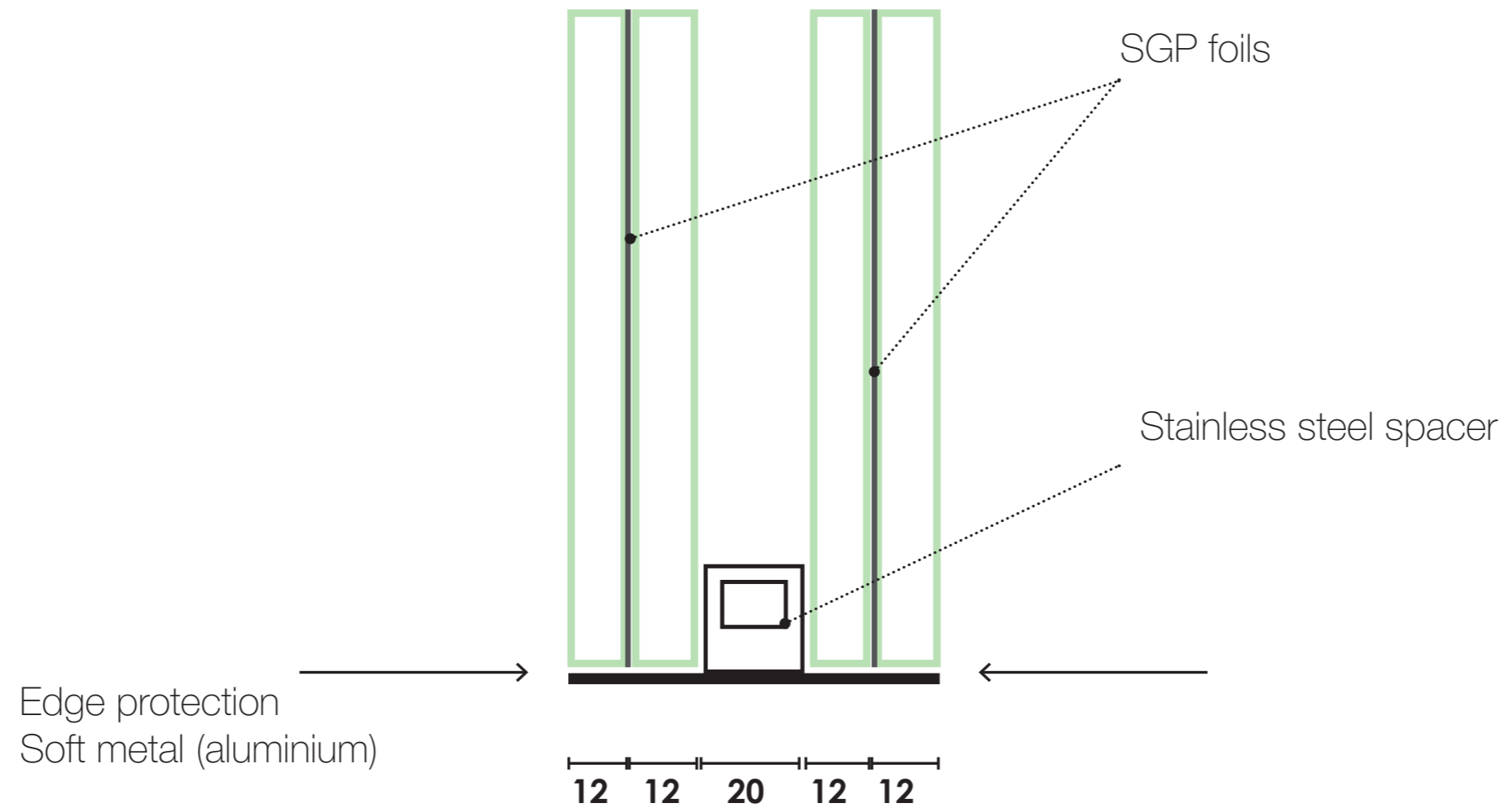
- Tensile strength ≤ 20 Mpa
- High elasticity
- Affected by temperature
- Load duration dependent
- Prone to creep
- Average tear strength

SentryGlas Plus **SGP** (DuPont™)

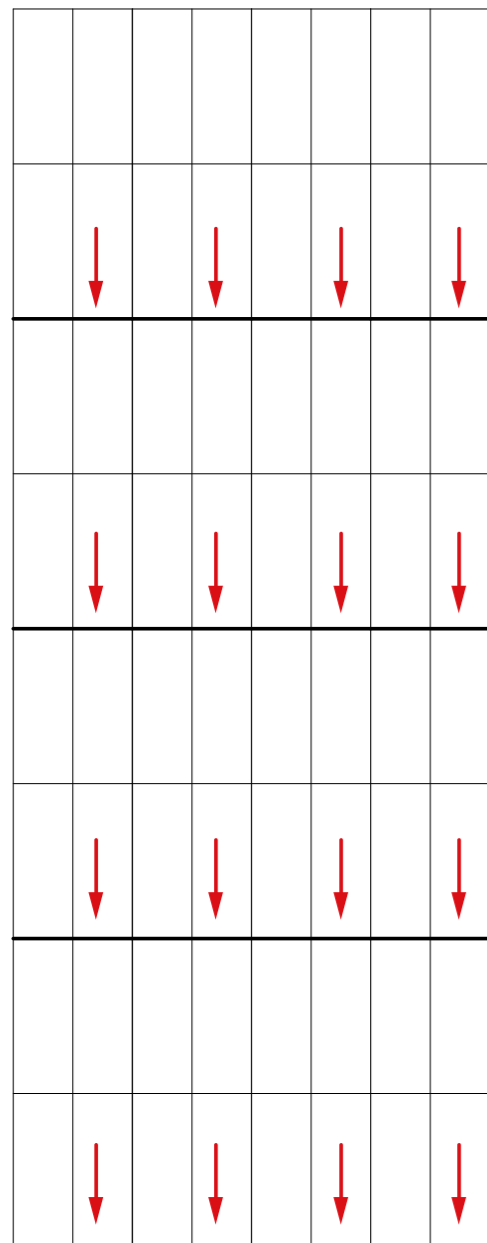
- Tensile strength 300 MPa
- 100 times more rigid structure
- Less affected by temperature
- Load duration dependent
- 5 times higher tear strength
- Difficult in lamination
- Thinner laminates



EDGE PROTECTION

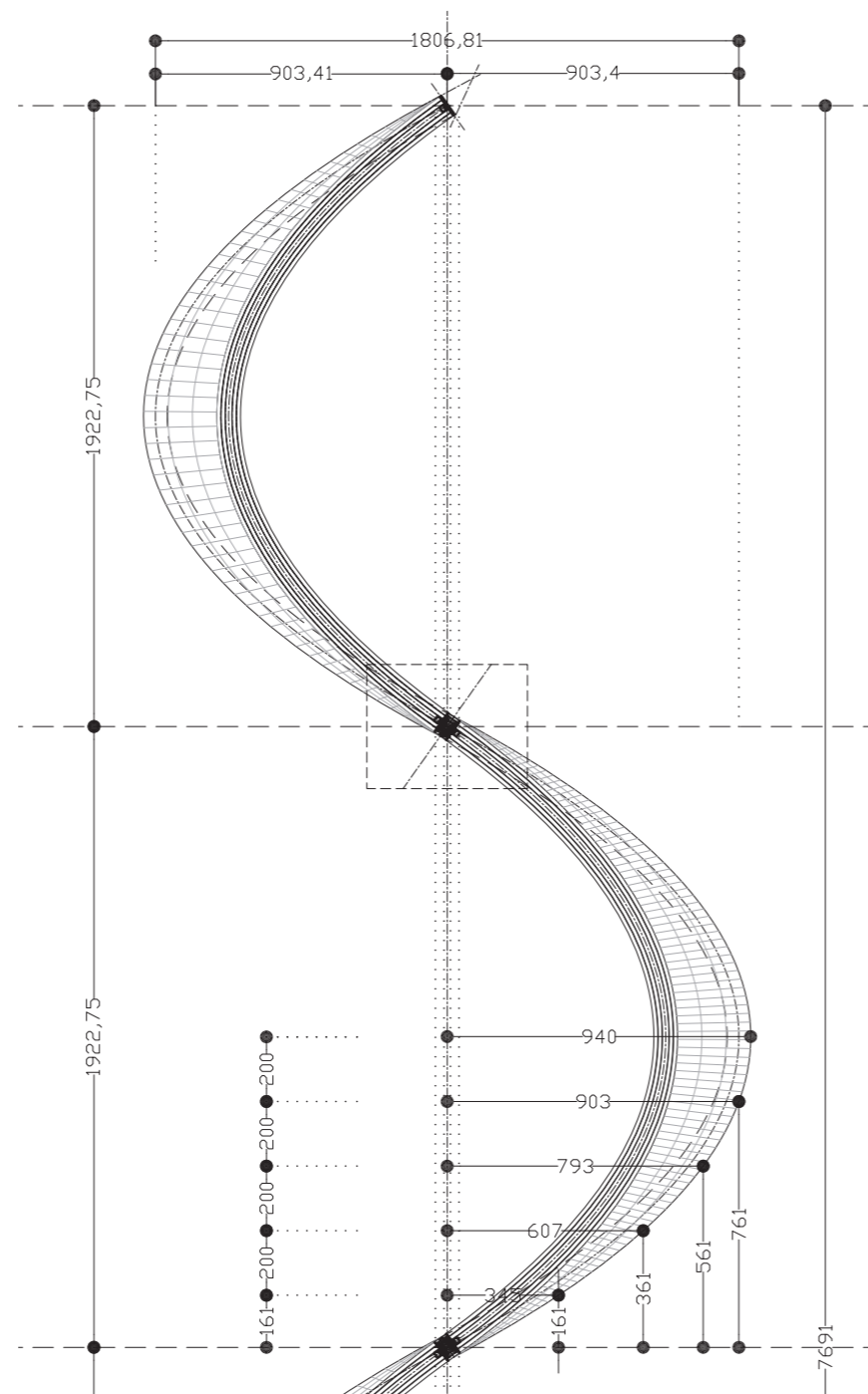


LOAD BEARING SCHEME



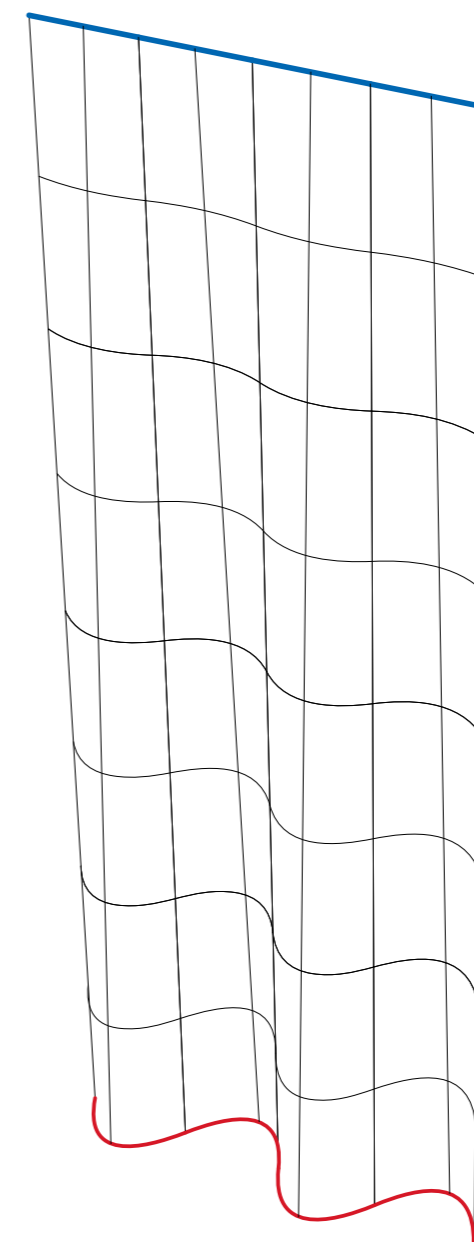
Dead load is carried in stacking

- _Keeps the glass under compression
- _Avoid vertical substructure
- _Increase transparency in vertical joints



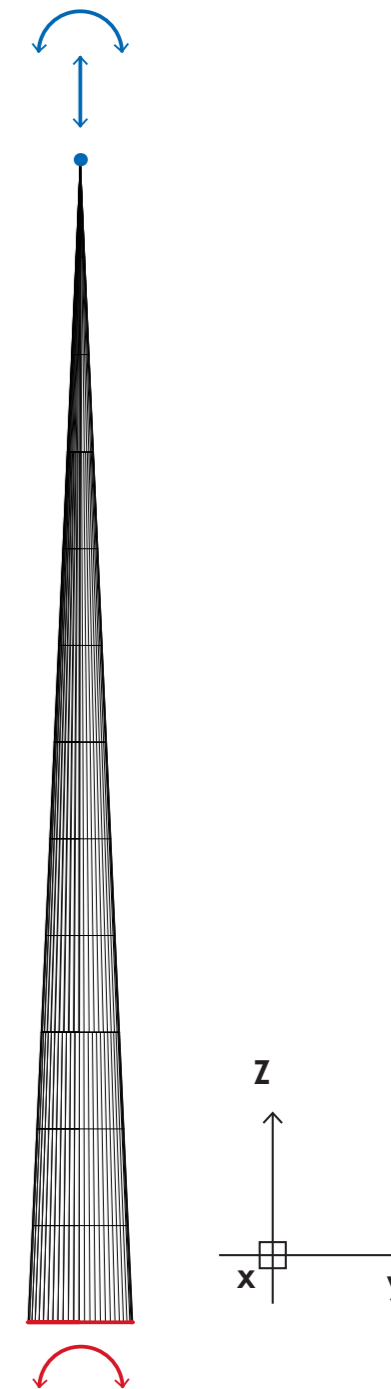
Wind load is counteracted by stiff geometry

- _Waveheight to 1/20 of the span
- _Bottom wave **1800** mm
- _Middle wave **1000**mm
- _Symmetrical
- _Pyramidoid scheme that enhances stability
- _Low gravity center



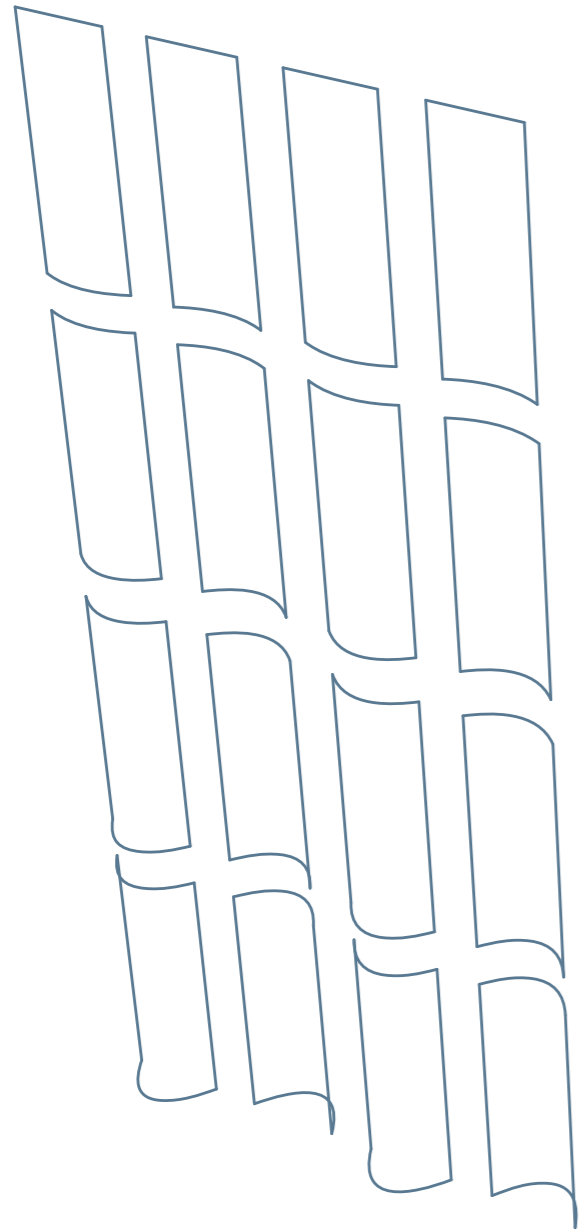
Edge supports

- _Bottom linear (hinge)
- _Top linear (roller) z - axis
- _Sides are free to move



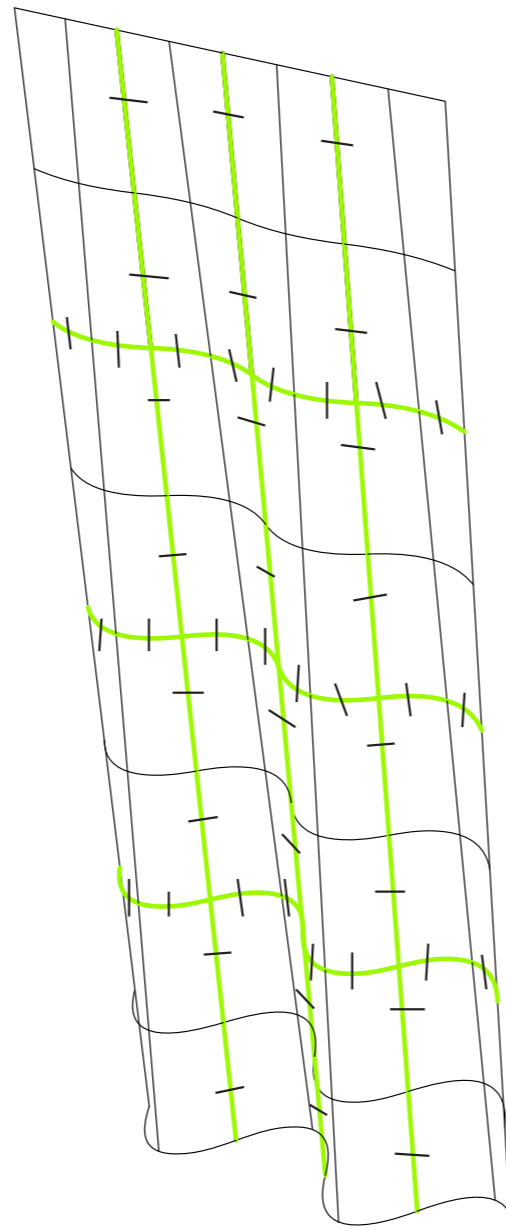
STRUCTURE
LEVEL (MACRO)

LOAD BEARING SCHEME / CONDITIONS



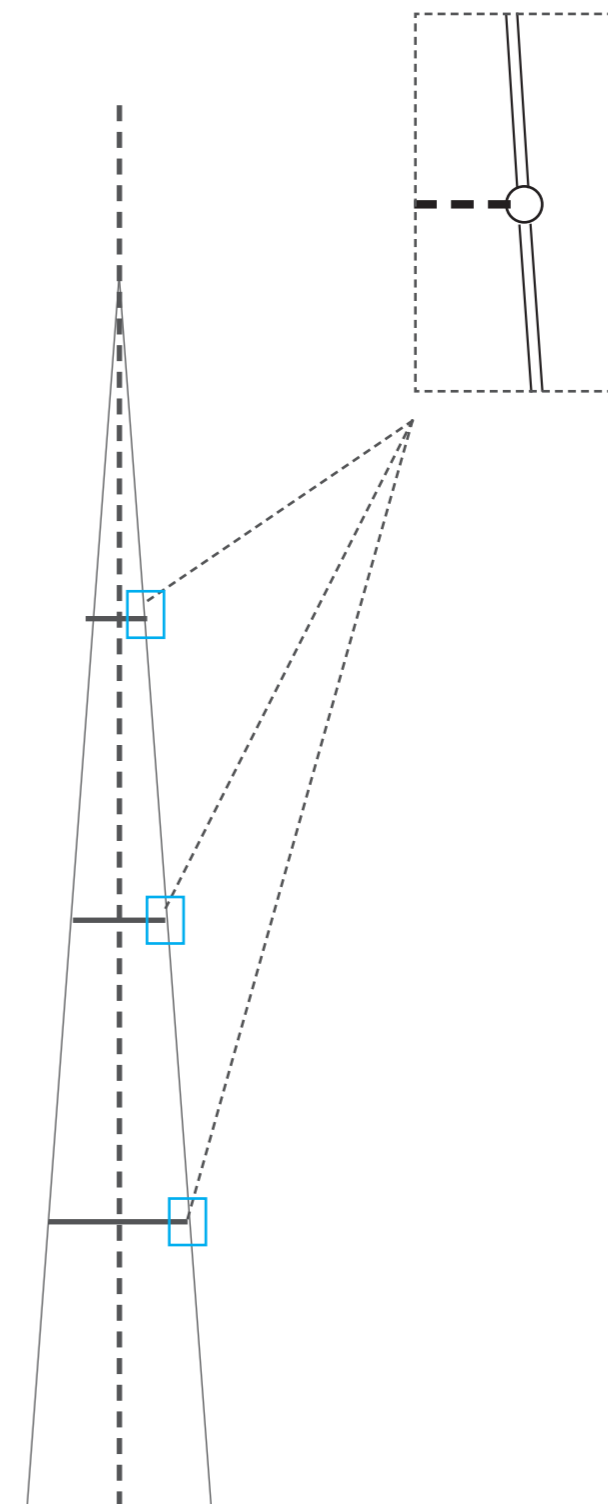
Segmentation of the facade

- _ 4 segments vertically
- _ 4 segments horizontally
- _ Maximum manufacturable sizes



Intermediate connections

- _ Secure continuity of surface
- _ Transfer forces and moments (Firm)
- _ Should not perform as hinge



Intermediate joint should not act as a hinge.

STRUCTURE
LEVEL (MACRO)

CONNECTIONS / REQUIREMENTS

01 Strength

The connections to bear the loads imposed on the facade:

- _Dead load
- _Lateral loads

02 Geometry

Their geometry should ensure continuity of the surfaces. Take into account the complexity of the surface.

03 Robustness

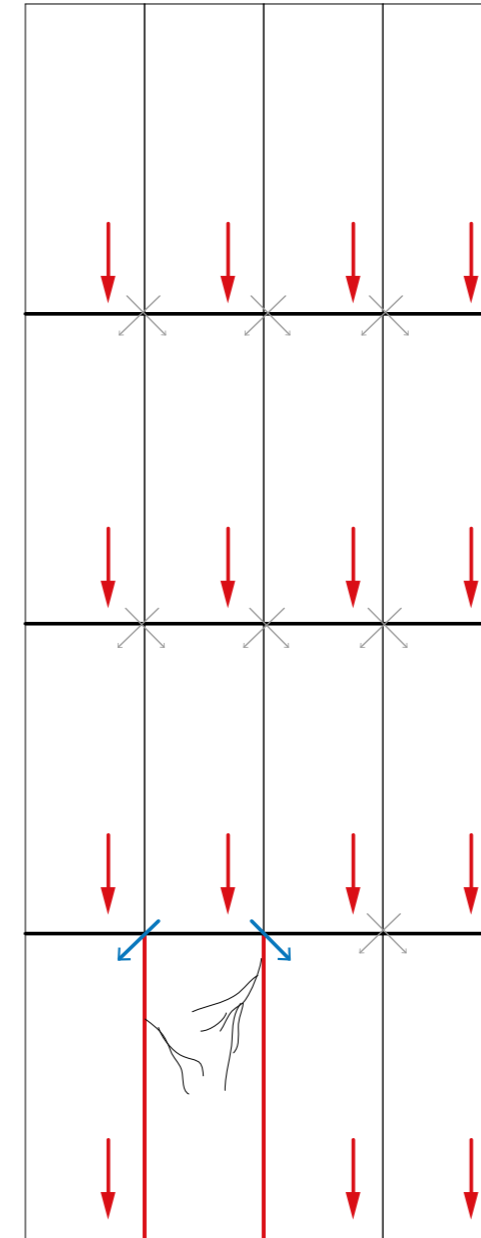
Provide alternative load paths in case of failure of one panel or more.

04 Size

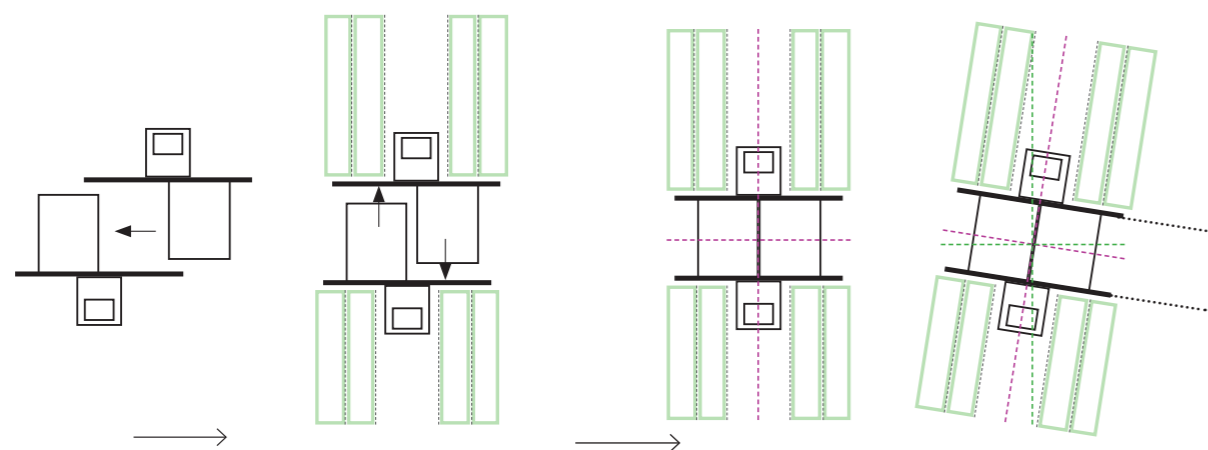
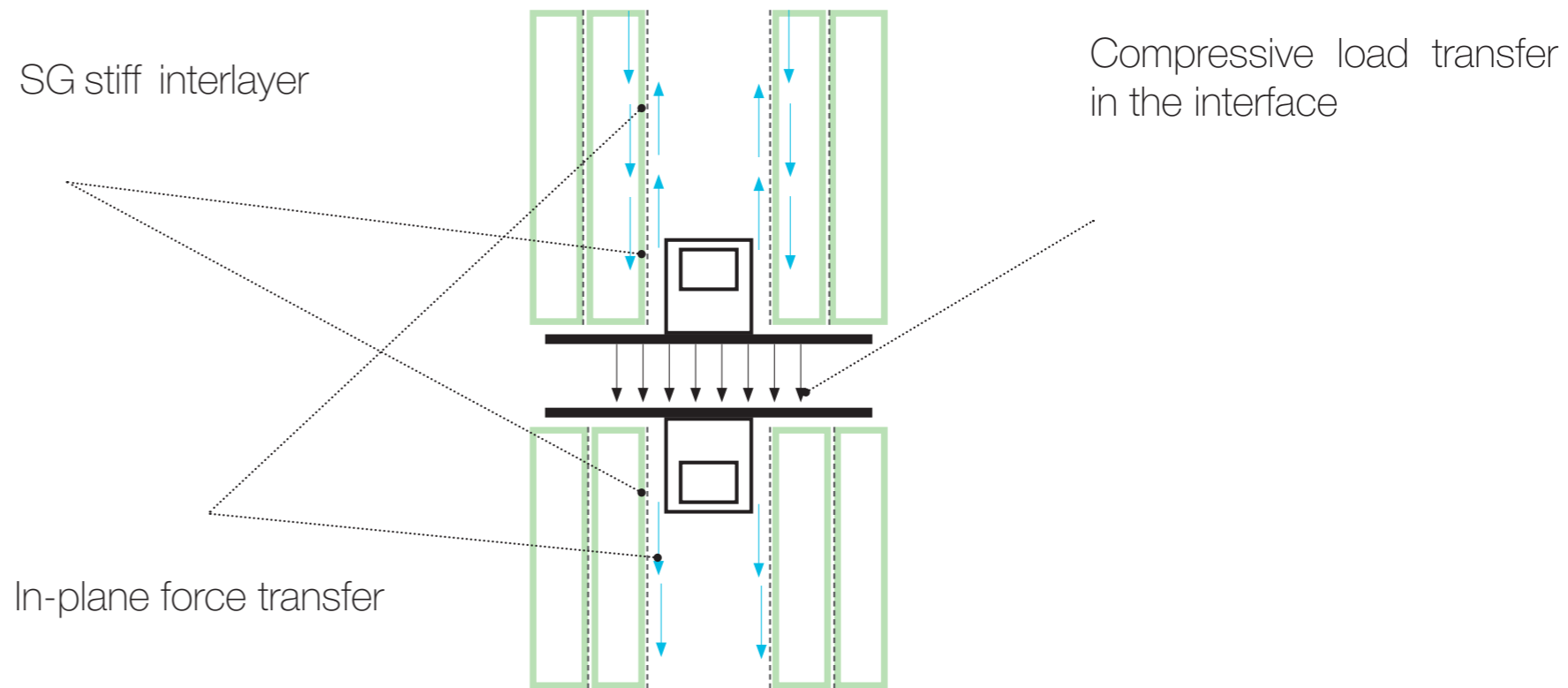
Increase the level of transparency by being as small as possible. Smallest existing size now **150mm**.

05 Installation

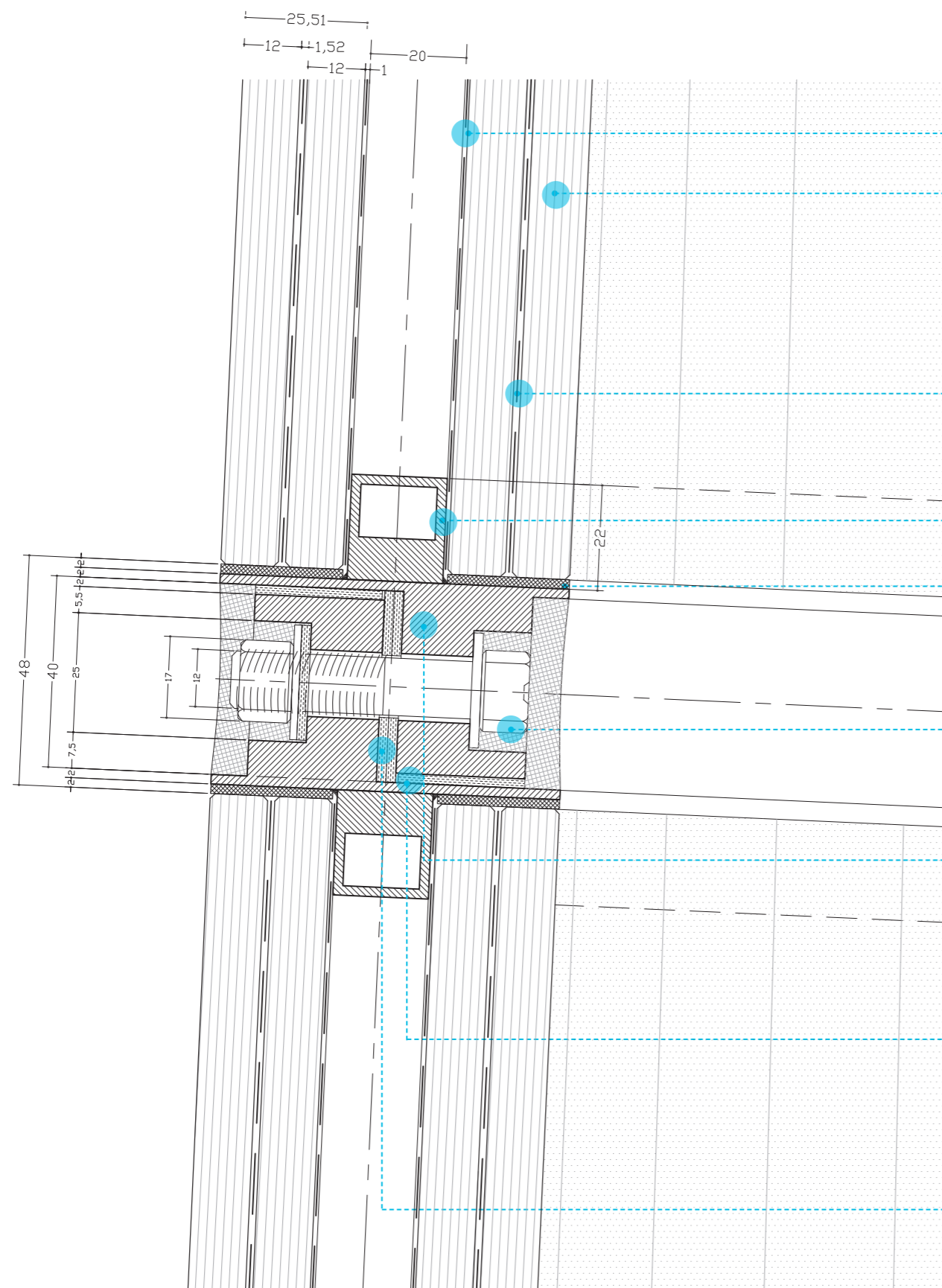
Take into account the assembly process with the appropriate tolerances.



- 01 Avoid contact of glass with hard materials
- 02 Structural spacer and edge used as an interface to transfer the forces between the glass.
- 03 The geometry of the joint should follow the perpendicularity of the curved surface.
- 04 According to the fabrication deviations $\pm 2\text{mm}$ tolerances are introduced as intended to avoid overlapping profiles.



Interlocking geometry following the normals of the surface



Sentry Glas Interlayer

Used in the inner side of the ply to laminate the to stainless steel spacer with the attached connection.

12 mm HS Soda Lime Glass

The annealed glass is being hot bended and afterwards processed to achieve by water jet cutting the perpendicularity of the edge. After that it can be tempered to pre-stress it.

Sentry Glas Plus Interlayer

The SGP is used to laminate the plies for securing post breaking behavior.

20/22 mm hollow stainless steel spacer

Produced by special extrusion, bending and twisted

2mm Silicone bushing

Used to take up the tolerances between the glass and the stainless steel edge. (+- 2mm from the hot bending process)

12mm Bolt

Fastening the two profiles.

Stainless steel extruded profile

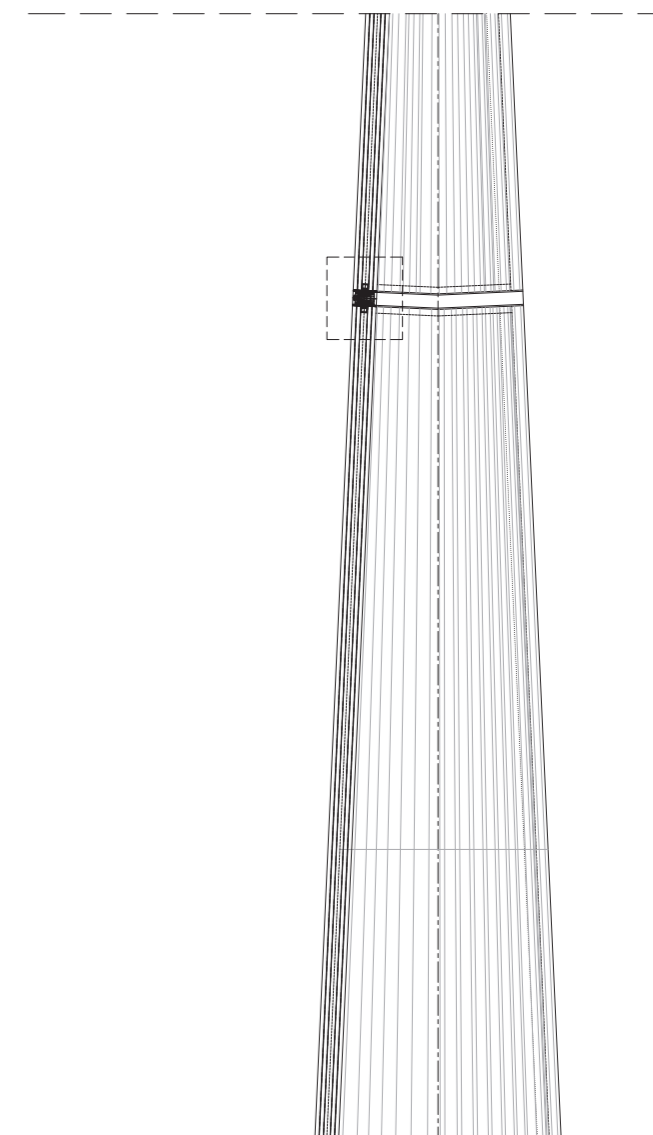
The profile is produced with special extrusion process. After that is bended and twisted to the shape. The tolerances are intended 4mm in the middle (between profiles) to facilitate installation.

2mm Neoprene sheet (hardness 90-100)

Taking up the tolerances from the profiles manufacturing deviation. This interface has not been completed in design.

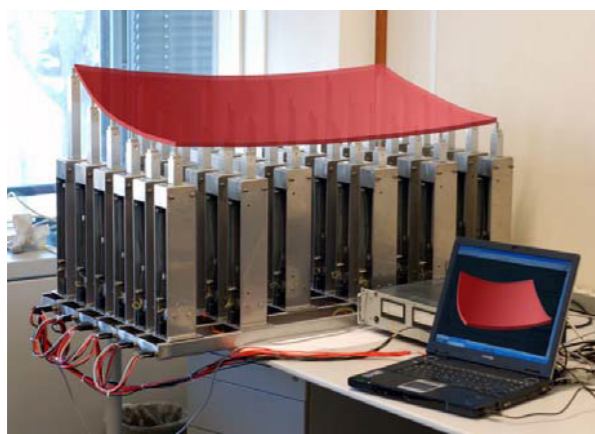
4mm rubber ring

Taking up the tolerances from the profiles manufacturing deviation. Helps to provide the buffer for the tightening of the bolt.



CONNECTIONS / FABRICATION STEPS

Glass



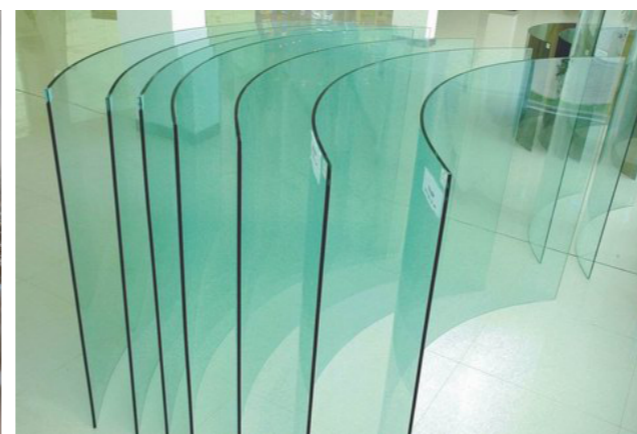
Annealing and bending

Adjustable mould - 'Flex-rod' system. Actuators adjusted according to computer model output.



Water jet cutting

Water jet cutting the edges of glass so as to achieve the perpendicularity across the edges.



Strengthening

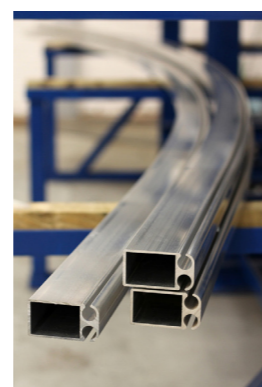
Heat strengthening glass after the bending process. Chemical strengthening could be a second option because of the geometry

Connector



Stainless Steel extrusion & forming

Using special machines for the aircraft industry stainless steel extrusions that fit the diameter of 140 mm are possible. Used for producing the spacers. After that the shapes can be bent and twisted.



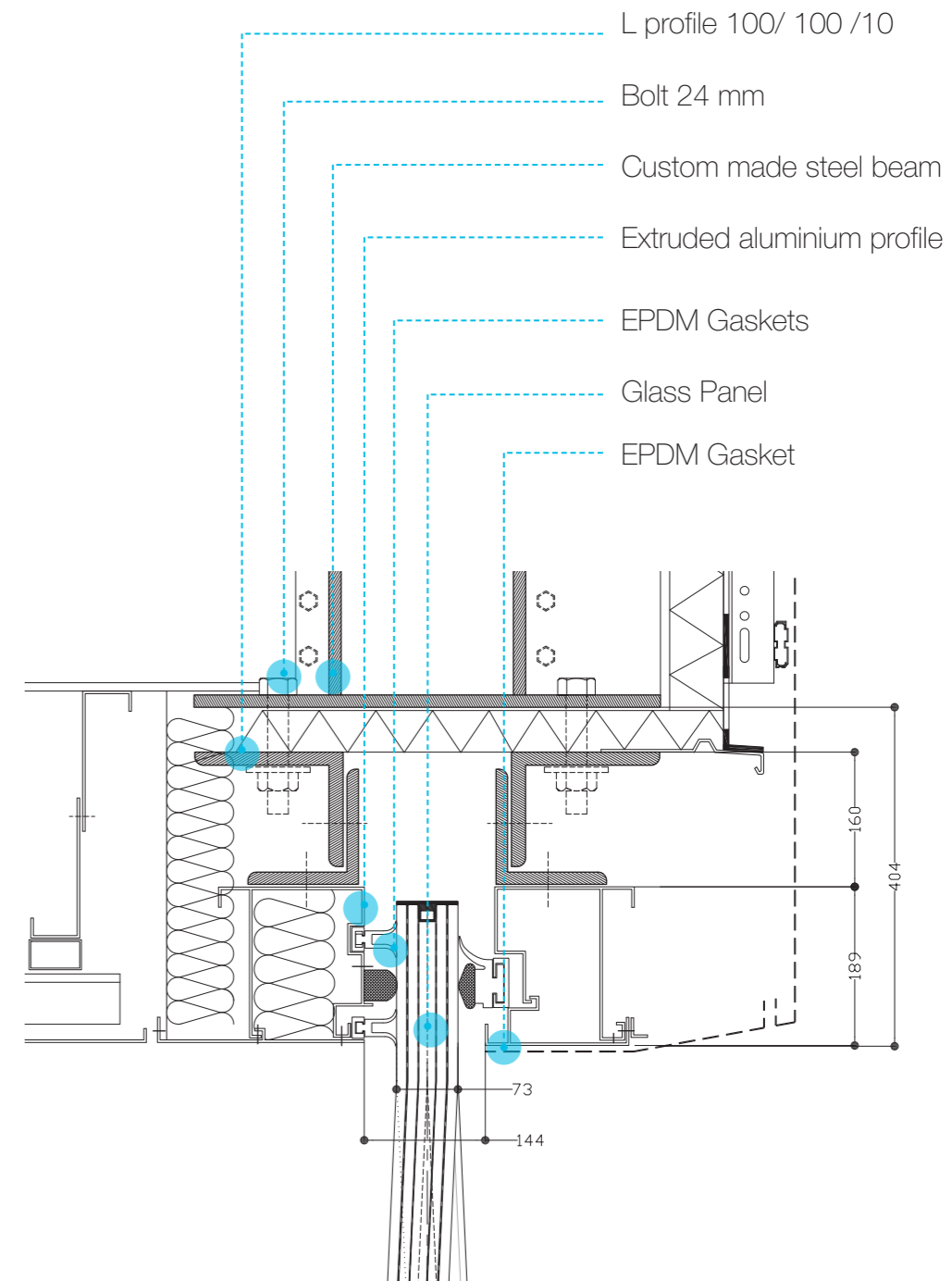
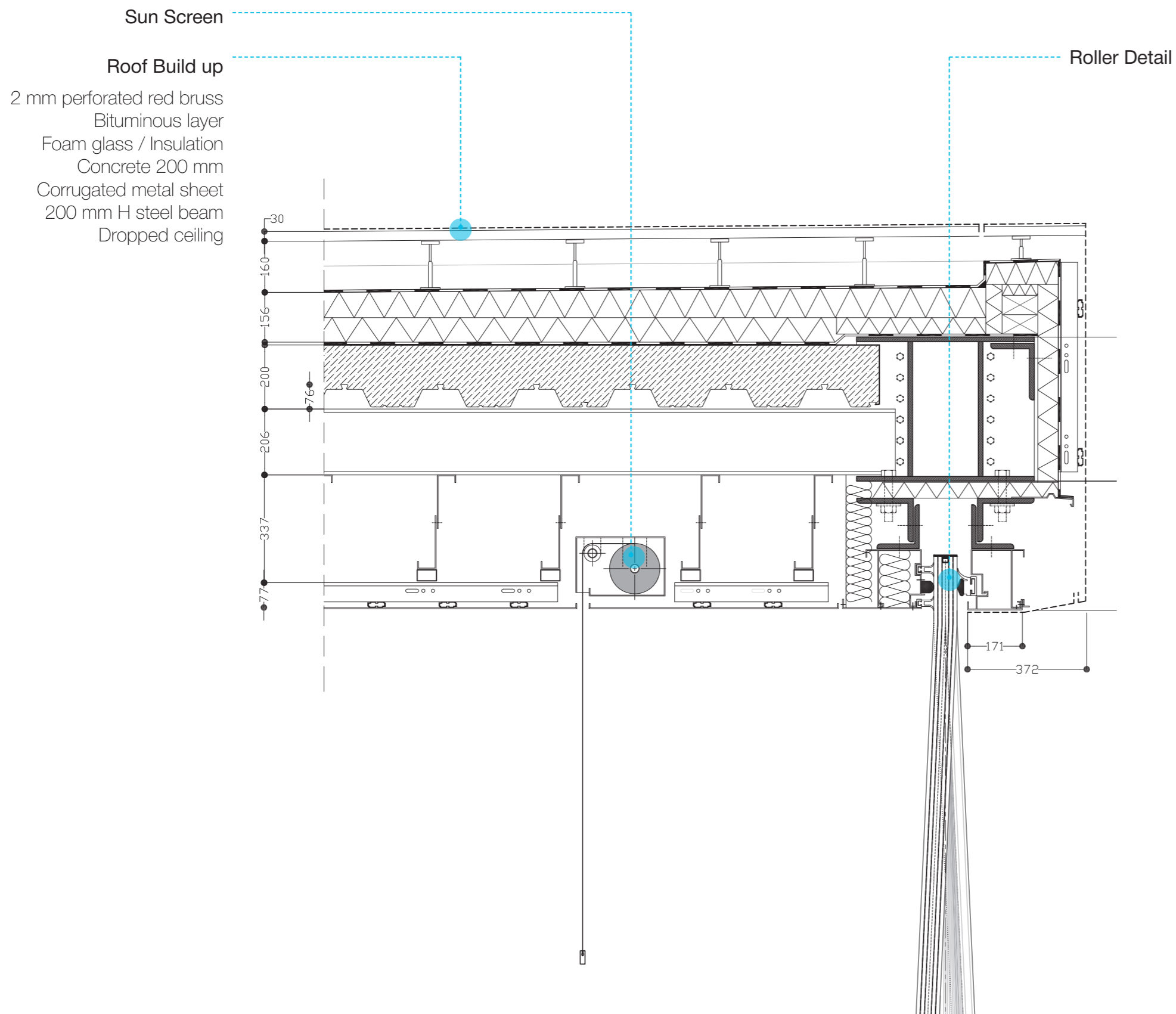
Aluminium extrusion & forming

Aluminium extruded parts are used for producing the connector and edge piece later on they are bended and twisted together to form the final profile shape.

Lamination of the components into one element / panel

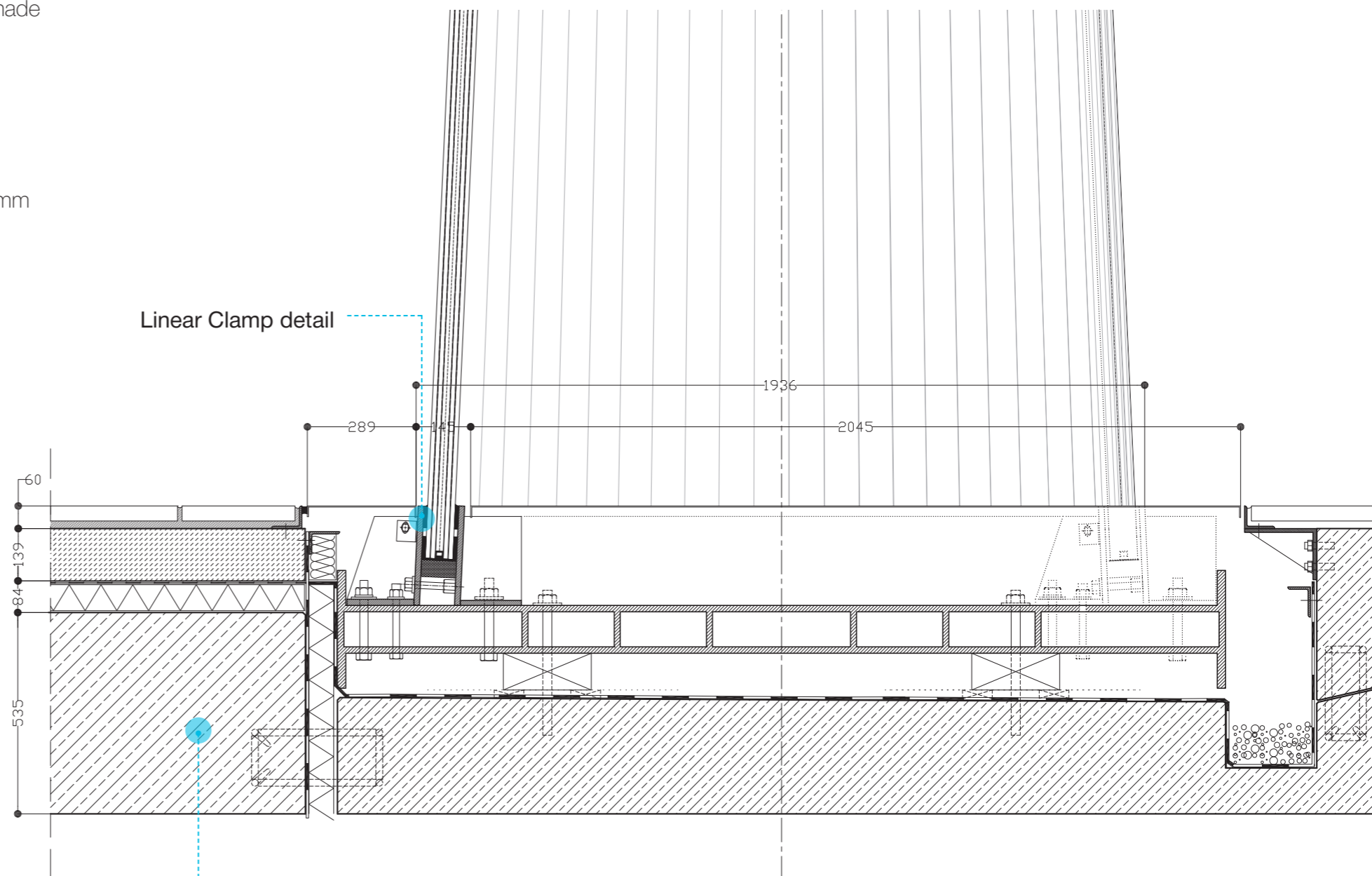
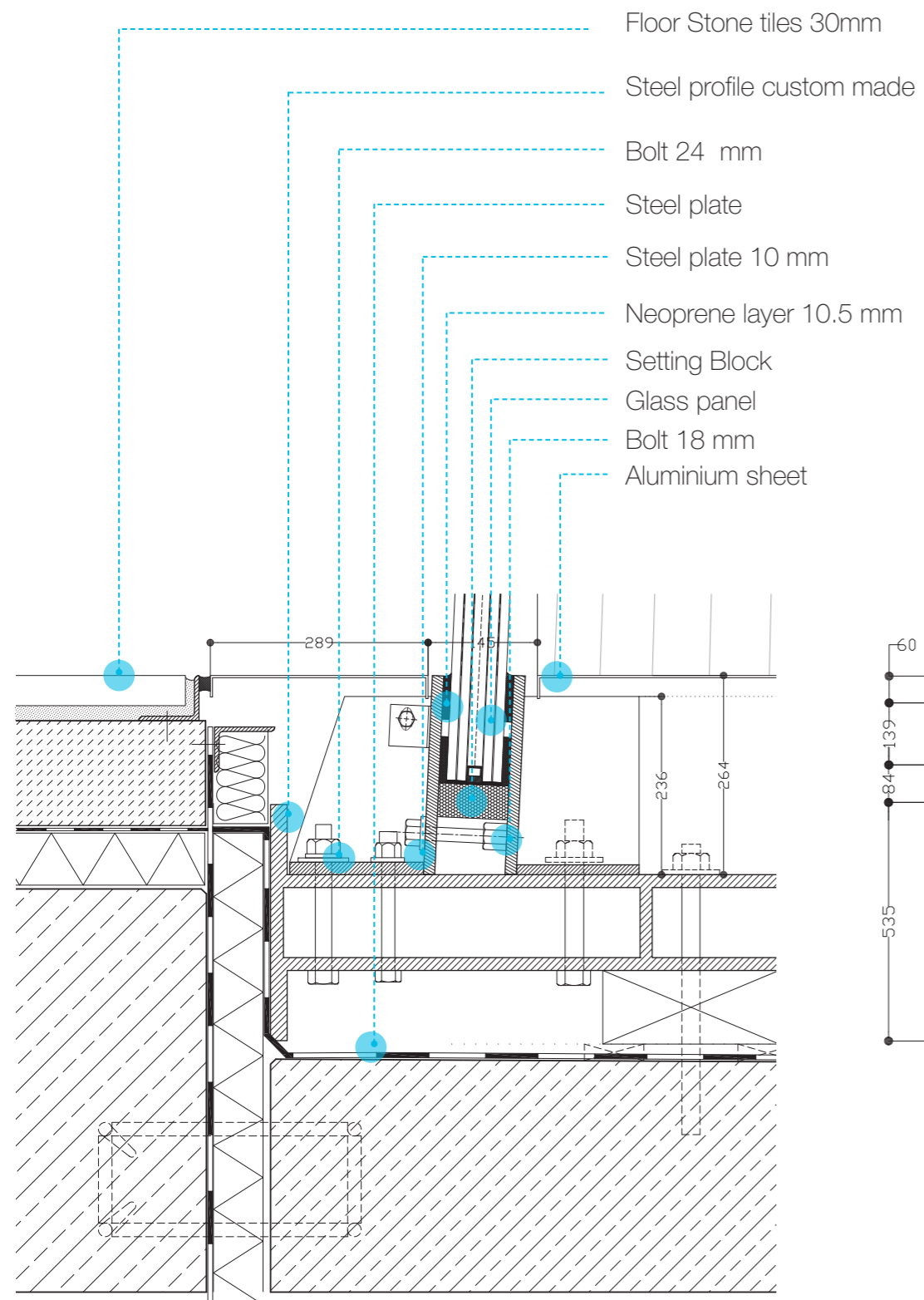


CONNECTIONS / DETAILING



STRUCTURE
LEVEL (MACRO)

CONNECTIONS / DETAILING



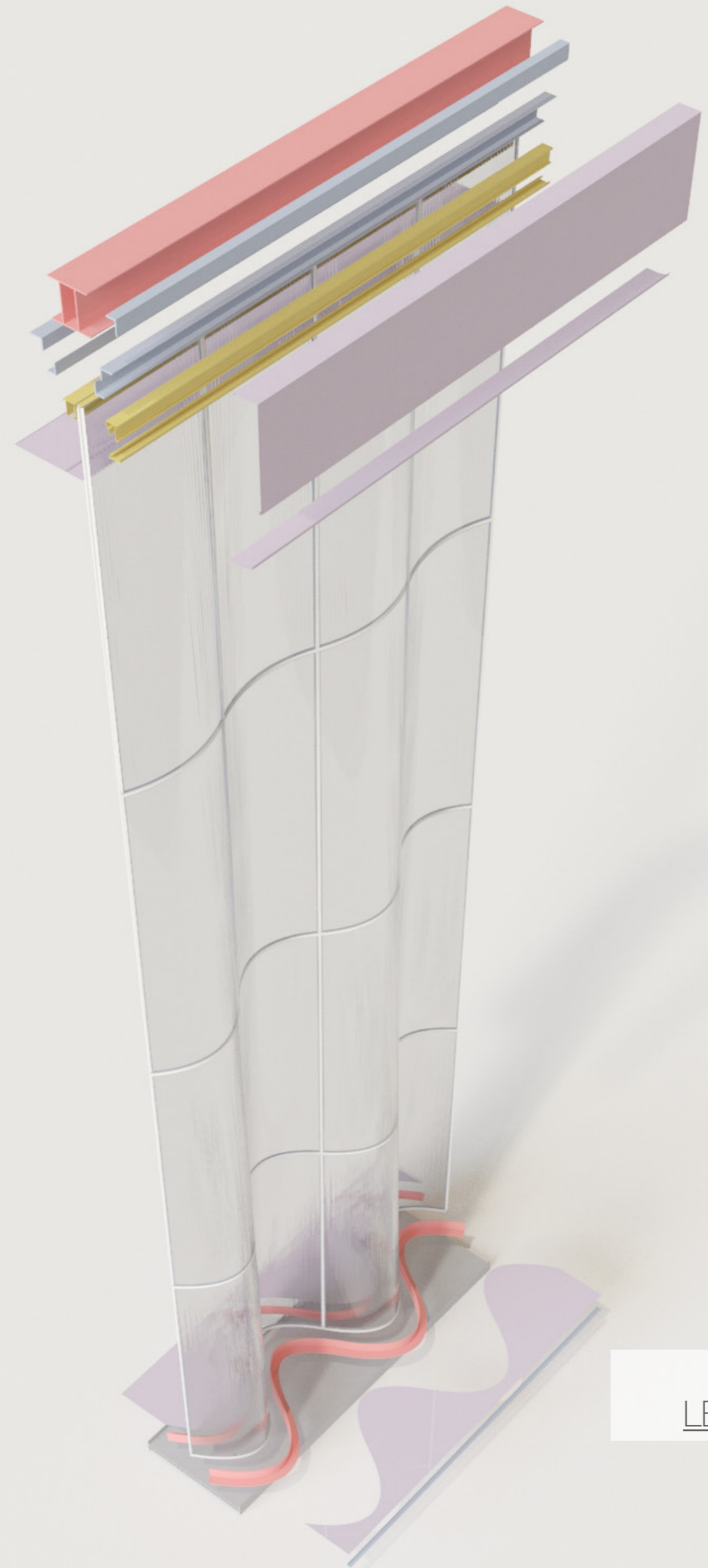
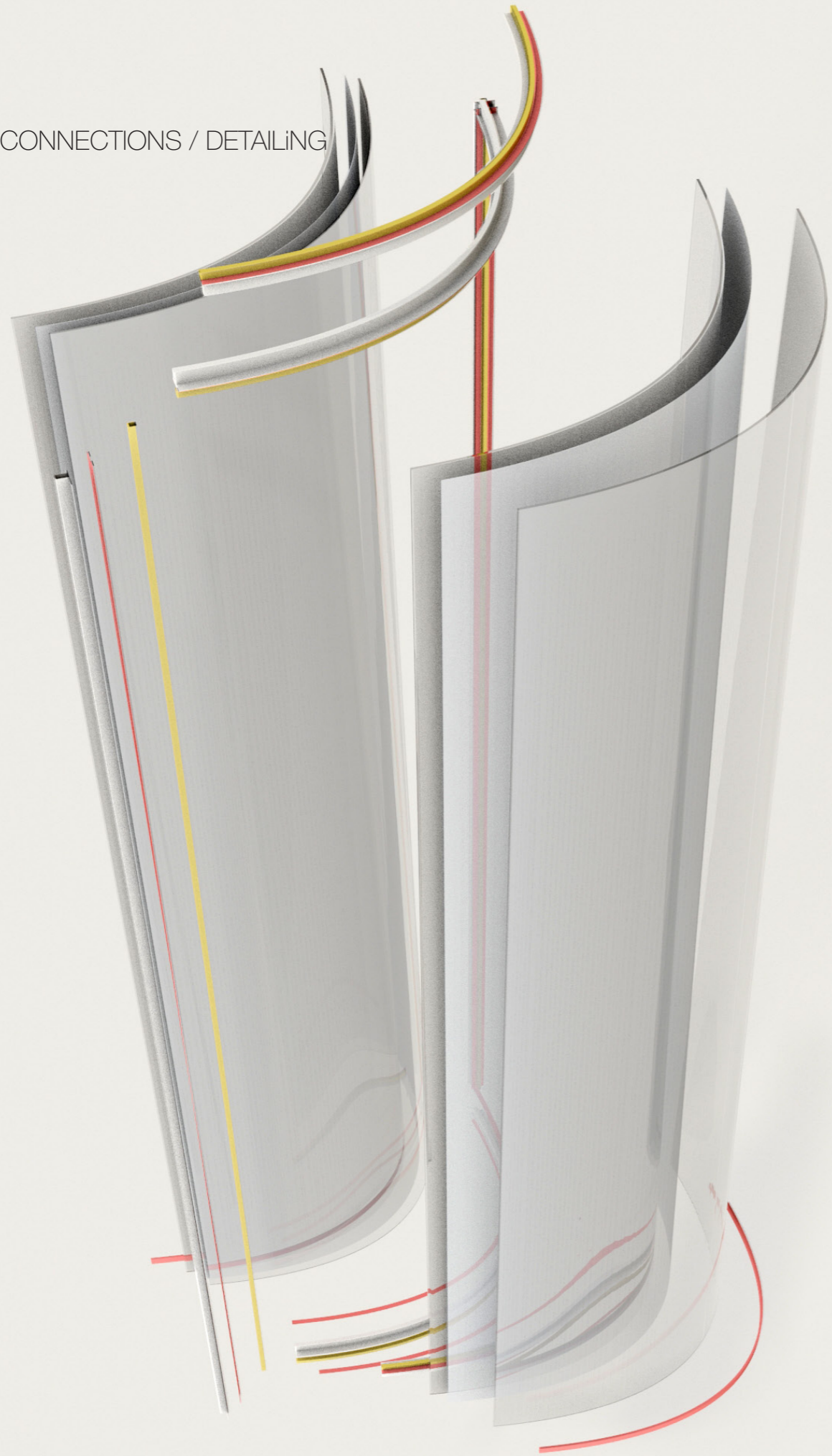
Linear Clamp detail

Floor Build up

- Stone tiles 30mm
- Mortar 20mm
- Cement screed 140mm
- Polyethylene membrane
- Insulation
- Concrete 530mm

STRUCTURE
LEVEL (MACRO)

CONNECTIONS / DETAILING

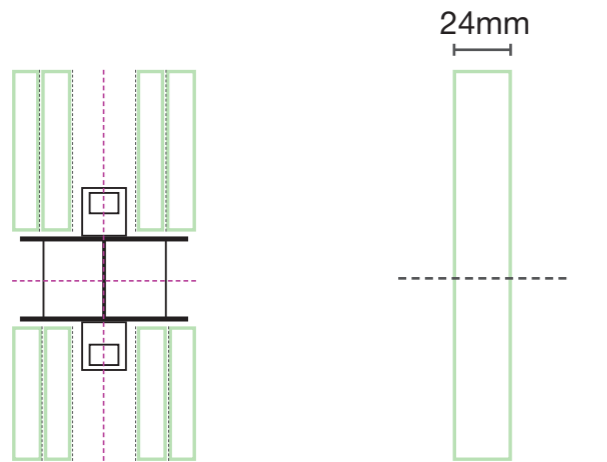


STRUCTURE
LEVEL (MACRO)

MODEL DESCRIPTION

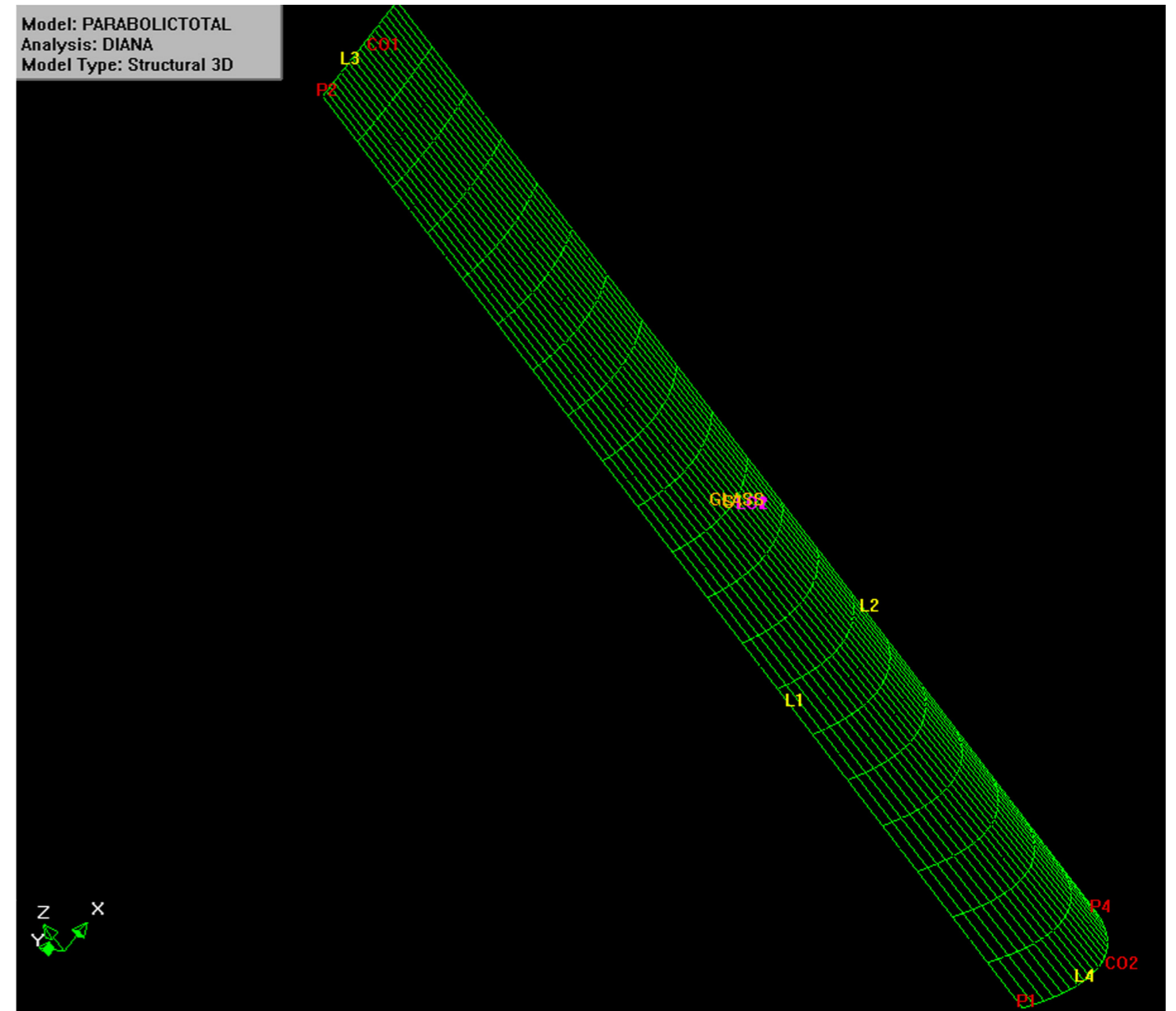
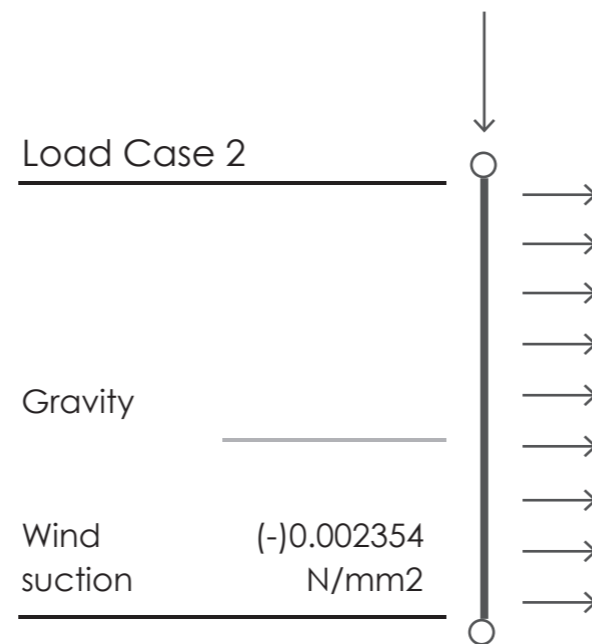
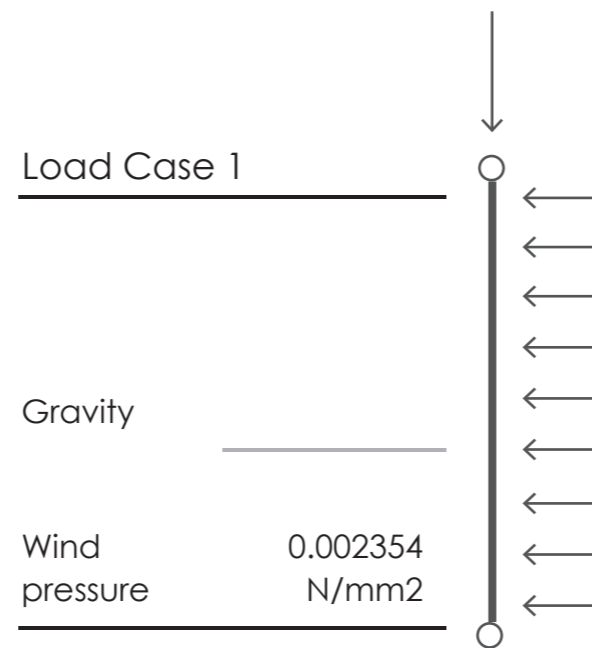
Simplified model

- _24 mm monolithic glass
- _One surface top to bottom
- _No separations between the panels
- _Model of **one segment**
- _One material (Soda Lime Glass)
- _No joints modelled
- _Restraint at the **top** and **bottom**
- _2 Loading scenarios
- _Mesh type curved shell **QU8 CQ40S**



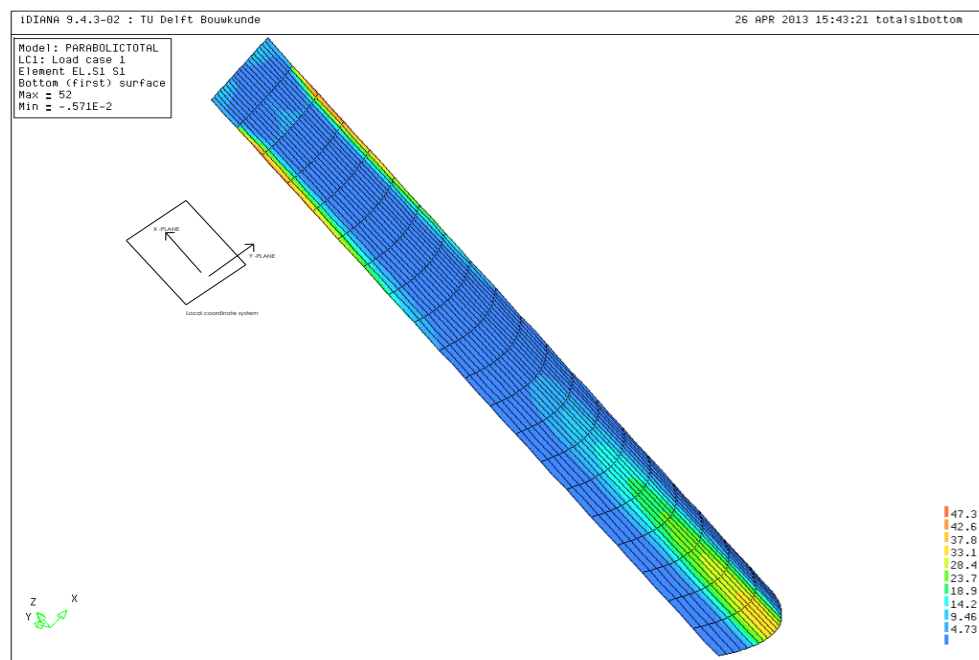
Physical

Simplified



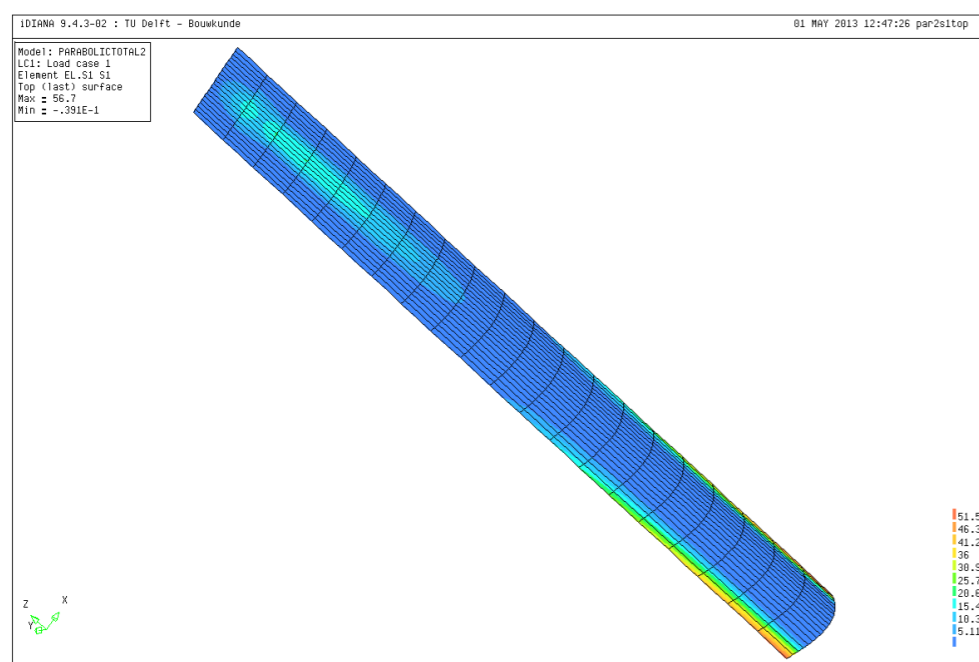
PERFORMANCE
SIMULATIONS

ULTIMATE LIMIT STATE



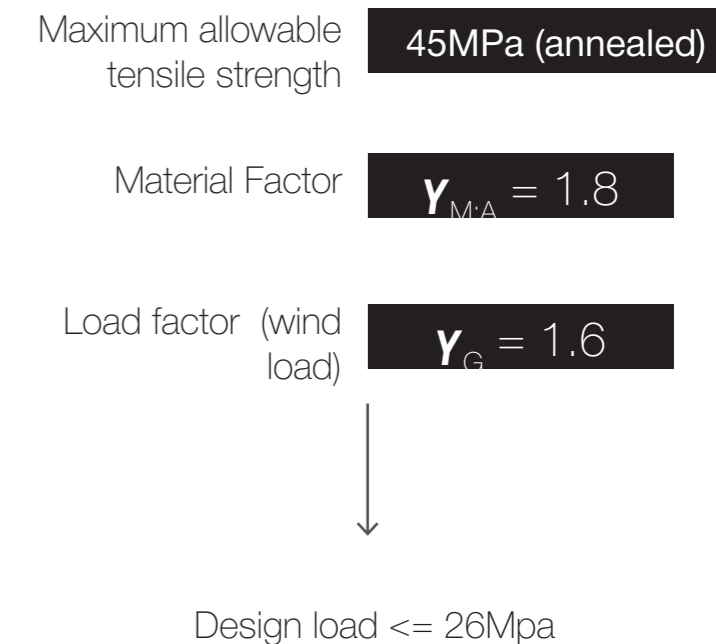
Load Case 1	Max	Min
EL. S1. S1/ Principle stress 1 (algebraic largest) (N/mm2)		
Bottom surface	52	-5.71E-03
Top surface	113	-5.88E-03

Load case 1
 Maximum tensile stress (bottom) = 52MPa
 For 2 laminated panes equals the maximum



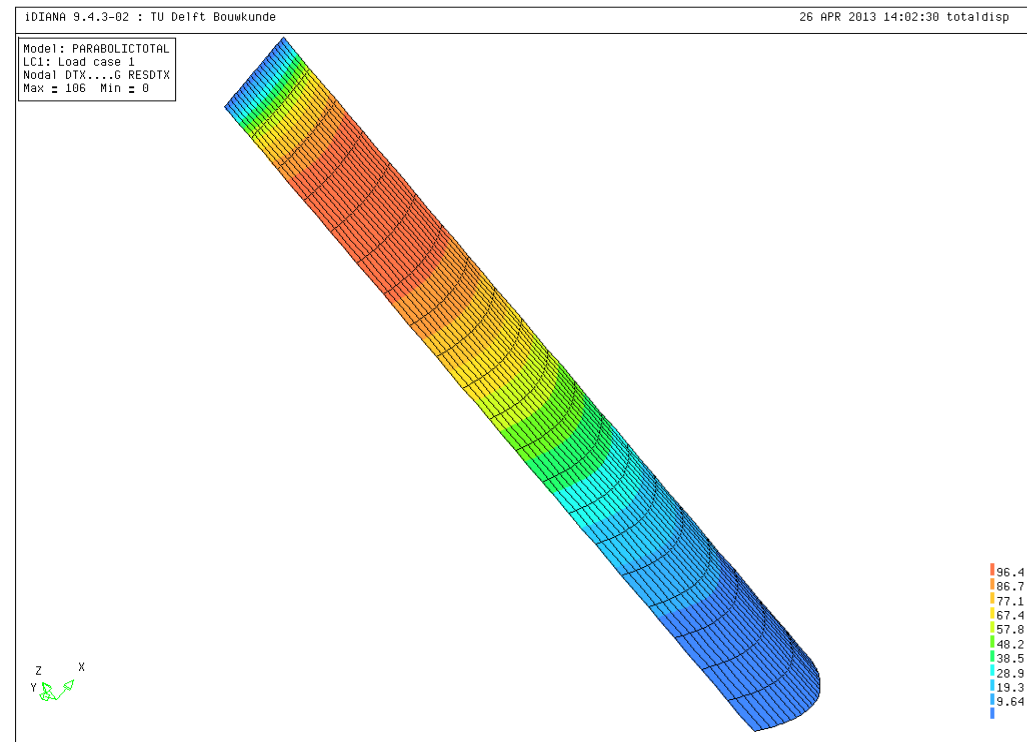
Load Case 2	Max	Min
EL. S1. S1/ Principle stress 1 (algebraic largest) (N/mm2)		
Bottom surface	60.2	-3.62E-02
Top surface	56.7	-3.91E-02

Load case 2
 Maximum tensile stress (top) = 56.7MPa
 For 2 laminated panes is just above the maximum



PERFORMANCE
 SIMULATIONS

SERVICEABILITY LIMIT STATE



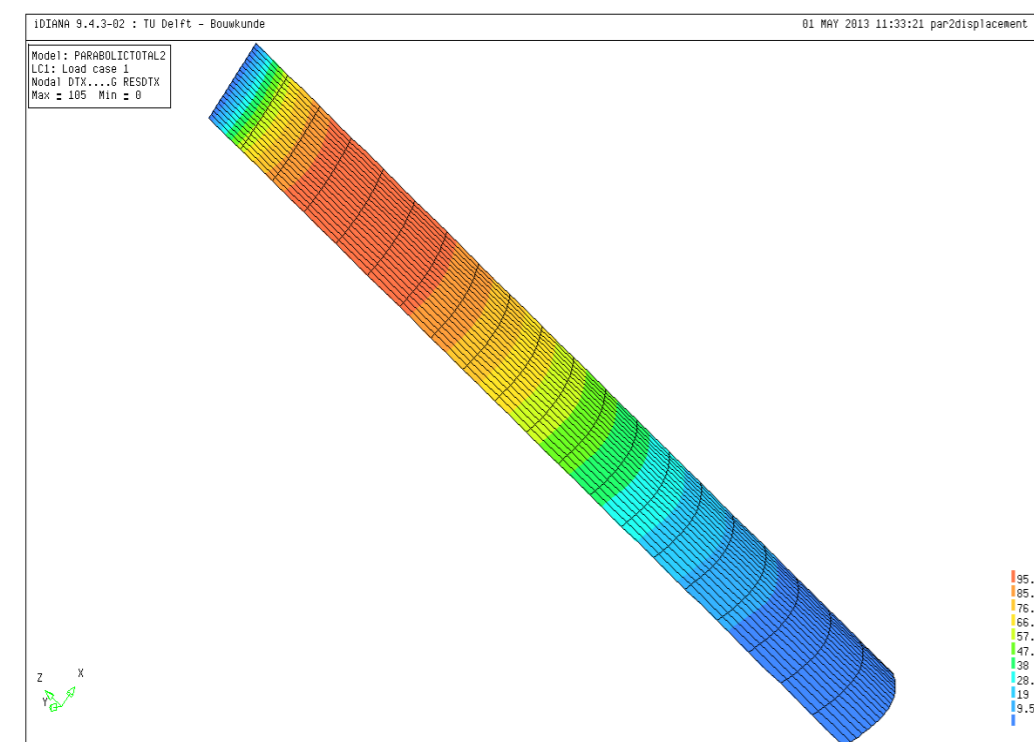
Load Case 1	Max	Min
FBX...G RESFBX / support reaction	1.37E+05	
DTX...G RESDTX / total displacement		106

Maximum allowable deflection **1/65 of span**
OR
50 mm

Span **20000 mm**

Allowable deflection **307 mm**

Load case 1
Maximum displacement 106 mm < 307 mm



Load Case 2	Max	Min
FBX...G RESFBX / support reaction	1.33E+05	
DTX...G RESDTX / total displacement		105

Load case 2
Maximum displacement 105 mm < 307 mm

Ultimate Limit State

- 1 | Increase accuracy in the modelling of the surface
- 2 | Conduct additional laboratory test on specimens
- 3 | Increase the thickness of the glass
- 4 | Use Fully Tempered glass

Serviceability Limit State

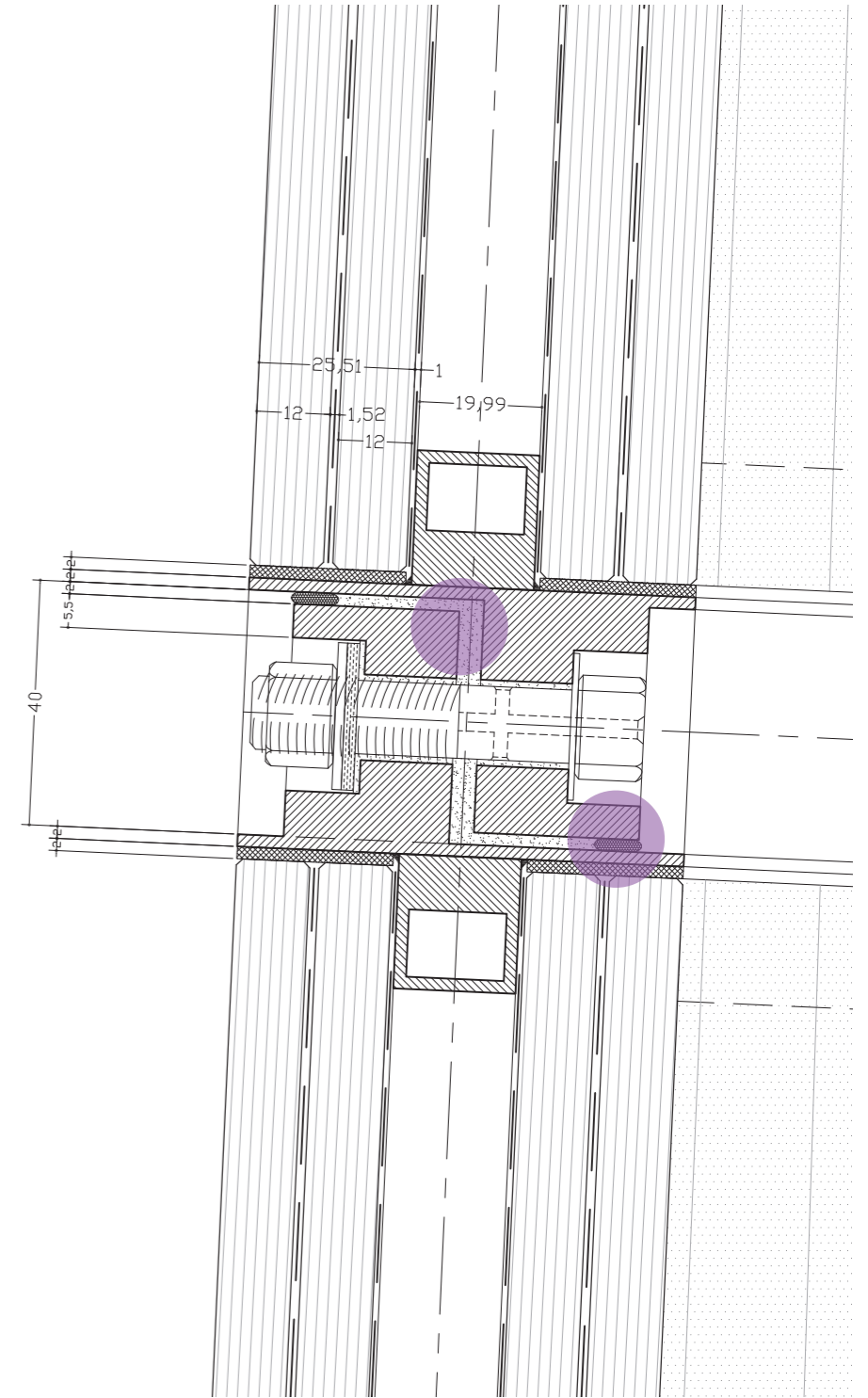
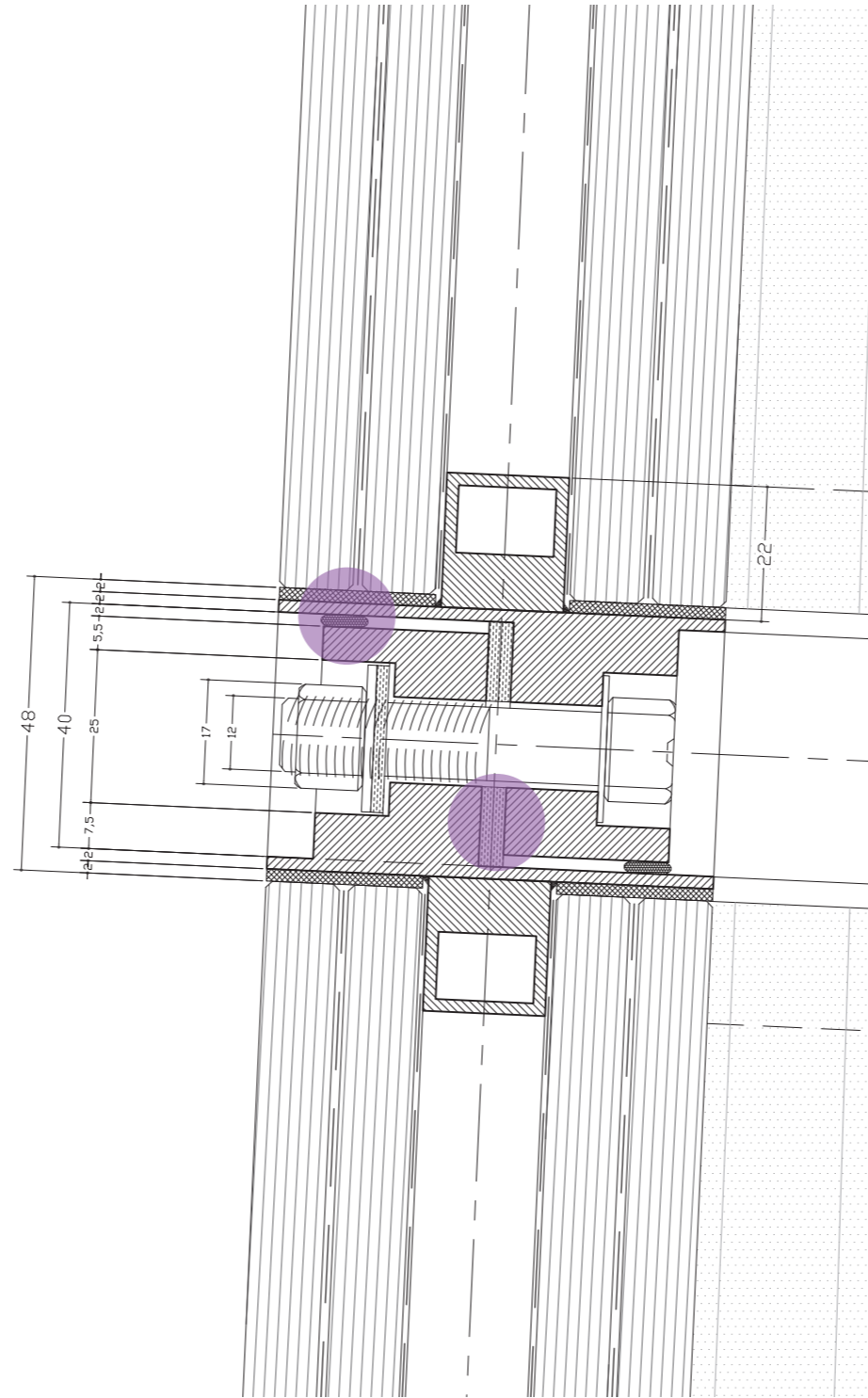
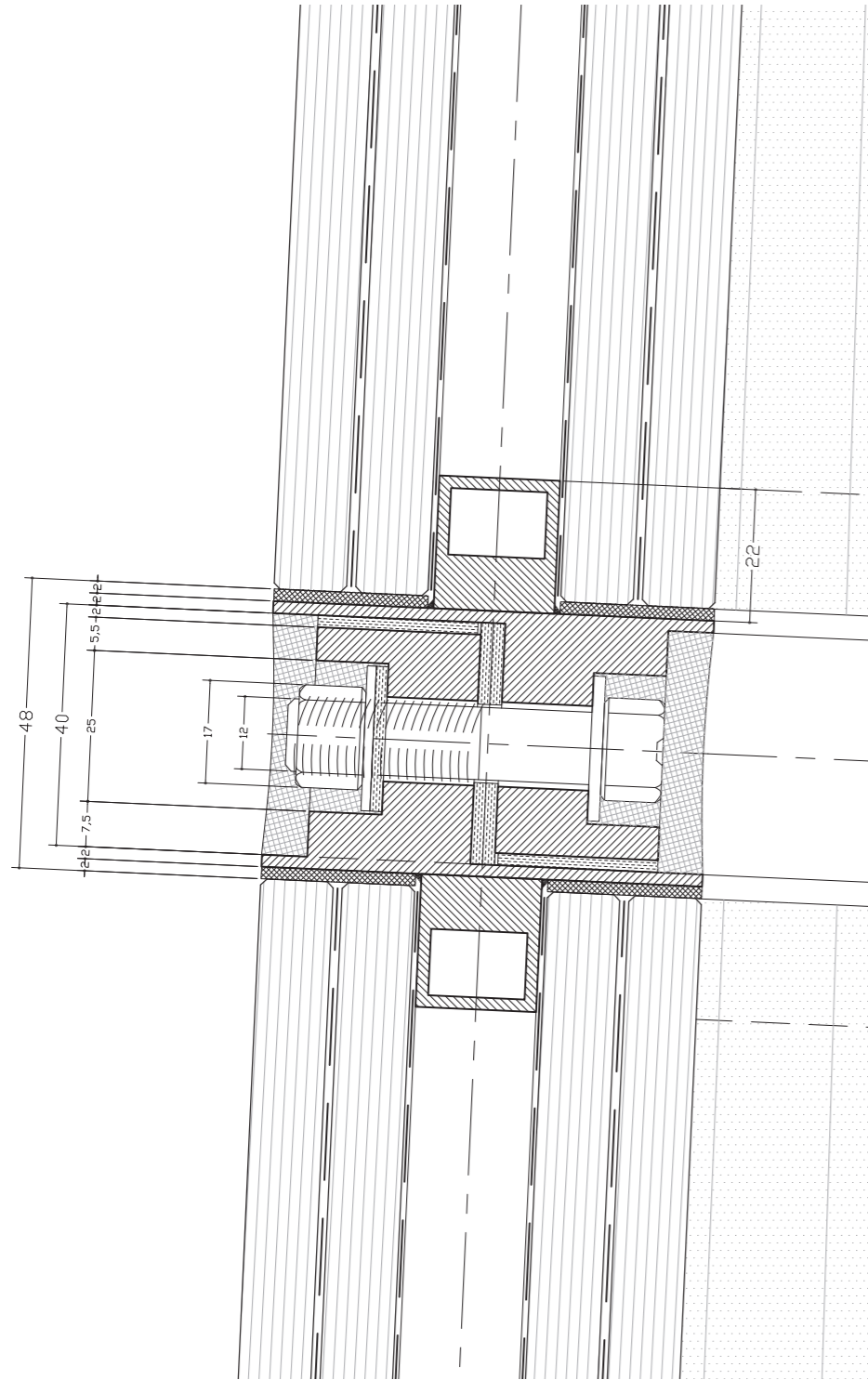
- 1 | We cannot take into account the lower limit of 50mm deflection since it is not given for the certain geometry
- 2 | Increase the accuracy of the calculations / The spacer stiffness could have spring action.
- 3 | The connection of the facade to the wall should allow for deflections of 100mm

- 1 | The maximum transparency can be achieved for a glass facade of large scale by utilizing a self-supporting geometry like the one proposed
- 2 | We can improve the structural performance through the stiffness of the curved geometry and provide a safe structure
- 3 | We can maximize transparency in the curved geometry by using the special type of joint that is embedded in the laminate and can transfer forces via the spacer and an interlocking geometry
- 4 | The size of connection achieved can be **33 mm**

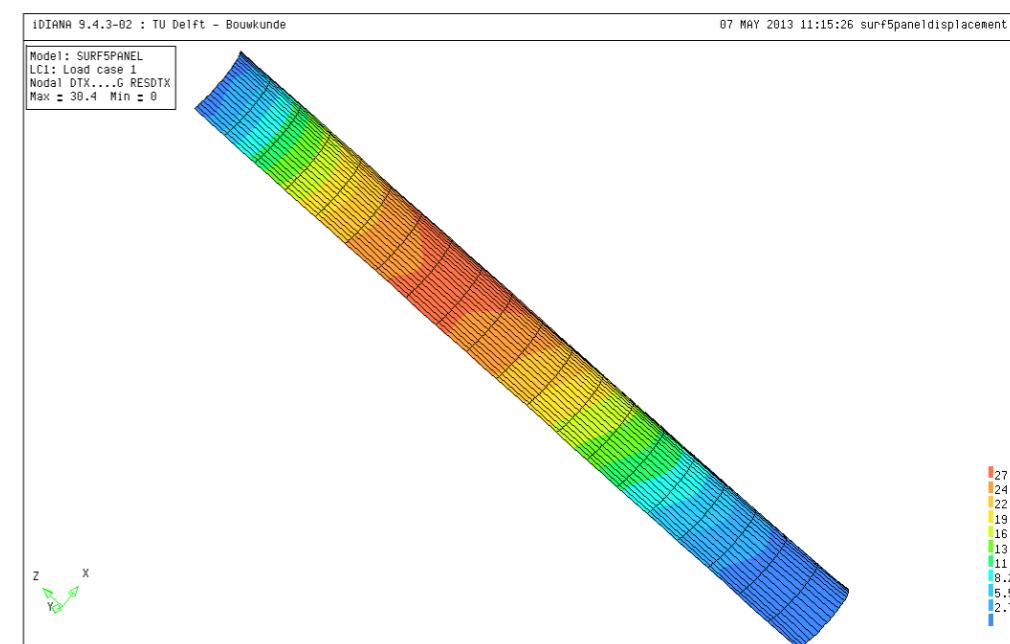
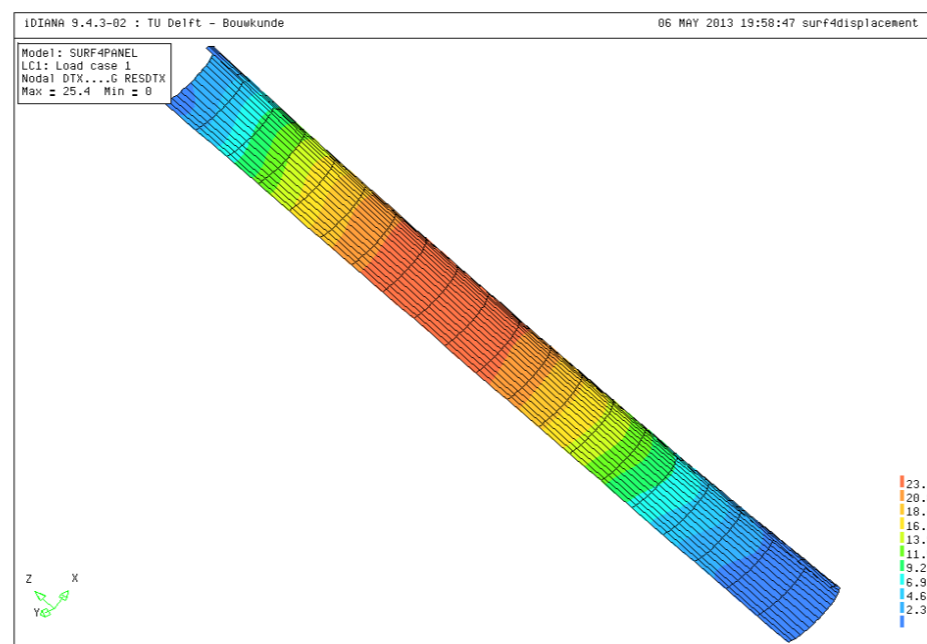
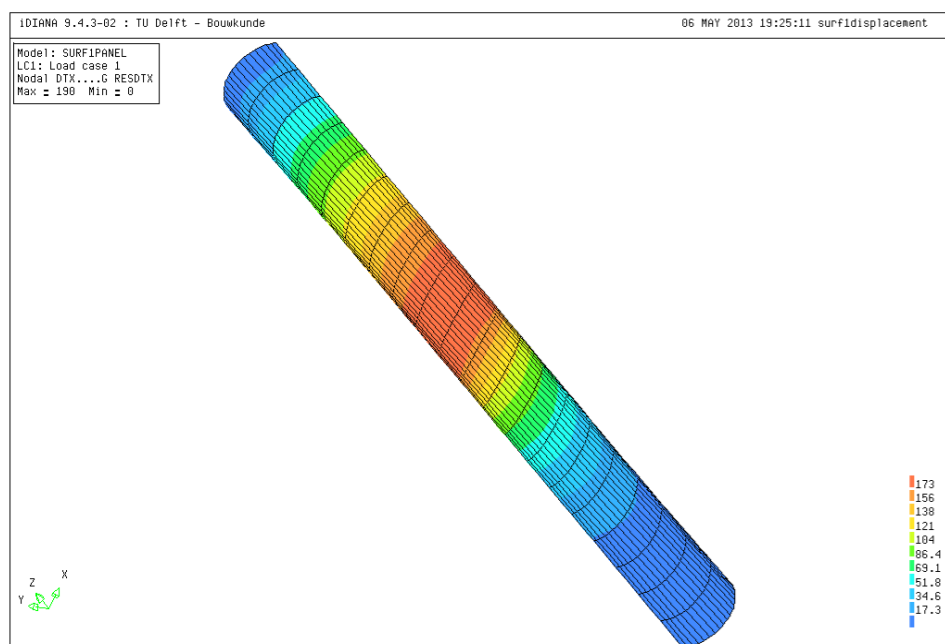


/// Thank you ///

APPENDIX / ALTERNATIVES OF CRITICAL DETAIL



APPENDIX / ALTERNATIVES SURFACES SIMULATION



Panel 1 / Twisted along middle

Nr. of Surfaces	1
Nr. of Lines	4
Nr. of Points	4
Mesh type surface	qu8 cq40s
Mesh type midlines	
Material surface	Glass
Material midlines	
Load Case 1	
Gravity	
Wind pressure	0.002354 N/mm2

Load Case 1	Max	Min
FBX...G RESFBX / support reaction	1.14E+05	1.20E+02
DTX...G RESDTX / total displacement (mm)	190	0
EL. S1. S1/ Principle stress 1 (algebraic largest) (N/mm2)		
Bottom surface	49.7	-2.47E-01
Top surface	38.5	-3.15E-02
EL. S1. S2/ Principle stress 2 (N/mm2)		
Bottom surface	13.2	-5.11E+00
Top surface	10.6	-1.06E+01
EL. S1. S3/ Principle stress 3 (algebraic smallest) (N/mm2)		
Bottom surface	3.01E-02	-8.99E+01
Top surface	2.82E-02	-1.14E+02

Panel 2 / Corrugated (reduced in the middle)

Nr. of Surfaces	1
Nr. of Lines	4
Nr. of Points	4
Mesh type surface	qu8 cq40s
Mesh type midlines	
Material surface	Glass
Material midlines	
Load Case 1	
Gravity	
Wind pressure	0.002354 N/mm2

Load Case 1	Max	Min
FBX...G RESFBX / support reaction	7.25E+04	4.48E+02
DTX...G RESDTX / total displacement (mm)	25.4	0
EL. S1. S1/ Principle stress 1 (algebraic largest) (N/mm2)		
Bottom surface	26.8	-1.97E-02
Top surface	27.8	-2.09E-02

Panel 1 / Corrugated (reduced towards the top)

Nr. of Surfaces	1
Nr. of Lines	4
Nr. of Points	4
Mesh type surface	qu8 cq40s
Mesh type midlines	
Material surface	Glass
Material midlines	
Load Case 1	
Gravity	
Wind pressure	0.002354 N/mm2

Load Case 1	Max	Min
FBX...G RESFBX / support reaction	7.86E+04	8.68E+01
DTX...G RESDTX / total displacement (mm)	30.4	0
EL. S1. S1/ Principle stress 1 (algebraic largest) (N/mm2)		
Bottom surface	29.4	-2.15E-02
Top surface	28.3	-2.00E-02