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RESEARCH ARTICLE OPEN ACCESS

Hybrid Geothermal and PV Installations for Cooling and Heating Systems: Synergy for Sustainability in Tertiary and Industry Sectors

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ABSTRACT

Recent studies confirm the potential efficiency of geothermal resources for maintaining comfortable building temperatures through cooling and heating solutions. In addition, a variety of initiatives have been promoted to effectively reduce both environmental concerns and energy crisis by the integration of renewables. Under this framework, this paper describes and assesses hybrid geothermal and photovoltaic (PV) installations to provide sustainable solutions. Hybrid geothermal–PV systems are evaluated as a strategic opportunity to increase the presence of geothermal energy within the hybrid heating, ventilation, and air-conditioning (HVAC) market. While upfront capital costs associated with geothermal technology can suppose some barriers, the synergistic coupling with PV installations can provide a compelling solution and reliable energy supply, in terms of both economic feasibility and the energy (electricity) consumption. With this aim, a detailed economic and energy analysis is then conducted to evaluate such hybrid solutions connected to the grid, including potential energy storage system. HVAC demand optimized battery energy storage system (ESS) and PV installation connected to the grid are considered as hybrid renewable solution in a Mediterranean location case study based on the tertiary and industry sectors. It is carried out by the authors from real energy demand data collected for 3 years. Simulation results demonstrate that the proposed hybrid system reduces electricity consumption by 25% compared to a conventional air-to-air HVAC configuration, while geothermal operation achieves 34% lower heating demand and 26% lower cooling demand. These improvements highlight the hybrid system potential for enhanced energy efficiency and load-shifting capability in tertiary and industry sectors.

1 | Introduction

In recent decades, economic growth has mostly raised living standards in developed countries. At the same time, such economic growth has been responsible for the decrease in natural resources and increase in emissions [1]. Subsequently, the association between economic growth rate, energy demand, financial

development, and globalization has recently promoted an international debate among different sectors, aiming to propose alternative pathways in a more sustainable manner. Among the different key-role of current societies, energy is considered as a crucial driver. In this way, Svobodova et al. [2] identified the high country-level dependencies and the necessity of global

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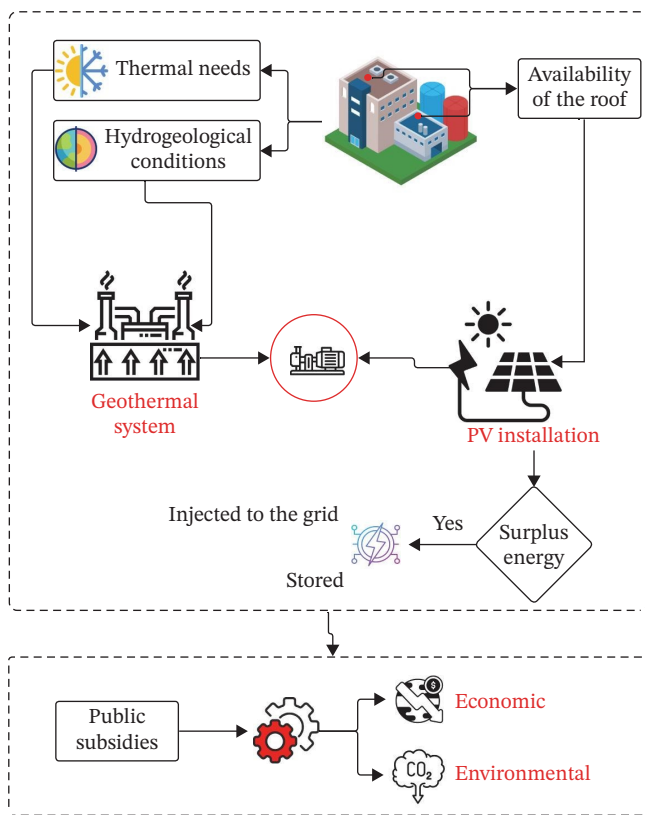


FIGURE 1 | General overview. Research framework.

2.1 | Shallow Geothermal System Design

In a GSHP system, thermal energy is extracted from the fluid circulating within a closed-loop ground heat exchanger using a geothermal heat pump, which transfers heat to the building. The fluid is then reheated as it moves through the ground loop, ensuring a continuous exchange of energy. During cooling mode operating conditions, this process is reversed. This renewable resource is, thus, able to provide sustainable heating and cooling solutions for a variety of potential applications—including residential, tertiary, or industrial customers; as well as for specialized needs such as cooling data centers. Shallow geothermal systems typically consist of vertical closed-loop boreholes, which facilitate heat exchange with the subsurface. These systems rely on the GSHP to either increase or decrease the temperature obtained from the ground to meet the thermal set-point operating conditions. Circulating pumps and associated equipment are designed to distribute conditioned thermal energy throughout building installations. A significant challenge of geothermal energy projects is commonly the availability of detailed geothermal resource mapping [48]. If comprehensive data is available, uncertainties are significantly reduced during the exploration phase, potentially lowering development costs. In the proposed methodology, a preliminary GIS-based environmental analysis is first conducted to assess the geothermal resource and to evaluate suitable technologies based on subsurface characteristics. The analysis focused on the assessment of subsurface thermal conductivity is determined by both lithological properties and the degree of water saturation [49]. The peak daily thermal requirements for both heating and cooling determine the GSHP capacity. The corresponding power electricity demand is then calculated based on the GSHP COP and seasonal performance factor (SPF), along with the thermal

demand [50]. After determining the thermal load requirements, the subsequent stage involves designing the borehole field to extract the required thermal energy from the ground. This design process takes into account not only the annual thermal energy demand, but also the subsurface hydrogeological properties, previously assessed through a GIS-based analysis. The entire geothermal system, including the borehole field, is then modeled using the earth energy designer (EED) software [51]; being one of the most used tools during the geothermal calculation sequence [52]. The EED tool incorporates factors such as geological conditions, borehole dimensions, thermal properties of the heat transfer fluid, and building energy requirements to simulate the thermal behavior of the geothermal borehole system. This approach ensures precise design optimization and performance evaluation of the geothermal system, allowing for a more efficient and reliable solution. As Sáez Blázquez et al. [53] affirmed, EED has undergone extensive enhancements, positioning it as a robust tool for the design and optimization of GSHP systems. In particular, EED enables precise configuration of vertical closed-loop geothermal systems, with the capability to evaluate both average and peak monthly fluid temperatures over the designated operational period. Moreover, the latest version of EED offers extended functionality, operating at an L4 software level, which enhances its capacity to model complex scenarios and further refines system performance predictions.

2.2 | PV Installation Design

A PV system comprises various components, including solar panels, electrical connections, inverters, cables, and support structures. A grid-connected PV system can be considered as an electrical power generator supplying electricity to the grid, and making it accessible to any connected user [54]. The system's capacity is determined by its intended application, with kilowatt-peak (kWp) systems designed for residential and tertiary use—mainly in self-consumption mode; and megawatt-peak (MWp) systems for large-scale PV power plants—commonly connected to the grid from the supply-side and sometimes in self-consumption mode for large industrial customers. Off-grid PV installations, mostly referred to as self-consumption systems, supply electricity solely for on-site use, with any surplus energy discarded. In the development of a PV power plant design, the geographic location of the site is carefully analyzed to determine the optimal tilt of the panel based on latitude. Moreover, the orientation of the panels towards true south is commonly considered as critical, as proper alignment maximizes solar exposure, and thus, improves energy capture [55].

The electrical power demand of the system is estimated by calculating the hourly power consumption (kWh). Subsequently, the total energy consumed over a 24-h period (kWh/day) is determined. Based on the energy demand, a PV system is proposed with enough power capacity to cover the majority of the required consumption [56]. Once the rated capacity of the PV system is determined and the orientation and positioning of the PV panels are defined, the energy generation per hour is estimated using the PVsyst simulation software [57]. PVsyst calculates the power output by considering the specific location of the PV installation, with solar irradiance data obtained from the SolarGIS meteorological database [58]. Table 2 provides an overview of the key meteorological parameters available for download from

TABLE 2 | Database of SolarGIS.

Data	Units
Global horizontal irradiation	W h/m ²
Direct normal irradiation	W h/m ²
Diffuse horizontal irradiation	W h/m ²
Sun altitude (elevation) angle	°
Sun azimuth angle	°
Air temperature (at 2 m)	°C
Atmospheric pressure	hPa
Relative humidity	%
Wind speed at 10 m	m/s
Wind direction at 10 m	°
Precipitate water	kg/m ²

SolarGIS. It is used to design the PV power plant and estimate the annual energy output in MWh/year. By selecting the type and number of PV modules and inverters, a detailed simulation of the PV plant can be then performed. Some loss factors can be incorporated into the simulation, including transmission losses through cables, energy consumption of transformation equipment, and losses due to soiling or dust accumulation on the PV panels, among others [59]. These factors ensure a more accurate representation of the PV power plant performance under real conditions.

2.3 | BESS Design

BESSs enables more efficient RES utilization and prevents energy wastage [60]. BESS contribute to grid stabilization, frequency regulation, emergency power supply, and industrial-scale peak shaving, which can help reduce electricity costs [61]. Incorporating battery storage presents significant challenges, such as increased capital costs, the requirement for advanced battery chemistries, and environmental implications associated with the manufacture and end-of-life disposal [62]. While battery prices remain relatively high due to the nascent nature of the industry, production costs are steadily declining [63]. Thus, different types of batteries are available, each with different applications depending on factors such as cycle life, cost, and performance. Lead-acid batteries are the most cost-effective option, featuring low self-discharge and a wide operating temperature range. Due to their affordability, they are widely used in

various applications, including vehicle batteries, substation backup power, marine applications, emergency lighting systems, and telecommunications backup equipment. Sodium sulfur (NaS) batteries, which require their electrolyte to be maintained at high temperatures (around 300°C), offer long life cycles (up to 4500 cycles), although their high cost limits their usage in some applications. Lithium-ion (Li-ion) batteries are the most common choice for BESS. These batteries are highly versatile, with long life cycles (ranging from 5000 to 10,000 cycles), low self-discharge, and high energy density. Although initially expensive, the growing electric vehicle market and advancements in battery technology have led to reduced manufacturing costs, consequently lowering the price of Li-ion batteries. Subsequently, the integration of appropriately sized ESS, combined with accurate ESS sizing strategies in renewable energy applications [64], represents a promising approach to ensure greater stability in electric power availability and deserves further investigation [65]. Moreover, the deployment of solar PV systems coupled with battery storage has expanded considerably, driven by their operational flexibility and the progressive decline in battery technology costs [66]. The proposed solution is designed to include the BEES exclusively as an auxiliary component for electrical energy management purposes, enabling either the injection of surplus electricity into the grid or its storage in dedicated high-capacity units. Thermal integration is excluded from the operational framework to maintain design simplicity and prioritize electrical flexibility, dynamic load balancing, and grid stability over combined heat and power (CHP) strategies. An example of thermal battery storage for a residential building can be found in reference [67]. However, this hybrid solution required an additional heating load of 1.85 kW from the furnace.

3 | Case Study: Industrial and Tertiary Building

The hybrid geothermal–battery–PV case study is located in an industrial area with a high daily economic activity and energy consumption rate. The purpose is reduce a large electricity demand and thermal energy consumption by considering real data collected over the last 3 years for a tertiary and industrial building. The electric and thermal demand profiles are used to design the hybrid installation according to Section 2. The hybrid installation includes a PV installation, geothermal system and a possible BESS solutions to manage the surplus energy. Results are also compared to a conventional HVAC system in terms of energy and economic analysis. The case study is located in Albacete, Southeast of Spain, a continental climate city with cold winters and hot summers (Figure 2A). This temperature range



FIGURE 2 | Location of case study (A). Roof of the tertiary and industrial building (B).

requires high thermal energy needs for heating and cooling purposes, regardless of the weather season. This fact involves high energy thermal consumption in both winter and summer periods. The city is located at a latitude of 39°. The solar irradiation can then be translated into a large amount of PV energy generated throughout the year [68], which is sufficient to supply the peak energy consumption of the whole equipment. The proposed hybrid solution is, therefore, based on a geothermal installation, with a stable temperature achieved throughout the year, at a minimum cost to obtain this heat energy. The heat could be extracted from underground using a geothermal pump powered by a PV installation located on the roof of the building (Figure 2B). The possibility of different combinations of geothermal PV solar hybrids is also considered in the results (Section 4.2). Indeed, a BESS can be also used to store surplus energy and, subsequently, to be demanded by the customer—in a self-consumption mode; or sold during off-peak hours by considering the electric market price evolution. Aiming to evaluate the different solutions, various installations are proposed and compared. Depending on the thermal and electric energy demand, and by considering the potential surplus energy along the year, it could be possible to store such energy for future demand requirements, or even to create industrial energy communities to decrease power demand and optimize resources in a more renewable and sustainable scenario; being currently a topic of interest by the authors.

To evaluate the shallow geothermal potential of the study area, the underground conditions were first assessed (Table 3). The lithology consists of various materials, including sinkholes, marls, lime-stones, gravels, and sands, as summarized in Figure 3. The materials have similar thermal properties, with an average thermal conductivity of 2.8 W/mK and a thermal capacity of $2.5 \times 10^6 \text{ J m}^{-3} \text{ K}^{-1}$, estimated according to the Spanish

UNE-100715-1 standard [69]. Information regarding the hydro-geological units was collected from the Groundwater Bodies Watershed Hydrology Plan (2015–2021) [70]. This data informed two key decisions: (i) the assessment of the potential presence of an aquifer that meets the conditions for thermal exploitation and (ii) the measurement of the depth at which the water table is located, thus enabling a better understanding of groundwater dynamics and system feasibility. Ultimately, no suitable aquifer was identified in the area, indicating the necessity of a closed-loop system. However, the water table was found to be very shallow, meaning the materials were largely water-saturated. This fact increases the thermal conductivity of the materials, enhancing the overall efficiency of the geothermal system.

4 | Results and Discussion

4.1 | General Overview and PV Power Plant Configurations

Based on the analysis of the thermal consumption of the Spanish customer, the peak thermal demand is estimated to reach 210 kW during winter and 197 kW in summer. To meet this demand, a geothermal heat pump—42 kW electrical capacity—is considered enough to extract the thermal energy required for the industrial and tertiary building under study. One of the notable new features recently introduced in Spain was the allowance for both individual and collective (shared) self-consumption [71]. This regulation specifies that the user and the owner of the PV installation can be distinct individuals or legal entities, enabling greater flexibility in system ownership and operation. Furthermore, individual self-consumption systems can operate either with or without surplus energy, meaning the excess electricity generated can either be fed into the distribution grid or not. However, for shared self-consumption, surpluses must be fed

TABLE 3 | Parameters and properties.

Ground properties			
Undisturbed ground temperature	14.7°C	Ground thermal conductivity	2.8 W/mK
Ground thermal capacity	$2.5 (10^6 \text{ J m}^{-3} \text{ K}^{-1})$	—	—
Length heating/cooling season			
Heating days/year	150	Cooling days/year	215
Borehole parameters			
Threshold fluid temperature (winter)	−2°C	Borehole depth	100 m
Threshold fluid temperature (summer)	35°C	—	—
Borehole radius	0.1 m	Simulated time	50 years
Borehole thermal resistance	0.1 mK/W	—	—
Thermal energy extracted from the ground			
Q_{BHE} (heating mode)	11.63 MWh/year	Q_{BHE} (cooling mode)	15.57 MWh/year
Q_{BHE} (heating mode)	1.33 W	Q_{BHE} (cooling mode)	1.77 W
Borehole field			
Borehole type	Single U-tube	Borehole number	307
Borehole field	370 m × 100 m	Borehole separation	6 m

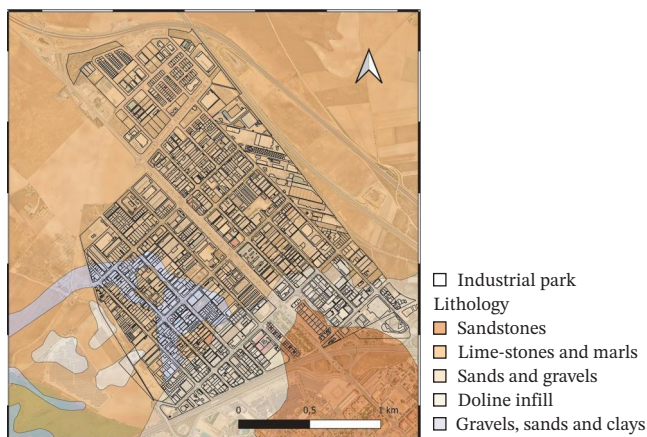


FIGURE 3 | Lithology in the area.

into the grid due to the inherent use of the distribution network [72]. A key factor in determining the economic viability of these systems is the complex compensation for surplus energy. As a result, the legislator has implemented a simplified compensation mechanism based on the net-billing model, available for PV installations smaller than 100 kW rate power, and thus, providing a more accessible alternative for small-scale users [73]. Therefore, and aiming to explore various hybrid energy solutions as case study, four PV power plants and configurations up to 100 kWp with battery storage were proposed and compared in terms of both economic and energy analysis.

An initial 40 kWp PV installation is considered to partially offset the electricity power demand of the geothermal heat pump, though it is not enough to cover the full power demand. This solution allows for a comparison between the electricity generation profile, energy consumption, and surplus energy. As illustrated in Figure 4, the PV installation is capable of generating enough power to cover both geothermal and cooling demand profiles. However, during summer months, particularly in July, the cooling demand values rise significantly, requiring additional electricity demand from the grid. In Figure 4, the blue graph represents air-to-air consumption, while the orange line shows PV power generation during July.

Aiming to meet the geothermal pump demand (42 kW) and able to cover all demand of cooling energy needs, a 60 kWp PV installation scenario is subsequently considered for evaluation. Analyzing the PV installation generation profile (Figure 5), it is capable of covering the daily demand along the year; even during winter months when the energy thermal demand is considerable higher. Although the energy cost can be significantly reduced, the purchase of electricity at night is still required, as any BESS is not then considered to be included in this case study.

Regarding a 80 kWp PV installation, it provides surplus energy in every month of the year. This PV power plant is oversized in comparison to the thermal energy demand, in order to increase the profitability of the installation by the introduction of BESS. Therefore, PV generation was higher than the power demand and, consequently, the results gives an additional amount of generated power able to be fed to the grid or stored into BESS for a subsequent use. Figure 6 shows the results for this scenario. As can be seen, the PV power generation profile (orange line) always

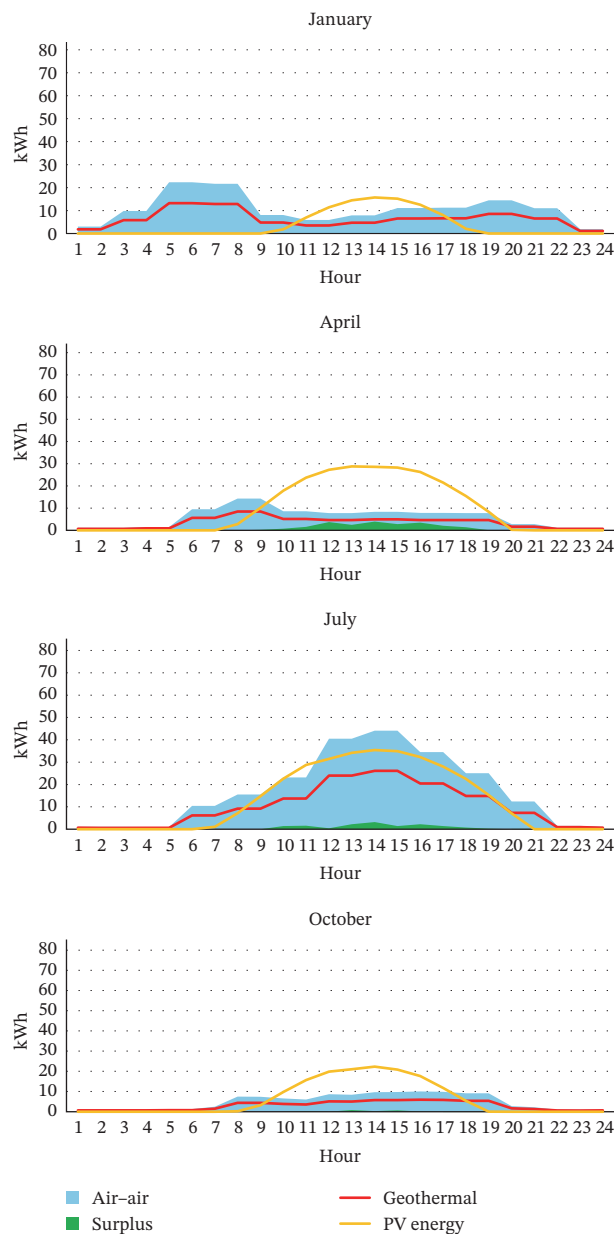


FIGURE 4 | A 40 kWp PV installation. Power generation and demand profile.

remains higher than the geothermal demand (red line) and estimated air–air conventional equipment (see blue graph profile).

Finally, a 100 kWp PV installation is designed (Figure 7). In this specific case, the number of PV modules was almost doubled in comparison to the 40 kWp scenario. By considering the power generation profile, a higher PV electricity production is able to be used for nonthermal demand of the tertiary and industrial building, such as lighting, other equipment in general. Results are summarized in Figure 8. As can be seen, a remarkable amount of surplus energy is estimated during the year, being significantly relevant in spring and autumn, as solar irradiation provides more generated power electricity than the thermal demand is required, due to soft outdoor temperatures reached in these seasons. Subsequently, such surplus energy could be stored for future consumption periods or fed to the grid.

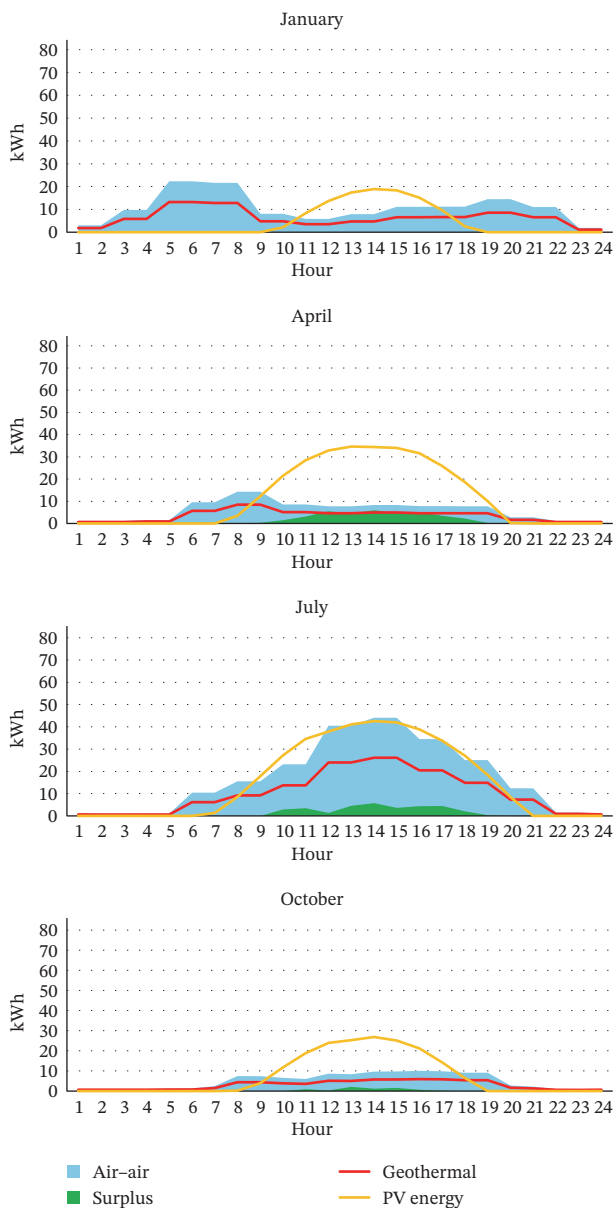


FIGURE 5 | A 60 kWp PV installation. Power generation and demand profile.

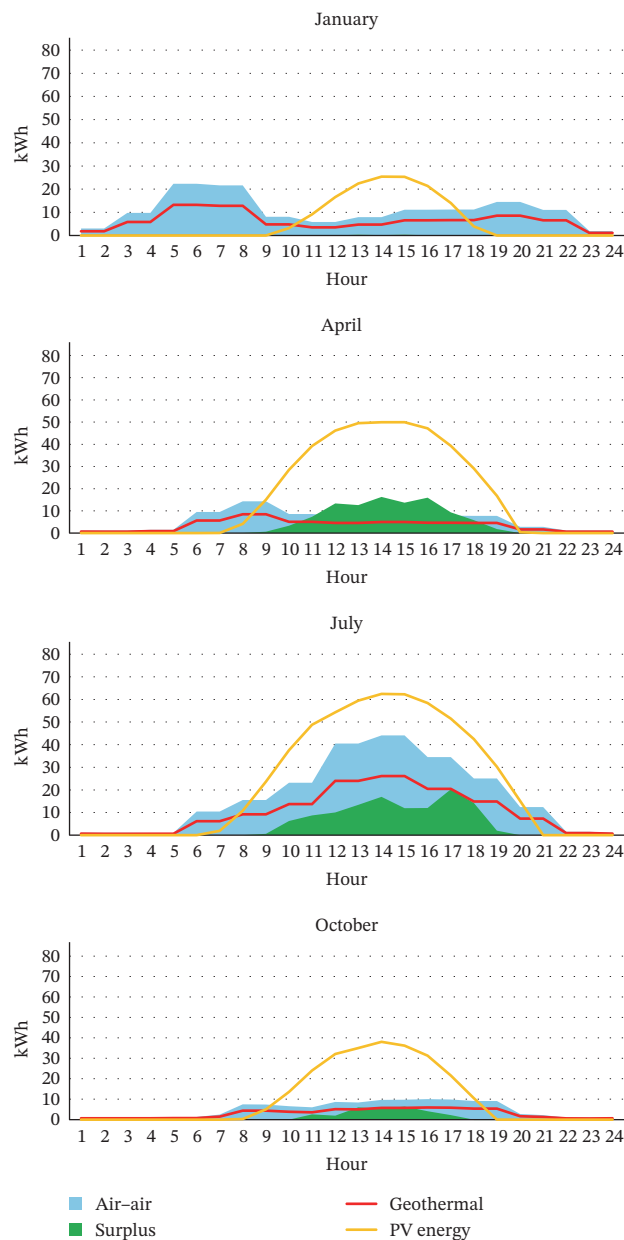


FIGURE 6 | A 80 kWp PV installation. Power generation and demand profile.

4.2 | Shallow Geothermal System Design

A thermal base load was estimated by considering the minimum mean fluid temperature: 11.2°C in winter and 25.9°C in summer. Peak thermal loads were estimated by considering -2 and 35°C for heating and cooling accordingly. These temperature values correspond to the averaged temperature during winter and summer, respectively, for former, and the latter corresponds to the minimum average temperature during the winter and the maximum averaged temperature during summer. The borehole length is 100 m and the simulation period spans 25 years. Locations of proposed boreholes are represented in Figure 9. The energy extracted from the underground was estimated at 91 MWh/year for heating mode, and 90 MWh/year for the cooling operation conditions per borehole (Table 3). These values correspond

to specific heat extraction rate for the heating mode, ranging from 4.3 to ±21.6 W/m; and from 4.51 to ±27.3 W/m for the cooling mode.

The proposed GSHP has a COP of 4.6 for the heating mode and SPF of 4.4 for cooling mode, according to the Spanish Heat Pumps Inventory [74]. In total, 1400 m of boreholes are needed to reach the energy demanded, split into 14 boreholes. The current Spanish rule UNE 100715-1-2014 [75] establishes a safe distance of 3 m between the boreholes and the building infrastructure, and 6 m among the boreholes themselves. In total, a borehole field network of 12 × 13 m² is proposed. Figure 9 shows the designed borehole network in a specific area next to the case study building—considered as tertiary and industrial building example. In comparison to conventional air-to-air HVAC systems, geothermal cooling solution has a higher COP, demanding lower power

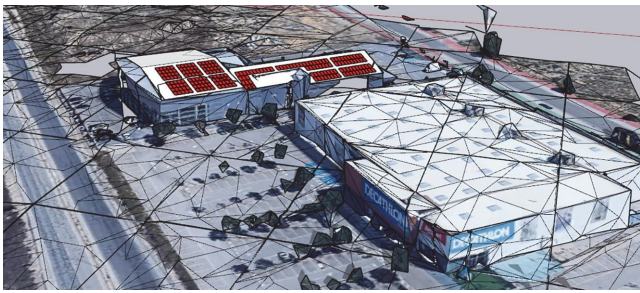


FIGURE 7 | A 100 kWp PV power plant. General overview and PV modules layout.

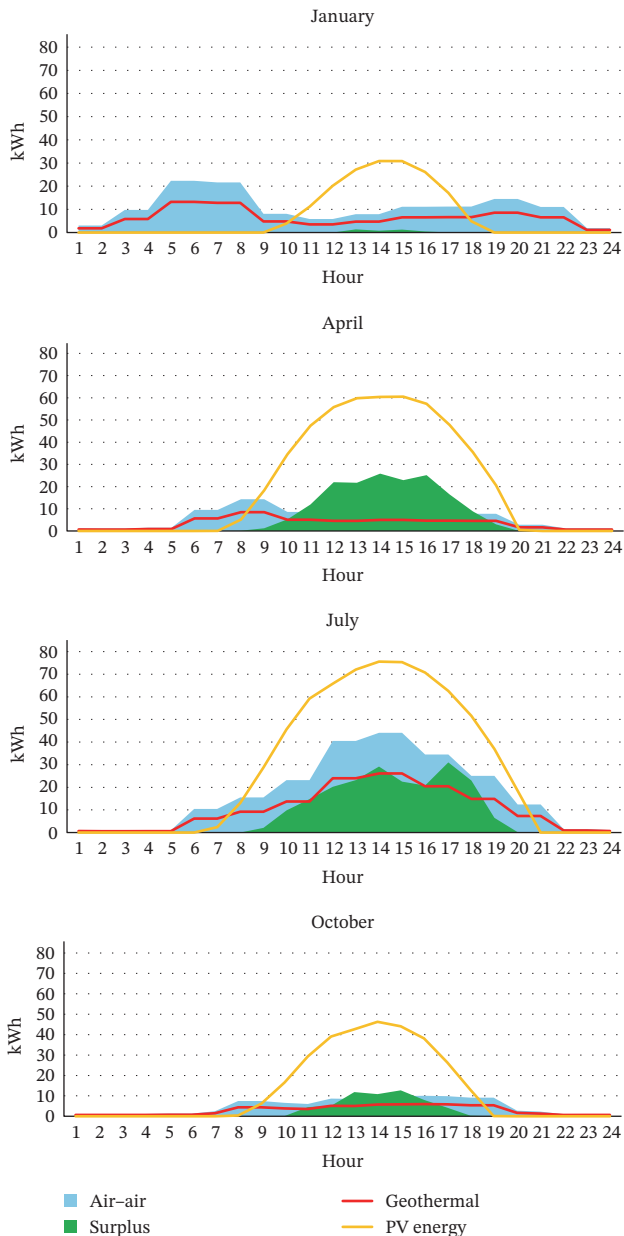


FIGURE 8 | A 100 kWp PV installation. Power generation and demand profile.

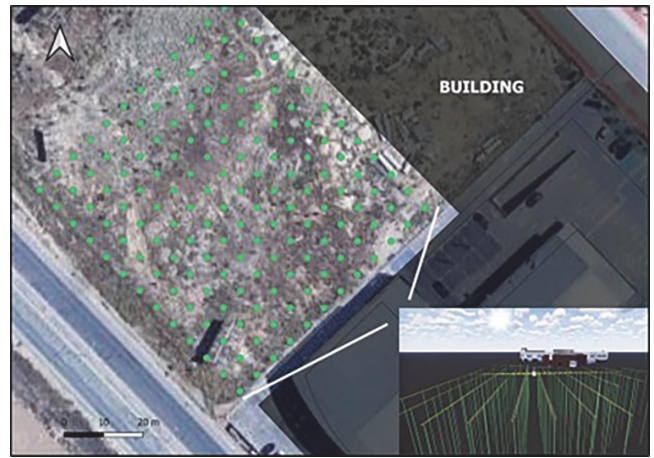


FIGURE 9 | Location of boreholes.

TABLE 4 | Surplus energy. Comparison of solutions.

PV rate power (kWp)	Geothermal system (kW h/year)	Conventional HVAC system (kw h/year)
40	3610.41	2221.48
60	6692.40	4434.76
80	22,206.04	16,306.12
100	38,708.44	29,578.82

electricity profiles. Subsequently, the energy surplus of geothermal solutions is higher than air-air cooling HVAC conventional system (Table 4).

4.3 | BESS

The BESS selection was based on the surplus energy profiles (Table 4). The different PV system scenarios outlined in Section 4.1 directly influenced the surplus energy available, thereby affecting the size and cost of the selected BESS. After evaluating multiple technologies, Li-ion batteries were chosen due to their compatibility with PV systems and extended cycle life [76], despite their higher initial investment cost [77]. The estimated capacities for each BESS solution are presented in Table 5. In conclusion, the use of Li-ion batteries provides a balanced trade-off between performance and cost-efficiency, particularly

TABLE 5 | BESS capacity (Ah).

PV power plant (kWp)	Voltage (V)	Geothermal cooling (A h)	Conventional HVAC cooling (A h)
40	24	520	320
60	24	770	510
80	24	3200	2350
100	48	2800	2200

when integrated with PV systems. Their long cycle life and reliability, despite the initial investment, make them suitable for renewable energy applications that aim to maximize the usage of surplus energy. Future improvements in battery cost reduction and efficiency will further enhance the feasibility and attractiveness of these systems for both residential and commercial applications. By properly sizing the BESS according to surplus energy profiles, significant energy savings and increased self-consumption of renewables could be achieved, aligning with current sustainability goals.

4.4 | Economic Analysis

The economic analysis is focused on the comparison of conventional air–air cooling system and geothermal-based solution. The large performance difference between geothermal and conventional cooling is –34% for thermal heating and –26% for thermal cooling demand. Therefore, the energy saving to maintain the same operating conditions is around 25% lower per day, if geothermal energy solution is selected. An analysis of the initial capital expenditure in comparison to ongoing maintenance costs—see Table 6, reveals the inherent profitability of each installation. The results validate that geothermal systems exhibit superior economic performance when compared to conventional cooling systems. This fact is attributed to lower operating expenses and enhanced energy efficiency, leading to higher long-term returns on investment. Consequently, geothermal technology presents a more cost-effective solution for sustainable cooling applications. Additionally, a 20-year analysis indicates that by the 9th year, the initial investment difference of €40,000 between the geothermal energy solution and the conventional air-to-air HVAC systems is fully recovered (Table 7). Subsequently, geothermal energy solutions have become more profitable, mainly because of their significantly lower maintenance costs. This fact highlights the long-term financial advantages of geothermal systems, making them a more economically sustainable option throughout the installation life cycle [78]. The system was evaluated over a projected lifetime of 25 years, considering an electricity cost of 0.20 €/kWh. Operational parameters include 1500 annual operating hours for the compressor and 1800 h for the circulation pump. The installed capacity comprises a 7 kW circulating pump (CCP) and a 32 kW heat pump (CHP). Annual operating expenses were estimated at €2520 for the circulating pump and €4773 for the heat pump, reflecting both energy consumption and maintenance requirements.

TABLE 6 | Economic analysis of cooling system.

Annual analysis	Geothermal	Conventional air–air
Electricity consumed	47.68 MW h	80.51 MW h
Thermal energy produced	214.58 MW h	250.79 MW h
Initial investment	120,000 €	80,000 €
OPEX	7152.65 €/year	12,076.98 €/year
LCOH	33.33 €/MW h	48.16 €/MW h

TABLE 7 | Net present value (NPV).

Year	OPEX geothermal (€)	OPEX conventional air–air (€)	Savings (€)	NPV (€)
0	0	0	0	–40,000.00
1	7152.65	12,076.98	4924.33	–35,075.67
2	14,305.31	24,153.96	9848.65	–30,151.35
3	21,457.96	36,230.94	14,772.98	–25,227.02
4	28,610.61	48,307.92	19,697.31	–20,302.69
5	35,763.27	60,384.90	24,621.64	–15,378.36
6	42,915.92	72,461.88	29,545.96	–10,454.04
7	50,068.58	84,538.87	34,470.29	–5,529.71
8	57,221.23	96,615.85	39,394.62	–605.38
9	64,373.88	108,692.83	44,318.94	4318.94
10	71,526.54	120,769.81	49,243.27	9243.27
11	78,679.19	132,846.79	54,167.60	14,167.60
12	85,831.84	144,923.77	59,091.92	19,091.92
13	92,984.50	157,000.75	64,016.25	24,016.25
14	100,137.15	169,077.73	68,940.58	28,940.58
15	107,289.81	181,154.71	73,864.91	33,864.91
16	114,442.46	193,231.69	78,789.23	38,789.23
17	121,595.11	205,308.67	83,713.56	43,713.56
18	128,747.77	217,385.65	88,637.89	48,637.89
19	135,900.42	229,462.63	93,562.21	53,562.21
20	143,053.07	241,539.61	98,486.54	58,486.54

The Spanish electric self-consumption regulation was initially governed by Royal Decree 15/2018, and later amended by Royal Decree-Law 244/2019. Self-consumption includes PV installations with a contracted power capacity below 100 kW and does not provide any compensation for surplus electricity fed back into the grid. The primary cost to account for is the initial investment, which consists of the net cost plus the applicable value added tax (VAT). The surplus energy of each cooling system solutions and PV installations were subsequently considered for the BESS budget. It also included inverter efficiency, battery depth of discharge and charger efficiency, assuming one-day of autonomy. Table 8 shows the cost of each battery equipment, according to each cooling system and PV power plant solution.

In order to perform a comprehensive analysis of all factors, the ratio called “rate of return” was determined and evaluated (Table 9). It was compared the annual savings on the electricity bill versus the initial investment: initial investment of PV installation and battery; annual electricity savings, depending on the refrigeration system; OPEX of the refrigeration system.

The rate of return of geothermal energy is higher than that of the air–air system in all cases. There are even air–air installations in which the maintenance cost and the initial investment exceed the annual savings, so the ratio is negative, indicating the

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