

The Zalmhaven tower

An investigation on the possibilities of prefab concrete in a high rise building

Literature study

Report 2:

Building plans
Bending and shear deformation
Calculations made by Zonneveld ingenieurs
Fault Tree Analysis

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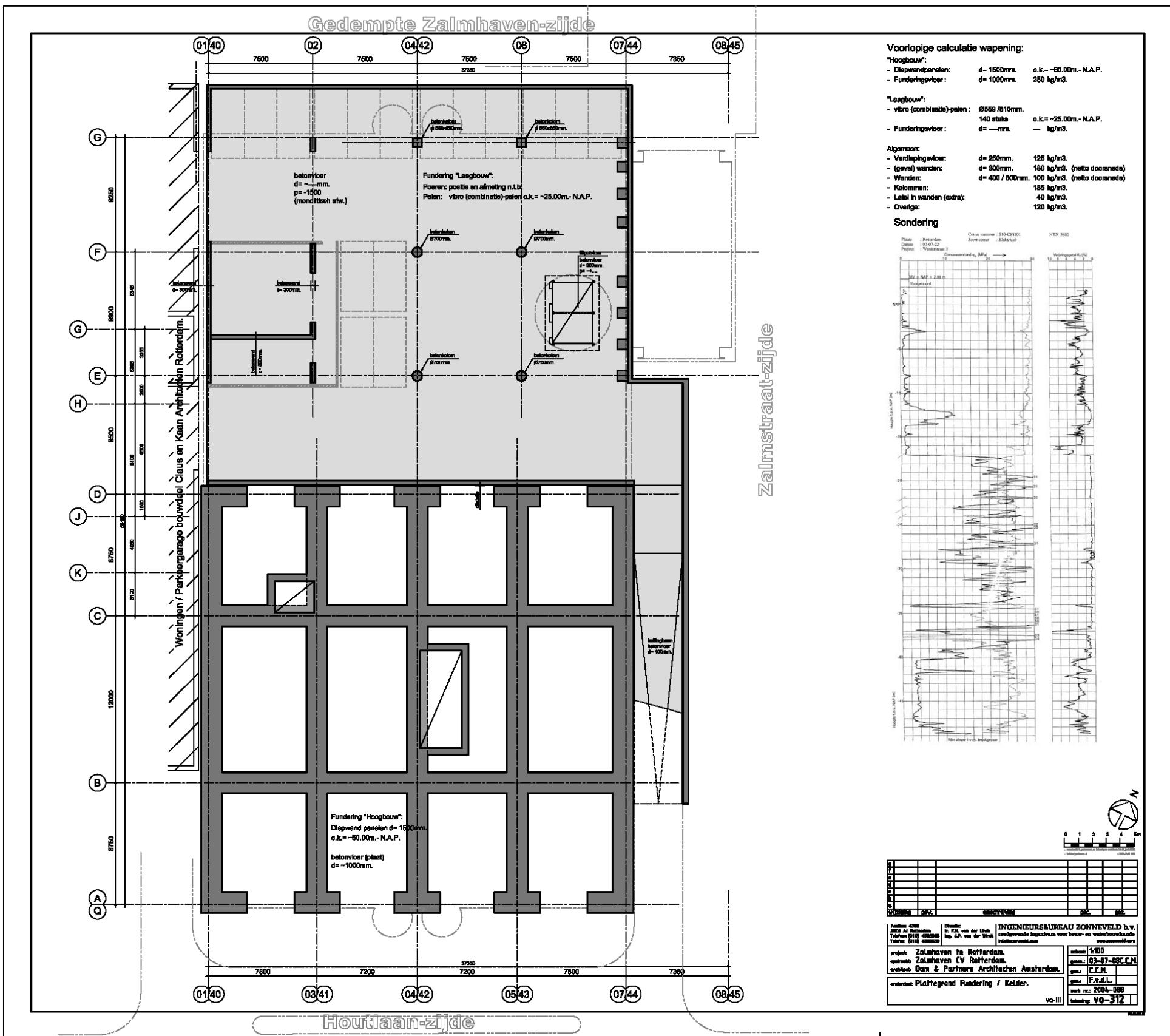
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Delft University of Technology
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Ingenieursstudio DCK/ Delft University of Technology

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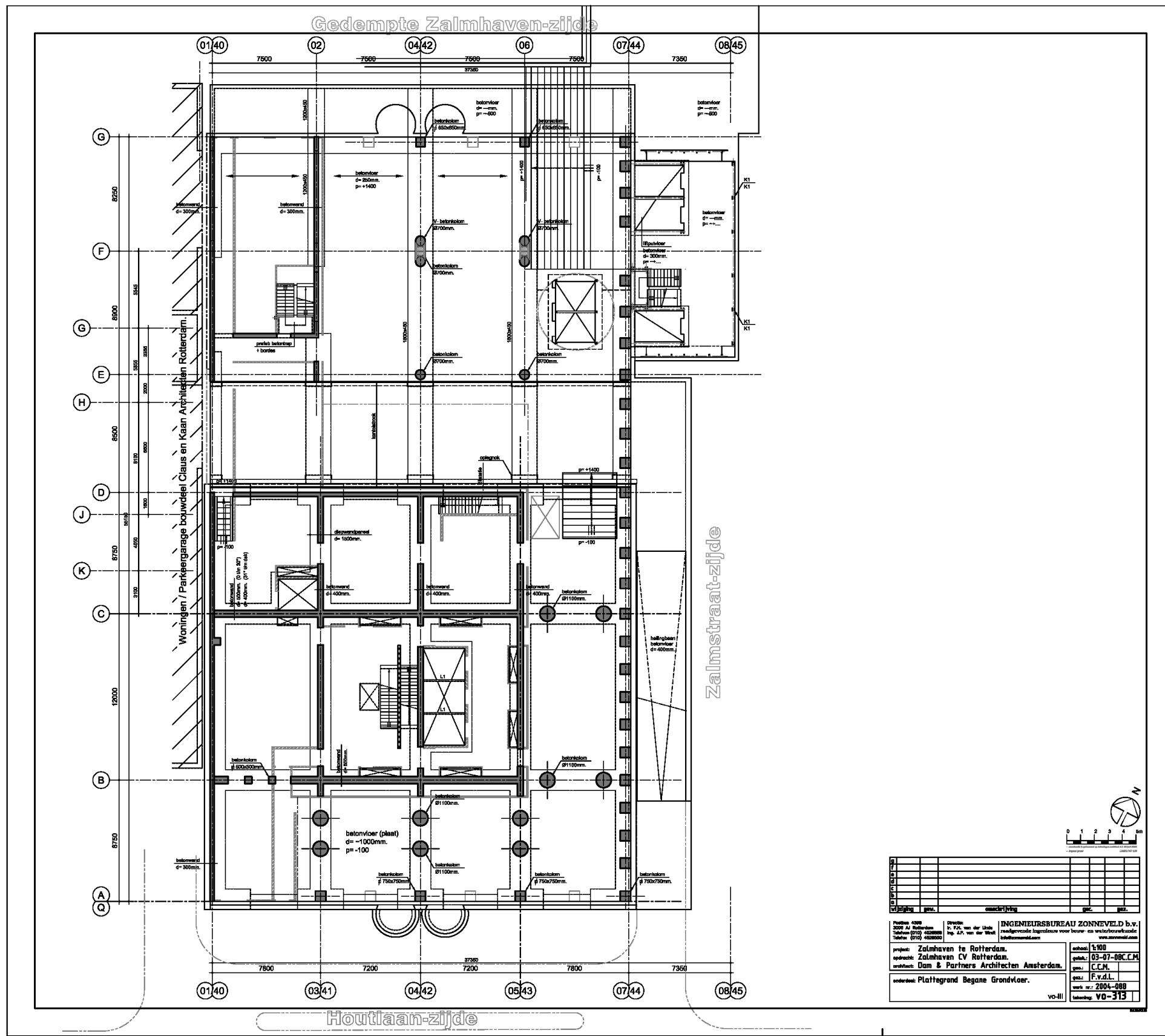
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1 Floor plans of the Zalmhaven tower

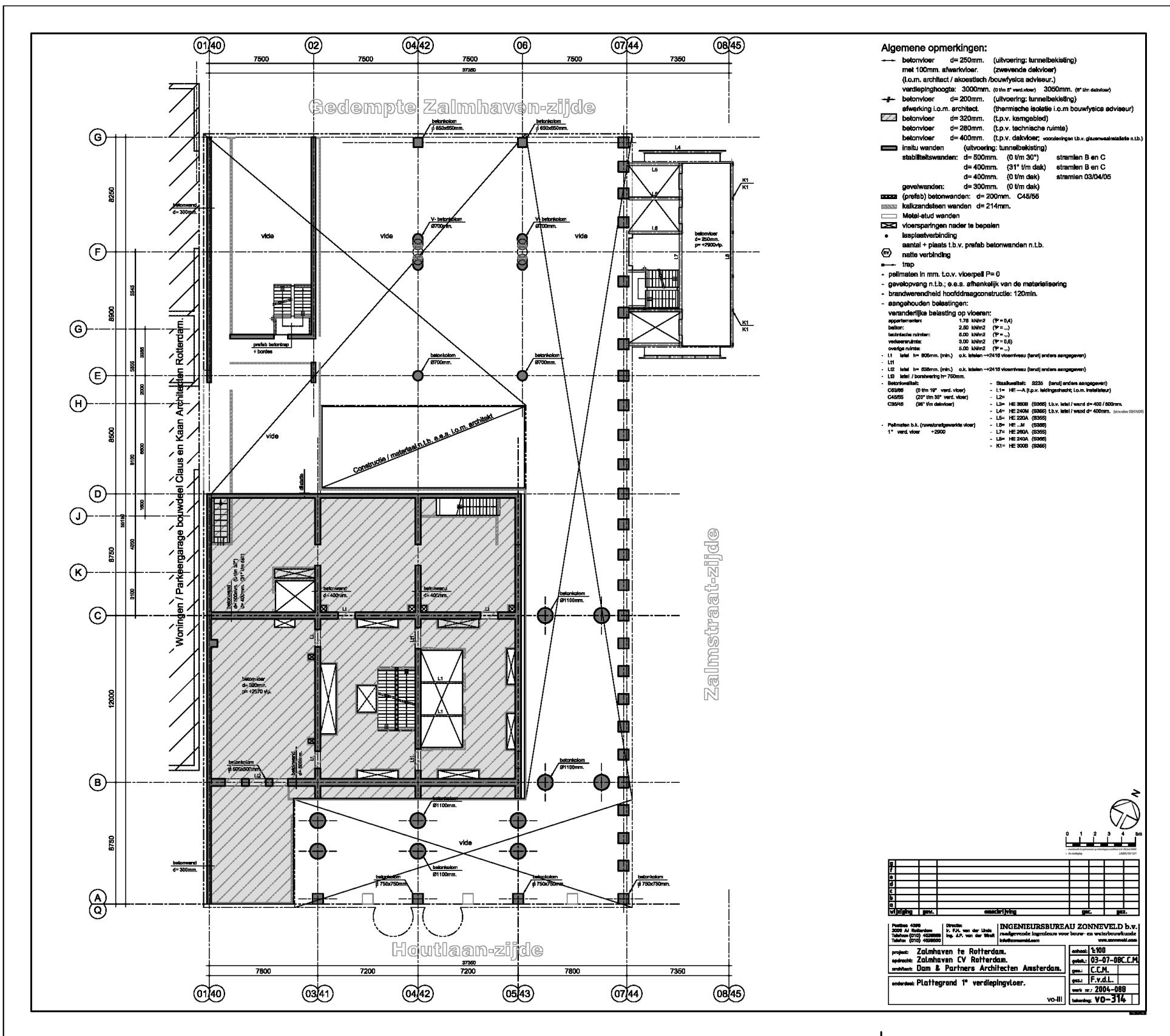
Level: basement.



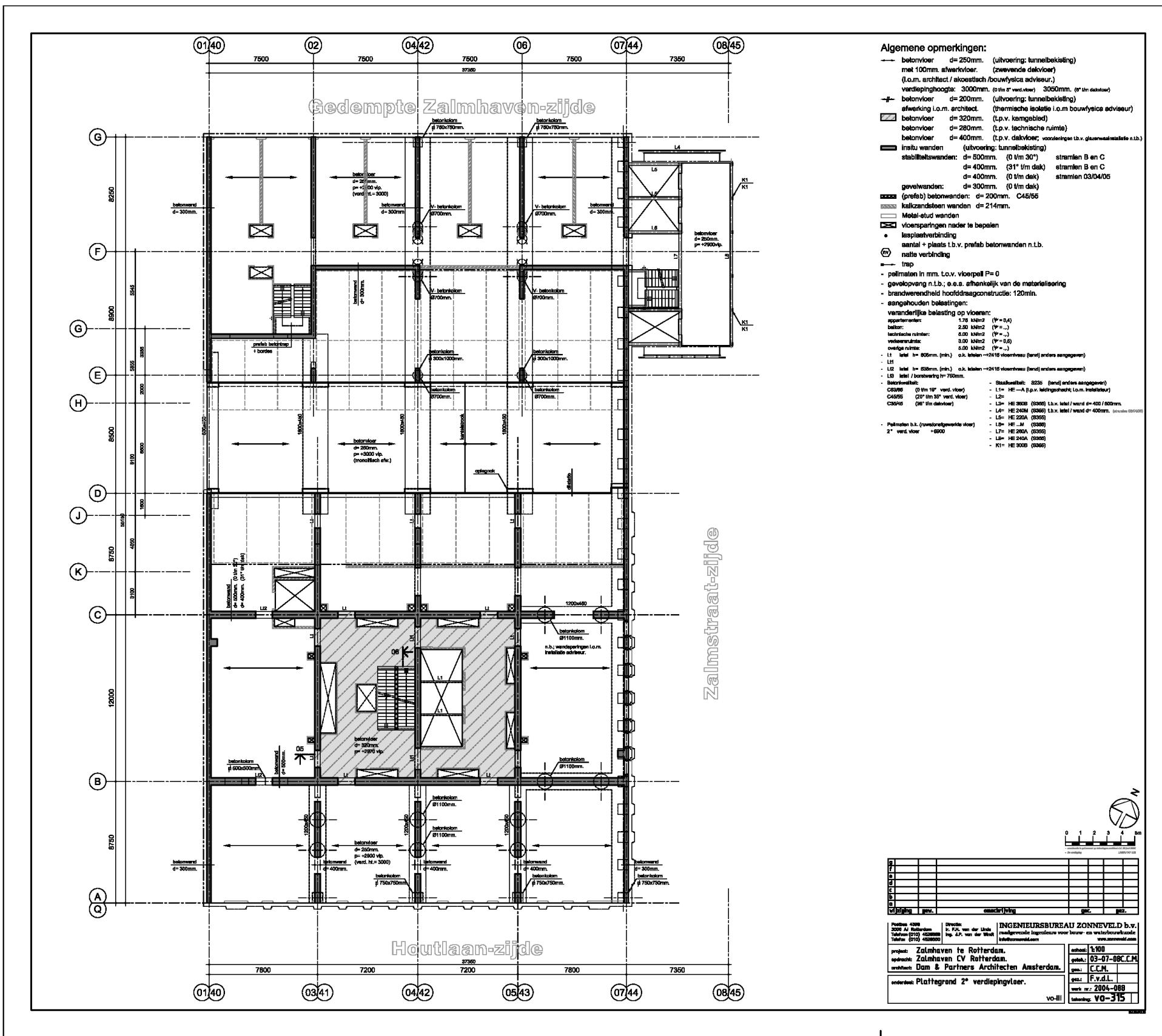
Level: ground floor



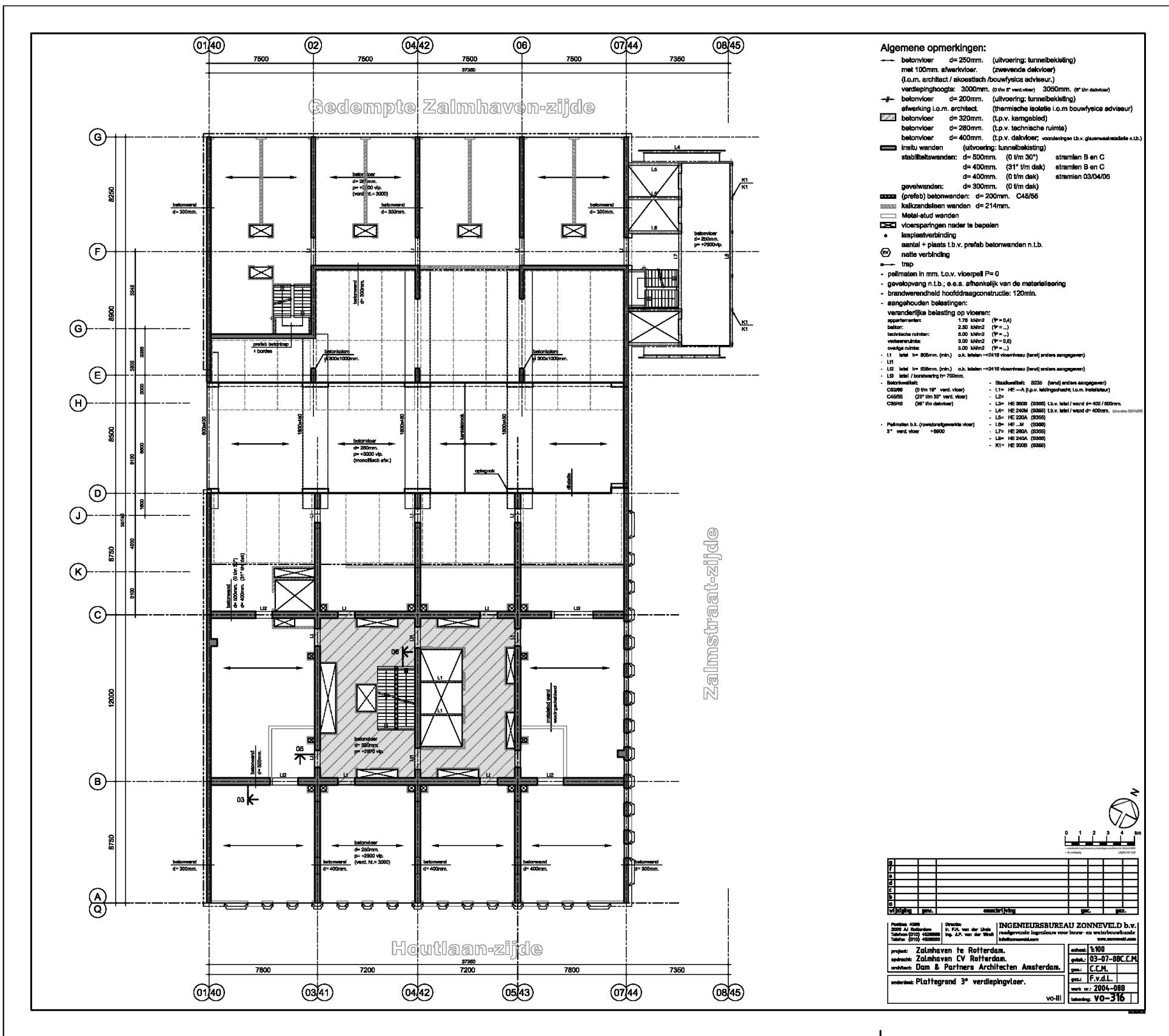
Level: first floor



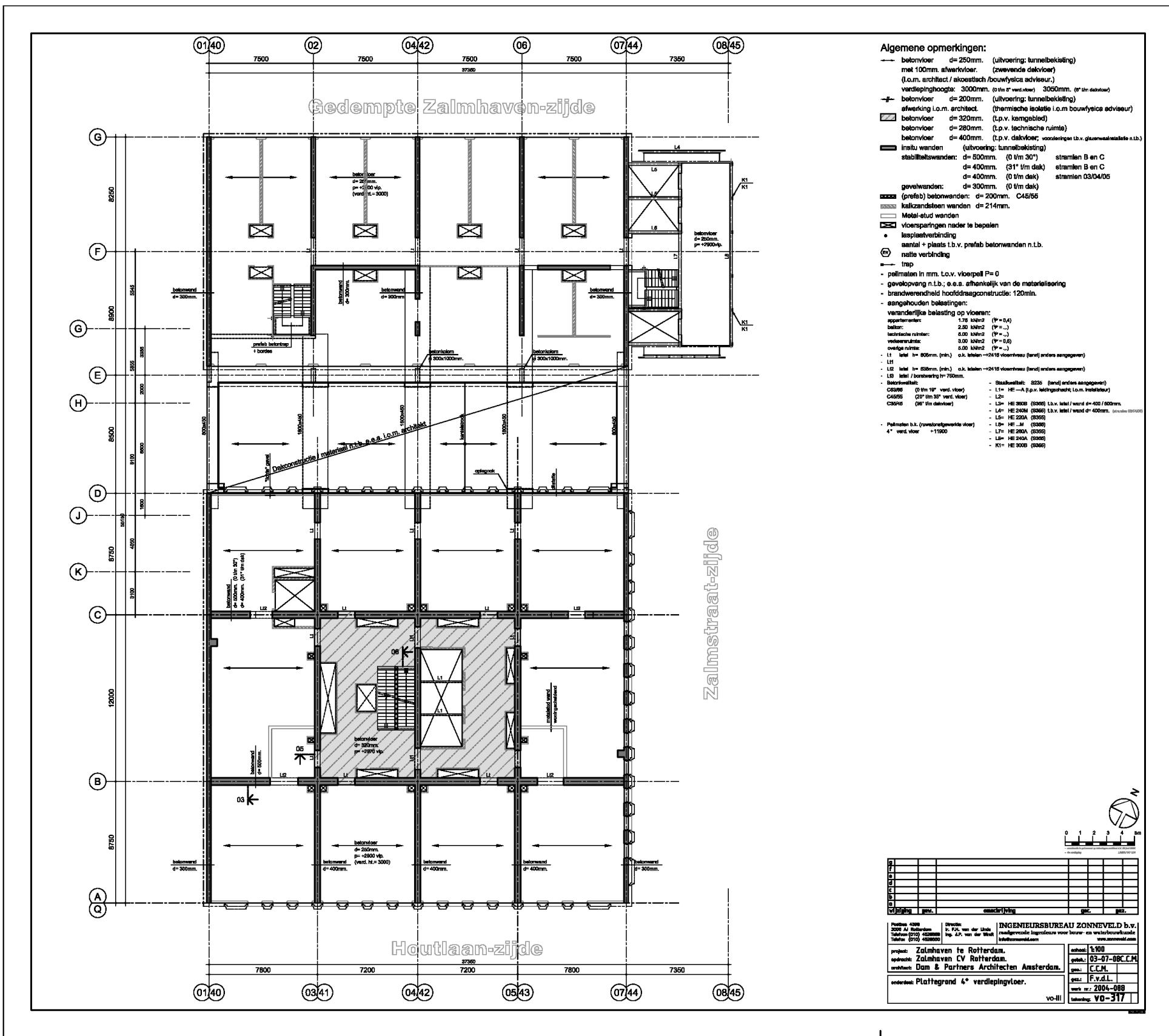
Level: second floor



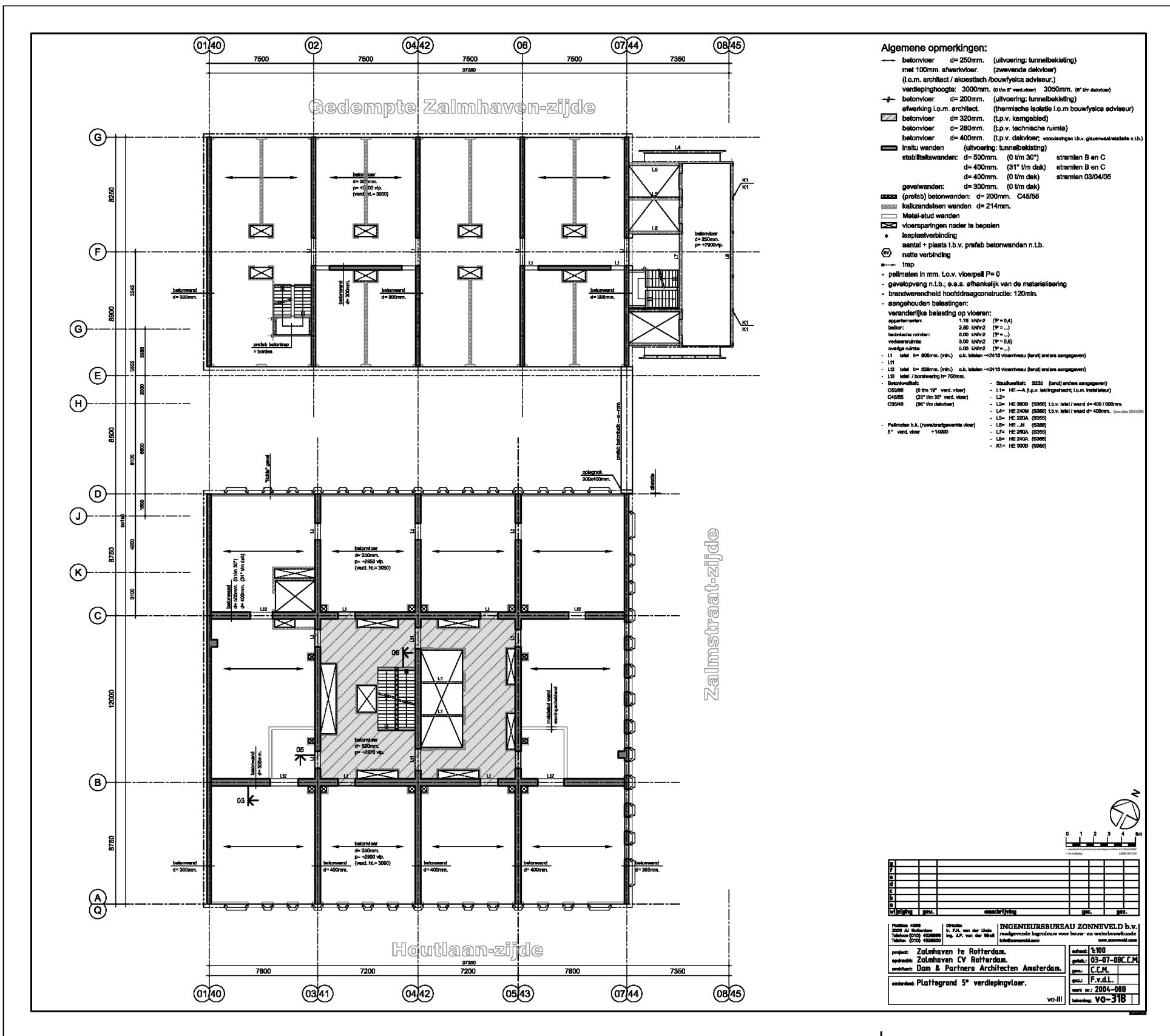
Level: third floor



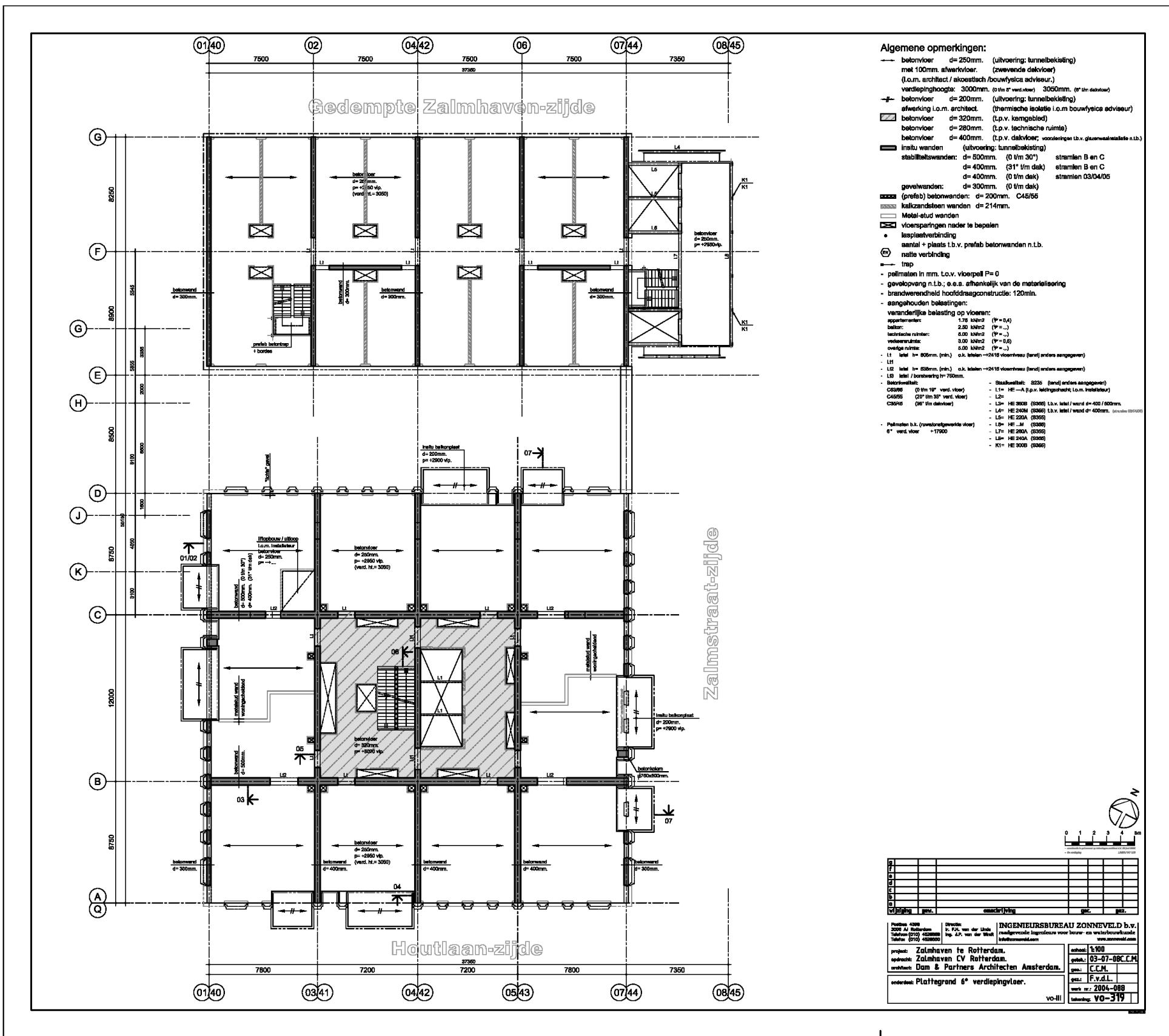
Level: fourth floor



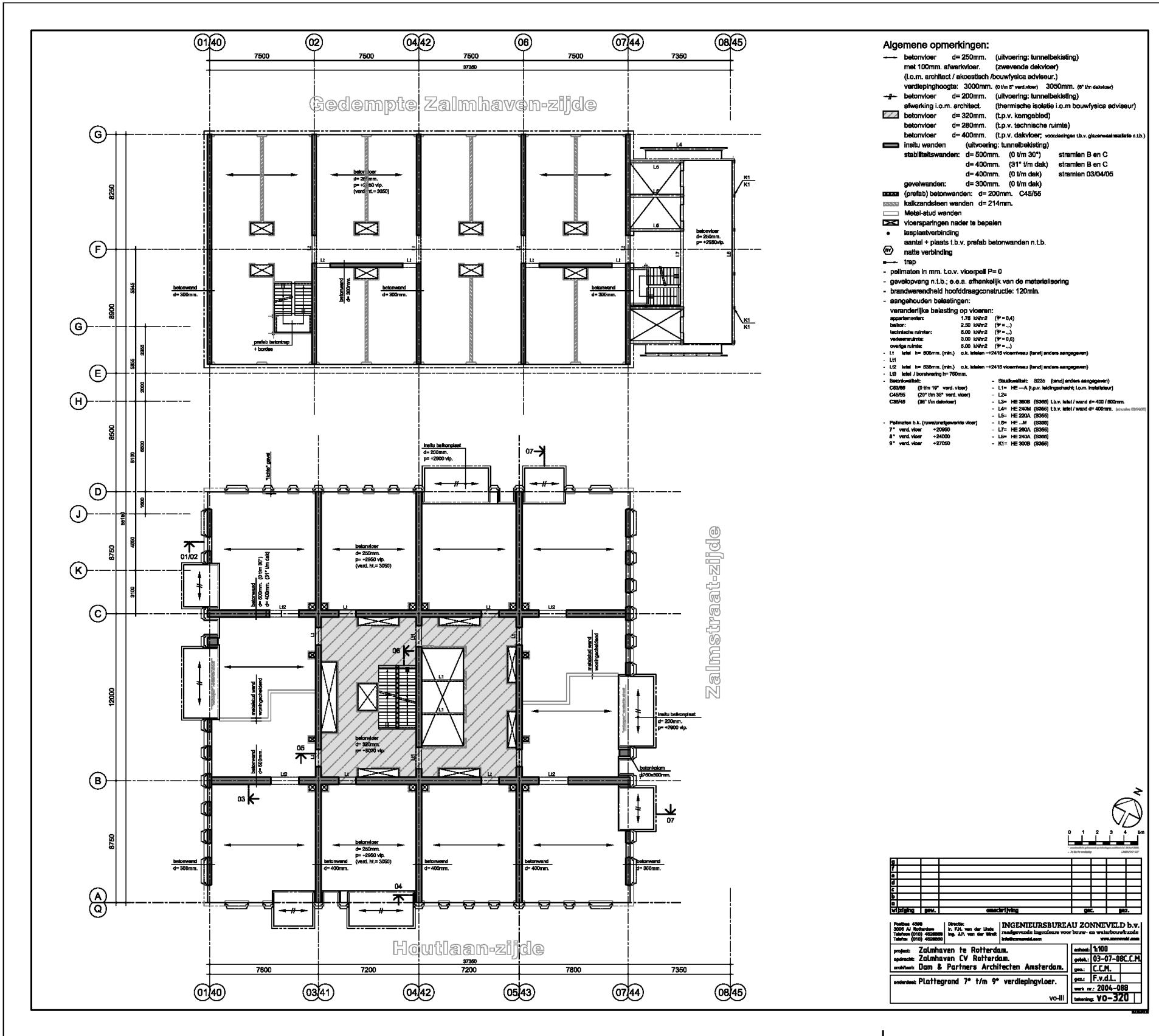
Level: fifth floor



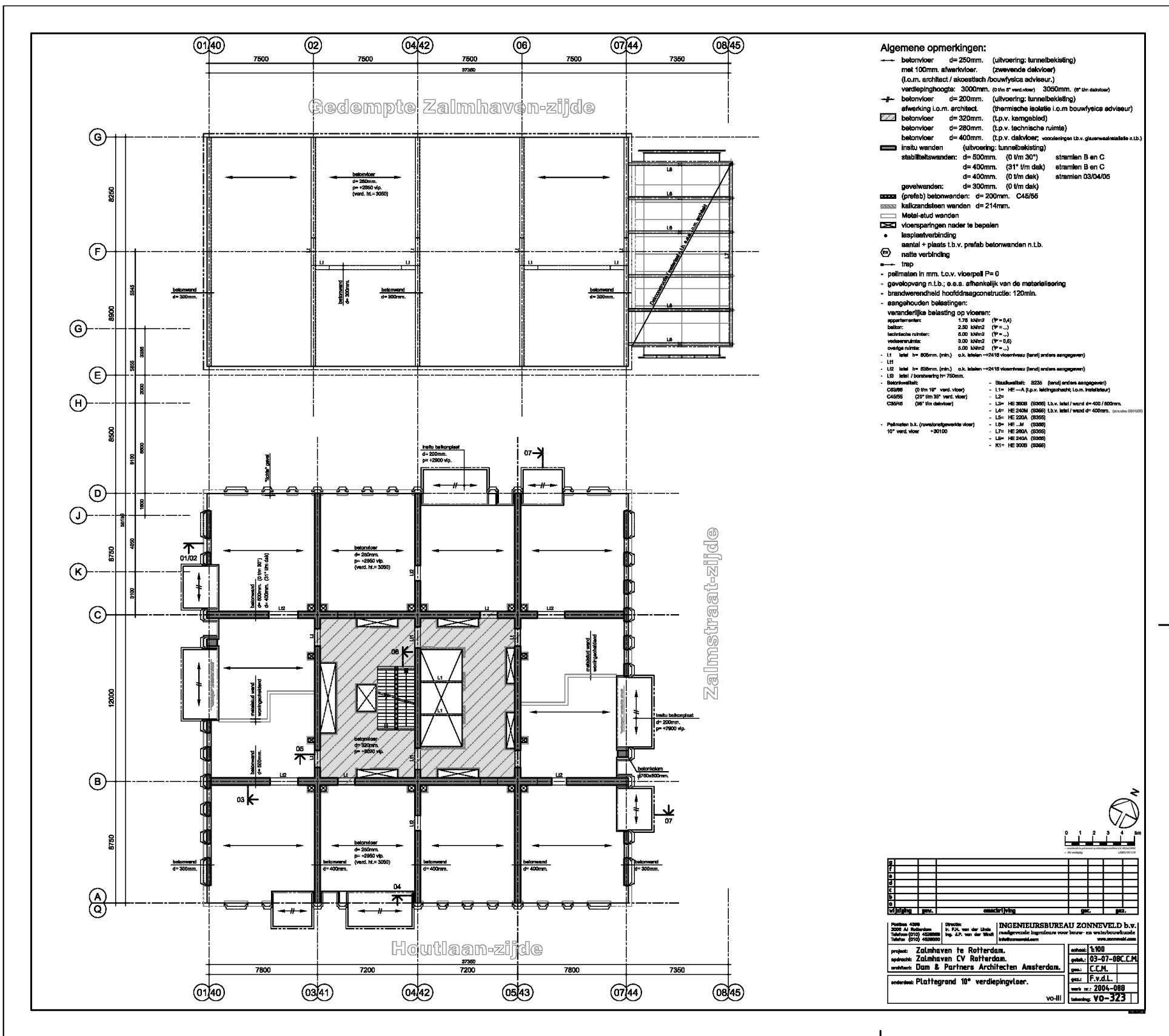
Level: sixth floor



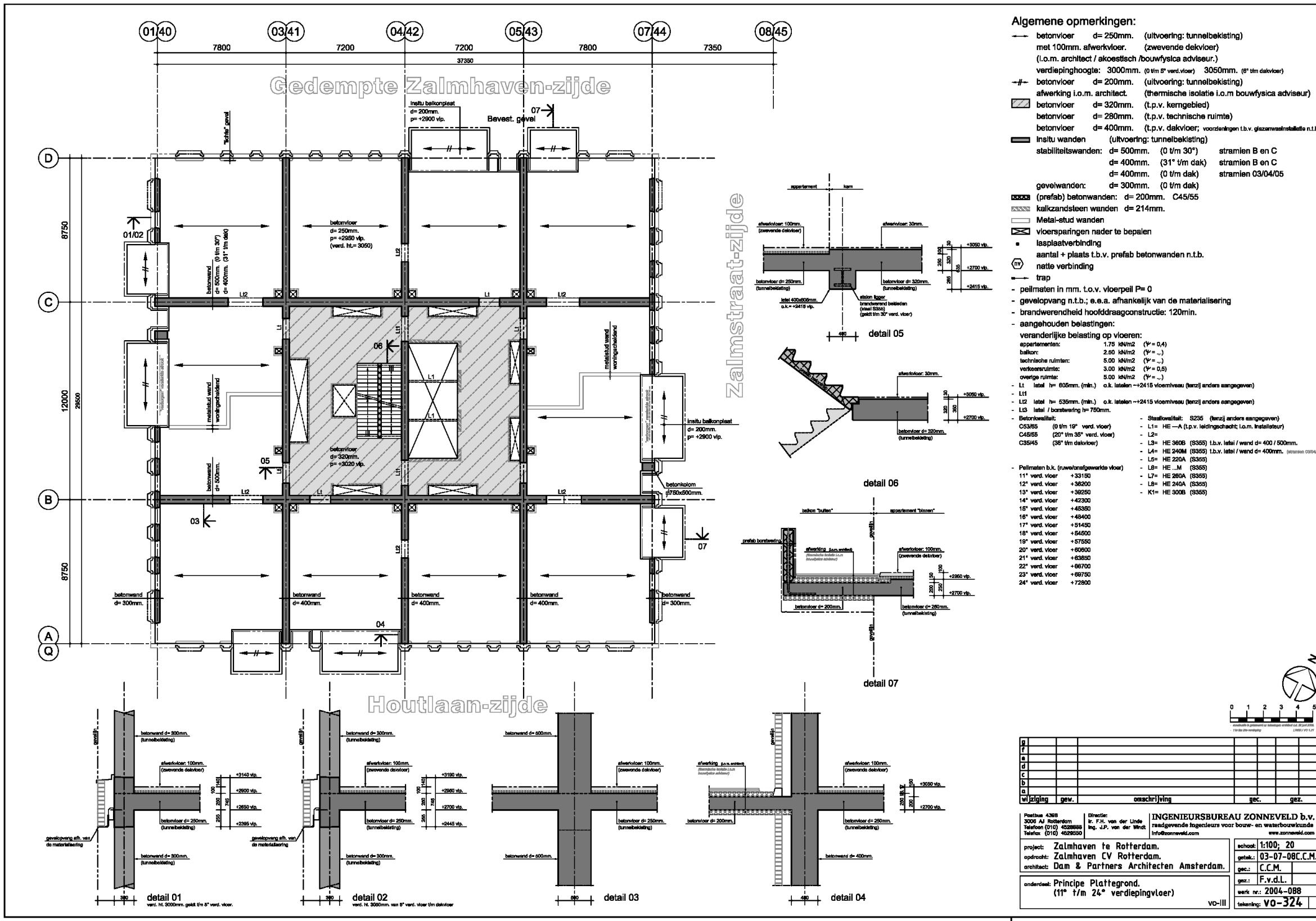
Level: seventh floor till ninth floor



Level: tenth floor



Level: eleventh floor till twenty-fourth floor



2 Bending and shear deformation

Floor	[m]	[m]	[mm]				
	Floor height	Total height	Total height	w (beam bending)	w (shear beam)	w (combination)	Shear defl of total
GF	6,00	0,01	10,00	1,07728E-06	0,000246122	0,000247199	99,5642062
2	3,00	6,01	6010,00	0,381389804	0,145700282	0,527090086	27,64238708
3	3,00	9,01	9010,00	0,848593992	0,216765999	1,065359991	20,34673734
4	3,00	12,01	12010,00	1,492643581	0,286724141	1,779367722	16,11382165
5	3,00	15,01	15010,00	2,308026785	0,355574708	2,663601493	13,34939588
6	3,05	18,01	18010,00	3,289319084	0,4233177	3,712636784	11,40207686
7	3,05	21,06	21060,00	4,451544666	0,491054323	4,942598989	9,93514392
8	3,05	24,11	24110,00	5,774223201	0,557646144	6,331869345	8,806974901
9	3,05	27,16	27160,00	7,251931784	0,623093163	7,875024947	7,912269067
10	3,05	30,21	30210,00	8,879340739	0,68739538	9,566736119	7,185265397
11	3,05	33,26	33260,00	10,65121361	0,750552795	11,40176641	6,582776458
12	3,05	36,31	36310,00	12,56240718	0,812565408	13,37497259	6,075267835
13	3,05	39,36	39360,00	14,60787145	0,873433219	15,48130467	5,641857952
14	3,05	42,41	42410,00	16,78264965	0,933156227	17,71580588	5,267365391
15	3,05	45,46	45460,00	19,08187823	0,991734434	20,07361266	4,940488047
16	3,05	48,51	48510,00	21,50078688	1,049167839	22,54995472	4,65263834
17	3,05	51,56	51560,00	24,03469851	1,105456442	25,14015495	4,397174336
18	3,05	54,61	54610,00	26,67902926	1,160600242	27,8396295	4,16887819
19	3,05	57,66	57660,00	29,42928849	1,214599241	30,64388773	3,963593822
20	3,05	60,71	60710,00	32,28107879	1,267453437	33,54853223	3,777969865
21	3,05	63,76	63760,00	35,23009598	1,319162832	36,54925881	3,609273826
22	3,05	66,81	66810,00	38,27212911	1,369727424	39,64185654	3,45525549
23	3,05	69,86	69860,00	41,40306045	1,419147215	42,82220767	3,31404496
24	3,05	72,91	72910,00	44,6188655	1,467422203	46,08628771	3,184075516
25	3,05	75,96	75960,00	47,91561299	1,51455239	49,43016538	3,064024524
26	3,05	79,01	79010,00	51,28946486	1,560537774	52,85000264	2,952767637
27	3,05	82,06	82060,00	54,7366763	1,605378356	56,34205466	2,849342939
28	3,05	85,11	85110,00	58,25359572	1,649074136	59,90266986	2,7529226
29	3,05	88,16	88160,00	61,83666475	1,691625115	63,52828987	2,66279026
30	3,05	91,21	91210,00	65,48241825	1,733031291	67,21544954	2,578322845
31	3,05	94,26	94260,00	69,18748431	1,773292665	70,96077698	2,498975829
32	3,05	97,31	97310,00	72,94858424	1,812409237	74,76099348	2,424271204
33	3,05	100,36	100360,00	76,76253259	1,850381007	78,6129136	2,353787593
34	3,05	103,41	103410,00	80,62623713	1,887207975	82,5134451	2,287152079
35	3,05	106,46	106460,00	84,53669885	1,922890141	86,45958899	2,224033405
36	3,05	109,51	109510,00	88,49101197	1,957427505	90,44843947	2,164136293
37	3,05	112,56	112560,00	92,48636394	1,990820067	94,47718401	2,107196661
38	3,05	115,61	115610,00	96,52003544	2,023067826	98,54310327	2,05297759
39	3,05	118,66	118660,00	100,5894004	2,054170784	102,6435712	2,001265896
40	3,05	121,71	121710,00	104,6919259	2,08412894	106,7760548	1,951869212
41	3,05	124,76	124760,00	108,8251723	2,112942294	110,9381146	1,904613488
42	3,05	127,81	127810,00	112,9867932	2,140610845	115,1274041	1,859340843
43	3,05	130,86	130860,00	117,1745355	2,167134595	119,3416701	1,815907716
44	3,05	133,91	133910,00	121,3862391	2,192513542	123,5787526	1,77418326
45	3,05	136,96	136960,00	125,6198373	2,216747688	127,836585	1,734047955
46	3,05	140,01	140010,00	129,8733567	2,239837031	132,1131937	1,695392389
47	3,05	143,06	143060,00	134,1449168	2,261781573	136,4066984	1,658116206
48	3,05	146,11	146110,00	138,4327308	2,282581312	140,7153121	1,622127171
49	3,05	149,16	149160,00	142,7351047	2,30223625	145,037341	1,58734036
50	3,05	152,21	152210,00	147,050438	2,320746385	149,3711844	1,553677434
51	3,05	155,26	155260,00	151,3772232	2,338111718	153,7153349	1,521066014
52	3,05	158,31	158310,00	155,7140463	2,354332429	158,0683785	1,489439109
53	3,05	161,36	161360,00	160,0595863	2,369407979	162,4289943	1,458734624
54	3,05	164,41	164410,00	164,4126155	2,383338906	166,7959544	1,428894912
55	3,05	167,46	167460,00	168,7719995	2,396125031	171,1681245	1,399866381
56	3,05	170,51	170510,00	173,136697	2,407766354	175,5444633	1,371599142
57	3,05	173,56	173560,00	177,50576	2,418262875	179,9240229	1,344046691
58	3,05	176,61	176610,00	181,8783337	2,427614594	184,3059483	1,317165624
59	3,05	179,66	179660,00	186,2536566	2,435821511	188,6894781	1,290915389
60	3,05	182,71	182710,00	190,6310604	2,442883626	193,073944	1,265258054
61	3,05	185,76	185760,00	195,0099698	2,448800939	197,4587708	1,240158099
62	3,05	188,81	188810,00	199,3899032	2,453573449	201,8434766	1,215582238
63	3,05	191,86	191860,00	203,7704717	2,457201158	206,2276729	1,191499242
64	3,05	194,91	194910,00	208,15138	2,459684065	210,6110641	1,167879796
65	3,05	197,96	197960,00	212,5324259	2,46102217	214,9934481	1,144696358
66	4,05	202,01	202010,00	218,3499193	2,461029646	220,8109489	1,114541492

$$w = \frac{q}{24EI} (x^4 - 4x^3l + 6x^2l^2) \quad w = \frac{q}{2GA} (2lx - x^2)$$

$$\begin{aligned} q &= 71,302 \text{ N/mm} \\ E &= 21700 \text{ N/mm}^2 \\ I_{zz} &= 3,05E+15 \text{ mm}^4 \\ G &= 9041,66667 \text{ N/mm}^2 \\ A &= 64080000 \text{ mm}^2 \\ I &= 200000 \text{ mm} \$$

3 Calculations made by Zonneveld ingenieurs

Due to confidentiality, these calculations cannot be displayed.

4 Fault Tree Analysis

