

RUPTURA

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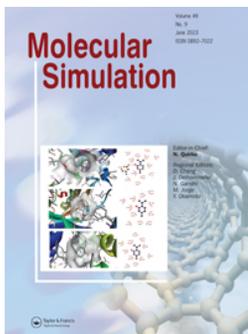
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RUPTURA: simulation code for breakthrough, ideal adsorption solution theory computations, and fitting of isotherm models

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ABSTRACT

We present the RUPTURA code (<https://github.com/iraspa/ruptura>) as a free and open-source software package (MIT license) for (1) the simulation of gas adsorption breakthrough curves, (2) mixture prediction using methods like the Ideal Adsorption Solution Theory (IAST), segregated-IAST and explicit isotherm models, and (3) fitting of isotherm models on computed or measured adsorption isotherm data. The combination with the RASPA software enables computation of breakthrough curves directly from adsorption simulations in the grand-canonical ensemble. RUPTURA and RASPA have similar input styles. IAST is implemented near machine precision but we also provide several explicit mixture prediction methods that are non-iterative and potentially faster than IAST. The code supports a wide variety of isotherm models like Langmuir, Anti-Langmuir, BET, Henry, Freundlich, Sips, Langmuir-Freundlich, Redlich-Peterson, Toth, Unilan, O'Brien & Myers, Asymptotic Temkin, and Bingel & Walton. The isotherm model parameters can easily be obtained by the fitting module. Breakthrough plots and animations of the column properties are automatically generated. In addition to highlighting the code, we also review all the developed techniques from literature for mixture prediction, breakthrough simulations, and isotherm model fitting, and provide a tutorial discussing the workflows.

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Breakthrough; fixed-bed; IAST; isotherm model; RUPTURA

Nomenclature

T	absolute temperature, K
R	universal gas constant, $8.314464919 \text{ J mol}^{-1} \text{ K}^{-1}$
S	entropy, J K^{-1}
V	volume, m^3
L	length of packed bed adsorber, m
m	mass, kg
N	number of molecules, –
N_c	number of components, –
n	number of moles, –
p, p_r	total pressure in the bulk fluid phase, Pa
f	fugacity, Pa
ϕ	fugacity coefficient, –
μ_i	chemical potential of component i , J mol^{-1}
q_i	adsorbed loading of species i , mol (kg framework) ⁻¹
\bar{q}_i	average molar loading of species i , mol (kg framework) ⁻¹
q_i^*	adsorbed loading of pure component i evaluated at the mixture T and Ω , mol (kg framework) ⁻¹
q_r	total loading of the mixture, mol (kg framework) ⁻¹
$q(f)$	absolute loading of the adsorbed phase as a function of fugacity, mol (kg framework) ⁻¹
$q(p)$	absolute loading of the adsorbed phase as a function of pressure, mol (kg framework) ⁻¹
q^{sat}	saturation loading, mol (kg framework) ⁻¹
q_{eq}	equilibrium loading, mol (kg framework) ⁻¹
b	equilibrium constant, Pa^{-1}
θ	fractional loading, –
x_i	mole fraction of species i in the adsorbed phase, –

y_i	mole fraction of component i in the bulk fluid phase, –
t	time, s
v	interstitial gas velocity entering the packed bed, m s^{-1}
ε_b	packed bed void fraction, –
\mathcal{D}	axial dispersion coefficient, $\text{m}^2 \text{ s}^{-1}$
D_m	molecular diffusion coefficient, $\text{m}^2 \text{ s}^{-1}$
D_K	Knudsen diffusion coefficient, $\text{m}^2 \text{ s}^{-1}$
D_s	surface diffusion coefficient, $\text{m}^2 \text{ s}^{-1}$
D_{MS}	Maxwell-Stefan diffusion coefficient, $\text{m}^2 \text{ s}^{-1}$
D_F	Fick diffusion coefficient, $\text{m}^2 \text{ s}^{-1}$
k	mass transfer coefficient, s^{-1}
ρ_b	bed density, kg m^{-3}
	particle density, kg m^{-3}
ρ_f	fluid phase density, kg m^{-3}
Ω	grand potential ($\Omega = U - TS - \sum_i \mu_i N_i$), J (kg framework) ⁻¹
ψ	reduced grand potential ($\psi = -\Omega/(RT)$), mol (kg framework) ⁻¹
Γ	thermodynamic correction factor, –
r_p	particle size, m
GCMC	Grand-Canonical Monte Carlo
PSA	Pressure swing adsorption
TSA	Temperature swing adsorption
SSP-RK	Strong-Stability Preserving Runge-Kutta

Subscripts

i	refers to component i
T	refers to total mixture or pressure

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* indicates a property of the pure component evaluated at the mixture T and Ω

1. Introduction

The separation of mixtures are of extreme importance to chemists and chemical engineers [1]. Adsorption based methods are often implemented for the separation of industrial processes such as separation of hydrocarbons [2], CO₂ capture [3], water purification [4], refrigeration [5], etc. Adsorptive separation processes are divided into two broad categories: (a) continuous flow systems and (b) cyclic batch systems [6]. In a continuous flow system, the fluid phase passes through a fixed bed of solid adsorbents. The capacity of the adsorbents depends on the fluid phase velocity and residence time. To maintain the counter-current contact, the adsorbent must be circulated continuously or the circulation should be mimicked through clever semi-continuous design, e.g. by switching process streams [6]. Such requirements lead to a complex design of the separation system and reduced operational flexibility [6]. An example of such a system is the Simulated Moving Bed (SMB) which is widely used for chromatographic applications [7]. Moving bed systems are designed to regenerate adsorbents by another bed by displacement and this is not a common large-scale industrial adsorption setup. In cyclic batch systems, the bed is alternately saturated and regenerated [6]. Based on the method of regenerating the adsorbent, the cyclic systems can be categorised into: (a) Pressure Swing Adsorption (PSA) and (b) Temperature Swing Adsorption (TSA) [8]. In TSA, the adsorber column is regenerated by heating the bed using a hot stream of non-adsorbing gas. This operation is performed at a temperature at which the adsorbed species desorb from the bed and are carried away along with the stream of hot gas. TSA has been widely used for gas drying and volatile organic compound recovery [8]. In PSA, desorption is achieved by lowering the pressure of the column at a constant temperature which is followed by purging of a non-adsorbing stream of gas to remove the desorbed species [6]. Vacuum Pressure Swing Adsorption (VPSA) is a kind of PSA which is used for hydrogen purification, CO₂ capture, and air separation [8].

PSA is a non-cryogenic gas separation technology that achieves very high purity [9]. Pressure-swing adsorbents are operated in cyclic steady-state consisting of a minimum of two fixed beds with adsorbent, which continuously cycle through four dynamic process steps (Skarstrom cycle [10]): pressurisation, adsorption, blow-down, and desorption. The use of more adsorbent columns improves the outlet gas purity and recovery rate because of the possibility of accommodating more pressure equalisation steps in each PSA cycle [11–13]. Pressure equalisation is a process where gas leaving the first column being depressurised is used to partially pressurise the second adsorbent column [13]. Apart from improving the recovery and purity, this process also reduces the energy consumption. The frequency of regeneration is high in case of PSA adsorption systems [6] and it does not have much impact on the adsorbent structures. These systems are designed based on short cycles [6] (ca. seconds to minutes).

The frequency of regeneration is a crucial factor in designing TSA-based systems. This is because, frequent thermal regeneration processes can adversely affect the adsorbent structure [6]. Therefore, TSA units are typically designed for longer cycles [6] (ca. hours to days) of operation.

Important factors that determine the economics of PSA units are [14]: (1) high selectivity for the adsorption of one component over the other components present in the gas mixture, (2) high working (adsorption) capacity between the conditions of regeneration and adsorption, (3) mild conditions for regeneration (usually induced by pressure or temperature swings), (4) high stability and resistance against impurities and moisture, and (5) fast adsorption kinetics. These factors most often exclude each other, and chemists and materials scientists attempt to find and rationalise the ‘sweet spot’ for designing adsorbents [14]. In particular, in addition to selectivity, working capacity and recyclability (including the kinetics and energy of regeneration) are also key performance parameters [15]. The working capacity is the difference in loading of the preferentially adsorbed component at the adsorption pressure minus the loading at the purge pressure [16]. The adsorptive delivery should be maximised considering the entire adsorption-desorption cycle [17]. Based on this, an optimal enthalpy of adsorption change can be estimated. Experimental screening of potential adsorbent materials for use in PSA services is time consuming. Therefore, computational screening of possible adsorbent materials for their performance factors is crucial.

Adsorption processes in fixed-bed columns are influenced by first order factors (adsorption equilibrium isotherms) and second order factors (kinetics of intra/inter-particle mass/heat transfer, film/heat mass transfer, dispersion, nature of fluid flow, wall heat transfer) [6,19,20]. The performance of adsorbents in fixed-bed adsorbents can be evaluated by performing ‘breakthrough’ simulations. A schematic diagram of fixed-bed adsorber is shown in Figure 1. A fixed bed packed with particles containing porous materials is pressurised and

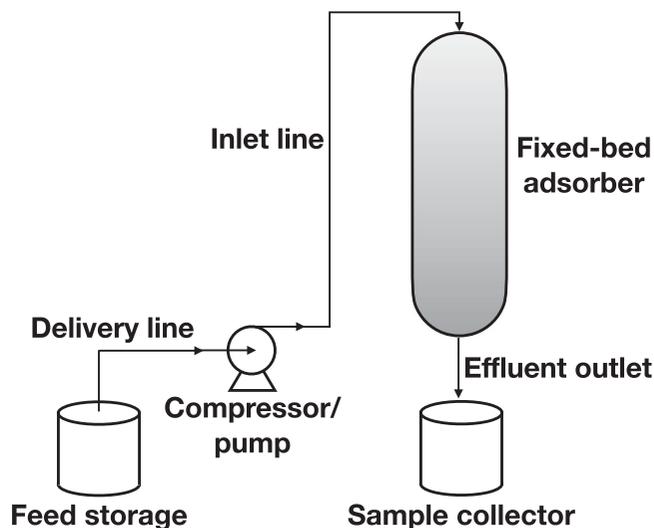


Figure 1. (Colour online) Schematic diagram of fixed-bed adsorber. A peristaltic compressor/pump is used to maintain a constant flow rate. In most gas-phase adsorbents, the gas enters from the top and flows down through the bed, while in a typical liquid system the column fills upwards [18]. The outlet of the bed is connected to a sample collector.

purged with a carrier gas. A fluid is added to the carrier gas and the change of the component concentrations along the column and at the outlet of the fixed bed are recorded. Depending upon process objectives, a fixed-bed operation may be divided into three types: saturation adsorption, elution, and chromatography [20]. For saturation adsorption, a feed solution is passed through a column packed with adsorbents for the purpose of removal of the preferentially adsorbed component. This process continues until the adsorbents become sufficiently saturated, and the solute removal rate diminishes to the extent that termination of operation becomes necessary. Elution (desorption) is a process in which a solvent is passed through a column of adsorbents saturated with solutes. For chromatographic applications, a pulse of the mixture is introduced into a carrier fluid flowing through a column packed with adsorbents [20]. Pulse breakthrough is affected by both adsorption and desorption.

Despite the importance of breakthrough simulations, there is a lack of open-source software to predict breakthrough curves in fixed-bed adsorbers. In this article, we present such a software package named 'RUPTURA'. The code is available under the MIT license and downloadable from github (<https://www.github.com/iraspa/ruptura>). Mixture prediction and breakthrough simulations rely on isotherm models that can be obtained by fitting isotherm data. RASPA [21,22] is a software package for simulating adsorption of molecules in nanoporous materials. The combination with RASPA enables computation of breakthrough curves directly from the pure component adsorption simulations in the grand-canonical ensemble. RUPTURA and RASPA have similar input styles. RUPTURA contains three modules of workflow encountered in this field: (1) the computation of step and pulse breakthrough, (2) the prediction of mixture adsorption (used in the breakthrough equations) based on pure component isotherms, and (3) the fitting of isotherm models on raw (computed or measured) isotherm data. Many isotherm models have been published in the literature [20,23–27]. We included isotherm models like Langmuir, BET, Henry, Freundlich, Sips, Langmuir-Freundlich, Redlich-Peterson, Toth, Unilan, O'Brien & Myers and Asymptotic Temkin, as well as their multi-site versions or combinations of those. The implemented mixture prediction methods are: Ideal Adsorption Solution Theory (IAST) [28], segregated IAST [29], Explicit Isotherm (EI) model [30] and Segregated Explicit Isotherm (SIAS) model [31]. IAST is computed fast and near machine precision. The breakthrough simulations include axial dispersion and the Linear Driving Force (LDF) model for mass-transfer [32], and use a numerically stable method called Strong-Stability Preserving Runge-Kutta (SSP-RK) for the numerical integration [33–37].

We foresee our code being used in (industrial) research for screening adsorbents for separation processes based on PSA, and TSA but also for teaching in chemistry and chemical engineering classes. Hence, in this article we combine the presentation of our code with a review of the underlying theory and methodologies, and a tutorial. The teaching aspect is also the reason why the numerical schemes and fitting procedure are described in detail. The tutorial aspect also implied that we aim to make our code as easy to use as

possible, and that the generation of breakthrough pictures and movies is automatic. It is also vital that researchers and students would be able to play around with examples that run in the order of minutes. This is interactive enough to investigate the effect of adsorption, axial dispersion, mass-transfer coefficients, column void fraction, flow velocity, and column length on the breakthrough and separation efficiency. To achieve even higher computational speed, we included isotherm models of explicit nature (EI and SEI) that, although limited to Langmuir behaviour, work for any number of components [30].

Our article is organised as follows. We begin by explaining models for pure component isotherms (Section 2) and discuss the methodology to predict mixture results from pure component isotherm in Section 3. Such methodologies include IAST and we detail our implementation and validate it by comparing it to previous work. Section 4 contains the theory on breakthrough simulations and our detailed numerical implementation. In Section 5, we focus on our genetic-algorithm implementation of isotherm fitting. We close our article with a description of the installation instructions (Section 6), the input format and options (Section 7), a tutorial (Section 8), and a troubleshooting section (Section 9). Our main findings are summarised in Section 10.

2. Isotherm models

2.1. Introduction

Adsorption is a surface process that involves the transfer of a molecule from a bulk fluid to a solid surface. Physical adsorption is caused by Van der Waals forces (includes dipole–dipole, dipole-induced dipole, London forces, and possibly hydrogen bonding) [38,39]. An *adsorbate* is a molecule adsorbed on the surface of the solid material, and the solid material is referred to as the *adsorbent*. An adsorption process is the addition of adsorbate to the adsorbent by increasing the adsorptive pressure, while desorption is the removal of adsorbate from the adsorbent by decreasing the adsorptive pressure or/and increasing the temperature [39,40]. Experimental adsorption data are routinely reported as *net* or *excess* amounts adsorbed, while simulations such as molecular simulations measure *absolute* adsorption. The excess adsorbed amount refers to the difference between the actual (absolute) amount adsorbed and the amount that would be present in the same volume at the density of the fluid in the bulk phase [41,42]. The net adsorbed amount has a reference state that does not require the knowledge of the adsorbent volume, and the solid and adsorbed phase are being treated as an entity [43]. Statistical thermodynamic theories and molecular simulations of adsorption of gases on porous solids are formulated in the language of absolute thermodynamic variables [44].

The fundamental concept in adsorption science is the adsorption isotherm, i.e. the equilibrium relation between the quantity of the adsorbed material and the pressure or concentration in the bulk fluid phase at constant temperature [40]. Mathematically, we can describe absolute adsorption of an adsorbate on an adsorbent with a smooth, continuous function $q(c_i)$ that represents the dependency of the adsorbed phase

concentration q_i of a component i on the fluid phase concentrations c_i

$$q_i = q(c_1, c_2, \dots, c_{N_c}) \quad \text{at constant } T \quad (1)$$

Common units for the loading q include mol/(kg framework) and mg/(mg framework) with $q \geq 0$. For a single component system, we generally have $dq/dp \geq 0$. The adsorption of a component depends not only on the concentration of this component, c_i , but also on the equilibrium concentrations of all other components. Likewise, we could describe adsorption from an ideal gas phase by substituting the fluid phase concentrations by partial pressures in the gas phase

$$q_i = q(p_1, p_2, \dots, p_{N_c}) \quad \text{at constant } T \quad (2)$$

The adsorption equilibrium of a single adsorbate can be described by the adsorption isotherm

$$q = q(p) \quad \text{at constant } T \quad (3)$$

In general, an increase in the temperature will lead to a decreased amount adsorbed at a given pressure. In case the isotherm model has a well-defined saturation loading q^{sat} , a fractional loading θ can be defined

$$\theta(p) = \frac{q(p)}{q^{\text{sat}}} \quad (4)$$

The Henry coefficient H_K for adsorption is defined as

$$H_K = \lim_{p \rightarrow 0} \frac{q(p)}{p} = \lim_{p \rightarrow 0} \frac{dq}{dp} \quad (5)$$

The Henry coefficient is the slope of the isotherm at very low pressure. In this infinite dilution regime, there are no adsorbate-adsorbate interactions, and adsorption is linearly related to the affinity of the adsorbate. Note that the Henry coefficient depends on temperature.

2.2. Isotherm models

Isotherm models are well described in various resources [20,23–27]. New isotherm models continue to be developed. For example, the new Bingle-Walton isotherm model allows for a continuous, mathematical description of general type V isotherms, which appear in novel flexible MOFs or many water adsorption cases [45]. We will describe some of the isotherm models that are implemented in RUPTURA. The mathematical description for the functional form, the Henry coefficient, the saturation value, and the order of input of the arguments in the code are summarised in Table 1. The derived formulas for the inverse of the isotherm are listed in Table 2.

2.2.1. Langmuir model

The Langmuir equation is the cornerstone of all theories of adsorption. Langmuir (1918) was the first to propose a coherent theory of adsorption onto a flat surface based on a kinetic viewpoint [46]. The assumptions of the Langmuir model are:

- (1) The surface is homogeneous: all adsorption sites are energetically identical.
- (2) The adsorption is localised: one molecule per adsorption site (monolayer).
- (3) There are no lateral interactions between adsorbed molecules.

These assumptions are often true for chemisorption. Using these assumptions, the Langmuir isotherm can be derived as:

$$q(p) = q^{\text{sat}} \frac{bp}{1+bp} \quad q^{\text{sat}} \geq 0, b > 0 \quad (6)$$

where q^{sat} is the saturation capacity and b is the coefficient of adsorption representing the affinity of the molecule. In the limit of high pressure, the isotherm will approach q^{sat} . At

Table 1. Isotherm models, Henry and saturation regime, and the order of input of the arguments in RUPTURA.

Model	Equation	Henry	saturation	b_0	b_1	b_2
Langmuir [46]	$q(p) = q^{\text{sat}} \frac{bp}{1+bp}$	bq^{sat}	q^{sat}	q^{sat}	b	
n -site Langmuir	$q(p) = \sum_i q_i^{\text{sat}} \frac{b_i p}{1+b_i p}$	$\sum_i b_i q_i^{\text{sat}}$	$\sum_i q_i^{\text{sat}}$	q^{sat}	b	
BET [47]	$q(p/p^0) = q^{\text{sat}} \frac{b(p/p^0)}{(1-c(p/p^0))(1-c+b(p/p^0))}$	$\frac{bq^{\text{sat}}}{1-c}$	$\frac{bq^{\text{sat}}}{(1-c)(1-c+b)}$	q^{sat}	b	c
Anti-Langmuir [24]	$q(p) = \frac{ap}{1-bp}$	a	X	a	b	
Henry	$q(p) = ap$	a	X	a		
Freundlich [48]	$q(p) = ap^{1/\nu}$	X	X	a	ν	
Sips [49]	$q(p) = q^{\text{sat}} \frac{(bp)^{1/\nu}}{1+(bp)^{1/\nu}}$	X	q^{sat}	q^{sat}	b	ν
n -site Sips	$q(p) = \sum_i q_i^{\text{sat}} \frac{(b_i p)^{1/\nu_i}}{1+(b_i p)^{1/\nu_i}}$	X	$\sum_i q_i^{\text{sat}}$	q^{sat}	b	ν
Langmuir-Freundlich [50]	$q(p) = q^{\text{sat}} \frac{bp^\nu}{1+bp^\nu}$	X	q^{sat}	q^{sat}	b	ν
n -site Langmuir-Freundlich	$q(p) = \sum_i q_i^{\text{sat}} \frac{b_i p_i^\nu}{1+b_i p_i^\nu}$	X	$\sum_i q_i^{\text{sat}}$	q^{sat}	b	ν
Redlich-Peterson [51]	$q(p) = \frac{ap}{1+bp^\nu}$	a	X	a	b	ν
Toth [52–54]	$q(p) = q^{\text{sat}} \frac{bp}{[1+(bp)^\nu]^{1/\nu}}$	bq^{sat}	q^{sat}	q^{sat}	b	ν
Unilan	$q(p) = q^{\text{sat}} \frac{1}{2\eta} \ln \left[\frac{1+be^\eta p}{1+be^{-\eta} p} \right]$	bq^{sat}	q^{sat}	q^{sat}	b	η
O'Brien & Myers [55]	$q(p) = q^{\text{sat}} \left[\frac{bp}{1+bp} + \sigma^2 \frac{bp(1-bp)}{2(1+bp)^2} \right]$	$q^{\text{sat}} b(1 + \frac{\sigma^2}{2})$	q^{sat}	q^{sat}	b	σ
Quadratic [56,57]	$q(p) = q^{\text{sat}} \frac{bp+2cp^2}{1+bp+cp^2}$	bq^{sat}	$2q^{\text{sat}}$	q^{sat}	b	c
Asymptotic Temkin [58,59]	$q(p) = q^{\text{sat}} \frac{bp}{1+bp} + q^{\text{sat}} \theta \left(\frac{bp}{1+bp} \right)^2 \left(\frac{bp}{1+bp} - 1 \right)$	bq^{sat}	q^{sat}	q^{sat}	b	θ
Bingle & Walton [45]	$q(p) = q^{\text{sat}} \frac{1 - \exp[-(a+b)p]}{1+(b/a) \exp[-(a+b)p]}$	aq^{sat}	q^{sat}	q^{sat}	a	b

Table 2. Isotherm models and their inverse.

Model	inverse
Langmuir	$p(q) = \frac{q}{b(q^{\text{sat}} - q)}$
<i>n</i> -site Langmuir	numerical
BET	$p(q) = \frac{-bq^{\text{sat}} + bq - cq + c^2q \pm \sqrt{4bcq(q-cq) + (-bq^{\text{sat}} + bq - cq + c^2q)^2}}{2bcq}$
Anti-Langmuir	$p(q) = \frac{q}{(a+bq)}$
Henry	$p(q) = q/a$
Freundlich	$p(q) = \left(\frac{q}{a}\right)^\nu$
Sips	$p(q) = \frac{1}{b} \left(\frac{q}{q^{\text{sat}} - q}\right)^\nu$
<i>n</i> -site Sips	numerical
Langmuir-Freundlich	$p(q) = \left(\frac{q}{q^{\text{sat}}b - qb}\right)^{1/\nu}$
<i>n</i> -site Langmuir-Freundlich	numerical
Redlich-Peterson	numerical
Toth	$p(q) = \frac{q}{(q^{\text{sat}}b - qb)^{1/\nu}}$
Unilan	$p(q) = \frac{e^{\eta} (\exp(\frac{2\eta q}{q^{\text{sat}}}) - 1)}{b(e^{2\eta} - \exp(\frac{2\eta q}{q^{\text{sat}}}))}$
O'Brien & Myers	not shown here
Quadratic	$p(q) = \frac{-bq^{\text{sat}} + bq \pm \sqrt{(bq^{\text{sat}} - bq)^2 + 4q(2cq^{\text{sat}} - cq)}}{2(2cq^{\text{sat}} - cq)}$
Asymptotic Temkin	not shown here
Bingel & Walton [45]	numerical

Notes: The inverse of the O'Brien & Myers and Temkin model are too long to write down here, but can easily be computed symbolically using Mathematica. Note that multi-site combinations will always need to be computed numerically.

very low pressures, we obtain Henry's law, with a Henry coefficient of bq^{sat} .

The bi-Langmuir suggested by Graham [60] is the simplest model for adsorption onto a non-homogeneous surface [24]

$$q(p) = q_1^{\text{sat}} \frac{b_1 p}{1 + b_1 p} + q_2^{\text{sat}} \frac{b_2 p}{1 + b_2 p} \quad (7)$$

in which the subscripts refer to the two adsorption sites. In general, a heterogeneous surface with several distinct types of homogeneous adsorption sites can be modeled with an *n*-site model:

$$q(p) = \sum_{i=1}^n q_i^{\text{sat}} \frac{b_i p}{1 + b_i p} \quad (8)$$

with a saturation value $\sum_i q_i^{\text{sat}}$ and Henry coefficient value $\sum_i b_i q_i^{\text{sat}}$. Multi-site models are required to model isotherms with inflections ('kinks'). Molecular simulations were able to explain the molecular origins of inflections in isotherms by examining the locations of molecules as a function of pressure [61,62].

2.2.2. Anti-Langmuir model

The anti-Langmuir model describes the behaviour where with increased concentration or pressure, the adsorbed loading increases towards infinity [63]. At very low concentration or pressure, this model obeys Henry's law. The anti-Langmuir isotherm expression reads [24,63]:

$$q(p) = \frac{ap}{1 - bp} \quad 0 \leq p \leq 1/b, \quad b \geq 0 \quad (9)$$

In Equation (9), *a* represents the Henry coefficient in mol kg⁻¹ Pa⁻¹ and *b* is the equilibrium constant in Pa⁻¹. The anti-Langmuir model does not have a saturation loading as the maximum loading can increase up to infinity at pressure or concentration equal to 1/*b*.

2.2.3. Henry model

All isotherms should in principle converge to Henry's law at infinite dilution. In the Henry's regime, the amount adsorbed is proportional to the pressure. The Henry's isotherm model is described by

$$q(p) = ap \quad (10)$$

where *a* is the energetic constant (Henry constant), and only depends on temperature.

2.2.4. BET model

The Brunauer, Emmett, and Teller (BET) model extends adsorption to multi-layers [47]:

$$q(p) = q^{\text{sat}} \frac{b_s(p)}{(1 - b_l(p))(1 - b_l + b_s(p))} \quad (11)$$

where *b_s* and *b_l* are the equilibrium constants of adsorption on the bare surface and on a layer of previously adsorbed adsorbates, respectively. Similar to the Langmuir model, it is derived from kinetic adsorption-desorption relations. The assumptions made in this model are:

- (1) Each molecule in the first adsorbed layer provides an adsorption site for the second layer, and so on.
- (2) Molecules in the second and subsequent layers are assumed to behave essentially as those in the bulk liquid.

2.2.5. Freundlich model

Boedeker proposed the following empirical isotherm equation [48]

$$q(p) = ap^{1/\nu} \quad (12)$$

for the adsorption of polar compounds on polar adsorbents, where the exponent 1/*ν* is smaller than unity. It has been popularised by Freundlich and therefore known as the Freundlich isotherm. The Freundlich isotherm can be considered a composite of Langmuir isotherms with different *b* values representing patches of adsorption sites with different adsorption energies [64]. It was shown that summing up a number of Langmuir isotherms leads to Freundlich-type isotherms [65]. The isotherm model can describe adsorption on many heterogeneous surfaces well. However, the model is unable to describe any plateauing trend and also does not have a Henry's regime (in fact, the initial slope is infinite). As a result, some authors have mentioned that this isotherm type is unsuitable for the calculation of the reduced grand potential and other thermodynamic properties [66].

2.2.6. Sips model

Sips proposed an equation similar in form to the Freundlich equation, but it has a finite limit when the pressure is sufficiently high [49]:

$$q(p) = q^{\text{sat}} \frac{(bp)^{1/\nu}}{1 + (bp)^{1/\nu}} \quad (13)$$

In this model, the additional parameter ν is a parameter characterising the heterogeneity of the system. The theoretical basis of the equation is described in the book of Do [23]. There also exists a multi-site form

$$q(p) = \sum_i q_i^{\text{sat}} \frac{(b_i p)^{1/\nu_i}}{1 + (b_i p)^{1/\nu_i}} \quad (14)$$

The Sips isotherm does not have the correct limiting behaviour at low pressure, i.e. it does not have a Henry's regime (Equation (5) diverges), except when $\nu = 1$.

2.2.7. Langmuir-Freundlich model

The Langmuir-Freundlich model is given by [50]

$$q(p) = q^{\text{sat}} \frac{b p^\nu}{1 + b p^\nu} \quad (15)$$

and has the combined form of Langmuir and Freundlich equations. The constant ν is often interpreted as the heterogeneity factor. Values of unity indicate a material with homogeneous binding sites and the isotherm model reduces to the Langmuir model. There also exists a multi-site form

$$q(p) = \sum_i q_i^{\text{sat}} \frac{b_i p^{\nu_i}}{1 + b_i p^{\nu_i}} \quad (16)$$

The Langmuir-Freundlich isotherm does not have the correct limiting behaviour at low pressure, i.e. it does not have a Henry's regime, except when $\nu = 1$.

2.2.8. Redlich-Peterson model

The Redlich-Peterson isotherm is an empirical isotherm mix of the Langmuir and Freundlich isotherms. The numerator is the same as the Langmuir isotherm and has the advantage of possessing a Henry region at infinite dilution [51]

$$q(p) = \frac{a p}{1 + b p^\nu} \quad (17)$$

The parameter a can not be interpreted as the saturation loading, except when $\nu = 1$ [64].

2.2.9. Toth model

The previous isotherm models have their limitations. The Freundlich, Sips, and Langmuir-Freundlich equations are not valid at very low pressures, while the Henry, Freundlich, and Redlich-Peterson model do not have a finite saturation value. One of the empirical equations that is popularly used and satisfies the two end limits is the Toth equation [52–54]:

$$q(p) = q^{\text{sat}} \frac{b p}{[1 + (b p)^\nu]^{1/\nu}} \quad (18)$$

The Toth equation has been used for fitting data of many adsorbates such as hydrocarbons, carbon oxides, hydrogen sulfide, alcohols on activated carbon, and zeolites [23].

2.2.10. Unilan model

The Unilan model owns its name from UNI, for Uniform distribution and LAN, for Langmuir local model [23]. The Unilan

model is described by

$$q(p) = q^{\text{sat}} \frac{1}{2\eta} \ln \left[\frac{1 + b e^\eta p}{1 + b e^{-\eta} p} \right] \quad (19)$$

η is a measurement of the heterogeneity of the adsorbent. High values indicate a highly heterogeneous system. Being a three-parameter model, also the Unilan equation is very often used to describe many data of hydrocarbons, carbon oxides on activated carbon and zeolites. The Unilan equation has the correct behaviour at low and high pressures. In the limit of $\eta = 0$ the Langmuir isotherm is recovered.

2.2.11. O'Brien & Myers

The O'Brien and Myers isotherm model is obtained as a truncation to two terms of a series expansion of the adsorption integral equation in terms of the central moments of the adsorption energy distribution [23,55]

$$q(p) = q^{\text{sat}} \left[\frac{b p}{1 + b p} + \sigma^2 \frac{b p (1 - b p)}{2(1 + b p)^3} \right] \quad (20)$$

where σ is a measure of the width of the adsorption energy distribution.

2.2.12. Quadratic model

Statistical thermodynamics suggests that the general form of an isotherm equation should be the ratio of two polynomials of the same degree [57]. The polynomial Langmuir isotherm model, derived from statistical mechanics, reads:

$$q(p) = q^{\text{sat}} \frac{b p + c p^2 + d p^3 + \dots}{1 + b p + c p^2 + d p^3 + \dots} \quad (21)$$

In practise, the second order isotherm is often used, called the quadratic isotherm model [56,57]

$$q(p) = q^{\text{sat}} \frac{b p + 2c p^2}{1 + b p + c p^2} \quad (22)$$

The loading is convex at low pressures but changes concavity as it saturates, yielding an S-shape, i.e. the isotherm exhibits an inflection point.

2.2.13. Asymptotic approximation to the Temkin model

The Temkin isotherm is derived using a mean-field arguments and asymptotic approximation [58,59]

$$q(p) = q^{\text{sat}} \frac{b p}{1 + b p} + q^{\text{sat}} \theta \left(\frac{b p}{1 + b p} \right)^2 \left(\frac{b p}{1 + b p} - 1 \right) \quad (23)$$

Here, q^{sat} and b have the same meaning as in the Langmuir isotherm, and θ describes the strength of adsorbate-adsorbate interactions ($\theta < 0$ for attraction).

2.2.14. Bingel & Walton model

The Bingel and Walton isotherm model allows for a continuous, mathematical description of general type V isotherms, which appear in novel flexible MOFs or many water adsorption cases [45]. The model is based on the Bass model of innovation diffusion developed in the late 1960s [67]. This model describes the adoption and diffusion of an invention over

time and has been widely used in market sales and technology forecasting. Bingel and Walton applied the Bass model to adsorption, where early-adopters can be seen as the intrinsic high-affinity adsorption sites of the surface. The word-of-mouth contribution of slower innovations refers to adsorption mechanisms that are mainly driven by molecules of the same species that are already adsorbed and thus present in the adsorbed phase. The Bingel-Walton adsorption equation reads [45]

$$q(p) = q^{\text{sat}} \frac{1 - \exp[-(a+b)p]}{1 + (b/a) \exp[-(a+b)p]} \quad (24)$$

where $a > 0$ is the intrinsic adsorption affinity between the adsorbate and the adsorbent, and b is the clustering coefficient describing strong adsorbate-adsorbate interactions. The simple model combines the effects of early-adopters and word-of-mouth, resulting in curves that resemble either the type I adsorption isotherm shape or S-shaped curves. The location of the inflection point is $\log(b/a)/(a+b)$. For small values of a and large values of b the isotherm shape becomes strongly step-wise. In the limit of $b \rightarrow 0$ the isotherm becomes an exponential function

$$q(p) = q^{\text{sat}}(1 - \exp[-ap]) \quad (25)$$

while in the limit of $a \rightarrow 0$ the adsorption becomes zero. In the limit of $b \rightarrow -a$, the isotherm reduces to the Langmuir model

$$q(p) = q^{\text{sat}} \frac{ap}{1 + ap} \quad (26)$$

The model has a Henry coefficient of aq^{sat} and a saturation loading of q^{sat} .

2.3. Reduced grand potential

Thermodynamics is the study of energy and its transformations but more generally tries to establish relationships between basic concepts like internal energy U , entropy S , number of particles N , volume V , temperature T , pressure p , and chemical potential μ to describe the behavior of matter and make predictions. For the mixture vapour-liquid equilibrium, the Gibbs-Duhem equation [68]

$$SdT - Vdp + \sum_i n_i d\mu_i = 0 \quad (27)$$

shows that the independent variables which define the standard states for the components of the mixture are T and p . We can compare the Gibbs-Duhem equation to the differential for a solid material [69]

$$SdT + d\Omega + \sum_i n_i d\mu_i = 0 \quad (28)$$

and see that the standard states for mixture adsorption will be determined by T and Ω [69]. The grand potential Ω is the characteristic state function for the grand-canonical ensemble and the unit of Ω is J/(kg framework). At constant

temperature, we have

$$d\Omega = -SdT - \sum_i n_i d\mu_i = - \sum_i n_i d\mu_i \quad (29)$$

which is the 'Gibbs adsorption' equation. Replacing chemical potential μ_i by the fugacity f_i

$$d\Omega = -RT \sum_i n_i d \ln \left[\frac{f_i}{f_0} \right] \quad (30)$$

where f_0 is a reference fugacity to make the argument of the logarithm dimensionless. Replacing fugacity by pressure and integrating for pure-component adsorption from the unadsorbed state at zero pressure, we obtain the grand potential Ω [6,44,70,71]

$$\begin{aligned} \Omega_i &= -RT \int_0^{p_i^*} q_i^*(p) d \ln(p) \\ \text{or } \Omega_i &= -RT \int_0^{p_i^*} \frac{q_i^*(p)}{p} dp \end{aligned} \quad (31)$$

where $q_i^*(p)$ is the loading of pure component i given as a function of the pressure. Physically, the grand potential is the free energy change associated with isothermal immersion of fresh adsorbent in the bulk fluid. The absolute value of the grand potential is the minimum isothermal work necessary to clean the adsorbent [72]. In calculations, it is convenient to introduce a reduced grand potential ψ [69]:

$$\psi(p_i^*) \equiv - \frac{\Omega_i}{RT} = \int_0^{p_i^*} \frac{q_i^*(p)}{p} dp \quad (32)$$

The reduced grand potential has units of mol/kg. The integration limit p_i^* is a property of the pure component property, i.e. it is the pressure at a given reduced grand potential. This quantity is known as the sorption pressure (in analogy to the saturation pressure in vapour-liquid equilibrium) and also as the hypothetical pressure. Importantly, the reduced grand potential is defined in terms of absolute adsorption and can be computed from the adsorption isotherm. In Tables 3 and 4 we list the derived expressions for the reduced grand potential and the sorption pressure (the inverse of the reduced grand potential), respectively, for the various isotherm models.

3. Prediction of mixture isotherms

3.1. Introduction

A key point in adsorption process development is knowledge on multi-component adsorption equilibria [19]. Experimental methods for (mixture) gas adsorption are recently reviewed by Shade et al. [81]. Direct measurement of mixture adsorption equilibria remains complicated and time consuming, and mixture adsorption prediction using theoretical models is still the default tool [82]. These theoretical models can be validated by explicit grand-canonical Monte Carlo simulations [83] for mixture adsorption.

One of the commonly used model is the extended Langmuir which was developed by Butler and Ockrent [84] to describe competitive adsorption. For an N_c component mixture, the

Table 3. Reduced grand potential for isotherm models.

Model	reduced grand potential $\psi(p)$
Langmuir [23]	$\psi(p) = q^{\text{sat}} \ln [1 + bp]$
n -site Langmuir [23]	$\psi(p) = \sum_i q_i^{\text{sat}} \ln [1 + b_i p]$
BET [63]	$\psi(p) = q^{\text{sat}} \ln \left[\frac{1+bp-cp}{1-cp} \right]$
Anti-Langmuir [24]	$\psi(p) = -\frac{a}{b} \ln [1 - bp]$
Henry	$\psi(p) = ap$
Freundlich [23]	$\psi(p) = avp^{1/\nu}$
Sips [23]	$\psi(p) = q^{\text{sat}} \nu \ln [1 + (bp)^{1/\nu}]$
n -site Sips	$\psi(p) = \sum_i q_i^{\text{sat}} \nu \ln [1 + (b_i p)^{1/\nu_i}]$
Langmuir-Freundlich [73]	$\psi(p) = \frac{q^{\text{sat}}}{\nu} \ln [1 + bp^\nu]$
n -site Langmuir-Freundlich	$\psi(p) = \sum_i \frac{q_i^{\text{sat}}}{\nu_i} \ln [1 + b_i p^{\nu_i}]$
Redlich-Peterson [74,75]	$\psi(p) = ap {}_2F_1(1, 1/\nu, 1 + 1/\nu, -bp^\nu)$ ($bp^\nu < 1$)
	$= \frac{a}{\nu b^{1/\nu}} \left[\frac{\pi}{\sin(\pi/\nu)} + \sum_{k=1}^{\infty} (-1)^k \left(\frac{1}{bp^\nu} \right)^{k-1/\nu} \frac{1}{k-1/\nu} \right]$ ($bp^\nu > 1$)
Toth [73,76]	$\psi(p) = q^{\text{sat}} bq {}_2F_1(1/\nu, 1/\nu, 1 + 1/\nu, -(bp)^\nu)$ ($bp^\nu < 1$)
	$= q^{\text{sat}} \left(\theta - \frac{\theta}{\nu} \ln [1 - \theta^\nu] - \sum_{k=1}^{\infty} \frac{\theta^{k\nu+1}}{k\nu[k\nu+1]} \right)$
Unilan [73]	$\psi(p) = q^{\text{sat}} \frac{1}{2\eta} (\text{Li}_2(-be^{-\eta}p) - \text{Li}_2(-be^{\eta}p))$
O'Brien & Myers [23,74]	$\psi(p) = q^{\text{sat}} \left[\ln [1 + bp] + \frac{\sigma^2 bp}{2(1+bp)^2} \right]$
Quadratic [63]	$\psi(p) = q^{\text{sat}} \ln [1 + bp + cp^2]$
Asymptotic Temkin [77]	$\psi(p) = q^{\text{sat}} \left(\ln [1 + bp] - \frac{1}{2} \theta \left(\frac{bp}{1+bp} \right)^2 \right)$
Bingel & Walton [45]	numerical

Notes: The potentials are additive for multi-site models. Note that our expression for the Unilan is the same as Santori et al. [73] but several terms in their expression actually cancel out. Note that the expression for Asymptotic Temkin of Simon et al. [77] contains typos. The dilogarithm function (Li_2) defined by the power series $\text{Li}_2(z) = \sum_{n=1}^{\infty} \frac{z^n}{n^2}$ $|z| < 1$. In RUPURA, we use the freely available implementation by Alexander Voigt [78]. The hypergeometric function ${}_2F_1$ defined by the power series for $|z| < 1$ [79] ${}_2F_1(a, b; c; z) = \sum_{k=0}^{\infty} \frac{(a)_k (b)_k}{(c)_k} \frac{z^k}{k!}$ where $(q)_k$ is the (rising) Pochhammer symbol. The hypergeometric function can be computed by e.g. Gosper's algorithm [80]. Note that the computation of the reduced grand potential for Redlich-Peterson and Toth isotherms is hence computationally much more expensive than for the other isotherm models.

Table 4. Sorption pressures for isotherm models.

Model	sorption pressure $p^*(\psi)$
Langmuir	$p^*(\psi) = \frac{1}{b} (\exp[\psi/q^{\text{sat}}] - 1)$
n -site Langmuir	numerical
BET	numerical
Anti-Langmuir	$p^*(\psi) = \frac{1}{b} (1 - \exp[-\psi b/a])$
Henry	$p^*(\psi) = \frac{\psi}{a}$
Freundlich	$p^*(\psi) = \left(\frac{\psi}{av} \right)^\nu$
Sips	$p^*(\psi) = \frac{1}{b} \left(\exp \left[\frac{\psi}{\nu q^{\text{sat}}} \right] - 1 \right)^\nu$
n -site Sips	numerical
Langmuir-Freundlich	$p^*(\psi) = \left(\frac{\exp[\nu\psi/q^{\text{sat}}] - 1}{b} \right)^{1/\nu}$
n -site Langmuir-Freundlich	numerical
Redlich-Peterson	numerical
Toth	numerical
Unilan	numerical
O'Brien & Myers	numerical
Quadratic	$p^*(\psi) = \frac{-b \pm \sqrt{b^2 - 4c + 3c \exp[\psi/q^{\text{sat}}]}}{2c}$
Asymptotic Temkin	numerical
Bingel & Walton	numerical

Notes: Models with an analytical inverse for the reduced grand potential are an order of magnitude faster than models that have to be numerically inverted.

adsorption of component i reads [84]

$$q_i = \frac{q_i^{\text{sat}} b_i p_i}{1 + \sum_{j=1}^{N_c} b_j p_j} \quad (33)$$

The extended Langmuir is only dynamically consistent when all components have the same saturation value [85]. If not, the extended Langmuir is only empirical in nature. Jain and Snoeyink [86] proposed an extension of the Langmuir equation for binary mixtures that is based on the assumption that only a fraction of the adsorption sites that are available for a component can also be occupied by the other component.

$$q_1 = \frac{(q_1^{\text{sat}} - q_2^{\text{sat}}) b_1 p_1}{1 + b_1 p_1} + \frac{q_2^{\text{sat}} b_1 p_1}{1 + b_1 p_1 + b_2 p_2} \quad (34)$$

$$q_2 = \frac{q_2^{\text{sat}} b_2 p_2}{1 + b_1 p_1 + b_2 p_2} \quad (35)$$

Many extensions of the Langmuir, Freundlich, Toth, and Redlich-Peterson equations have been developed to model mixture adsorption isotherms [64]. A thermodynamic framework for computing the mixture adsorption is the Ideal Adsorption Solution Theory (IAST) developed by Myers and Prausnitz [28]. For systems following the Langmuir isotherm, IAST is identical to the extended Langmuir equation for mixtures, if the saturated amounts are equal [87]. IAST is a predictive model which uses only the pure component data (it does not require any mixture data), is thermodynamically consistent, and is independent of the actual model of physical adsorption [88]. Even after 50 years of its development, IAST continues its role as a benchmark method in describing mixture adsorption [82]. The applicability of IAST continues to be evaluated on novel materials [89–91] and for special circumstances, for example adsorption in the presence of framework deformations [92]. Gharagheizi and Sholl recently evaluated IAST on more than 400 examples in which binary adsorption data and single-component data are available in the same publication [93]. Other implicit multi-component adsorption models are [37]: Vacancy Solution Theory (VST) [94], Real Adsorption Solution Theory (RAST) [95,96], Spreading Pressure Dependent equation (SPD) [97], Predictive Real Adsorption Solution Theory (PRAST) [98], Multi-component Potential Adsorption Theory (MPAT) [99], Segregated Ideal Adsorbed Solution Theory (SIASST) [29], and Generalized Predictive Adsorbed Solution Theory (GPAST) [100].

3.2. Ideal adsorption solution theory (IAST)

Myers and Monson applied solution thermodynamics to adsorption in porous materials leading to equations similar to those for vapour-liquid equilibria [69]. In IAST calculations, the central quantity is the reduced grand potential ψ_i :

$$\psi_i(f_i^*) = \int_0^{f_i^*} \frac{q_i^*(f)}{f} df \quad (36)$$

The reduced grand potential has units of mol/kg. This quantity is related to the spreading pressure (Π) (or solid-fluid

interfacial tension) which is analogous to pressure but in two dimensions [77]. The relation between reduced grand potential and spreading pressure is as follows [77]:

$$\psi(f_i^*) = \frac{\Pi A}{RT} \quad (37)$$

In Equation (37), A is the area of the adsorbent in m^2 . The spreading pressure was used in early IAST work based on quasi two-dimensional adsorption at a planar surface using the Gibbs excess formalism [28], but is replaced with the reduced grand potential in the more recent IAST work based on thermodynamics of adsorption in a three-dimensional pore network [69]. Equations written in the language of solution thermodynamics have been derived without any discussion of a dividing surface, Gibbs excess, or spreading pressure and lead to equations similar to those for vapour-liquid equilibria [69].

Following the excellent detailed descriptions of IAST by Murthi and Snurr [70] and Myers and Monson [69], for a fluid at constant temperature, we have [101]

$$d\mu_i = RT d \ln \left[\frac{f_i}{f^0} \right] \quad (38)$$

In Equation (38), f^0 is the reference fugacity which is considered to be equal to 1 bar. Integrating this equation at constant T and Ω from a state of pure i to a state at an arbitrary mole fraction [70]

$$\mu_i(T, \Omega, x) - \mu_i^*(T, \Omega, x) = RT \ln \frac{f_i(T, \Omega, x)}{f_i^*(T, \Omega, x)} \quad (39)$$

where the superscript $*$ indicates a property of the pure component evaluated at the mixture T and Ω , and f_i is the fugacity of component i in the adsorbed phase. The proposed definition of an ideal solution for adsorption in porous materials is [69]:

$$\mu_i^{\text{id}}(T, \Omega, x) - \mu_i^{\text{id},*}(T, \Omega, x) \equiv RT \ln x_i \quad (40)$$

Equation (40) is equivalent to the equation of the chemical potential of an ideal solution in the bulk. It is the only assumption needed in the Ideal Adsorption Solution Theory (IAST) of Myers and Prausnitz [28]. Using $\mu = \mu^{\text{id}} + \mu^{\text{ex}}$ and subtracting Equation (40) from Equation (39) yields

$$\mu_i^{\text{ex}} = RT \ln \frac{f_i(T, \Omega, x)}{x_i f_i^*(T, \Omega)} \quad (41)$$

$$= RT \ln \gamma_i \quad (42)$$

since the argument of the logarithm is defined as the activity coefficient (γ_i) of component i and we have [70]

$$f_i(T, \Omega, x) = \gamma_i x_i f_i^*(T, \Omega) \quad (43)$$

The phase equilibrium (iso-fugacity) condition is expressing that the fugacity of a component in the gas phase ($f_i^{(g)}$) is in equilibrium with the mixture at the specified T and Ω

$$f_i^{(g)}(T, P, y) = \gamma_i x_i f_i^*(T, \Omega) \quad (44)$$

This equation may be rewritten in terms of the pressure by replacing the fugacity (f_i) with $y_i \phi_i P$

$$y_i \phi_i P = \gamma_i x_i f_i^* \quad (45)$$

where ϕ is the fugacity coefficient in the fluid phase. At equilibrium, the reduced grand potentials of the individual species are the same. The set of equations to be solved in terms of fugacities, assuming an ideal adsorbed solution and γ_i set to unity, is

$$y_i \phi_i P_T = x_i f_i^*(\psi) \quad (46)$$

where $f_i^*(\psi)$ is the fugacity at which each pure component is at the same reduced grand potential, ψ , and temperature of the mixture. In Real Adsorbed Solution Theory (RAST) the non-ideal behaviour of the adsorbed phase is accounted for by the use of activity coefficients (γ_i) [95].

When gas-phase pressures are sufficiently low, the fugacities in the previous equations may be replaced by pressures. For liquid systems the same set of equations applies with pressure replaced by concentration [102]. For simplicity here we will refer always to pressure, with the understanding that all the results will apply to the corresponding liquid system. We note also that using pressure implies the assumption of an ideal gas (for gases) or ideal liquid mixture (for liquids) and that fugacity should replace pressure in a rigorous extension to high-pressure gas systems or non-ideal liquid mixtures.

The $2N_c + 1$ basic equations for IAST are [23,28]:

$$y_i P_T = p_i = x_i p_i^*(\psi) \quad i = 1, 2, \dots, N_c \quad (47)$$

(N_c equations)

$$\sum_{i=1}^{N_c} x_i = 1 \quad (1 \text{ equation}) \quad (48)$$

$$\psi = \psi_1 = \psi_2 = \dots = \psi_{N_c} \quad (N_c \text{ equations}) \quad (49)$$

which can be solved for the $2N_c + 1$ unknowns which includes: (1) N_c values of mole fractions in the adsorbed phase x_i , (2) 1 value of the reduced grand potential ψ , and (3) N_c values of the sorption pressure of the pure component p_i^* that give the same reduced grand potential as that of the mixture.

Equation (47) is analogous to Raoult's law that states that the partial pressure of each component of an ideal mixture of liquids is equal to the vapour pressure of the pure component multiplied by its mole fraction in the mixture. Note that Equations (47)–(49) do not contain any information on the vacancy and the amount that has been adsorbed. The specific adsorption area of a given species is inversely proportional to q_i . The total amount adsorbed q_T can be calculated from the Gibbs adsorption isotherm Equation (29) assuming zero mass or volume change upon adsorption, and is given by [69]

$$\frac{1}{q_T} = \sum_{i=1}^{N_c} \frac{x_i}{q_i^*} \quad (50)$$

where q_i^* is the adsorbed amount of pure component i at the sorption pressure p_i^*

$$q_i^* = q(p_i^*) \quad (51)$$

Knowing the total amount adsorbed, the amount contributed by component i is given by

$$q_i = x_i q_T \quad (52)$$

Equations (47)–(52) form a set of powerful equations for the IAS theory. If the total pressure and the mole fractions in the gas phase are given, then the unknowns can be computed:

- N_c mole fractions in the adsorbed phase (x_i)
- N_c sorption pressures (p_i^*)
- the total amount adsorbed and the component amount adsorbed

This is the most common use case and occurs for example in computing mixture isotherms from pure component isotherms, and the use of IAST in fixed-bed adsorbers. However, the inverse problem can be posed as well. In that case, the adsorbed mole fractions x_i and the total adsorbed amount q_T are given and the following unknowns have to be calculated:

- N_c mole fractions in the gas phase (y_i)
- N_c sorption pressures (p_i^*)
- the total pressure (p_T)

or the adsorbed mole fractions x_i and the total pressure are given and the following unknowns have to be calculated:

- N_c mole fractions in the gas phase (y_i)
- N_c sorption pressures (p_i^*)
- the total amount adsorbed (q_T)

Note that the correct fundamental thermodynamic variable is the absolute adsorbed amount and there is only one possible definition of the ideal adsorbed solution [71]. Another remark is that, in IAST, the form of the adsorption isotherm equation for pure components is arbitrary and can take any form which fits the data best [103]. However, we note that, especially the low pressure data needs to be accurately represented and errors at low pressures lead to large errors in multi-component calculations.

3.3. IAST numerical example

To illustrate the IAST algorithm, we consider two pure component Langmuir-Freundlich isotherms

$$\text{Component 1: } q_{s,1} \frac{b_1 p^{v_1}}{1.0 + b_1 p^{v_1}} \quad (53)$$

$$\text{Component 2: } q_{s,2} \frac{b_2 p^{v_2}}{1.0 + b_2 p^{v_2}} \quad (54)$$

and we list code-snippets that can be directly copied-and-pasted in Mathematica. We first define the parameters of the isotherms

$$\begin{aligned} q_{s1} &= 6.3; & q_{s2} &= 5.3; \\ b_1 &= 2.0; & b_2 &= 1.0; \\ nu_1 &= 0.75; & nu_2 &= 1.5; \end{aligned}$$

where we assume that $q_{s,i}$ is in units of mol/(kg framework), b_i in units of 1/Pa, pressure in units of Pa, and v_i dimensionless (Note that $b_i p^{v_i}$ is dimensionless). Specifying the fluid-phase mole fractions and total pressure

$$\begin{aligned} p &= 5; \\ y_1 &= 0.4; & y_2 &= 0.6; \end{aligned}$$

we first have to find the reduced grand potential ψ that is consistent with the adsorbed phase mole fractions adding up to unity. Filling in (see Table 4)

$$p_i^*(\psi) = \frac{1}{b_i^{1/v_i}} \left[\exp\left(\frac{v_i \psi}{q_i^{\text{sat}}}\right) - 1 \right]^{1/v_i} \quad (55)$$

into Equation (129), and using Mathematica we can numerically solve for psi

```
FindRoot[ y1*p/((1.0/(b1^(1.0/nu1)))
*(Exp[ nu1 psi/qs1]-1.0)^(1.0/nu1))+
y2*p/((1.0/(b2^(1.0/nu2)))*(Exp[ nu2
psi/qs2]-1.0)^(1.0/nu2))-1.0,
{psi, 10}]
```

The root is psi=13.6755 mol/(kg framework). This process is illustrated in Figure 2(a). Note that the functional relation between the sum of the adsorbed mole fractions and the reduced grand potential is monotonic (which can be exploited by bi-section algorithms). We can obtain the sorption pressures p_1 and p_2 (that correspond to the reduced grand potential ψ) using

$$\begin{aligned} p_1 &= (1/(b_1^{1.0/nu_1})) * (Exp[nu_1 * 13.6755 / qs_1] - 1.0)^{1.0/nu_1} \\ p_2 &= (1/(b_2^{1.0/nu_2})) * (Exp[nu_2 * 13.6755 / qs_2] - 1.0)^{1.0/nu_2} \end{aligned}$$

and we obtain $p_1=2.59899$ and $p_2=13.0167$ Pa. The adsorbed-phase mole fractions x_1 and x_2 are

$$\begin{aligned} x_1 &= y_1 * p / p_1 \\ x_2 &= y_2 * p / p_2 \end{aligned}$$

and we obtain $x_1 = 0.769531$ and $x_2 = 0.230472$, graphically depicted in Figure 2(b). With psi and x_1 and x_2 , the total adsorbed amount, q_T , can be calculated

$$\begin{aligned} q_T &= 1.0 / (0.769531 / (q_{s1} * b_1 * p_1^{nu_1} / (1.0 + b_1 * p_1^{nu_1})) + \\ &\quad (0.230472 / (q_{s2} * b_2 * p_2^{nu_2} / (1.0 + b_2 * p_2^{nu_2})))) \end{aligned}$$

leading to $q_T = 5.09176$ mol/(kg framework).

$$q_1 = x_1 * q_T$$

$$q_2 = x_2 * q_T$$

and we have $q_1 = 3.91827$ and $q_2 = 1.17351$ mol/(kg framework).

Using the following Mathematica code, we can generate the IAST prediction as a function of pressure

```
pressurebegin = 10^(-4);
pressureend = 10^10;
numberpoints = 100;
For[ i = 1, i <= numberpoints, i++,
p = 10^(((Log10[ pressureend] - Log10
[ pressurebegin] ) *
(i/(numberpoints - 1.0))) + Log10
[ pressurebegin] );
root = psi /.
```

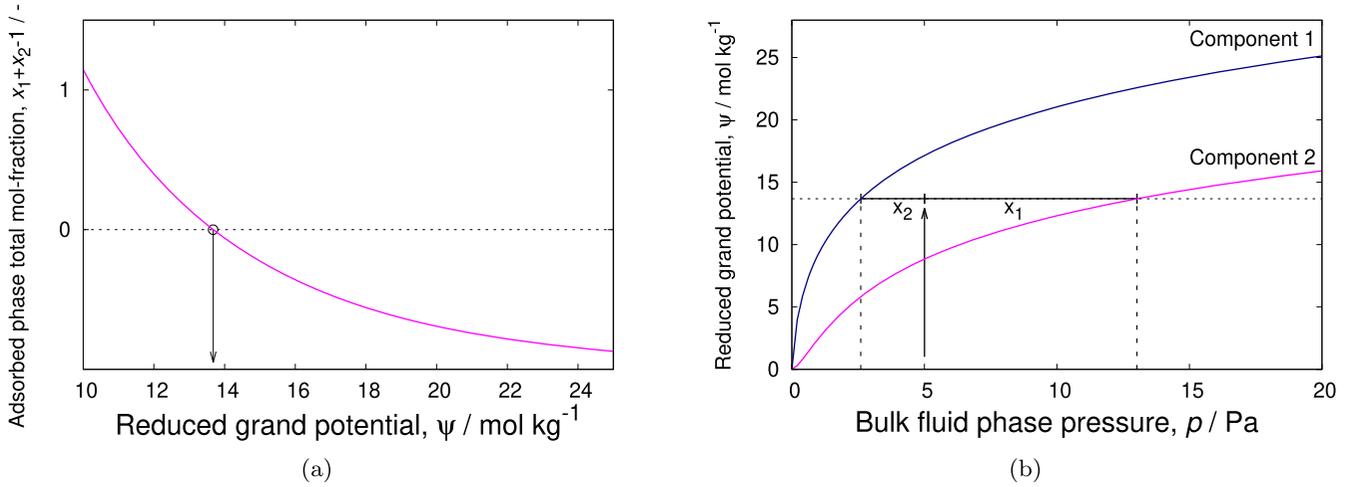


Figure 2. (Colour online) IAST algorithm: (a) adsorbed phase mole fraction as a function of the reduced grand potential (b) graphical representation of the basic IAST relationship. The sum of the adsorbed phase mole fractions is unity at reduced grand potential $\psi = 13.6755$ mol/(kg framework). By using $(\sum_i x_i) - 1$, a root-finding algorithm can be used. Note that that $\sum_i x_i$ has a monotonic relation to the reduced grand potential, hence it is also amenable to bi-section methods.

```

FindRoot[
  y1*p/((1.0/(b1^(1.0/nu1)))* (Exp
[ nu1 psi/(qs1) ] - 1.0)^(1.0/nu1)) +
  y2*p/((1.0/(b2^(1.0/nu2)))* (Exp[ nu2
psi/(qs2) ] - 1.0)^(1.0/
nu2)) - 1.0, {psi, 10}];
p1 = (1.0/(b1^(1.0/nu1)))* (Exp[ nu1*root/
qs1] - 1.0)^(1/nu1);
p2 = (1.0/(b2^(1.0/nu2)))* (Exp[ nu2*root/
qs2] - 1.0)^(1/nu2);
x1 = y1*P/((1.0/(b1^(1.0/nu1)))* (Exp
[ nu1*root/qs1] - 1.0)^(1.0/nu1));
x2 = y2*P/((1.0/(b2^(1.0/nu2)))* (Exp
[ nu2*root/qs2] - 1.0)^(1.0/nu2));
qT = 1.0/(x1/(qs1*b1*p1^nu1/(1 +
b1*p1^nu1)) +
x2/(qs2*b2*p2^nu2/(1 + b2*p2^nu2)));
Print[ p, " ", x1*qT, " ", x2*qT]

```

The result is plotted in Figure 3 which shows pure component and mixture isotherms for a binary mixture. Adsorption for the component with the highest saturation loading dominates at high pressures.

3.4. Analytic mixture prediction methods

3.4.1. Multi-component Langmuir

In the book of Do [23], the multi-component Langmuir is derived from the IAST equations. Equations (47) and (48) can be combined to yield [104]

$$\sum_{i=1}^{N_c} \frac{p_i}{p_i^*} = \sum_{i=1}^{N_c} x_i = 1 \quad (56)$$

This closure equation can be used to reduce the problem to a single nonlinear algebraic equation in ψ :

$$\frac{p_1}{p_1^*(\psi)} + \dots + \frac{p_{N_c}}{p_{N_c}^*(\psi)} = 1 \quad (57)$$

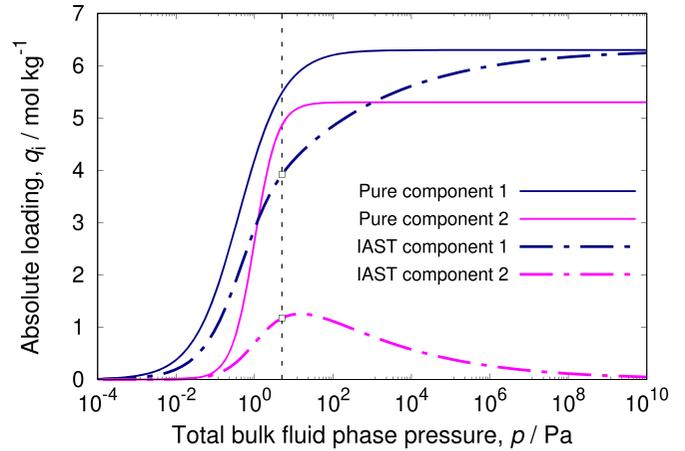


Figure 3. (Colour online) Example of IAST prediction for a binary mixture described by Langmuir-Freundlich isotherms. At 5 Pa total pressure and gas-phase mole fractions $y_1 = 0.4$ and $y_2 = 0.6$, we find adsorbed absolute loadings of $q_1 = 3.92$ and $q_2 = 1.17$ mol/kg. Typically in a mixture, a component with the highest saturation loading will drive the other components out at high pressures.

We can then use the expressions for the pure component sorption pressure (p_i^*) and use these as input in Equation (57). For the single component Langmuir isotherm

$$q_i = q_i^{\text{sat}} \frac{b_i p_i}{1 + b_i p_i} \quad (58)$$

we obtain

$$\begin{aligned} \psi(p^*) &= \int_0^p \frac{q(p)}{p} dp = q_i^{\text{sat}} \int_0^{p^*} \frac{b}{1 + bp} dp \\ &= q_i^{\text{sat}} \ln[1 + bp^*] \end{aligned} \quad (59)$$

Inverting this equation, we have

$$p^*(\psi) = \frac{\exp\left[\frac{\psi}{q_i^{\text{sat}}}\right] - 1}{b} \quad (60)$$

Filling this into Equation (57), we obtain

$$\frac{b_1 p_1}{\exp\left(\frac{\psi}{q_1^{\text{sat}}}\right) - 1} + \frac{b_2 p_2}{\exp\left(\frac{\psi}{q_2^{\text{sat}}}\right) - 1} = 1 \quad (61)$$

which can be analytically solved for ψ when the saturation capacities q_1^{sat} and q_2^{sat} are equal.

$$\exp\left(\frac{\psi}{q^{\text{sat}}}\right) = 1 + b_1 p_1 + b_2 p_2 \quad (62)$$

Using this in Equation (60) we find the sorption pressures

$$p_i^*(\psi) = \frac{b_1 p_1 + b_2 p_2}{b_i} \quad (63)$$

Substituting the sorption pressures into Raoult's law Equation (47), we obtain the adsorbed phase mole fractions

$$x_i = \frac{b_i p_i}{b_1 p_1 + b_2 p_2} \quad (64)$$

The total amount adsorbed is obtained by substituting Equation (58), (63), and (64) into Equation (50)

$$q_T = q^{\text{sat}} \frac{b_1 p_1 + b_2 p_2}{1 + b_1 p_1 + b_2 p_2} \quad (65)$$

and the adsorbed amount contributed by the component i is

$$q_i = q^{\text{sat}} \frac{b_i p_i}{1 + b_1 p_1 + b_2 p_2} \quad i = 1, 2 \quad (66)$$

which is the extended Langmuir equation (Equation (33)) with equal saturation capacities.

3.4.2. Analytic Taylor series expansions of LeVan and Vermeulen [105]

Le Van and Vermeulen [105] derived the explicit isotherms for binary mixtures from the Gibbs adsorption isotherm. These authors considered single site Langmuir and Freundlich isotherms for the pure components. However, this method can be extended to any kind of pure component isotherms, provided these isotherms have an explicit expression for the reduced grand potential (ψ) in terms of pure component pressure (p_i^*). This method is applicable for cases where the saturation capacities of the components are close to each other [23]. The derivation is as follows:

According to IAST, the reduced grand potential for pure component i is (ψ_i) is expressed as

$$\psi_i = \int_0^{p_i^*} \frac{q_i}{p_i} dp_i \quad (67)$$

Also, the reduced grand potential of the mixture (ψ^{mix}) is considered to be equal to the pure-component grand potential (ψ_i) at pressure, p_i^* for component i and the temperature of the mixture, i.e.

$$\psi_i = q_i^{\text{sat}} \ln \left(1 + b_{i,1} p_i^* + b_{i,2} (p_i^*)^2 \right) \quad (68)$$

For the ideal adsorbed solution, the partial pressures and the adsorbed phase composition are related by Raoult's law analogy.

$$p_i = x_i p_i^*(\psi) \quad (69)$$

In Equation (69), p_i^* is the pure component pressure in equilibrium with an adsorbed phase of the component i at the reduced grand potential (ψ) and temperature of the mixture. p_i is the partial pressure of component i and x_i is the mole fraction in the adsorbed phase. Using the relation $\sum_i^{N_c} x_i = 1$ and substituting x_i using Equation (69) yields

$$\frac{p_1}{p_1^*} + \frac{p_2}{p_2^*} = 1 \quad (70)$$

The single component isotherms (Langmuir and Freundlich) are substituted into Equation (67) which on integration yields expressions for pure component pressures (p_1^* , p_2^*). These expressions are used to further substitute p_1^* and p_2^* in Equation (70). The resulting expression, which is a function of p_1 , p_2 and ψ is expanded using Taylor series to obtain an explicit expression. The reduced grand potential ψ is differentiated to calculate the binary isotherms.

$$q_i = p_i \frac{\partial \psi}{\partial p_i} \quad (71)$$

Le Van and Vermeulen [105] derived the expressions for binary mixtures where both components either obey Langmuir, or Freundlich isotherms in their pure form.

(1) Langmuir Isotherms

For pure component i , the reduced grand potential (ψ_i) equals:

$$\psi = q_i^{\text{sat}} \ln(1 + b_i p_i^*) \quad (72)$$

$$p_i^* = \frac{1}{b_i} \left[\exp\left(\frac{\psi}{q_i^{\text{sat}}}\right) - 1 \right] \quad (73)$$

p_1^* and p_2^* in Equation (70) are substituted using Equation (73), which yields

$$\frac{b_1 p_1}{\exp\left(\frac{\psi}{q_1^{\text{sat}}}\right) - 1} + \frac{b_2 p_2}{\exp\left(\frac{\psi}{q_2^{\text{sat}}}\right) - 1} = 1 \quad (74)$$

Since the reduced grand potentials for the pure components are equal to the mixture (Equation (68)), ψ will be used as the grand potential for both the components. To proceed with the derivation, the following parameters are defined:

$$q^{\text{sat}} = \frac{q_1^{\text{sat}} + q_2^{\text{sat}}}{2} \quad (75)$$

$$\epsilon = \frac{q_1^{\text{sat}} - q_2^{\text{sat}}}{2q^{\text{sat}}} \quad (76)$$

Combining Equations (75) and (76) yields

$$q_1^{\text{sat}} = q^{\text{sat}}(1 + \epsilon) \quad (77)$$

$$q_2^{\text{sat}} = q^{\text{sat}}(1 - \epsilon) \quad (78)$$

Now, Equation (74) is expanded using the Taylor series for ψ about $\epsilon = 0$.

$$\psi = \psi|_{\epsilon=0} + \frac{\epsilon}{1!} \frac{d\psi}{d\epsilon}|_{\epsilon=0} + \frac{\epsilon^2}{2!} \frac{d^2\psi}{d\epsilon^2}|_{\epsilon=0} + \dots \quad (79)$$

Le Van and Vermeulen obtained isotherms for the binary mixture components using the Taylor expansion of Equation (74). The isotherms are calculated using Equation (71). The grand potential (ψ) is as follows

$$\psi = q^{\text{sat}} \ln(1 + b_1 p_1 + b_2 p_2) \quad (80)$$

In Equation (80), q^{sat} is the average saturation loading which depends on the nature of the Taylor expansion (i.e. the number of terms considered in the expansion). These authors have derived explicit isotherms by considering two, and three terms Taylor series expansion of ψ .

(A) Two term expansion:

$$q^{\text{sat}} = \frac{q_1^{\text{sat}} b_1 p_1 + q_2^{\text{sat}} b_2 p_2}{b_1 p_1 + b_2 p_2} \quad (81)$$

$$q_1^{\text{sat}} = q^{\text{sat}} \frac{b_1 p_1}{1 + b_1 p_1 + b_2 p_2} + \Delta_{L2} \quad (82)$$

where

$$\Delta_{L2} = (q_1^{\text{sat}} - q_2^{\text{sat}}) \times \frac{b_1 b_2 p_1 p_2}{(b_1 p_1 + b_2 p_2)^2} \ln(1 + b_1 p_1 + b_2 p_2) \quad (83)$$

(B) Three term expansion:

$$q^{\text{sat}} = \frac{b_1 p_1 q_1^{\text{sat}} + b_2 p_2 q_2^{\text{sat}}}{b_1 p_1 + b_2 p_2} + 2 \frac{(q_1^{\text{sat}} - q_2^{\text{sat}})^2}{q_1^{\text{sat}} + q_2^{\text{sat}}} \frac{b_1 b_2 p_1 p_2}{(b_1 p_1 + b_2 p_2)^2} \times \left[\left(\frac{1}{b_1 p_1 + b_2 p_2} + \frac{1}{2} \right) \ln(1 + b_1 p_1 + b_2 p_2) - 1 \right] \quad (84)$$

$$q_1^{\text{sat}} = q^{\text{sat}} \frac{b_1 p_1}{1 + b_1 p_1 + b_2 p_2} + \Delta_{L2} (1 + \Delta_{L3}) \quad (85)$$

where

$$\Delta_{L3} = \frac{q_1^{\text{sat}} - q_2^{\text{sat}}}{q_1^{\text{sat}} + q_2^{\text{sat}}} \frac{1}{b_1 p_1 + b_2 p_2} \left[\frac{(b_2 p_2)^2 + 2(b_2 p_2) - 4(b_1 p_1) - (b_1 p_1)^2}{b_1 p_1 + b_2 p_2} \ln(1 + b_1 p_1 + b_2 p_2) + \frac{3(b_1 p_1)^2 + 4(b_1 p_1) + b_1 b_2 p_1 p_2 - 2(b_2 p_2) - 2(b_2 p_2)^2}{1 + b_1 p_1 + b_2 p_2} \right] \quad (86)$$

The multi-component adsorption isotherm for component 2 can be obtained by simply interchanging the subscripts 1, and 2 in the above equations.

(2) Freundlich Isotherm

An approach similar to the above case is applied to a binary mixture where the pure components obey the

Freundlich isotherm which is shown below

$$q_i^{\text{sat}} = b_i p_i^{\nu_i} \quad (87)$$

The reduced grand potential (ψ) equation in terms of the partial pressure is

$$\begin{aligned} & \left(\frac{b_1}{\nu_1} \right)^{1/\nu_1} p_1 \exp \left(-\frac{1}{\nu_1} \ln \psi \right) \\ & + \left(\frac{b_2}{\nu_2} \right)^{1/\nu_2} p_2 \exp \left(-\frac{2}{\nu_2} \ln \psi \right) \\ & = 1 \end{aligned} \quad (88)$$

For unequal Freundlich exponents (ν_i) but very close to each other, the value of ψ can be computed using the Taylor series expansion. The expression for the adsorbed loadings for the components in the mixture are derived using the Taylor series expansion of ψ about ϵ (Equation (79)). For Freundlich isotherms, ϵ is

$$\epsilon = \frac{\nu_1 - \nu_2}{\nu_1 + \nu_2} \quad (89)$$

In Equation (89), ν_1 and ν_2 are the Freundlich exponents for component 1 and 2 respectively. The expression for the adsorbed loading for component 1 (q_1) is shown below, a detailed derivation for which can be found in Ref. [105].

$$q_1 = \frac{\bar{\nu} \left(\frac{b_1}{\nu_1} \right)^{1/\nu_1} p_1}{\left[\left(\frac{b_1}{\nu_1} \right)^{1/\nu_1} p_1 + \left(\frac{b_2}{\nu_2} \right)^{1/\nu_2} p_2 \right]^{1-\bar{\nu}}} + \Delta_{F2} \quad (90)$$

where

$$\begin{aligned} \Delta_{F2} = & (\nu_1 - \nu_2) \frac{\left(\frac{b_1}{\nu_1} \right)^{1/\nu_1} p_1 \left(\frac{b_2}{\nu_2} \right)^{1/\nu_2} p_2}{\left[\left(\frac{b_1}{\nu_1} \right)^{1/\nu_1} p_1 + \left(\frac{b_2}{\nu_2} \right)^{1/\nu_2} p_2 \right]^{2-\nu}} \\ & \times \ln \left[\left(\frac{b_1}{\nu_1} \right)^{1/\nu_1} p_1 + \left(\frac{b_2}{\nu_2} \right)^{1/\nu_2} p_2 \right] \end{aligned} \quad (91)$$

$$\bar{\nu} = \frac{\nu_1 \left(\frac{b_1}{\nu_1} \right)^{1/\nu_1} p_1 + \nu_2 \left(\frac{b_2}{\nu_2} \right)^{1/\nu_2} p_2}{\left(\frac{b_1}{\nu_1} \right)^{1/\nu_1} p_1 + \left(\frac{b_2}{\nu_2} \right)^{1/\nu_2} p_2} \quad (92)$$

3.4.3. Analytic approach of Ilic et al. [106]

Ilic et al. [106] derived an explicit competitive isotherm model for binary mixtures, where the pure components obey quadratic isotherms. For pure components, the reduced grand potential is

$$\psi_i = q_i^{\text{sat}} \ln \left(1 + b_{i,1} p_i^* + b_{i,2} (p_i^*)^2 \right) \quad (93)$$

The grand potential of the mixture is considered to be equal to the pure-component grand potential (ψ_i) at pressure, p_i^* for

component i and the temperature of the mixture, i.e.

$$\psi = \psi_1 = \psi_2 \quad (94)$$

Using Equations (93), and (94) and considering the saturation capacities of the components to be equal ($q_1^{\text{sat}} = q_2^{\text{sat}}$), we obtain

$$\ln \left(1 + b_{1,1}p_1^* + b_{1,2}(p_1^*)^2 \right) = \ln \left(1 + b_{2,1}p_1^* + b_{2,2}(p_1^*)^2 \right) \quad (95)$$

In Equation (95), $b_{i,j}$ represents equilibrium constant. This equation can be reformulated using a cubic polynomial which is defined as a function of the adsorbed mole fraction of component 1 (x_1).

$$F(p_1, p_2, x_1) = A(p_1, p_2)x_1^3 + B(p_1, p_2)x_1^2 + C(p_1, p_2)x_1 + D(p_1, p_2) \quad (96)$$

where

$$A(p_1, p_2) = \alpha p_1 + p_1 > 0 \quad (97)$$

$$B(p_1, p_2) = p_1(\beta p_1 - 2\alpha) - p_2(1 + \gamma p_2) \quad (98)$$

$$C(p_1, p_2) = p_1(\alpha - 2\beta p_1) \quad (99)$$

$$D(p_1) = \beta p_1^2 \quad (100)$$

$$\alpha = \frac{b_{1,1}}{b_{2,1}} > 0 \quad (101)$$

$$\beta = \frac{b_{1,2}}{b_{2,1}} \geq 0 \quad (102)$$

$$\gamma = \frac{b_{2,2}}{b_{2,1}} \geq 0 \quad (103)$$

$$b_{i,1} > 0, \quad i = 1, 2 \quad (104)$$

$$b_{i,2} \geq 0, \quad i = 1, 2 \quad (105)$$

The root (x_1) of this cubic polynomial (Equation (96)) can be derived analytically by applying the formulae of Cardano [107]. The problem is solved by selecting the physically meaningful root out of the three obtained roots. Once the value of x_1 is computed, the adsorbed loading for component i (q_i) is calculated using the following expression [77]:

$$q_i = \left[\frac{x_1}{q_1^*(p_1^*)} + \frac{1 - x_1}{q_2^*(p_2^*)} \right] x_i \quad (106)$$

In Equation (106), x_i is the adsorbed mole fraction of component i , q_i^* is the adsorbed loading for pure component i , and p_i^* is the corresponding gas phase pressure.

(1) Quadratic isotherm (component 1) and BET isotherm (component 2)

$$\frac{x_1}{p_1} = \frac{(b_{1,1}(1 - b_{2,2}p_1) - b_{1,2}p_1) + \sqrt{(b_{1,1}(1 - b_{2,2}p_1) - b_{1,2}p_1)^2 + 4b_{1,2}(b_{1,1}p_1 + b_{2,1}p_1)(1 - b_{2,2}p_1)}}{2(b_{1,1}p_1 + b_{2,1}p_1)} \quad (114)$$

3.4.4. Analytic approach of Tarafder and Mazzotti [63]

Tarafder and Mazzotti obtained explicit isotherms for binary mixtures using IAST, where the pure components obey Langmuir-, anti-Langmuir- [24], Brunauer-Emmett-Teller (BET)-, and quadratic-type adsorption isotherms. These mixture isotherms are valid only when the saturation capacities of the components are identical ($q_1^{\text{sat}} = q_2^{\text{sat}} = q^{\text{sat}}$).

Assuming both the fluid and the adsorbed phase as ideal

$$p_i = p_i^* x_i \quad (i = 1, 2) \quad (107)$$

p_i is the concentration of component i in the mixture, p_i^* is the pure component concentration, and q_i^{sat} is the saturation loading in Equation (107). Explicit solutions for the adsorbed phase mole fractions (x_1 and x_2) are derived from

$$\psi \left(\frac{p_1}{x_1} \right) = \psi \left(\frac{p_1}{x_2} \right) \quad (108)$$

$$x_1 + x_2 = 1 \quad (109)$$

The reduced grand potentials (ψ) for component i , computed based on the above mentioned single component isotherms are as follows:

• Langmuir

$$\psi_i = q_i^{\text{sat}} \ln(1 + b_i p_i^*) \quad (110)$$

• Anti-Langmuir

$$\psi_i = -q_i^{\text{sat}} \ln(1 - b_i p_i^*) \quad (111)$$

• BET

$$\psi_i = q_i^{\text{sat}} \ln \left(\frac{1 - (b_{i,1}p_i^* + b_{i,2}p_i^{*2})}{1 - b_{i,2}p_i^*} \right) \quad (112)$$

• Quadratic

$$\psi_i = q_i^{\text{sat}} \ln(1 + b_{i,1}p_i^* + b_{i,2}p_i^{*2}) \quad (113)$$

In Equations (110) and (111), b_i is the equilibrium constant. Similarly, in Equations (112) and (113), $b_{i,j}$ ($j = 1, 2$) represents the equilibrium constants. The adsorbed mole fraction of component 1 (x_1), and the total adsorbed loading ($q_T = q_1 + q_2$) are calculated for different cases depending on the type of single component isotherms followed by each component in the mixture.

$$q_T = q^{\text{sat}} \left[\frac{x_1(x_1^2 + b_{1,1}p_1x_1 + b_{1,2}p_1^2)}{(b_{1,1}x_1 + 2b_{1,2}p_1)p_1} + \frac{(x_2 - b_{2,2}p_1)(x_2 - b_{2,2}p_1 + b_{2,1}p_1)}{b_{2,1}p_1} \right]^{-1} \quad (115)$$

- (2) Quadratic isotherm (component 1) and Langmuir isotherm (component 2)

$$\frac{x_1}{p_1} = \frac{(b_{1,1} - b_{1,2}p_1) + \sqrt{(b_{1,1} - b_{1,2}p_1)^2 + 4b_{1,2}(b_{1,1}p_1 + b_2p_1)}}{2(b_{1,1}p_1 + b_2p_1)} \quad (116)$$

$$q_T = q^{\text{sat}} \left[\frac{x_1(x_1^2 + b_{1,1}p_1x_1 + b_{1,2}p_1^2)}{(b_{1,1}x_1 + 2b_{1,2}p_1)p_1} + \frac{x_2(x_2 + b_2p_1)}{b_2p_1} \right]^{-1} \quad (117)$$

- (3) Quadratic isotherm (component 1) and anti-Langmuir isotherm (component 2)

$$\frac{x_1}{p_1} = \frac{(b_{1,1}(1 - b_2p_1) - b_{1,2}p_1) + \sqrt{(b_{1,1}(1 - b_2p_1) - b_{1,2}p_1)^2 + 4b_{1,2}(b_{1,1}p_1 + b_2p_1)(1 - b_2p_1)}}{2(b_{1,1}p_1 + b_2p_1)} \quad (118)$$

$$q_T = q^{\text{sat}} \left[\frac{x_1(x_1^2 + b_{1,1}p_1x_1 + b_{1,2}p_1^2)}{(b_{1,1}x_1 + 2b_{1,2}p_1)p_1} + \frac{x_2(x_2 - b_2p_1)}{b_2p_1} \right]^{-1} \quad (119)$$

3.4.5. Analytic approach of Van Assche et al. [30] (Implemented in RUPTURA)

Van Assche et al. [30] derived an explicit multi-component adsorption model for arbitrary number of components. This model accounts for the effects of the size of the adsorbing

components. The explicit isotherms (EI) are derived using the concepts of statistical mechanics. In this model, the components are arranged based on their saturation capacities as shown below.

$$q_{N_C}^{\text{sat}} \geq q_{N_C-1}^{\text{sat}} \geq \dots \geq q_2^{\text{sat}} \geq q_1^{\text{sat}} \quad (120)$$

The largest component or the one with the smallest saturation capacity is considered to adsorb first. The adsorbent is considered to be a lattice divided into grids of uniform size. Once, the adsorption of the 1st component takes place, the remaining lattice is further subdivided such that the com-

ponent with the next smallest saturation capacity adsorbs. The process continues until the last component adsorbs. While dividing the lattice each time into uniform grids, the grid size is taken to be the ratio of the saturation capacities of the corresponding component and its preceding counterpart ($q_i^{\text{sat}}/q_{i-1}^{\text{sat}}$). The adsorption isotherm for component i in a mixture of N_C components is [30]:

$$q_i = (q_i^{\text{sat}} b_i p_i) \frac{1}{\beta} \prod_{k=1}^i \alpha_k \quad (121)$$

where

$$\alpha_1 = 1 \quad (122)$$

$$\alpha_i = \left[\left(\dots \left(\left(\left(1 + b_{N_C} p_{N_C} \right)^{\frac{q_{N_C}^{\text{sat}}}{q_{N_C-1}^{\text{sat}}}} + b_{N_C-1} p_{N_C-1} \right)^{\frac{q_{N_C-1}^{\text{sat}}}{q_{N_C-2}^{\text{sat}}}} + b_{N_C-2} p_{N_C-2} \right)^{\frac{q_{N_C-2}^{\text{sat}}}{q_{N_C-3}^{\text{sat}}}} \dots + b_{i+1} p_{i+1} \right)^{\frac{q_{i+1}^{\text{sat}}}{q_i^{\text{sat}}}} + b_i p_i \right] \frac{q_i^{\text{sat}}}{q_{i-1}^{\text{sat}} - 1} \quad (123)$$

$$\beta = \left[\left(\dots \left(\left(\left(1 + b_{N_C} p_{N_C} \right)^{\frac{q_{N_C}^{\text{sat}}}{q_{N_C-1}^{\text{sat}}}} + b_{N_C-1} p_{N_C-1} \right)^{\frac{q_{N_C-1}^{\text{sat}}}{q_{N_C-2}^{\text{sat}}}} + b_{N_C-2} p_{N_C-2} \right)^{\frac{q_{N_C-2}^{\text{sat}}}{q_{N_C-3}^{\text{sat}}}} \dots + b_2 p_2 \right)^{\frac{q_2^{\text{sat}}}{q_1^{\text{sat}}}} + b_1 p_1 \right] \quad (124)$$

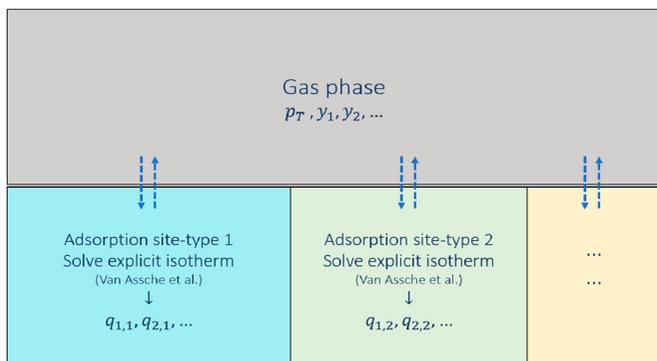


Figure 4. (Colour online) Schematic representation of the Segregated Explicit Isotherm (SEI) model which accounts for the separate thermodynamic equilibrium of the adsorbed phases with the gas phase at different adsorption sites. Each adsorbed phase is separately in thermodynamic equilibrium with the gas phase and it is represented by the adsorption isotherm proposed by Van Assche et al. [30]. The gas phase has a total pressure of p_T and the gas phase mole fractions of the components in the mixture are represented by y . In the adsorbed phase j , the loading of the component i is q_{ij} .

Algorithm 1 Procedure for calculating the equilibrium loadings for components in mixtures using the analytic approach of Van Assche et al. [30].

Arrange the components in ascending order based on the value of the saturation loadings (q_i^{sat}).

$$q_1^{\text{sat}} \leq q_2^{\text{sat}} \leq \dots \leq q_{N_c}^{\text{sat}} \leq q_{N_c}^{\text{sat}}$$

Calculate the ratios of q_i^{sat} (n_i) for each component

$$n_i = \frac{q_i^{\text{sat}}}{q_{i-1}^{\text{sat}}}$$

$$n_1 = 1$$

$$\alpha_j = (\alpha_{j+1} + k_j p_j)^{n_j}$$

$$\alpha_{N_c+1} = 1$$

Equilibrium loading for each component at the j th site

$$q_i = q_i^{\text{sat}} k_i p_i \frac{1}{\alpha_j} \prod_{m=1}^i \frac{\alpha_m}{\alpha_{m+1} + k_m p_m}$$

Rearrange the adsorbed loadings in the original order as provided in the input.

return q_i

For a binary model, the equations read

$$q_1 = q_1^{\text{sat}} \frac{b_1 p_1}{(1 + b_2 p_2) \frac{q_2^{\text{sat}}}{q_1^{\text{sat}}} + b_1 p_1} \quad (125)$$

$$q_2 = q_2^{\text{sat}} \frac{b_2 p_2 (1 + b_2 p_2) \frac{q_2^{\text{sat}}}{q_1^{\text{sat}} - 1}}{(1 + b_2 p_2) \frac{q_2^{\text{sat}}}{q_1^{\text{sat}}} + b_1 p_1} \quad (126)$$

The procedure to calculate the explicit adsorption isotherms is shown in Algorithm 1. This model reduces to the classical Langmuir equation for pure component isotherms. The proposed model was found to offer a very reasonable approximation of the IAST for adsorbates obeying the Langmuir equation, even with very differing saturation capacities. The model was also demonstrated to show excellent performance in a process simulator case study [108].

3.4.6. Segregated explicit isotherm (SEI) [31] (Implemented in RUPTURA)

The Segregated Explicit Isotherm (SEI) is the modified version of the multicomponent explicit isotherm discussed above [31]. The explicit isotherm is modified to incorporate the effects of a heterogeneous adsorption surface. This extended model is

applicable when the adsorbent is composed of distinct adsorption sites and the preferred adsorption sites varies for the components in the mixture. The concept of Swisher et al. [29] used for developing the Segregated Ideal Adsorbed Solution Theory (SIASST) model is adopted in this model. Separate thermodynamic equilibrium between the gas phase and the adsorbed phase is considered at each type of adsorption site. Swisher et al. [29] computed equilibrium loadings for the mixture components using IAST at each type of adsorption site (Section 3.5.8). For this purpose, unary isotherm parameters are required as input which are obtained by fitting these isotherms to pure component adsorbed loading data. These data can be obtained using grand-canonical Monte Carlo (GCMC) simulations or experiments. However, GCMC is more conveniently used than performing experiments because collecting isotherm data using experiments can be time consuming [109]. Different isotherms can be used for each type of adsorption sites. The mixture loadings computed at each adsorption site are summed up to estimate the overall equilibrium loadings for each components. Similarly, in the SEI model, the adsorption isotherms developed by Van Assche et al. [30] are solved at each type of adsorption sites (Figure 4) and the overall adsorbed loading for each component is obtained by summing up these loadings. The adsorption isotherm of the i th component at the j th adsorption site is shown below.

$$q_{i,j} = \left(q_{i,j}^{\text{sat}} k_{i,j} p_i \right) \frac{\left[\prod_{m=1}^i \alpha_{m,j} \right]}{\beta_j} \quad (127)$$

In Equation (127), $\alpha_{m,j}$ and β_j are computed as shown in Equations (122)–(124). The overall equilibrium loading for each component in an adsorbent with N_{sites} types of distinct adsorption sites is calculated as follows:

$$q_i = \sum_{j=1}^{N_{\text{sites}}} q_{i,j} \quad (128)$$

If the adsorbent is composed of single type of adsorption sites, then both SEI and EI are essentially identical. Unlike IAST and SIASST, these models (EI and SEI) do not involve any iterative procedure to compute the equilibrium loadings. This increases the speed of calculations significantly. This is advantageous when SEI and EI are incorporated into another model (such as breakthrough curve model) [31,108]. The simulation run time drops significantly compared to the models with IAST implementation [31].

3.5. Numerical methods to solve the IAST

3.5.1. The 'nested loop algorithm' [104]

Myers and Valenzuela presented a simple method for solving the IAST [104] that is iterative in nature exploiting the Newton-Raphson method [23,28,110]. Tien et al. extended and improved the algorithm in order to reduce the computation time [110,111]. The method is conceptually elegant, but has slower convergence and is dependent on a good first guess for convergence. This algorithm consists of the calculation of the reduced grand potential (ψ) and then an analytic

inversion of the reduced grand potential to obtain expressions for the pure component sorption pressure (p_i^*) as a function of the reduced grand potential.

Generalizing the procedure to solve IAST, named the ‘nested loop’ algorithm by Mangano et al. [112], the total pressure and gas phase composition are specified and a nested problem of a highly nonlinear system of equations is solved [23,104,110]. Equations (47) and (48) can be combined to yield

$$F(\psi) = \sum_{i=1}^{N_c} x_i - 1 = \sum_{i=1}^{N_c} \frac{y_i p}{p_i^*(\psi)} - 1 = 0 \quad (129)$$

which is a function of only the reduced grand potential (ψ). In the nested loop approach, a single implicit equation determines the solution of the IAST. To solve Equation (129) for the reduced grand potential, an iterative method like the Newton-Raphson method can be used [23]. In Newton’s method, the derivative of the reduced grand potential can be computed for any isotherm from [112]

$$\frac{d\psi_i}{dp_i^*} = \frac{q_i^*(p_i^*)}{p_i^*} \quad (i = 1, 2, \dots, N_c) \quad (130)$$

and

$$\frac{dF(\psi)}{d\psi} = - \sum_{i=1}^{N_c} \frac{y_i p}{p_i^*(\psi) q_i^*(p_i^*)} \quad (131)$$

$p_i^*(\psi)$ can be calculated using Equation (36), either analytically or numerically depending on the pure component isotherm equation. The resulting procedure is described in the book of Do [23].

$$\psi^{k+1} = \psi^k - \frac{F(\psi^{(k)})}{F'(\psi^{(k)})} \quad (132)$$

$$F(\psi^{(k)}) = \sum_{i=1}^{N_c} \frac{y_i p}{p_i^*(\psi^{(k)})} - 1 \quad (133)$$

$$F'(\psi^{(k)}) = \left[- \sum_{i=1}^{N_c} \frac{y_i p}{[p_i^*(\psi)] q_i^*} \right]_{\psi=\psi^{(k)}} \quad (134)$$

An appropriate selection of the initial condition guarantees convergence [112]:

$$\psi = \min[\psi_i(p_i^*)] \quad (135)$$

The initial guess for ψ from Myers and Valenzuela [104] and Do [23]

$$\psi = \sum_{i=1}^{N_c} y_i \psi(p_i^*) \quad (136)$$

does not guarantee convergence strictly [112]. Convergence can be improved by combining Newton with a line search due to the monotonous nature of $F(\psi)$. The nested loop is a very fast numerical method if there exist explicit expressions for the sorption pressures.

3.5.2. FastIAS [88]

The FastIAS approach by O’Brien and Myers expresses the system of $N_c - 1$ equalities as [74,88]

$$\begin{aligned} \psi_1(p_1^*) &= \psi_2(p_2^*) \\ \psi_2(p_2^*) &= \psi_3(p_3^*) \\ &\vdots \\ \psi_{N_c-1}(p_{N_c-1}^*) &= \psi_{N_c}(p_{N_c}^*) \end{aligned} \quad (137)$$

$$\sum_{i=1}^{N_c} \frac{p_i}{p_i^*} = 1$$

This system constitute N_c nonlinear algebraic equations

$$G(\mathbf{p}^*) = 0 \quad (138)$$

and equates the reduced grand potentials of successive components. The elements of the vector G are:

$$G_i(p^*) = \psi_i(p_i^*) - \psi_{i+1}(p_{i+1}^*) \quad i = 1, \dots, N_c - 1 \quad (139)$$

$$G_{N_c}(p^*) = \sum_{i=1}^{N_c} \frac{p_i}{p_i^*} - 1 \quad (140)$$

The N_c -variable Newton-Raphson method may be expressed as for the k th iteration

$$p^{*(k+1)} \leftarrow p^{*(k)} - \delta^{(k)} \quad (141)$$

where δ is determined from the following linear equation

$$\Phi \cdot \delta = G \quad (142)$$

O’Brien and Myers added the following update rule to δ [113]

$$p_i^{*(k+1)} = \frac{1}{2} p_i^{*(k)} \quad \text{if } p_i^{*(k)} + \delta^{(k)} < 0 \quad (143)$$

to ensure that the sorption pressures are always positive. The matrix Φ is the Jacobian matrix obtained by differentiating the vector G with respect to vector p^* .

$$\Phi_{ij}^{(k)} = \left(\frac{\partial G_i(p^{*(k)})}{\partial p_j^{*(k)}} \right)_{p^*=i=j} \quad (144)$$

Due to the properties of the reduced grand potential Equation (36) we have

$$\frac{\partial \psi(p_i^*)}{\partial p_i^*} = \frac{q(p_i^*)}{p_i^*} \quad (145)$$

and the elements of Φ are

$$\Phi_{i,i} = \frac{q(p_i^*)}{p_i^*} \quad i = 1, \dots, N_c - 1 \quad (146)$$

$$\Phi_{i,i+1} = - \frac{q(p_{i+1}^*)}{p_{i+1}^*} \quad i = 1, \dots, N_c - 1 \quad (147)$$

$$\Phi_{N_c,i} = - \frac{p_i}{(p_i^*)^2} \quad i = 1, \dots, N_c \quad (148)$$

phase concentrations or partial pressures (p_i) can be obtained. This method was developed for binary mixtures and is useful when an analytic expression for the reduced grand potential (ψ) cannot be obtained (e.g. pure components obeying Redlich-Peterson isotherm). However, this method is also applicable to cases where pure components obey other types of isotherms such as Langmuir, Freundlich, Sips, etc. In addition, the value of the bulk phase concentration of component 2 in pure form (p_2^*) should be determined using numerical procedures, such as the Newton-Raphson method based on the guessed value for the bulk phase concentration of component 1 in pure form (p_1^*). The guessing parameter in the numerical solution (p_1^*) changes in the iterative procedure until the criteria ($\psi_1 = \psi_2$) is met. Therefore, this procedure requires tremendous effort to find the equilibrium concentrations. The numerical integration scheme is shown below. Redlich-Peterson isotherm is considered for the pure components.

$$\psi = \int_0^p \frac{q}{p} dp = \int_0^p \frac{k_R}{1 + a_R p^\beta} dp \quad (166)$$

For pure components 1 and 2, the expressions for ψ are:

$$\psi_1 = \int_0^{p_1^*} \frac{k_{R,1}^*}{1 + a_{R,1}^* p^{\beta_1^*}} dp \quad (167)$$

$$\psi_2 = \int_0^{p_2^*} \frac{k_{R,2}^*}{1 + a_{R,2}^* p^{\beta_2^*}} dp \quad (168)$$

$$\frac{1}{q_T} = \frac{x_1}{q_1^*} + \frac{x_2}{q_2^*} \quad (169)$$

In Equation (169), q_T is the total loading, and x_1 and x_2 are the mole fractions of the components 1 and 2 respectively. q_1^* and q_2^* are the pure component loadings. Using the values for q_1 , and q_2 , x_1 , x_2 , and q_T can be obtained as follows:

$$q_T = q_1 + q_2 \quad (170)$$

$$x_1 = \frac{q_1}{q_T} \quad (171)$$

$$x_2 = \frac{q_2}{q_T} \quad (172)$$

Applying the Redlich-Peterson equation in Equation (169) yields

$$\frac{1}{q_T} = \frac{x_1}{\frac{k_{R,1}^* p_1^*}{1 + a_{R,1}^* p_1^{\beta_1^*}}} + \frac{x_2}{\frac{k_{R,2}^* p_2^*}{1 + a_{R,2}^* p_2^{\beta_2^*}}} \quad (173)$$

Another numerical method such as Newton-Raphson is required to solve Equation (173). In this approach, is computed from a given value of p_1^* . Then the values of ψ_1 and ψ_2 are obtained by applying the numerical integration scheme for Equations (167) and (168). The value of p_1^* is optimised till $\psi_1 = \psi_2$. The values of the

bulk phase concentration (p_1 and p_2) are obtained using Raoult's law analogy as shown below.

$$p_1 = x_1 p_1^* \quad (174)$$

$$p_2 = x_2 p_2^* \quad (175)$$

3.5.5. Padé approximants of Frey and Rodrigues [115]

In this study, an explicit solution for IAS theory is developed. It involves fitting the relation between the reduced grand potential (ψ) and the pure component gas phase pressure (p_i^*) to a three parameter Padé approximation [115]. This method can be applied to a variety of single component isotherms [115]. A Padé approximant can be used to represent the pure component pressure ($p_i^* = f^{-1}(\psi)$). The accuracy of the expression depends on the kind of approximant employed. An important idea presented in this publication is to fit the equivalent Padé representation directly to the experimental equilibrium data. One pitfall that can be quickly identified with this method is the inability of the Padé approximation to represent the equilibrium data accurately over sufficiently wide concentration ranges, as required for IAST calculations. The steps involved in this approach are as follows:

- (1) Determine the functions $\psi(p_i^*)$ and $p_i^*(\psi)$ for each component from the single component isotherms. For pure component i obeying Langmuir isotherm, $\psi(p_i^*)$ equals

$$\psi(p_i^*) = q_i^{\text{sat}} \ln(1 + b_i p_i^*) \quad (176)$$

For different values of p_i^* , ψ can be obtained using Equation (176). The expression for the pure component pressure ($p_i^*(\psi)$) is

$$p_i^*(\psi) = \frac{1}{k_i} \left(\exp\left(\frac{\psi}{q_i^{\text{sat}}}\right) - 1 \right) \quad (177)$$

- (2) Fit the function $p_i^*(\psi)$ to a three-parameter half Padé approximation

$$p_i^* = \frac{\psi}{a_i + f_i \psi + c_i \psi^2} \quad (178)$$

In Equation (178), a_i , f_i and c_i are the coefficients of the three parameter half Padé approximation.

- (3) Substitute Equation (178) into $\sum_{i=1}^{N_C} x_i = \sum_{i=1}^{N_C} p_i/p_i^* = 1$ which leads to a quadratic formula for ψ :

$$0 = \psi^2 \sum_{i=1}^{N_C} c_i p_i + \psi \sum_{i=1}^{N_C} f_i p_i - \psi + \sum_{i=1}^{N_C} a_i p_i \quad (179)$$

- (4) Determine the explicit multi-component isotherms by combining Equation (179) and $q_i = p_i \frac{\partial \psi}{\partial p_i}$ as shown below.

$$q_i = p_i \frac{\psi^2 c_i + \psi f_i + a_i}{1 - \sum_{i=1}^{N_C} f_i p_i - 2\psi \sum_{i=1}^{N_C} c_i p_i} \quad (180)$$

3.5.6. Surface B-splines fitting [116]

In this method, the IAST calculations are performed once for obtaining the multi-component adsorption data for each species

[116]. These datasets are fitted with B-splines to determine the set of coefficients involved in the equations for the splines. Once the coefficients are obtained, interpolation methods can be used to obtain the equilibrium loadings at any concentration.

B-splines are also known as the basis splines. They are constructed using polynomial functions joined at nodes. For a set of knots or nodes, λ_j (with $j = 0$ to $g + 1$), $g - k$ independent B-splines ($N_{i,k+1}(x)$) of degree k can be constructed [116]. Each spline function (s) is evaluated at $x \in [\lambda_0, \lambda_{g+1}]$ as follows

$$s(x) = \sum_{i=-k}^g a_i N_{i,k+1}(x) \quad (181)$$

In Equation (181), a_i are known as B-spline coefficients. $N_{i,k+1}(x)$ is obtained recursively using the following equation.

$$N_{i,k+1}(x) = \frac{x - \lambda_i}{\lambda_{i+k} - \lambda_i} N_{i,k}(x) + \frac{\lambda_{i+k+1} - x}{\lambda_{i+k+1} - \lambda_{i+1}} N_{i+1,k}(x) \quad (182)$$

$$N_{i,1} = \begin{cases} 1, & x \in [\lambda_i, \lambda_{i+1}] \\ 0, & x \notin [\lambda_i, \lambda_{i+1}] \end{cases} \quad (183)$$

B-splines can be applied to surface approximation using tensor products [116]. Considering a data point (x, y) belonging to $[\lambda_i, \lambda_{i+1}] \times [\mu_j, \mu_{j+1}]$, the spline (s) of degree, k in x , and l in y is as follows

$$s(x, y) = \sum_{i=-k}^g \sum_{j=-l}^h a_{i,j} N_{i,k+1}(x) M_{j,l+1}(y) \quad (184)$$

where $N_{i,k+1}(x)$ and $M_{j,l+1}(y)$ are the normalised B-splines defined on the knots, λ and μ respectively. This surface approximation can be used to calculate the equilibrium loadings in case of multi-component adsorption. For a binary mixture, the adsorption loadings ($q_1(p_1, p_2), q_2(p_1, p_2)$) can be calculated using Equation (184). The B-spline coefficients ($a_{i,j}$) are obtained by fitting the surface spline to the data points of the equilibrium loadings as a function of the bulk phase concentrations (p_1 and p_2). This reduces the amount of iterative calculations involved in IAST.

3.5.7. Approach of Landa et al. [74]

The approach of Landa et al. is based on transforming the algebraic system of IAST equations to a system of ODEs with one specified initial value [74]. Starting with

$$\psi(p_1^*) = \psi_i(p_i^*) \quad (i = 1, 2, \dots, N) \quad (185)$$

which after differentiation reads

$$\frac{d\psi(p_1^*)}{dp_1^*} = \frac{d\psi_i(p_i^*)}{dp_i^*} \frac{dp_i^*}{dp_1^*} \quad (i = 2, \dots, N) \quad (186)$$

Equation (186) can be transformed in an integration of a system of $N - 1$ decoupled ordinary differential equations

$$\begin{aligned} \frac{dp_i^*}{dp_1^*} &= \frac{q_i^*(p_i^*)}{p_i^*} \frac{p_i^*}{q_i^*(p_i^*)}, & p_i^*(0) &= 0 \quad (i = 2, \dots, N) \\ \frac{dp_1^*}{dp_1^*} &= 1, & p_1^*(0) &= 0 \quad (i = 1) \end{aligned} \quad (187)$$

The integration proceeds until the equilibrium condition Equation (129) is met.

The calculation of the reduced grand potential is avoided, as well as the inversion of ψ . The approach does not need a suitable vector of starting values to compute the desired adsorption equilibria.

3.5.8. Segregated IAST (SIAST) -- approach of Swisher et al. [29] (Implemented in RUPTURA)

Instead of considering the available adsorption volume as a continuous space, the adsorbent material is divided into several distinct adsorption sites in SIAST. The competitive adsorption at each type of site takes place separately which are separately in thermodynamic equilibrium with the gas phase [29], as shown in Figure 5. These sites are assumed to be uniform and hence, IAST is applied individually to each type of sites. Unary isotherm parameters are required as input to this model which can be obtained by fitting isotherm equations to equilibrium loading data of pure components. At each type of sites, different isotherms can be used. It is easier to obtain pure component loadings using grand-canonical Monte Carlo simulations than experiments. This because the later involves a time consuming procedure [109]. SIAST works better than IAST when there are distinct adsorption sites and the components in a mixture prefer certain adsorption sites over the others [29]. When there is multi-site adsorption, the competition experienced by different molecules vary at different types of these sites. Since IAST assumes the entire adsorbent as a uniform site, it cannot capture such variations.

In case of SIAST, the inverse of ψ is generally an explicit expression at each adsorption site (multi-site expressions are split up into their individual contributions per site). This helps in avoiding the iterations involved in calculating the pure component pressures (p_i^*) and makes the calculations much faster than the original IAST approach. If the inverse of ψ is not an explicit expression (e.g. Redlich-Peterson isotherm) [114], then SIAST will lose its advantage over IAST. Also, for adsorbents with single type of adsorption sites, IAST and SIAST are identical.

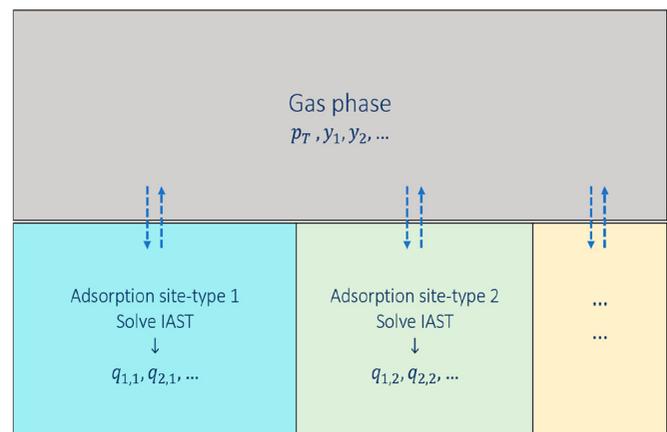


Figure 5. (Colour online) Equilibrium of each of the adsorbed phases with the gas phase in the Segregated Ideal Adsorbed Solution Theory (SIAST) model [29]. Each adsorbed phase is separately in equilibrium with the gas phase. The system is at a constant temperature. The gas phase has a total pressure of p_{tot} and the mole fraction of component i equals y_i . In the adsorbed phase j , the loading of component i is q_{ij} .

3.5.9. Direct search minimisation methods [73]

The method of Santori et al. [73] is based on the minimisation of an objective function representing the iso-reduced grand potential condition. The reduced grand potentials are expressed in terms of molar fractions x_i through a preliminary change of variable from p_i^* to x_i substitution

$$d \ln \left[\frac{p_T y_i}{x_i} \right] = -\frac{1}{x_i} dx_i \quad (188)$$

For the dual-site Langmuir, this becomes

$$\psi_i = \int - \left(\frac{q_{s1,i} b_{1,i} \left(\frac{p_T y_i}{x_i} \right)}{x_i + x_i b_{1,i} \left(\frac{p_T y_i}{x_i} \right)} + \frac{q_{s2,i} b_{2,i} \left(\frac{p_T y_i}{x_i} \right)}{x_i + x_i b_{2,i} \left(\frac{p_T y_i}{x_i} \right)} \right) dx_i \quad (189)$$

$$= \int \left(-\frac{q_{s1,i} + q_{s2,i}}{x_i} + \frac{q_{s1,i}}{x_i + p_T y_i b_{1,i}} + \frac{q_{s2,i}}{x_i + p_T y_i b_{2,i}} \right) dx_i \quad (190)$$

$$= -(q_{s1,i} + q_{s2,i}) \ln(x_i) + q_{s1,i} \ln(b_{1,1} y_i p_T + x_i) + q_{s2,i} \ln(b_{2,1} y_i p_T + x_i) \quad (191)$$

Santori et al. [73] derived similar expressions for the Toth, Unilan, and O'Brien-Myers functional forms. Using the derived reduced grand potentials ψ_i , the iso- ψ_i condition can be set as a minimisation problem. For the binary case we have

$$f_{\text{binary}}(x_i) = |\psi(x_1) - \psi(x_2)| \quad (192)$$

and ternary case we have

$$f_{\text{ternary}}(x_i, x_2) = |\psi(x_1) - \psi(x_2)| + |\psi(x_1) - \psi(x_3)| \quad (193)$$

For the more general ternary case, the optimisation problem is stated as: Minimise the objective function $f_{\text{ternary}}(x_i, x_2)$ subject to constraints $0 < x_1 < 1 - x_2$ and $0 < x_2 < 1 - x_1$. Santari et al. used Nelder-Mead minimisation algorithm [117] operated with a working precision of 10^{-8} , which resulted in final residuals ranging between 10^{-7} and 10^{-9} . The approach avoids pressure inversion and the initial guess, which are the typical requirements of the previous approaches. For binary systems, direct search minimisation approach was reported to be faster than the classic IAST equations solution approach up to 19.0 (dual-site Langmuir isotherm) and 22.7 times (Toth isotherm). In ternary systems, this difference decreases to 10.4 (O'Brien and Myers isotherm) times. Compared to the FastIAS approach [88], direct search minimisation is up to 4.2 times slower in ternary systems.

3.5.10. Approach of Mirzaei et al. [118]

Mirzaei et al. [118] developed a numerical solution for IAST, especially for cases where explicit expression for the reduced grand potential (ψ) is not available. Numerical integration is used to calculate ψ . In this approach, the guessing parameter is the adsorbed mole fraction of component 1 (x_1) which is not directly involved in the integration to calculate ψ . The adsorbed mole fraction of component 2 is calculated using

$$\sum_{i=1}^{N_C} x_i = 1 \quad (194)$$

The values of the pure component equilibrium concentrations are estimated as follows which are also the upper limit in the integration to calculate the grand potential (ψ)

$$p_i = x_i p_i^* \quad (195)$$

The grand potentials are calculated separately for both components using

$$\psi_i = \int_0^{p_i^*} \frac{q_i^*(p)}{p} dp \quad (196)$$

If the error ($|\psi_1 - \psi_2|$) is less than the predefined error value, then the total loading is calculated as shown below. Otherwise, the steps mentioned above are repeated with another guessed value for the adsorbed mole-fraction of component 1.

$$\frac{1}{q_T} = \sum_{i=1}^{N_C} \frac{x_i}{q_i^*} \quad (197)$$

Once, the total equilibrium loading (q_T) is obtained, q_1 and q_2 are calculated as follows

$$q_i = x_i q_T \quad (198)$$

The procedure for the numerical method developed by Mirzaei et al. [118] is shown in Figure 6.

3.6. Mixture prediction software

3.6.1. Benjamin [119]

M. Benjamin freely provided an Excel spreadsheet and a Java program that carries out the IAST calculations that can be used to calculate the equilibrium distribution of species in a competitive adsorption system, based on the IAST Model. A manuscript containing background information on the IAST and the usefulness of these programs has been published in ES&T [119].

3.6.2. pyIAST [77]

pyIAST [77] is an open-source Python package, pyIAST, to perform IAST calculations for an arbitrary number of components. pyIAST supports several common analytical models to characterise the pure-component isotherms from experimental or simulated data. Alternatively, pyIAST can use numerical quadrature to compute the spreading pressure for IAST calculations by interpolating the pure-component isotherm data. pyIAST can also perform reverse IAST calculations, where one seeks the required gas phase composition to yield a desired adsorbed phase composition.

3.6.3. GAIAS [120]

GAIAS (Genetic Algorithm IAST) [120] is a Fortran 2008 + standard compliant, free and open source project, aimed at using IAST to predict the loading of the gas mixture on the adsorbed phase, based only on the knowledge of the pure adsorption isotherms of the individual components.

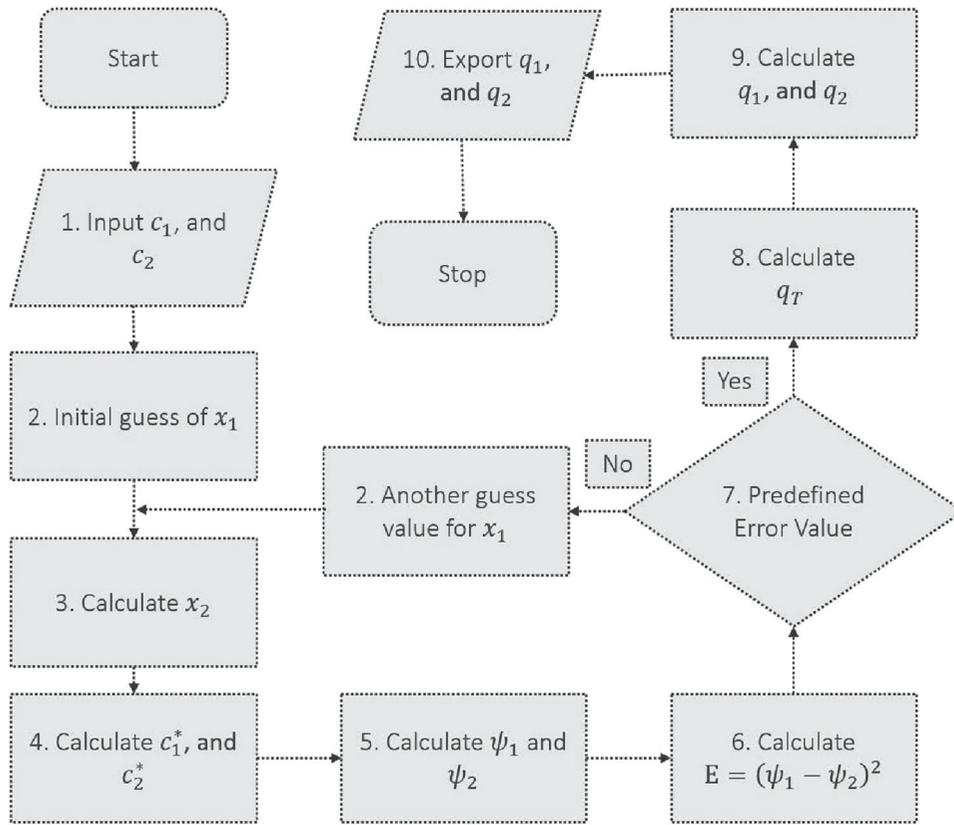


Figure 6. (Colour online) Numerical procedure to calculate equilibrium loadings for a binary mixture developed by Mirzaei et al. [118]. The bulk phase concentrations are the input to this approach and the adsorbed mole fraction for component 1 (x_1) is used as the guessed value. Based on x_1 , x_2 is estimated. Further, the grand potentials for components 1 and 2 are calculated separately and the difference between these two values are computed. If the difference is less than the predefined error value, then the total equilibrium loadings and the loadings for each component are determined. Otherwise, a new guessed value for component 1 is considered and the steps (3–7) are repeated.

Algorithm 2 IAST calculation using bi-section. The tolerance value ϵ can be set to 10^{-15} .

```

function IAST( $\rho$ ,  $y_i$ )
   $\psi \leftarrow$  initial value
   $\sum_i x_i \leftarrow \sum_i y_i \times p/p_i^*(\psi)$   $\triangleright$  /* Equation (47) */
   $\psi_{\uparrow} \leftarrow \psi$   $\triangleright$  /* Initialize the top bracket with the initial  $\psi$  value */
   $\psi_{\downarrow} \leftarrow \psi$   $\triangleright$  /* Initialize the bottom bracket with the initial  $\psi$  value */
  if  $\sum_i x_i > 1$  then
    repeat
       $\psi_{\uparrow} \leftarrow 2 \times \psi_{\uparrow}$ 
       $\sum_i x_i \leftarrow \sum_i y_i \times p/p_i^*(\psi_{\uparrow})$   $\triangleright$  /* Equation (47) */
    until  $\sum_i x_i < 1$ 
  else
    repeat
       $\psi_{\downarrow} \leftarrow \psi_{\downarrow}/2$ 
       $\sum_i x_i \leftarrow \sum_i y_i \times p/p_i^*(\psi_{\downarrow})$   $\triangleright$  /* Equation (47) */
    until  $\sum_i x_i > 1$ 
  end if
  repeat
     $\psi \leftarrow \frac{1}{2}(\psi_{\uparrow} + \psi_{\downarrow})$   $\triangleright$  /* Use bisection to find the  $\psi$  within the interval */
     $\sum_i x_i \leftarrow \sum_i y_i \times p/p_i^*(\psi)$   $\triangleright$  /* Equation (47) */
    if  $\sum_i x_i > 1$  then
       $\psi_{\downarrow} \leftarrow \psi$   $\triangleright$  /* New range is  $\psi$  to  $\psi_{\uparrow}$  */
    else
       $\psi_{\uparrow} \leftarrow \psi$   $\triangleright$  /* New range is  $\psi_{\downarrow}$  to  $\psi$  */
    end if
  until  $\frac{|\psi_{\uparrow} - \psi_{\downarrow}|}{\frac{|\psi_{\uparrow} + \psi_{\downarrow}|}{2}} < \epsilon$   $\triangleright$  /* Iterate until  $\psi_{\uparrow}$  and  $\psi_{\downarrow}$  are equal to within precision  $\epsilon$  */
   $\psi \leftarrow \frac{1}{2}(\psi_{\uparrow} + \psi_{\downarrow})$   $\triangleright$  /* Final computed value of the reduced grand potential  $\psi$  */
   $\sum_i x_i \leftarrow \sum_i y_i \times p/p_i^*(\psi)$   $\triangleright$  /* Mole fractions sum to unity (within precision  $\epsilon$ ), Equation (48) */
  for  $i \in \{1, \dots, N_c\}$  do
     $x_i \leftarrow \frac{y_i p}{p_i^*(\psi)}$   $\triangleright$  /* Equation (47) */
  end for
   $1/q^T \leftarrow \sum_i \frac{x_i}{f_i(\psi)}$   $\triangleright$  /* Equation (50) */
  for  $i \in \{1, \dots, N_c\}$  do
     $q_i \leftarrow x_i q^T$   $\triangleright$  /* Equation (52) */
  end for
  return  $\psi$ ,  $x_i$ ,  $q_i$ 
end function
  
```

3.6.4. IAST++ [121]

IAST++ [121] is a user-friendly graphic user interface software that can fit the adsorption data to various isotherm models and use the ideal adsorbed solution theory (IAST) to obtain mixture isotherm data. The authors found FastIAS to be quite unstable because it uses the Newton-Raphson method that is highly sensitive to initial conditions and therefore solved the system of equations by minimising the square of the each equation and constraints using the downhill simplex (Nelder-Mead) method [117].

3.6.5. pyGAPS [122]

pyGAPS (Python General Adsorption Processing Suite) framework [122] is a versatile and extensible software package which can be used for both routine material characterisation as well as complex adsorption isotherm processing. It contains many common characterisation methods such as: Brunauer-Emmett-Teller and Langmuir surface area, t and α_s plots, pore size distribution calculations (Barrett-Joyner-Halenda, Dollimore-Heal, Horvath-Kawazoe, DFT/NLDFT kernel fitting), isosteric enthalpy calculations, ideal adsorbed solution theory calculations, isotherm modelling and more, as well as the ability to import and store data from Excel, CSV, JSON and SQLite databases. pyGAPS includes the IAST implementation from pyIAST, which has been wrapped for interoperability with pyGAPS isotherm models.

3.6.6. GraphIAST [123]

GraphIAST (Python General Adsorption Processing Suite) framework [123] is a simple, user-friendly program for IAST loading and selectivity predictions for binary gas mixtures based on the Python module pyIAST. The authors developed a graphical user interface resembling commonly known software and made three-dimensional selectivity predictions easily accessible within just a few clicks. The input and output data structure relies on the widely used *.csv format and isotherm data can be fitted with various established models.

3.7. IAST implementation in RUPTURA

3.7.1. FastIAS algorithm

The default IAS algorithm in RUPTURA is FastIAS. The implementation follows the description in Section 3.5.3. The original formulation of O'Brien and Myers is defined in terms of a reduced pressure. As a generalisation, we use the sorption pressures and a formulation that is isotherm model agnostic. However, instead of using a convergence test criteria like Equation (150), we use the standard deviation of the obtained reduced grand potentials (using 10^{-13} as default precision).

For efficiency reasons, we cache the computed sorption pressures and reduced grand-potentials (for breakthroughs for each grid point). Since the next computation is very likely close to the current solution, the next solution is usually found within only one or two FastIAS steps. However, the first computation for IAST and breakthrough usually starts at conditions where loadings, sorption pressures, and reduced grand potentials can be very small. We found that at these

conditions using Equation (136) worked better than using Equation (135) for initialisation.

3.7.2. Nested-loop algorithm using bisection

Our nested-loop implementation is based on

$$f(\psi) = \sum_{i=1}^N \frac{y_i p}{p_i^*(\psi)} = 1 \quad (199)$$

Our experience agrees with See et al. [121] that methods like Newton-Raphson do not seem able to numerically reduce the error to machine precision. We note that $\psi_i^*(p)$ is a continuous and importantly, monotonic function, and therefore also is its inverse $p_i^*(\psi)$. We therefore use bi-section on the reduced grand potential ψ . This automatically guarantees there is a single reduced grand potential ψ that is equal for all components. The decision to reduce or increase ψ is based on whether the sum of the adsorbed mole fractions is larger than unity or not. Additionally, we use the bi-section algorithm to obtain $p_i^*(\psi)$ for the supported isotherm types (see Table 1). The bisection algorithm is described in detail in Algorithm 2 for IAST and in Algorithm 3 for inverse computations. The algorithm of Hoseinpoori [124] is also based on bisection, but on $x_1 + x_2$, which is therefore limited to binary components.

For a function f on an interval $[a, b]$, bisection iterates through the following steps:

- (1) Calculate the midpoint $c = \frac{1}{2}(a + b)$
- (2) Calculate the function value at the midpoint, $f(c)$
- (3) If convergence criteria is not met, examine whether $f(c)$ is smaller or larger than unity and replace either $(a, f(a))$ or $(b, f(b))$ with $(c, f(c))$ and continue with the new (smaller) interval.

The method converges linearly with rate 1/2, i.e. the absolute error is halved at each step.

The bisection method is insensitive to the starting values. However, we also cache $p_i^*(\psi)$ for all components, so that subsequent evaluations use efficient starting values. The bisection method is slow, since (a) bisection itself is slow, (b) it needs the inverse reduced grand potential (numerically), and (c) the nested-loop algorithm requires many iterations. We have implemented this method based on its robustness and accuracy, i.e. it is able to always converge to machine precision. We use a relative tolerance of 10^{-15} . For our use cases in IAST and IAST in fixed-bed adsorption simulations, this was achieved in under 50 steps, even for complex 10-component mixtures.

The FastIAS method is much faster than the nested-loop algorithm using bisection method. Therefore, it is used as the default method in RUPTURA. We also plan to include the false position method [125] in the next version of RUPTURA.

3.8. Validation

Moon and Tien [110] and Landa et al. [74] considered a ten-component mixture described by the O'Brien and Myers

Algorithm 3 Inverse computation using bi-section. The tolerance value ϵ can be set to 10^{-15} .

```

function  $p(\psi)$ 
   $p \leftarrow$  initial value
   $p_{\uparrow} \leftarrow p$ 
   $p_{\downarrow} \leftarrow p$ 
  if  $\psi(p) > 1$  then
    repeat
       $p_{\uparrow} \leftarrow 2 \times p_{\uparrow}$ 
    until  $\psi(p_{\uparrow}) < 1$ 
  else
    repeat
       $p_{\downarrow} \leftarrow p_{\downarrow} / 2$ 
    until  $\psi(p_{\downarrow}) > 1$ 
  end if
  repeat
     $p \leftarrow \frac{1}{2}(p_{\uparrow} + p_{\downarrow})$ 
    if  $\psi(p) > 1$  then
       $p_{\downarrow} \leftarrow p$ 
    else
       $p_{\uparrow} \leftarrow p$ 
    end if
  until  $\frac{|p_{\uparrow} - p_{\downarrow}|}{|p_{\uparrow} + p_{\downarrow}|} < \epsilon$ 
   $p \leftarrow \frac{1}{2}(p_{\uparrow} + p_{\downarrow})$ 
  return  $p$ 
end function

```

\triangleright /* Initialize the top bracket with the initial p value */
 \triangleright /* Initialize the bottom bracket with the initial p value */
 \triangleright /* bottom bracket known, searching for top bracket */
 \triangleright /* top bracket known, searching for bottom bracket */
 \triangleright /* Use bisection to find the p within the interval */
 \triangleright /* New range is p to p_{\uparrow} */
 \triangleright /* New range is p_{\downarrow} to p */
 \triangleright /* Iterate until p_{\uparrow} and p_{\downarrow} are equal to within precision ϵ */

adsorption isotherm model

$$q(p) = q^{\text{sat}} \left[\frac{bp}{1+bp} + \sigma^2 \frac{bp(1-bp)}{2(1+bp)^3} \right] \quad (200)$$

with reduced grand potential [23,74]

$$\psi(p) = q^{\text{sat}} \left[\ln[1+bp] + \frac{\sigma^2 bp}{2(1+bp)^2} \right] \quad (201)$$

In Table 5, we compare our IAST results for a 10-component mixture of Moon and Tien [110], also used in Landa et al. [74]. We obtain similar qualitative results, but quantitatively different in the third digit. The tolerance for the results of Moon et al. was 10^{-5} . Our work uses a relative precision of 10^{-15} . Our computed total loading is $q_T = 2.26563527$ mol/kg, and the sum of the adsorbed phase mole fractions $\sum_i x_i = 1$ is normalised to machine precision, compared to $q_T = 2.3050$ mol/kg and $\sum_i x_i = 0.9912$ for Moon and Tien. The component reduced grand potentials for Moon and Tien are recomputed from the reported partial pressures and adsorbed mole fractions using Equation (201) and hence, the accuracy is limited

by the accuracy of the reported adsorbed mole fractions. Nevertheless, the data illustrate a relative precision of 10^{-5} which is not enough to enforce identical reduced grand potentials ψ_i for all components.

In Table 6 we compare our IAST results for a 10-component mixture of Landa et al. [74]. The relative and absolute tolerances for the results of Landau et al. are 10^{-10} and 10^{-12} , respectively. This work uses a relative precision of 10^{-15} . Our computed total loading is $q_T = 2.117678$ mol/kg, compared an absolute loading of $q_T = 2.1142$ mol/kg by Landau et al. Note the value of $\psi = 3.76951$ mol/kg of Landa et al., computed from their reported loading data. The error in ψ is here due to the limited precision of the reported loading $q_9 = 0.0010$ mol/kg. Using our value of $q_9 = 0.001042$ in the computation yields $\psi_9 = 3.68052$ mol/kg.

4. Fixed-bed adsorption simulations

4.1. Introduction

Most industrial separation processes take place at dynamic conditions [126]. Apart from adsorption isotherms, it is also

Table 5. Parameters for the O'Brien and Myers adsorption isotherm model considered by Moon and Tien [110] for a 10-component mixture at 300 kPa, $q_T = 2.3050$ mol/kg and $\sum_i x_i = 0.9912$.

component	q_i^{sat} [mol/kg]	b_i [Pa $^{-1}$]	σ_i [-]	p_i [kPa]	y_i [-]	ψ_i [mol/kg] (Ref. [110])	ψ_i [mol/kg] (this work)	x_i [-] (Ref. [110])	x_i [-] (this work)
1	5.0	1.0×10^{-5}	1.2	30.0	0.1	4.261	4.19182774500228	0.3129	0.321867
2	3.0	0.6×10^{-5}	1.1	30.0	0.1	4.191	4.19182774500229	0.0698	0.069755
3	4.0	0.09×10^{-5}	0.8	30.0	0.1	4.194	4.19182774500228	0.0164	0.016412
4	2.0	1.0×10^{-5}	1.2	60.0	0.2	4.191	4.19182774500229	0.0926	0.092559
5	3.5	0.3×10^{-5}	1.0	30.0	0.1	4.191	4.19182774500228	0.0459	0.045873
6	4.0	0.1×10^{-5}	1.1	15.0	0.05	4.201	4.19182774500229	0.0102	0.010241
7	2.0	1.5×10^{-5}	1.2	15.0	0.05	4.192	4.19182774500228	0.0347	0.034710
8	2.5	0.1×10^{-5}	1.15	15.0	0.05	4.170	4.19182774500228	0.0040	0.003953
9	4.0	0.01×10^{-5}	1.0	15.0	0.05	4.145	4.19182774500228	0.0010	0.000980
10	5.5	0.6×10^{-5}	1.0	60.0	0.2	4.192	4.19182774500228	0.4037	0.403652

Notes: The tolerance for the results of Moon et al. was 10^{-5} . This work uses a relative precision of 10^{-15} . Our computed total loading is $q_T = 2.26563527$ mol/kg, and the sum of the adsorbed phase mole fractions $\sum_i x_i = 1$ is normalised to machine precision.

Table 6. Parameters for the O'Brien and Myers adsorption isotherm model considered by Landau et al. [74] for a 10-component mixture, $q_r = 2.1142$ mol/kg.

component	q_i^{sat} [mol/kg]	b_i [Pa ⁻¹]	σ_i [-]	p_i [kPa]	y_i [-]	ψ_i [mol/kg] (Ref. [110])	ψ_i [mol/kg] (this work)	q_i [mol/kg] (Ref. [74])	q_i [mol/kg] (this work)
1	5.0	1.0×10^{-5}	1.2	30.0	0.1	3.68342	3.683573349491790	0.8443	0.845631
2	3.0	0.6×10^{-5}	1.1	3.0	0.01	3.68238	3.683573349491790	0.0192	0.019219
3	4.0	0.09×10^{-5}	0.8	3.0	0.01	3.69288	3.683573349491789	0.0043	0.004325
4	2.0	1.0×10^{-5}	1.2	15.0	0.05	3.68419	3.683573349491789	0.0677	0.067839
5	3.5	0.3×10^{-5}	1.0	60.0	0.2	3.68371	3.683573349491791	0.2467	0.247123
6	4.0	0.1×10^{-5}	1.1	60.0	0.2	3.68317	3.683573349491790	0.1093	0.109459
7	2.0	1.5×10^{-5}	1.2	30.0	0.1	3.68345	3.683573349491791	0.2032	0.203517
8	2.5	0.1×10^{-5}	1.15	60.0	0.2	3.68459	3.683573349491790	0.0446	0.044700
9	4.0	0.01×10^{-5}	1.0	6.0	0.02	3.76951	3.683573349491788	0.0010	0.001042
10	5.5	0.6×10^{-5}	1.0	33.0	0.11	3.68348	3.683573349491788	0.5739	0.574822

Notes: The relative and absolute tolerances for the results of Landau et al. are 10^{-10} and 10^{-12} , respectively. This work uses a relative precision of 10^{-15} . Our computed total loading is $q_r = 2.117678$ mol/kg.

important to evaluate properties like cyclic stability, long time stability, competitive adsorption and mass transfer kinetics [126]. Knowledge of these properties is vital for selecting an appropriate adsorbent for a specific separation process. These properties can be obtained using dynamic methods. In most dynamic methods, adsorbents are arranged in fixed beds [127] and the gas mixture is passed through them. Adsorption in fixed beds is carried out in cylindrical columns filled with particles of nanoporous materials. The nanoporous particles are held fixed in place and do not move (Figure 7). Adsorbents are commonly operated in a transient mode. Consequently, the compositions of the gas phase, and of the adsorbed molecules inside the adsorbent particles vary with position and time. Transient breakthrough curves are crucial for evaluating the performance of an adsorbent material to separate certain compounds, or to encapsulate a single component [128]. It is also important to acknowledge the fact that the study of breakthrough curves cannot be the sole criterion in designing an adsorption-based system. A full-scale process simulation is required to serve the purpose [129,130]. Measurements of breakthrough curves through experiments involves several steps ranging from preparing the samples to analyse the results [109]. This procedure can be very time consuming especially, when breakthrough curves are used to screen a large number of potential adsorbents for a specific separation process [109]. Therefore, breakthrough curve modelling can be very handy in designing adsorption based separation columns and selecting the best adsorbent material for the process.

The fluid containing the solute flows through the packed bed of adsorbents, usually at a constant mass flow rate. The

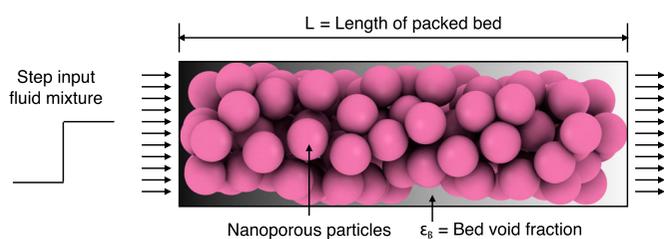


Figure 7. (Colour online) Schematic representation of a packed bed adsorber. The packed bed adsorber is a cylindrical column filled with nanoporous adsorbent material (crystalline or amorphous). When a fluid mixture is fed as input to the column, adsorption of various components present in the mixture takes place inside these nanoporous materials.

breakthrough curve has mainly three segments: the unsaturated zone, the mass transfer zone (MTZ) and the saturated zone [126]. These segments are shown in Figure 8. The unsaturated zone is the region where the fluid phase and the adsorbed phase are not in equilibrium. The majority of the adsorption of the components take place in this zone. The mass transfer zone (MTZ) is the range of the bed where the adsorption process rapidly progresses towards equilibrium. There is a rapid increase in the outlet concentration in this zone which is influenced by the mass transfer between the gas phase and the adsorbed phase [131], axial dispersion, and heat transfer effects [126]. During operation, this zone moves along the bed from the inlet point to the outlet point. Inside the MTZ, the loading of absolute adsorbates varies from the saturation limit to 0%. When the front edge of the MTZ reaches the end point of the bed, the 'breakthrough' occurs (often defined as when the concentration at the outlet reaches a predefined value, e.g. 1%, of the inlet concentration). The saturated zone determines the adsorption capacity of the components [126]. In this zone, the adsorbed phase is in

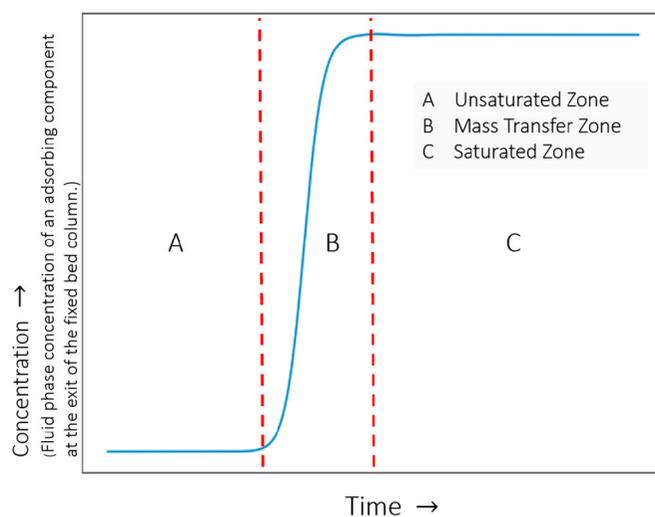


Figure 8. (Colour online) Different zones in a breakthrough curve at the exit of the fixed bed column. Fluid phase concentration of an adsorbing component as a function of time at the fixed bed column outlet. The profile is divided into three zones: (a) the unsaturated zone: where the maximum adsorption takes place, (b) mass transfer zone: where adsorption process progresses rapidly towards equilibrium, (c) saturated zone: where no more adsorption takes place as equilibrium between the fluid and the adsorbed phase is achieved.

equilibrium with the fluid phase. Therefore, no net mass transfer from the fluid phase to the adsorbed phase takes place.

When the fluid flows across the solid surface, a stagnant film forms along that surface. Molecules from the bulk interstitial phase are transported via axial convection onto the film. Inside the film there is velocity gradient in the direction of the flow but not in the perpendicular direction. Therefore, advection does not occur in the film and molecules diffuse across the stagnant film. The driving force of film diffusion is the concentration gradient located at the interface region between the exterior surface of the adsorbent particles and the bulk solution. The stagnant film thickness is proportional to the Reynolds number of the bulk fluid. The external mass transfer resistance is strongly dependent on the flow conditions, e.g. temperature, pressure, and superficial velocity [132]. The adsorbate molecules transfer between the fluid and adsorbent particles through several steps [132–134]:

- (1) transport of adsorbate from bulk fluid to the localised hydrodynamic boundary layer around the adsorbent,
- (2) interface diffusion between fluid phase and the exterior surface of the adsorbent (often called ‘external’, ‘inter-phase’, or ‘film’ diffusion),
- (3) intraparticle mass transfer involving pore diffusion and surface diffusion,
- (4) adsorption of molecules on the inner surface,
- (5) if the solid is a catalyst: reactions taking place at specific active sites inside the catalyst material,
- (6) desorption of the molecules from the inner surface,
- (7) diffusion of the products from the interior of the particle to the pore mouth at the external surface,
- (8) diffusion of the products from the external particle surface to the bulk fluid (inter phase diffusion).

Molecules in the column can move in both axial and radial directions. In case of plug flow behaviour, any variation in the radial direction is absent so the velocity of the fluid, the concentration, and the porosity are assumed to be constant across any cross-section of the bed perpendicular to the axis of the bed. Variation of the velocity in the radial direction can be neglected if the flow is not highly viscous and no considerable boundary layer is formed in that direction. The assumption of neglecting radial gradients is widely accepted [135–137]. The effects of dispersion in all directions are included in the axial dispersion term [6]. To account for the adsorption, we use the Linear Driving Force (LDF) model [32]. In this model, the adsorption of molecules from all directions into adsorbent particles is lumped into a single entity, called average adsorbed loading (q_i). One can also model the adsorption process by considering variation in the radial direction inside the zeolites. This is possible using the Fick diffusion model. Sircar and Huffman compared the LDF model with the rigorous Fick diffusion model [138]. These authors found that the details regarding the intra-pore diffusion are lost when breakthrough curves are modelled [138]. Therefore, the authors concluded that in most cases the LDF model is sufficient to account for the effects of adsorption.

Various mathematical models can be derived from conservation of mass, energy, and momentum and augmented by appropriate transport rate equations and equilibrium isotherms [139]. Mathematical models of fixed-bed columns for adsorption are reviewed by Tien [20,140], Worch [64,141], Siahpoosh et al. [142], Xu et al. [134], Shafeeyan et al. [137], Supian et al. [143], Unuabonah et al. [144], and many others. These models differ mainly in the form of the mass transfer rate, the form of the equilibrium isotherm, thermal effects, and the pressure drop along the bed. Fixed-bed column adsorption studies are reviewed by Patel [127] on removal of various contaminants from wastewater.

Fixed-bed models are either zero-phase, one-phase, two-phase or multi-phase resistance models [6,144]. A zero-phase model ignores mass transfer and assumes instantaneous equilibrium along the column. The one-phase resistance models assume local equilibrium in any cross section along the bed. These models take dispersion and/or diffusion into account but neglect intra-particle diffusion resistance and intra-particle axial dispersion. The one-phase models, known as chemical kinetic models, assume that the mass transfer rate is the difference between two opposing second-order reactions with different rate constants [145], and include [20,144]: the Thomas model [146], Bohart-Adams model [147], Yoon-Nelson models [148,149], and Clark model [150]. One-phase models have direct nonlinear mathematical expressions but are not very accurate in describing the breakthrough behaviour in a column [151]. Two-phase resistance models take into account both film and intra-particle diffusion. These models are more accurate than one-phase resistance models but have to be solved numerically. Multiphase resistance models take multiple types of diffusion (film diffusion, pore diffusion, and surface diffusion) into account. In the diffusion models, the particle is treated as a homogeneous phase [145]. Note that often surface reaction rates are assumed to be much faster than diffusion. Surface reactions should be considered when it affects the adsorption rate or is the controlling step. Plazinski et al. [152] reviewed sorption kinetic models including surface reaction mechanism. Medved and Cerny [153] reviewed surface diffusion of particles in porous media.

4.2. Theory

To model the fixed bed adsorber column, the following assumptions are considered [142]:

- The fixed bed is tubular and the adsorbent particles are spherical. The particles are packed uniformly into the fixed bed (no channeling occurs).
- No chemical reaction occurs in the column. This aspect will be considered in our future work.
- The fixed bed is initially filled with carrier gas.
- The gas phase behaves as an ideal gas mixture.
- The process is isothermal adsorption.
- The mass and velocity gradients are negligible in radial direction of the bed.
- The pressure gradient (if any) is invariant with time and column position and is not affected by the adsorption process.

- The fluid velocity is varying according to the total mass balance along the bed in multi-component systems. The fluid velocity will vary along the length of the column because of the variation in total pressure and/or adsorption of the molecules from the fluid phase.
- The axial dispersion is considered in the bulk phase.
- The carrier gas does not adsorb.
- The physical properties of the gas phase (axial dispersion coefficient and mass transfer coefficient) are those of the feed gas. These properties along with the properties (particle density and bed porosity) of the adsorbent are constant throughout the column.

For future versions of RUPTURA, we envision to include non-ideal gas behaviour, liquid phase conditions, non-isothermal breakthroughs, and chemical reactions.

We follow Worch [64] to outline the establishment of the material balance. Considering a differential volume element $dV = A_r dz$, it can be assumed that the amount of adsorbate that is adsorbed onto the adsorbent or accumulated in the void fraction of the volume element must equal the difference between the input and the output of the volume element. Input and output occurs by advection and axial dispersion. The general mass balance equation is as follows [64]

$$\dot{N}_{\text{accu.}} + \dot{N}_{\text{ads.}} = \dot{N}_{\text{adv.}} + \dot{N}_{\text{disp.}} \quad (202)$$

where \dot{N} represents the change of the amount of adsorbate with time, and the indices indicate the processes accumulation, adsorption, advection, and dispersion.

- The accumulation term is:

$$\dot{N}_{\text{accu}} = \varepsilon_b dV \frac{\partial c(t, z)}{\partial t} \quad (203)$$

where c represents the adsorbate concentration in the fluid phase, z is the distance along the bed length, t denotes time, and ε_b is the bed void fraction.

- The adsorption term is expressed as:

$$\dot{N}_{\text{ads}} = \rho_b dV \frac{\partial \bar{q}(t, z)}{\partial t} \quad (204)$$

$$= (1 - \varepsilon_b) \rho_p \frac{\partial \bar{q}(t, z)}{\partial t} \quad (205)$$

where ρ_b is the bed density, ρ_p is the particle density. The units of both ρ_b and ρ_p are $[\text{kg}/\text{m}^3]$. \bar{q} denotes the average concentration in adsorbent particle in $[\text{mol}/(\text{kg framework})]$, which forms a link between the fluid and solid phase mass balance equations.

- Advection is the transport of substances due to the bulk motion of the fluid in the axial direction and is the

difference between the input and output amount per unit time.

$$\dot{N}_{\text{adv}} = u(t, z)A_r c(t, z) - u(t, z + dz)A_r c(t, z + dz) \quad (206)$$

$$= -A_r \frac{\partial u(t, z)c(t, z)}{\partial z} dz \quad (207)$$

$$= -dV \frac{\partial u(t, z)c(t, z)}{\partial z} \quad (208)$$

$$= -\varepsilon_b dV \frac{\partial v(t, z)c(t, z)}{\partial z} \quad (209)$$

where v is the interstitial velocity of the gas phase (related to the superficial gas velocity u by $v = u/\varepsilon_b$).

- Assuming that the axial dispersion can be described by Fick's first law [154], the difference between input and output caused by dispersion is as follows:

$$\dot{N}_{\text{disp}} = \mathcal{D}\varepsilon_b A_r \left[\frac{\partial c(t, z)}{\partial z} \right]_{z+dz} - \mathcal{D}\varepsilon_b A_r \left[\frac{\partial c(t, z)}{\partial z} \right]_z \quad (210)$$

$$= \mathcal{D}\varepsilon_b A_r \frac{\partial^2 c(t, z)}{\partial z^2} dz \quad (211)$$

$$= \mathcal{D}\varepsilon_b dV \frac{\partial^2 c(t, z)}{\partial z^2} \quad (212)$$

where \mathcal{D} is the axial dispersion coefficient.

Introducing Equations (203), (205), (209), and (212) into Equation (202), dividing by the control volume (dV) and the bed void-fraction (ε_b), and applying the balance equation to each component, we obtain the main governing equation for the fixed-bed model [6,145].

$$\frac{\partial c_i(t, z)}{\partial t} = -\frac{\partial(v(t, z)c_i(t, z))}{\partial z} + \mathcal{D}_i \frac{\partial^2 c_i(t, z)}{\partial z^2} - \frac{1 - \varepsilon_b}{\varepsilon_b} \rho_p \frac{\partial \bar{q}_i(t, z)}{\partial t} \quad (213)$$

For the i th component, the component mass balance including axial dispersion term, an advection flow term, accumulation in the fluid phase, and source term caused by the adsorption process on the adsorbent particles. If the system is non-isothermal, an additional heat-balance is required [6].

4.3. Axial dispersion

Models that consider the dispersion are referred to as dispersed-flow models, whereas models that neglect dispersion are termed plug-flow models. In practice, most experiments are set up such that the plug flow assumption is valid. During the fluid flow through the packed bed, axial mixing takes place, which reduces the efficiency of the separation process by broadening the mass transfer zone. Axial mixing is caused by molecular diffusion, turbulent mixing, flow splitting, and rejoining around particles, Taylor dispersion, channeling, and wall effects [6,155]. These phenomena can be minimised by choosing proper bed and flow conditions. Axial dispersion does depend on the Reynolds number and therefore, changes along the column when appreciable amounts are adsorbed.

Table 7. Correlations for estimation of axial dispersion coefficient, D_z in fixed bed adsorbers.

Dispersion Model	Conditions	Authors
$D_z = \frac{2r_p v \varepsilon_b}{0.2+0.011 Re^{0.488}}$	$10^{-3} < Re < 10^3$	Chung and Wen [157]
$D_z = 0.7D_m + \frac{5r_p v}{1+4.4D_m/(r_p v)}$	valid for liquids	De Ligny [156]
$D_z = 0.7D_m + \frac{2r_p v \varepsilon_b}{0.18+0.008 Re^{0.59}/(r_p v)}$	–	Rastegar and Gu [158]
$D_z = 0.73D_m + \frac{0.5d_p v \varepsilon_b}{1+(9.7D_m)/(v \varepsilon_b d_p)}$	$0.008 < Re < 50, 0.0377 < d_p < 0.60 \text{ cm}$	Edwards and Richardson [159]
$D_z = \frac{20D_m}{\varepsilon_b} + \frac{0.5D_m Sc Re}{\varepsilon_b}$	–	Shafeeyan, da Silva [137,160]
$D_z = (0.45 + 0.55\varepsilon_b)D_m + r_p v$	–	Ruthven [6]

Notes: D_m is the molecular diffusivity, Sc is the Schmidt number and Re is the Reynolds number. r_p and d_p are the particle radius and particle diameter respectively. v represents velocity and ε_b is the bed porosity.

In particular, the Peclet number describes axial dispersion. The effects of all mechanisms that contribute to axial mixing are lumped into a single effective axial dispersion coefficient, D_z . Generally, the contribution from molecular diffusion and Eddy diffusion or turbulence is considered in the formulation of dispersion coefficient. Coupling theory is used to add the contribution of both the terms as shown in the equation stated below [156].

$$D_z = \gamma D_m + \frac{\lambda d_p v}{1 + CD_m/(d_p v)} \quad (214)$$

When intra-particle mass-transfer is neglected (if the product of Reynolds number and Schmidt number, $(Re \cdot Sc) \gg 1$, advection dominates diffusion), D_z can be estimated using Equation (214).

Table 7 shows various correlations to calculate axial dispersion coefficient, D_z . D_z is a function of molecular diffusivity (D_m), particle radius (r_p), fluid phase velocity (v) and bed porosity (ε_b). The molecular diffusivity, D_m used in the expression for axial dispersion coefficient can be calculated either using Molecular Dynamics [83,161,162] or the Chapman-Enskog theory [163,164]:

$$D_m = \frac{AT^{3/2}}{p\sigma_{12}^2\Omega} \left(\frac{1}{M_1} + \frac{1}{M_2} \right)^{0.5} \quad (215)$$

In Equation (215), A is an empirical constant of magnitude $1.859 \cdot 10^{-7}$. T is the temperature in [K] and p is the partial pressure of the molecule in [atm]. M is the molar mass in [g/mol]. σ_{12} is the average collision diameter between molecules 1 and 2 in [Å] and Ω is the temperature dependent collision integral. The expressions for σ_{12} and Ω [142] are as follows.

$$\sigma_{12} = \frac{1}{2}(\sigma_1 + \sigma_2) \quad (216)$$

$$\Omega = \left(44.54(k_b T/\varepsilon_{ij})^{-4.909} + 1.911(k_b T/\varepsilon_{ij})^{-1.575} \right)^{0.1} \quad (217)$$

$\sigma_{i,j}$ in Equation (216), and $\varepsilon_{i,j}$ in Equation (217) are the effective Lennard-Jones parameters [165,166] for a mixture of molecules i and j . $\varepsilon_{i,j}$ is defined by $\sqrt{\varepsilon_i \varepsilon_j}$ and k_b is the Boltzmann constant. The expressions for the Lennard-Jones parameters for a molecule i can be estimated as follows.

$$\sigma_i = 0.841 V_c^{1/3} \quad (218)$$

$$\varepsilon_i = 0.75 k_b T_c \quad (219)$$

In Equations (218) and (219), V_c and T_c are the critical volume and critical temperature of the molecule i respectively [142]. V_c is in [Å³] and T_c is in [K].

4.4. Mass transfer models

Inside nanoporous materials, molecules can diffuse into the framework via pore diffusion and surface diffusion [24]. Diffusion of the particles in the pores occurs through two transfer processes depending on the pore size [6]: (1) molecular diffusion, which results from collisions between molecules, dominates in macro pores, (2) Knudsen diffusion occurs for smaller pore sizes due to collisions between molecules and the pore wall. In the surface diffusion mechanism, molecules hop between adsorption sites. It is therefore strongly dependent on concentration. For much more details on diffusion in nanoporous materials, see Ref. [167] and references therein.

The term $\partial \bar{q}(t, z)/\partial t$ in Equation (213) describes adsorption and the overall rate of mass transfer from the fluid phase to the solid phase at time t and column distance z . The adsorbate molecules initially must cross the external film surrounding each adsorbent particle and then diffuse through and along the porous structure of the adsorbent. Many models are developed that differ in the rate-limiting mass transport step [134,144,168,169]: the Linear Driving Force (LDF) model [32], the homogeneous surface diffusion model [170], the film-solid diffusion model with a constant diffusivity [171], the branched pore kinetic-model [172], the pore diffusion model [6,173], the film-pore diffusion model [174], the diffusion flow-film particle diffusion model [175], the diffusion flow-local equilibrium model [176], the film pore and surface diffusion model [177–180], and the concentration-dependent surface diffusivity model [181] to name but a few. The most frequently applied approximate rate law to simplify the calculation is the LDF approximation [32]. In most cases, the LDF model is a good approximation to the exact but much more complicated surface and pore diffusion models [64].

Self-diffusion is a measure of the mobility of molecules due to their thermal motions, while collective diffusion is a dynamic process, involving many particles, due to their cooperative movements [182]. The collective diffusion is related to the transport diffusion coefficient by the thermodynamic factor [183–185], which can be obtained from the adsorption isotherms. Transport diffusion, taking the thermodynamic effects into account using a Fickian type of approach, can be incorporated in the equipment design equations. The differences

between collective and transport diffusion show that there are different viewpoints possible to study diffusion [184–186]:

- In the Fick approach, the fluxes \mathbf{N} are taken to be linearly dependent on the gradients of the loadings ∇c_i of all species with the ‘constants’ of proportionality being the Fick diffusivity matrix.
- In the Onsager approach, the fluxes are postulated as linear functions of the chemical potential gradients ($\nabla \mu_i$), with the proportionality constants being the Onsager coefficients L_{ij} .
- The Maxwell-Stefan formulation balances diffusive and drag forces, while Fick and Onsager postulate phenomenological flux expressions. The Maxwell-Stefan diffusivity can be related to Fick diffusivity as follows [183,187]

$$D_F = D_{MS} \Gamma \quad (220)$$

In Equation (220), D_{MS} is the Maxwell-Stefan diffusivity and D_F is the Fick diffusivity. Γ is the thermodynamic correction factor which is derived using chemical potential as the driving force [187]. This factor can be determined from adsorption isotherms after differentiation as shown below [187].

$$\Gamma \equiv \frac{\partial \ln f}{\partial \ln q} \quad (221)$$

In Equation (221), f is the fugacity and q is the adsorbed loading. To understand the underlying principles behind the diffusion process, it is more convenient to describe this phenomenon using Maxwell-Stefan diffusivity [187]. This approach clearly distinguishes between self diffusivity, diffusivity of a species inside an adsorbent, and diffusivity describing interaction between different species [187].

The viewpoints differ in how to set up the flux-driving force relationship for transport diffusion in nanoporous materials under non-equilibrium conditions [184,188–190].

In Onsager linear theory, the driving force of diffusion is the gradient of the chemical potential, μ , of the adsorbed particles. The diffusion flux \mathbf{J} is [191]

$$\mathbf{J} = -L \nabla \left(\frac{\mu}{T} \right) = -\frac{L}{T} \frac{\partial \mu}{\partial q} \nabla q \quad (222)$$

where L is the Onsager coefficient and q is the adsorption loading. From the practical point of view, the flux \mathbf{J} is usually related to the gradient diffusion coefficient D that depends on adsorption [191]

$$\mathbf{J} = -D \nabla q, \quad D = D_0 \frac{1}{k_B T} \frac{\partial \mu}{\partial \ln q} \quad (223)$$

where $D_0 = kL/q$ does not depend on adsorption and has the meaning of the diffusivity at zero loading. The driving force for diffusion is more correctly expressed in terms of chemical potentials, but Fick’s law provides a qualitatively and quantitatively correct representation of adsorption systems as long as the diffusivity is allowed to be a function of the adsorbate concentration [192]. However, for convenience, the diffusivity is often taken as the self-diffusivity and assumed to be a

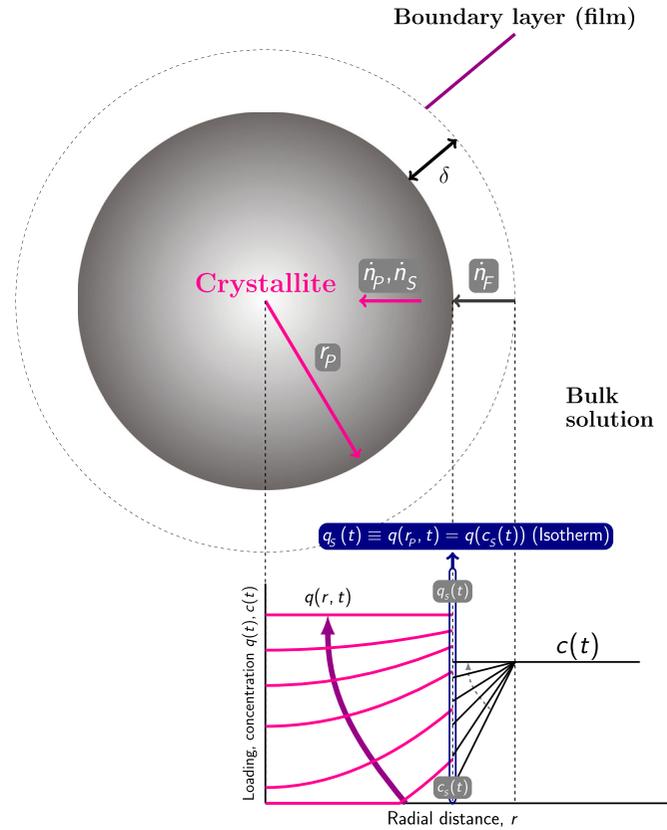


Figure 9. (Colour online) Loading and concentration profiles according to the pore diffusion model with external mass transfer resistance. The external mass transfer resistance is modeled using the film flux $\dot{n}_F(t) = K_f(c(t) - c_s(t))$, which is the linear difference of the concentration $c(t)$ in the bulk solution, and the concentration $c_s(t)$ at the surface of the crystallite. The flux $\dot{n}_T = \dot{n}_p + \dot{n}_s$ is the sum of the pore diffusion and surface diffusion: $\dot{n}_T = D_p \partial c_p / \partial r + \rho_p D_s \partial q / \partial r$. The continuity of the materials fluxes requires $\dot{n}_F = \dot{n}_T$. The surface is considered to be in equilibrium and the adsorbent loading $q(r_p, t) = q(p(t))$ is calculated from the isotherm with functional form q , where the pressure p is related to the surface concentration c_s via the ideal gas law as $p = RTc_s$.

constant. In the limit of zero loading, the self-, collective-, and transport diffusivities become equal.

Film diffusion comprises the transport of the adsorbate from the bulk fluid to the external surface of the adsorbent particle. As long as the state of equilibrium is not reached, the concentration at the external adsorbent surface is always lower than in the bulk fluid due to the continuing adsorption process. As a consequence, a concentration gradient results that extends over a boundary layer of thickness δ (schematically shown in Figure 9). The difference between the concentration in the bulk solution, c , and the concentration at the external surface, c_s , acts as a driving force for the mass transfer through the boundary layer. The mass transfer flux \dot{n}_F for the film diffusion can be derived from Fick’s law

$$\dot{n}_F = D_L \frac{dc}{d\delta} \quad (224)$$

leading to a film mass transfer equation [64]

$$\frac{d\bar{q}}{dt} = k_F \frac{a_{VR}}{\rho_B} (c - c_s) \quad (225)$$

where k_F is the film mass transfer coefficient in $[\text{ms}^{-1}]$, c_s the concentration at the external surface, and the external surface

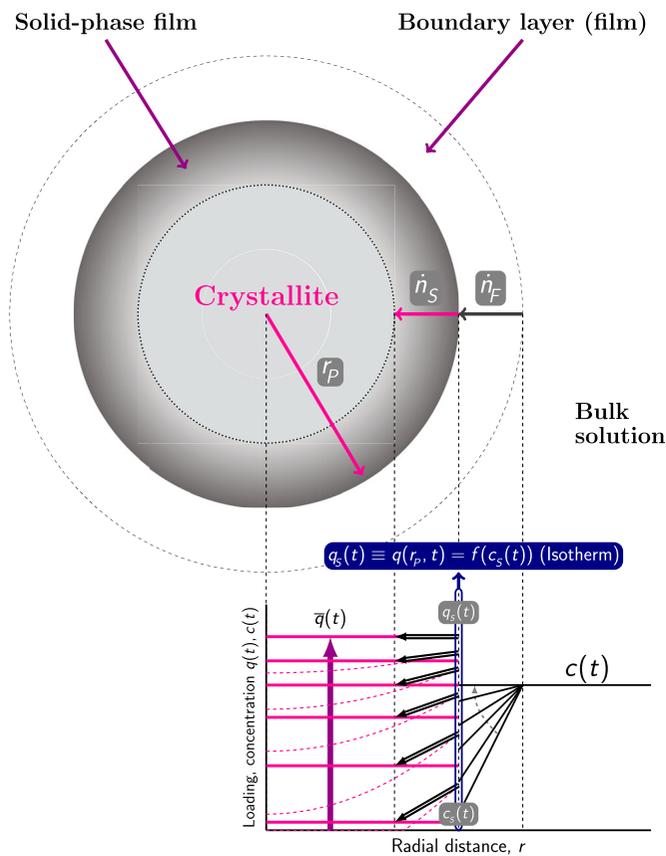


Figure 10. (Colour online) Loading and concentration profiles according to the Linear Driving Force (LDF) model with external mass transfer resistance. The LDF model assumes that there is linear gradient within the solution-side film and within a comparable fictive solid film. The film flux $\dot{n}_F(t) = K_f(c(t) - c_s(t))$ is the linear difference of the concentration $c(t)$ in the bulk solution, and the concentration $c_s(t)$ at the surface of the crystallite. The solid flux \dot{n}_s is the linear difference between the equilibrium loading q_s at the surface and the average loading \bar{q} : $\dot{n}_s(t) = \rho_p k_s(q_s(t) - \bar{q}(t))$, where ρ_p is the particle density, k_s is the intra-particle mass transfer coefficient. The continuity of the materials fluxes requires $\dot{n}_s = \dot{n}_F$. The surface is considered to be in equilibrium and the adsorbent loading $q(r, t) = q(p(t))$ is calculated from the isotherm with functional form q , where the pressure p is related to the surface concentration c_s via the ideal gas law as $p = RTc_s$.

related to the column (a_{VR}) is

$$a_{VR} = A_s / V_B \tag{226}$$

where A_s is the external adsorbent surface area and V_B is the fixed-bed volume. For spherical particles, $a_{VR} = (1 - \epsilon_b)3/r_p$. In most practical cases, the film diffusion influences only at the beginning of the adsorption process. At later stages of the process, the intra-particle diffusion becomes more important.

The local equilibrium model ignores the mass transfer resistance, and assumes that the mass transfer between solid adsorbent particles and external gas is instantaneous.

$$\frac{\partial q_i}{\partial t} = \frac{\partial q_i^*}{\partial t} \tag{227}$$

where q_i is the average amount of component i adsorbed, q_i^* is the amount adsorbed at equilibrium given by the selected adsorption isotherm model. Because of neglecting the mass transfer resistance, the model has accepted limitation in the practical applications.

In the Homogeneous Surface Diffusion Model (HSDM) [170,193], the main diffusion mechanism is the surface diffusion. The HSDM assumptions are the following [194]:

- mass balance around a spherical shell element.
- internal mass transfer is only governed by surface diffusion.
- external mass transfer is governed by a linear driving force.
- at the solid/fluid interface, there is continuity between external mass transfer and internal diffusion.
- at the solid/fluid interface, there is equilibrium between adsorbate concentration in the fluid and adsorbate load on the surface.
- the adsorbent particle is assumed to be spherical and homogeneous.

The adsorbent is assumed to be a uniform medium in which the solute adsorbs on the surface and diffuses inwards with an effective diffusivity in accordance with Fick's law. For surface diffusion, the mass transfer rate per unit of surface area, \dot{n}_s , is obtained using Fick's law as

$$\dot{n}_s = \rho_p D_s \frac{\partial q}{\partial r} \tag{228}$$

where D_s is the surface diffusion coefficient and r is the radial coordinate. Imposing a material balance and assuming D_s to be constant leads to the basic mathematical form of the HSDM for a spherical particle [64,140,195]:

$$\frac{\partial q}{\partial t} = \frac{D_s}{r^2} \frac{\partial}{\partial r} \left(r^2 \frac{\partial q}{\partial r} \right) = D_s \left(\frac{\partial^2 q}{\partial r^2} + \frac{2}{r} \frac{\partial q}{\partial r} \right) \tag{229}$$

The homogeneous surface diffusion model is closely related to the homogeneous solid diffusion model and the film-solid diffusion model [196]. In the homogeneous solid diffusion model, all solute within the particle, whether it is in pore fluid or adsorbed by particle skeleton is lumped into a single quantity, q [195].

In the Pore Diffusion Model (PDM) [6], the adsorbate transport within the adsorbent particles takes place in the pore fluid, instead of on the surface. For pore diffusion, the mass transfer rate per unit of surface area, \dot{n}_s , is again obtained using Fick's law as

$$\dot{n}_p = D_p \frac{\partial c_p}{\partial r} \tag{230}$$

where D_p is the pore diffusion coefficient and r is the radial coordinate. In the surface diffusion model, the adsorbent is considered to be homogeneous, and the adsorption equilibrium is assumed to exist only at the outer surface of the adsorbent particle. In the case of pore diffusion, however, the adsorption equilibrium has to be considered at each point of the pore system. In general, it is assumed that there is a local equilibrium between the pore fluid concentration and the solid-phase concentration. Imposing a material balance leads to a more complicated description [64,195]

$$\rho_p \frac{\partial q}{\partial t} + \epsilon_p \frac{\partial c_p}{\partial t} = D_p \left(\frac{\partial^2 c_p}{\partial r^2} + \frac{2}{r} \frac{\partial c_p}{\partial r} \right) \tag{231}$$

In the Pore and Surface Diffusion Model (PSDM) [177], the

adsorbate transport within the adsorbent particles takes place via surface and pore diffusion. The total flux is then given as the sum of the fluxes caused by surface diffusion and by pore diffusion [64,195]

$$\dot{n}_t = \dot{n}_s + \dot{n}_p = \rho_p D_s \frac{\partial q}{\partial r} + D_p \frac{\partial c_p}{\partial r} \quad (232)$$

$$\frac{\partial q}{\partial t} = D_s \left(\frac{\partial^2 q}{\partial r^2} + \frac{2}{r} \frac{\partial q}{\partial r} \right) + \frac{D_p}{\rho_p} \left(\frac{\partial^2 c_p}{\partial r^2} + \frac{2}{r} \frac{\partial c_p}{\partial r} \right) \quad (233)$$

The concentration profiles for film and pore/surface diffusion are schematically shown in Figure 9.

The intra-particle diffusion models discussed so far include partial derivatives with respect to time and radial coordinate, which causes an increased effort for the numerical solution. The Linear Driving Force (LDF) model states that the rate of adsorption is proportional to the amount of adsorbate still required to achieve equilibrium [195]. The equation for the flux is approximated by

$$\dot{n}_s = \rho_p k (q_s - \bar{q}) \quad (234)$$

where ρ_p is the particle density, k is the mass transfer coefficient, q_s is the adsorbent loading at the external surface of the adsorbent (which is a function of the bulk composition), and \bar{q} is the mean loading in the particle. The following mass transfer equation can be derived

$$\frac{d\bar{q}}{dt} = k (q_s - \bar{q}) \quad (235)$$

The uptake rate of a species into adsorbent particles is proportional to the linear difference between the concentration of that species at the outer surface of the particle q_s (equilibrium adsorption amount) and its average concentration within the particle \bar{q} . r_p is the crystallite particle radius.

The LDF model can be derived from a model with a concentration profile within the particle. Assuming a quadratic concentration profile leads directly to the LDF form [197]. Glueckauf [32] derived a general expression to account for the mass transfer of the molecules from the fluid phase into the adsorbent [197]. This expression is valid for arbitrary variation of surface concentration of the adsorbates inside the solid particles [32]. Glueckauf also showed that for larger values of the product of mass transfer coefficient (k) and time (t), the expression is identical to the LDF model [32]. The volume-averaged adsorption amount \bar{q} is given by

$$\bar{q}(t) = \frac{\int_0^{r_p} q(r, t) 4\pi r^2 dr}{\frac{4}{3} \pi r_p^3} = \frac{3}{r_p^3} \int_0^{r_p} q(r, t) r^2 dr \quad (236)$$

Taking the derivative we get

$$\frac{\partial \bar{q}}{\partial t} = \frac{3}{r_p} \int_0^{r_p} \frac{\partial q}{\partial t} r^2 dr \quad (237)$$

Substituting the diffusion equation for spherical geometry [170,177]

$$\frac{\partial q(r, t)}{\partial t} = D \nabla^2 q(r, t) = \frac{D}{r^2} \frac{\partial}{\partial r} \left[r^2 \frac{\partial q}{\partial r} \right] \quad (238)$$

into this equation we get

$$\frac{\partial \bar{q}}{\partial t} = \frac{3D}{r_p} \int_0^{r_p} \frac{\partial}{\partial r} \left(r^2 \frac{\partial q}{\partial r} \right) dr = \frac{3D}{r_p} \left[\frac{\partial q}{\partial r} \right]_{r=r_p} \quad (239)$$

In Equations (238) and (239), D is the Fickian diffusivity. Next, we consider a generalised concentration profile

$$q(t, r) = A(t) + B(t)r^n \quad (240)$$

The linear term has been left out on account of spherical symmetry [197]. $A(t)$ and $B(t)$ can be solved from the two boundary conditions

$$\left(\frac{\partial q}{\partial r} \right)_{r=0} = 0 \quad (241)$$

$$q(r = r_p) = q(t, r_p) \quad (242)$$

A general solution for the concentration profiles is

$$q(t, r) = \begin{cases} q(t, r_p) - \frac{n+3}{n} \frac{1}{r_p^n} [q(t, r_p) - \bar{q}] r^n & 0 \leq r \leq r_p \\ q(t, r_p) & r = r_p \end{cases} \quad (243)$$

Taking the derivative of the concentration profiles

$$\left[\frac{\partial q}{\partial r} \right]_{r=r_p} = \frac{n+3}{r_p} [q(t, r_p) - \bar{q}] \quad (244)$$

Finally, substituting the result for $n=2$ into Equation (239) leads to the LDF equation

$$\frac{\partial \bar{q}}{\partial t} = \frac{15D}{r_p^2} (q_s - \bar{q}) \quad (245)$$

Therefore, the LDF model can be deduced from assuming a quadratic concentration profile [195,197]. The precision of the LDF models can be improved by using higher order models [198]. The LDF concentration profiles are schematic shown in Figure 10.

Although the LDF model was originally developed as a simplified version of the surface diffusion model [64], it can also be related to the pore diffusion model. As shown for the combined surface and pore diffusion mechanism, an effective surface diffusion coefficient can be defined as

$$D_s = D_s + \frac{D_p}{\rho_p} \frac{\partial c_p}{\partial q} \approx D_s + \frac{D_p}{\rho_p} \frac{c_0}{q_0} \quad (246)$$

In Equation (246), c_0 and q_0 represent initial ($t=0$) fluid phase concentration and adsorbed loading of the component. It is also possible to link the mass transfer coefficient (k_s) used in the LDF model with the effective surface diffusion coefficient (D_s) by [197]

$$k_s = \frac{15D_s^{\text{eff}}}{r_p^2} = \frac{15D_s}{r_p^2} + \frac{15D_p}{r_p^2} \frac{c_0}{\rho_p q_0} \quad (247)$$

Surface diffusion as well as pore diffusion can be approximated by the LDF model. In fact, the LDF model can be viewed as a diffusion model where the overall kinetic constant in Equation (235) is a combination of all types of diffusivities such as the film diffusivity and the intra-particle pore

and surface diffusivities. The LDF model can also be extended to include coupled diffusion effects by using the Maxwell-Stefan diffusion formulation [199]. This model reduces the computational time significantly and is the most widely used model to describe the mass transfer kinetics. We have also incorporated this model in our code to account for the mass transfer kinetics. The LDF model includes competitive adsorption processes by combining it with a mixture adsorption prediction model that determines the relation between the concentrations and adsorbed amounts at the external surface.

4.5. Mixture loading prediction

In the multi-component breakthrough computation, the loading q_i of species i depends on the concentrations c_i of all N species

$$q_i = q(c_1, c_2, \dots, c_{N_c}) \quad (248)$$

This would require mixture isotherms over all possible ranges of mole fraction. The equilibrium loadings q_i for the components in the mixture are therefore computed from mixture prediction models like IAST using single-component adsorption isotherms. The total average molar loadings of the mixture (\bar{q}_T) within the crystallite is obtained by a summation over all N_c components.

$$\bar{q}_T(t, z) = \sum_{i=1}^{N_c} \bar{q}_i(t, z). \quad (249)$$

There are three possibilities to couple IAST equations in adsorptive bed dynamics [73]:

- (1) The reduced grand potential can be treated as a dependent variable of time and space and added to the system of differential equations, describing the bed dynamics [200].
- (2) Computation of the adsorption equilibrium separately at each time step.
- (3) A B-spline approach to pre-compute the equilibrium states [116]. B-splines are also known as the basis splines. These are constructed using polynomial functions joined at nodes. For a set of knots or nodes, λ_j , with $j = 0$ to $g + 1$, $g - k$ independent B-splines can be constructed. The summation of such independent splines leads to a spline function. Equilibrium loadings are calculated using IAST for the first time and then the coefficients involved in the B-spline functions are fitted to the data obtained. Further, interpolations are performed to calculate the equilibrium loadings. This helps in avoiding the iterative calculations involved in IAST when called inside the breakthrough code [116].

This first option results in a strongly non-linear system of differential-algebraic equations which is difficult to solve, computationally expensive and time consuming [73]. For more than two components, the B-spline approach results in additional multidimensional fitting issues, losing its advantages and limiting the applicability to the binary case

[73]. The second option is computationally less expensive than the first one as the IAST equations are solved separately to the bed dynamics. Unlike the B-spline approach, this method does not have limitations regarding the number of components present in the system. These advantages make the second method a popular approach for calculating equilibrium loading in fixed bed adsorption problems [73]. Therefore, we have also adopted this approach in our code.

In this work, the IAST equations are solved using the FastIAS and the Nested-Loop bisection method. The latter has the advantage of calculating equilibrium loadings up to machine precision (ca. 10^{-15}). A typical working precision considered by current IAST methods is ca. 10^{-8} [73]. Moreover, we have also incorporated the explicit isotherms mentioned in Section 3.4.5. These isotherms can account for the size-effects of the components on the adsorption behaviour. Originally, these equations were developed for adsorbents having single sites. We have extended this model to tackle multi sites adsorption [31]. We have used a segregated approach where the adsorbed phase is in equilibrium with the gas phase at each site. This method calculates equilibrium loadings with similar accuracy to the segregated IAST approach by Swisher et al [29]. The segregated approaches are useful in case of non-uniform adsorption surfaces, where IAST can be inadequate in calculating the correct equilibrium loadings [29].

The explicit isotherms do not require any iterations to calculate the loadings. For integration with the breakthrough model, this method makes the code about 3 times faster than using IAST [31]. Explicit isotherms are similar in speed as using FastIAS using caching, but are not iterative and hence always converging.

4.6. Existing breakthrough software

Different software is currently available for predicting breakthrough curves:

- Fixed-bed Adsorption Simulation Tool (FAST) [201]: It is a windows based software which is free of charge for academic or any other non-commercial purposes. It is licensed under a Creative Commons Attribution-NonCommercial-No Derivative Works 3.0 Unported License. FAST predicts the breakthrough curves for fixed bed type filters used in water treatment. The solid phase mass transfer can be modelled using a homogeneous surface diffusion model or LDF model.
- Multi-Flow Inversion of Tracer (MFIT) [202]: It is also a Windows based open-source software package for calculating breakthrough curves for tracer components present in ground water. This software is distributed under the Creative Commons Attribution 4.0 License.
- ProSim Dynamic Adsorption Column Simulation (ProSim DAC) [203]: It is a commercial software used for adsorption and regeneration steps in temperature swing adsorption (TSA), pressure swing adsorption (PSA), vacuum and temperature swing adsorption, etc. It finds its application in hydrogen refining, isotopic separation, emission control of volatile organic compounds and solvent recovery.

- 3P Sim [204]: It is a commercial software. 3P Sim is a part of the dynamic sorption analyser instrument, mixSorb L. It can calculate mixture isotherms from pure component isotherms and also evaluate breakthrough curves based on mass and energy balances.
- Aspen Adsorption [205]: Aspen Adsorption is a commercial flowsheet simulator. It is used to design, analysis, simulation, and optimisation of gas and liquid adsorption systems. It is used for both PSA and TSA processes.

Various commercial numerical platforms have been applied for the modeling of the PSA process [206], such as gPROMS [207], MATLAB [208] and FLUENT [209]. Many research groups have their own in-house breakthrough codes which are not released as open source codes. These include the work of Krishna and Baur [187], Rodriguez [19,160], Worch [64], Chung et al. [210], etc. Instead of the LDF model, Krishna and Baur solved a partial differential equation along the crystal diffusion path. The diffusive flux used in the model is provided by Maxwell-Stefan equations [187]. Maxwell-Stefan diffusivity formulation involves a thermodynamic correction factor and binary diffusivities correlating different species. These parameters are evaluated locally along the crystal diffusion path [187]. Chung et al. [210] used breakthrough curve modelling to screen nanoporous materials for hexane and heptane isomer separations. It is an isothermal model with LDF approximation for the mass transfer kinetics of the isomers and Darcy's equation [211] for the pressure drop along the length of the column.

4.7. Breakthrough model implementation

4.7.1. Model

The ideal gas law reads

$$c_i = \frac{y_i p_T}{RT} = \frac{p_i}{RT} \quad (250)$$

where y_i is the mole fraction of component i in the gas phase, p_T is the total pressure, p_i is the partial pressure, T is the gas temperature, and R the universal gas constant. Assuming ideal gas behaviour for the gas phase and isothermal conditions, the partial pressures in the gas phase at position z and time t are obtained by solving the material balance for each component $i = 1, \dots, N_c$ [6,145]. Here, the material balance shown in Equation (213) is modified in terms of the partial pressures as shown below.

$$\begin{aligned} \frac{1}{RT} \frac{\partial p_i(t, z)}{\partial t} &= -\frac{1}{RT} \frac{\partial(v(t, z)p_i(t, z))}{\partial z} \\ &+ \frac{1}{RT} \mathcal{D}_i \frac{\partial^2 p_i(t, z)}{\partial z^2} - \frac{1 - \varepsilon_b}{\varepsilon_b} \rho_p \frac{\partial \bar{q}_i(t, z)}{\partial t} \end{aligned} \quad (251)$$

Using the LDF approach yields

$$\frac{\partial \bar{q}_i(t, z)}{\partial t} = k_i (q_{eq,i} - \bar{q}_i) \quad (252)$$

Because of adsorption and dispersion, the interstitial velocity v in fixed-bed adsorption is not constant. To calculate the velocity profile, the material balance for the overall mixture is

considered by summing Equation (251) over all components

$$\begin{aligned} \frac{\partial p_T}{\partial t} &= -\frac{\partial(v p_T)}{\partial z} \\ &+ \sum_{i=1}^{N_c} \left(\mathcal{D}_i \frac{\partial^2 p_i}{\partial z^2} - RT \frac{1 - \varepsilon_b}{\varepsilon_b} \rho_p k_i (q_{eq,i} - \bar{q}_i) \right) \end{aligned} \quad (253)$$

The total pressure along the column is invariant with time and has a constant gradient along the length of the column. Therefore, Equation (253) is modified as shown below.

$$\begin{aligned} p_T \frac{\partial v}{\partial z} &= \sum_{i=1}^{N_c} \left(\mathcal{D}_i \frac{\partial^2 p_i}{\partial z^2} - RT \frac{1 - \varepsilon_b}{\varepsilon_b} \rho_p k_i (q_{eq,i} - \bar{q}_i) \right) \\ &- v \frac{\partial p_T}{\partial z} \end{aligned} \quad (254)$$

The pressure gradient ($\partial p_T / \partial z = \text{constant}$) can be calculated using the Ergun equation as shown below [212]. The Ergun equation considers both viscous and inertial effects. Apart from the Ergun equation, the Darcy [211], and Carman-Kozeny [213] equations could also be used but these equations are valid only for viscous flows.

$$\frac{\Delta P}{L} = \frac{150 \mu L (1 - \varepsilon_b)^2}{d_p^2 (\varepsilon_b)^3} v + \frac{1.75 L \rho_f (1 - \varepsilon_b)}{d_p (\varepsilon_b)^3} v |v| \quad (255)$$

In Equation (255), $\Delta P/L$ is the pressure gradient inside the column of length L . μ is the dynamic viscosity in [Pas], d_p is the particle diameter in [m], ε_b is the bed porosity, ρ_f is the density of the fluid in [kg/m^3] and v is the superficial velocity in [ms^{-1}]. Equations (251), (252) and (254) are solved together to obtain concentration profiles for all the components inside the column.

- Initial Conditions

Initially, the column is filled with only carrier gas. The carrier gas does not adsorb and hence, its equilibrium loading is zero. At the start of the breakthrough simulation, the pressure of the carrier gas is equal to the total pressure inside the column ($p_{\text{carrier gas}} = p_T$). Also, we have imposed the condition that $\partial p_T / \partial z = \text{constant}$ and the constant can be computed from Equation (255). Therefore, at $t = 0$, we have,

$$\sum_i \mathcal{D}_i \frac{\partial^2 p_i(t, z)}{\partial z^2} = \mathcal{D}_{\text{carrier-gas}} \frac{\partial^2 p_{\text{carrier-gas}}(t, z)}{\partial z^2} \quad (256)$$

$$= \mathcal{D}_{\text{carrier-gas}} \frac{\partial^2 p_T(t, z)}{\partial z^2} \quad (257)$$

$$= 0 \quad (258)$$

Using Equation (254), we obtain

$$\frac{\partial v}{\partial z} = -\frac{1}{p_T(z)} \left[v \frac{\partial p_T}{\partial z} \right] \quad (259)$$

and

$$\frac{\partial v}{v} = -\frac{1}{p_T(z)} \left[\frac{\partial p_T}{\partial z} \right] dz \quad (260)$$

Integrating both sides yields

$$\int_{v^{\text{in}}}^v \frac{dv}{v} = - \left[\frac{\partial p_T}{\partial z} \right] \int_0^z \frac{1}{p_T(z)} dz \quad (261)$$

$$\ln\left(\frac{v}{v^{\text{in}}}\right) = - \left[\frac{\partial p_T}{\partial z} \right] \int_0^z \frac{1}{\left(p_T + \frac{\partial p_T}{\partial z} z\right)} dz \quad (262)$$

$$\ln\left(\frac{v}{v^{\text{in}}}\right) = \ln\left(\frac{p_T^{\text{in}}}{p_T^{\text{in}} + \frac{\partial p_T}{\partial z} z}\right) \quad (263)$$

$$v = v^{\text{in}} \frac{p_T^{\text{in}}}{p_T^{\text{in}} + \frac{\partial p_T}{\partial z} z} \quad (264)$$

$$p_T(t, z) = p_T^{\text{in}} + \frac{\partial p_T}{\partial z} z \quad (265)$$

Equation (264) shows that at $t = 0$, the velocity is inversely proportional to the position inside the adsorber column. Initially, the pressure of the carrier gas is equal the total pressure as shown below

$$p_{\text{carrier gas}}(t = 0, z) = p_T(t = 0, z) \quad (266)$$

and the partial pressures for all other components are zero inside the column except at the inlet. Also, the adsorption loadings for the components are zero at the beginning.

$$p_i(t = 0, z > 0) = 0 \quad (267)$$

$$\bar{q}_i(t = 0, z) = 0 \quad (268)$$

- **Boundary Conditions**

At the inlet of the column, the partial pressures for each component is fixed. The velocity is also fixed at the inlet. At the outlet, the spatial gradient of the partial pressures are considered zero.

$$v(t, z = 0) = \frac{u^{\text{in}}}{\varepsilon_b} \quad (269)$$

Dirichlet boundary condition,

$$p_i(t, z = 0) = y_i^{\text{in}} \cdot p_T^{\text{in}} \quad (270)$$

Neumann boundary condition,

$$\frac{\partial p_i(t, z = L)}{\partial z} = 0 \quad (271)$$

Instead of using Dirichlet boundary conditions (Equation (270)) [214], the Danckwerts boundary condition $(-D_i \frac{\partial p_i(t, z=0)}{\partial z} + v(t, z = 0)p_i(t, z = 0) = v^{\text{in}}p_i^{\text{in}})$ [215] can also be used. If the values of the dispersion coefficients are not very high, then Dirichlet and Danckwerts boundary conditions should produce same results.

4.7.2. Numerical approach

Fixed bed adsorption involves mass transport equations for the transport of the mixture in the fluid phase. Adsorption of the components from the fluid phase to the adsorbent is modelled using the Linear Driving Force (LDF) model

as shown in Equation (252). The LDF model states that the rate of adsorption is proportional to the amount of adsorbate still required to achieve equilibrium [195]. The mass transfer rate is a function of the equilibrium loading of the components which is obtained either using IAST or explicit isotherm equations that account for the effects of the size of the molecules [30]. The expression for the velocity is obtained using the equation for the total pressure as shown in Equation (254). These equations form a system of differential algebraic equations involving partial differential equations (PDEs) and non-linear algebraic equations. Different methods can be used to solve this system of equations. Finite difference [216], finite volume [217] or finite element [218] methods are the common numerical approaches used to solve such equations. The method of lines [219] is a popular technique to solve such problems involving PDEs [206]. In this method, the PDEs are converted into ordinary differential equations (ODEs) and eventually, these equations can be solved using already available integration schemes for ODEs [219]. Another approach is to discretise both time and spatial domains simultaneously [206]. Nilchan et al. used orthogonal collocation method to discretise the time domain and finite element method for the spatial domain for optimising pressure swing adsorption systems [220]. Finite Volume Method (FVM) [221] and Finite Element Method (FEM) [222] are also used for discretising the time and spatial domains. In this work, method of lines will be used to solve the system of differential algebraic equations.

4.7.3. Method of lines

The method of lines is a technique to solve the partial differential equations in which all dimensions except one are discretised [219]. In this way, systems of PDEs can be converted into ODEs and solved using the integration schemes available for ODEs. The method of lines requires the system of PDEs to be a well posed initial value problem. Elliptical partial differential equations can also be solved using this method but certain special techniques needs to be introduced like the method of false transients [219,223]. A common example encountered in many scientific disciplines is a system of partial differential equations with spatial and temporal derivatives. In the method of lines, the spatial derivatives are discretised using numerical discretisation schemes like the finite difference method (FDM), the finite volume method (FVM) and the finite element method (FEM). The time derivatives are kept in their continuous form.

4.7.4. Spatial discretisation

As mentioned before spatial derivatives can be discretised using FDM, FVM and FEM.

- Finite Volume Method (FVM) [217]: The Finite volume method is based on the conservation of numerical fluxes at each grid point and involves the integration over the finite volume or the control volume (grid). Many physical laws are conservation laws especially in the field of fluid mechanics, heat and mass transfer etc [217]. This makes the FVM a popular method in these disciplines. The values

Table 8. First and second order derivatives discretised using the Finite Difference Method (FDM) method [216].

Derivatives	Discretisation	Scheme
$(\frac{\partial u}{\partial z})_j$	$\frac{u(j+1)-u(j)}{\Delta z} + O(\Delta z)$	Forward difference
$(\frac{\partial u}{\partial z})_j$	$\frac{u(j)-u(j-1)}{\Delta z} + O(\Delta z)$	Backward difference
$(\frac{\partial u}{\partial z})_j$	$\frac{u(j+1)-u(j-1)}{2\Delta z} + O(\Delta z)^2$	Central difference
$(\frac{\partial^2 u}{\partial z^2})_j$	$\frac{u(j+1)-2u(j)+u(j-1)}{(\Delta z)^2} + O(\Delta z)^2$	Central difference

of the dependent variables are stored at center of the grids or finite volumes.

- Finite Element Method (FEM) [218]: In this method, the region of concern is subdivided into geometrically simple finite sized elements. Within these elements, the derivatives are approximated as simple functions such as linear or quadratic polynomials. The data for the dependent variables are stored on the nodes of the grids.
- Finite Difference Method (FDM) [216]: It is the most direct method. It is easy to implement and efficient to solve for regular geometries. For complex geometries, the above two methods are preferred. The derivatives are discretised in the form of finite differences which are derived using a Taylor series expansion. Similar to FEM, FDM also stores the data of the dependent variables at the nodes of the grids.

For its ease of implementation, FDM is used for the discretisation of the spatial domain in this work. Discretisation depends on the order of the derivatives. Some examples for first and second order derivatives are shown below in Table 8.

4.7.5. Discretisation of the governing equations

- Mass Transport Equation: Before diving into the discretisation of the entire governing equations, it is important to explore the possibilities for discretising each physical phenomena individually. The mass transport equation consists of advective, dispersion and adsorption terms. The advective term ($\frac{\partial v p_i}{\partial z}$) can be discretised either using backward difference method or central difference method [224]:

$$\frac{\partial(v p_i)}{\partial z} = -\frac{v(j)p_i(j) - v(j-1)p_i(j-1)}{\Delta z} \quad (272)$$

Upwind scheme

$$\frac{\partial(v p_i)}{\partial z} = -\frac{v(j+1)p_i(j+1) - v(j-1)p_i(j-1)}{2\Delta z} \quad (273)$$

Central difference scheme

Equations (272) and (273) show the two variations of discretisation for the advection term. Index j in these equations represent grid points in the spatial direction. In this case, the backward differencing method is also known as the upwind scheme. Although it is first order accurate, it is highly suitable for strong advective flows

[217,224]. The central differencing scheme is second order accurate but leads to unstable solution or creates non-physical oscillations in the solution [224]. The central differencing scheme does not identify the directionality of the flow [217]. It considers the influence of all the neighbouring grid points at the current node. In an advection dominated flow, the directionality becomes important. For example, in an unidirectional flow, the flux at the current grid point is strongly influenced by the preceding grid point compared to the succeeding one. The upwind scheme takes into account the directionality of the flow [217]. Therefore, the upwind scheme is used for the advective terms in this work. We have used the 1st order upwind scheme. The spatial accuracy can be improved by using a 2nd order upwind scheme. However, the 1st order upwind scheme is easier to converge than the 2nd order scheme. Therefore, we have used the 1st order upwind scheme.

The mass transport equation (Equation (251) in Section 4.7) is discretised as follows.

$$\begin{aligned} \frac{\partial p_i}{\partial t} = & -\frac{v(j)p_i(j) - v(j-1)p_i(j-1)}{\Delta z} \\ & + D_i \frac{p_i(j+1) - 2p_i(j) + p_i(j-1)}{(\Delta z)^2} \\ & - RT \left(\frac{1 - \varepsilon_B}{\varepsilon_B} \right) \rho_p k_i (q_{eq,i}(j) - \bar{q}_i(j)) \end{aligned} \quad (274)$$

- Linear Driving Force (LDF): The LDF method is used to calculate the amount of molecules adsorbed in the adsorbent. At each grid point, the rate of adsorption is a linear function of the equilibrium loading and the actual adsorbed loading at that grid point which is shown below.

$$\frac{\partial \bar{q}_i}{\partial t} = k_i (q_{eq,i}(j) - \bar{q}_i(j)) \quad (275)$$

In Equation (275), the component mass transfer coefficients (k_i) are considered to be constants.

- Velocity: To calculate the velocity at each grid point the gradient of velocity in Equation (254) is discretised using the 1st order upwind scheme as shown below.

$$\left(\frac{\partial v}{\partial z} \right)_j = \frac{v(j) - v(j-1)}{\Delta z} \quad (276)$$

The discretised version of Equation (254) equals:

$$\begin{aligned} v(j) = & v(j-1) \\ & - \Delta z \frac{1}{P_r} \sum_{i=1}^{N_c} \left(-D_i \frac{p_i(j+1) - 2p_i(j) + p_i(j-1)}{(\Delta z)^2} \right. \\ & \left. + RT \left(\frac{1 - \varepsilon_B}{\varepsilon_B} \right) \rho_p k_i (q_{eq,i}(j) - \bar{q}_i(j)) \right) \\ & - \Delta z \frac{1}{P_r} \left(v(j-1) \frac{\partial p_r}{\partial z} \right) \end{aligned} \quad (277)$$

4.7.6. Discretisation of initial and boundary conditions

- Initial Conditions

Below are the discretised versions of the initial conditions (Equations (264)–(268)) mentioned in Section 4.7.

$$v(0, j) = v(0, 0) \frac{p_T(0, 0)}{p_T(0, 0) + \frac{\partial p_T}{\partial z} j \cdot \Delta z} \quad (278)$$

$$p_T(0, j) = p_T(0, 0) + \frac{\partial p_T}{\partial z} j \cdot \Delta z \quad (279)$$

$$p_{\text{carrier gas}}(0, j) = p_T(0, j) \quad (280)$$

$$p_i(0, j > 0) = 0 \quad (281)$$

$$\bar{q}_i(0, j) = 0 \quad (282)$$

- Boundary Conditions

Boundary conditions (Equations (269)–(271)) mentioned in Section 4.7 are discretised as follows.

$$v(t, 0) = \frac{u^{\text{in}}}{\varepsilon_b} \quad (283)$$

$$p_i(t, 0) = y_i^{\text{in}} \cdot p_T^{\text{in}} \quad (284)$$

$$p_i(t, N_{\text{grid}}) = p_i(t, N_{\text{grid}} - 1) \quad (285)$$

4.7.7. Time integration

Time integration in numerical analysis can be performed in several ways. Explicit and implicit are the two major methods to integrate the temporal derivatives. In explicit methods, the value for the variable at the current step is calculated as a function of the previous time steps [225]. In implicit methods, the present value for the variable depends on the current step. It is easier to implement an explicit method but has constraints due to stability issues [216]. For very stiff differential equations, impractically smaller time steps are required to achieve a stable solution. Implicit methods are always stable and capable of waiving off the smaller time step requirement. However, very large steps are not recommended for the sake of accuracy. Implicit methods can be difficult to implement especially when equations involve non-linearity. In the breakthrough curve model, the non-linearity occurs due to the calculation of the equilibrium loadings using IAST. IAST itself involves a system of non linear equations which are solved iteratively (e.g. bisection or the Newton-Raphson method). Further, when IAST is incorporated to the breakthrough curve model, the system of differential equations needs to be solved iteratively, if implicit method is used for discretisation. To explain the integration schemes (implicit and explicit), let us consider the following differential equation

$$\frac{dY}{dt} = F(Y, t) \quad (286)$$

This equation can be solved using either implicit or explicit methods as shown below.

$$Y(t + \Delta t) = Y(t) + \Delta t F(Y(t)) \quad \text{Explicit method} \quad (287)$$

$$Y(t + \Delta t) = Y(t) + \Delta t F(Y(t + \Delta t)) \quad \text{Implicit method} \quad (288)$$

$$Y(t + \Delta t) = Y(t) + \frac{\Delta t}{2} [F(Y(t + \Delta t)) + F(Y(t))] \quad (289)$$

Trapezoidal method [226]

Various time integration schemes are available in both implicit and explicit categories. Some common schemes are Forward Euler, Backward Euler and Crank-Nicolson [227]. Forward Euler is the simplest of all and is an explicit scheme (Equation (287)). Backward Euler is a fully implicit scheme (Equation (288)). The Crank-Nicolson method is a combination of both explicit and implicit scheme. It is the finite difference version of the trapezoidal rule (Equation (289)). Another possibility is to split $F(Y, t)$ into stiff and non-stiff parts. The stiff part can be solved using implicit methods and the non-stiff part using explicit methods [228,229] as shown below

$$Y(t + \Delta t) = Y(t) + \Delta t [F_1(Y(t + \Delta t)) + F_2(Y(t))] \quad \text{Implicit – Explicit method} \quad (290)$$

In Equation (290), for the stiff function ($F_1(Y(t + \Delta t))$), implicit methods can be used. For the non-stiff function ($F_2(Y(t))$), explicit methods can be used.

There are several families of time integrator like the Linear Multistep methods [227] and the Runge-Kutta family [225]. In the multistep methods, the derivatives are treated as functions of several timesteps from the past and the future. Examples are Adams Bashfort [225] and Adams Moulton [225] which are explicit schemes. The Backward Differencing Formula (BDF) is another example of linear multistep methods [225]. The BDF is implicit in nature and a popular method for solving stiff differential equations. Unlike multistep methods, the Runge-Kutta family involves only single time step methods. Rather, the derivatives are solved in several stages or trial steps to increase the order of accuracy. For the intermediate stages, the value of the independent variable at the midpoint of the interval is used. At each intermediate stage, half of the dependent variable calculated at the previous stage is used [227]. Both explicit and implicit Runge-Kutta methods are available in literature [227,230]. One of the commonly used Runge-Kutta method is the 4th order explicit method. Adaptive Runge-Kutta methods also exist where the error is calculated at each time step [231]. Based on this estimation, the time step is varied.

There is a relatively new class of Runge-Kutta Methods which are known as Strong Stability Preserving Runge-Kutta (SSP-RK) [33,34,36,37]. Apart from the stability, these methods also enforce positivity, boundness and preserve monotonicity of the differential equations [37]. These are explicit methods and are stable under Courant–Friedrichs–Lewy (CFL) condition as shown below

[37].

$$\frac{u\Delta t}{\Delta z} \leq 1 \quad (291)$$

In Equation (291), u is a magnitude of dimension, length/time, Δt is the time step and Δz is the spatial grid size. $\Delta z/u$ is also known as forward Euler time (Δt_{FE}). According to the CFL criterion, Δt must be less than or equal to Δt_{FE} . There are several variations of SSP-RK (e.g. 3rd order, 5th order) [36]. The SSP-RK(3,3) method is used in RUPTURA which is shown below. It is a third order method and involves three stages [37]:

$$Y(t + \Delta t)^{(1)} = Y(t) + \Delta t F(Y(t)) \quad (292)$$

$$Y(t + \Delta t)^{(2)} = \frac{3}{4} Y(t) + \frac{1}{4} Y(t + \Delta t)^{(1)} + \frac{1}{4} \Delta t F(Y(t + \Delta t)^{(1)}) \quad (293)$$

$$Y(t + \Delta t) = \frac{1}{3} Y(t) + \frac{2}{3} Y(t + \Delta t)^{(2)} + \frac{2}{3} \Delta t F(Y(t + \Delta t)^{(2)}) \quad (294)$$

In Equations (292)–(294), $Y(t)$ is the dependent variable and $F(Y(t))$ is the derivative of $Y(t)$. In the SSP-RK method, the first step is always a forward Euler step. The derivatives of the dependent variable are solved in several stages depending on the variation of the SSP-RK method. The 3rd order method is popular because it generates results almost as

accurate as its higher order counter parts and it involves fewer number of stages [36].

4.7.8. Breakthrough algorithm

Figure 11 shows the schematic of the algorithm to calculate the breakthrough curves. The first step in the algorithm is to specify the initial conditions for partial pressures, total pressure, adsorbed loadings and velocity. Based on the initial conditions, equilibrium loadings at each grid point are calculated either using IAST or adsorbate size dependent explicit isotherms [30]. Next, the variables (partial pressure, adsorbed loading, total pressure, velocity) are determined at each time step. The SSP-RK(3,3) method is used for the time integration. This method involves three stages. At each stage, the temporal derivatives of the partial pressures and the adsorption loadings are calculated which are used to update the new values of partial pressure and adsorbed loadings. Based on the newly estimated partial pressures, the total pressure is calculated at each grid point, after which, the equilibrium loading, and velocity are calculated. The values obtained at the third stage are considered to be the final values at each time steps. The process is repeated until the final time step is reached.

4.8. Pulse breakthrough

RUPTURA also includes pulse-style breakthrough curve modeling. Instead of using a step input for the adsorbing components of the mixture, a pulse input is used. The pulse breakthrough curve allows us to identify whether the adsorbent is able to fractionate different components in a mixture [232]. The

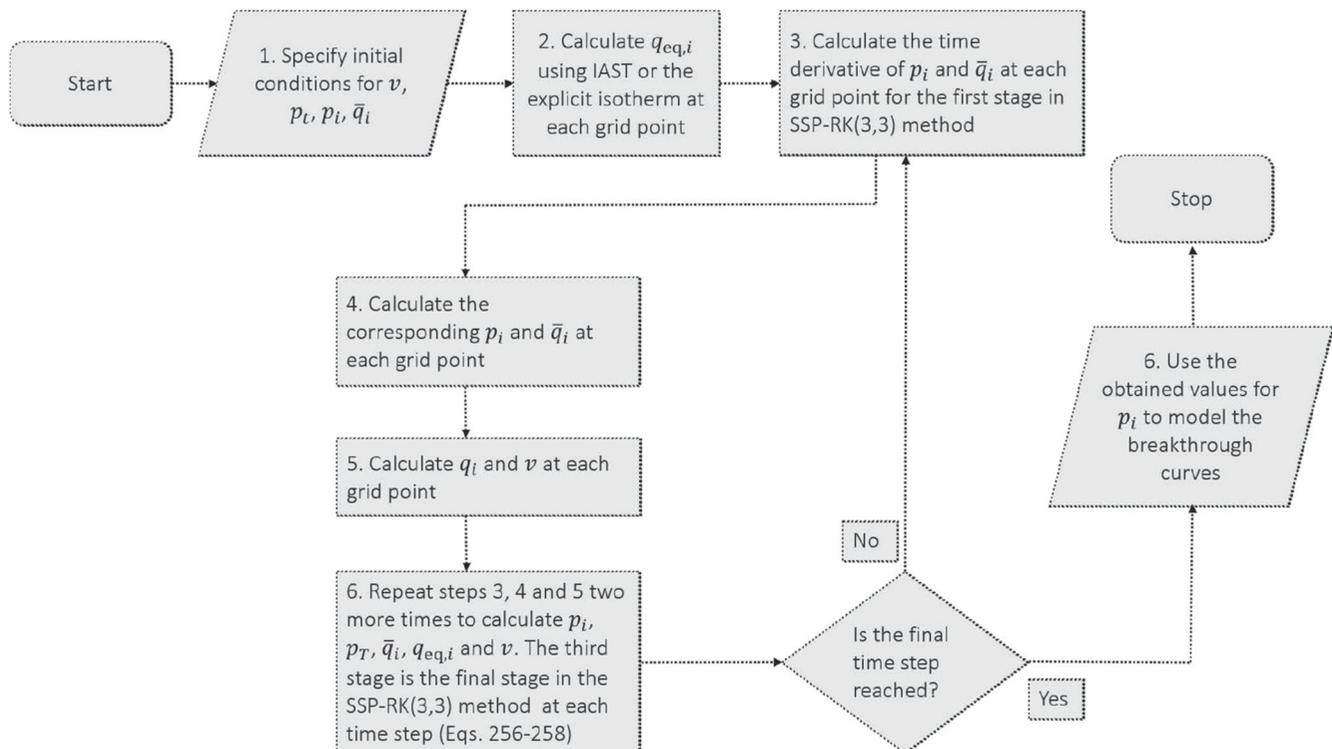


Figure 11. (Colour online) Algorithm to calculate the breakthrough curve. It is based on the method of lines (MOL) technique to solve the system of differential algebraic equations. Time integration is done using an explicit method called Strong Stability preserving Runge-Kutta (SSP-RK(3,3)) as shown in Equations (292)–(294). We first calculate the temporal derivatives of the partial pressures (p_i) and the adsorbed loadings (\bar{q}_i). Until the final time step is reached, we update the values of p_i , p_T , \bar{q}_i , $q_{eq,i}$ and v at each time step.

breakthrough curves are dome shaped. The inlet concentrations for the adsorbing components become zero after the specified time period. On reaching the maximum concentration, the breakthrough curve gradually falls back to zero concentration level. If there is sufficient time gap between the peaks of the breakthrough curves for the components in a mixture, then it indicates that the adsorbent is suitable for the separation of the components.

All the equations and the conditions remain identical to the step breakthrough model, except for the inlet boundary conditions for the components in the mixture. The modified boundary conditions are shown below.

$$p_i(t, z = 0) = \begin{cases} p_i^{\text{in}}, & 0 \leq t < t_{\text{pulse}} \\ 0, & t \geq t_{\text{pulse}} \end{cases} \quad (295)$$

$$p_{\text{carrier gas}}(t, z = 0) = \begin{cases} p_{\text{carrier gas}}^{\text{in}}, & 0 \leq t < t_{\text{pulse}} \\ p_T^{\text{in}}, & t \geq t_{\text{pulse}} \end{cases} \quad (296)$$

In Equations (295) and (296), t_{pulse} is the time period for which the inlet concentrations of the adsorbing components are non-zero.

Figures 12(a,b) show examples of pulse-style breakthrough curves for the mixture of C_6 isomers: n-hexane (nC_6), 3-methyl pentane ($3mC_5$), 2,2-dimethyl butane ($22dmC_5$), and 2,3-dimethyl butane ($23dmC_4$) in BEA-type zeolite at 523K and 12 bar. The dome-shaped breakthrough curves of nC_6 and $22dmC_4$ are very close to each other which means the separation of these two isomers is difficult. It is easier to separate nC_6 and ($22dmC_5$) for the operating conditions mentioned in Figure 12. This is because the peaks of their breakthrough curves are separated by a considerable time gap. A longer column (Figure 12 (b)) enhances separation. However, the trade-off is that the retention time inside the bed increases for the adsorbing components. As a result, the amount of a specific component recovered will be lower for the longer column. This can be clearly seen in Figure 12. The peaks of the breakthrough curves in Figure 12 (b) are shorter than those in Figure 12(a).

4.9. Validation

Jolimaitre et al. [233] considered the separation of mono and di-branched hydrocarbons in MFI-type (silicalite) zeolite. This study includes both experimental analysis and a breakthrough curve model. To validate our model, we use the experimental breakthrough curve data generated by Jolimaitre et al. [233]. It involves the separation of 2-methyl butane ($2mC_4$) and 2-methyl pentane ($2mC_5$). The experiments are conducted at 473 K and 5 bar and Nitrogen (N_2) is used as the carrier gas.

Experimental breakthrough conditions for the separation of $2mC_4$ and $2mC_5$ in MFI-type zeolite are shown in Table 9 [233]. This includes the inlet concentrations of the components in the mixture (c_i^{in}), their corresponding partial pressures (p_i^{in}) and mole fraction (y_i^{in}). The interstitial velocity (v) at the inlet is $0.0197 \text{ [ms}^{-1}\text{]}$ [233] and the bed porosity (ϵ_b) is 0.4.

The axial dispersion coefficients (\mathcal{D}) are calculated using the following equation as shown in Table 7:

$$\mathcal{D} = (0.45 + 0.55\epsilon_b)D_m + 0.5d_p v \quad (297)$$

In Equation (297), D_m is the molecular diffusion coefficient in $[\text{m}^2\text{s}^{-1}]$, d_p is the particle diameter in [m] and v is the velocity of the fluid phase in .

The mass transfer coefficient (k) is calculated using Equation (235). This equation shows that k is proportional to the effective diffusion coefficient, (D^{eff}) which is obtained as follows [6]:

$$D^{\text{eff}} = \left(\frac{1}{D_m} + \frac{1}{D_k} \right)^{-1} \quad (298)$$

In Equation (298), D_m is the molecular diffusion coefficient and D_k is the Knudsen diffusion coefficient. The units of both the diffusivities are in $[\text{m}^2\text{s}^{-1}]$. D_m is obtained using Equations (215). The expression for Knudsen diffusivity is

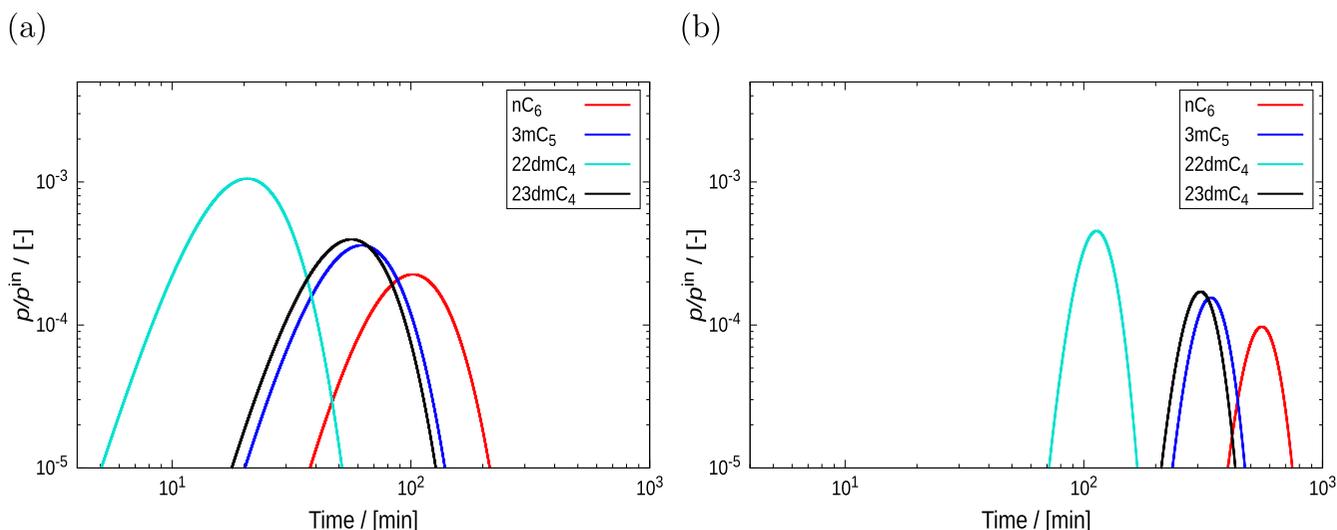


Figure 12. (Colour online) Examples of pulse-style breakthrough curve simulation for the mixture of C_6 isomers: n-hexane (nC_6), 3-methyl pentane ($3mC_5$), 2,2-dimethyl butane ($22dmC_4$), and 2,3-dimethyl butane ($23dmC_4$) in BEA-type zeolite at 523 K and 12 bar. Isothermal and isobaric conditions are imposed on the fixed bed column of length (a) 0.1 m and (b) 0.5 m. The bed porosity (ϵ_b) is 0.2. Helium is used as the carrier gas. The inlet mole fractions for the C_6 isomers are considered to be 0.01975. The interstitial velocity (v) at the inlet is 0.019 ms^{-1} . 5s is the pulse time (t_{pulse}).

Table 9. Experimental conditions for separation of 2mC₄, 2mC₅.

	$c_i^{\text{in}} / [\text{mol m}^{-3}]$	$p_i^{\text{in}} / [\text{bar}]$	y_i^{in}
2mC ₄	6.27	0.245	0.049
2mC ₅	6.60	0.260	0.052

Notes: It includes the inlet concentrations (c_i^{in}), corresponding partial pressures (p_i^{in}) and the mole fractions (y_i^{in}).

Table 10. Values of dispersion coefficient (D) and mass transfer coefficient (k) for 2mC₄ and 2mC₅.

	$D / [\text{m}^2 \text{s}^{-1}]$	$k / [\text{s}^{-1}]$
2mC ₄	$4.79 \cdot 10^{-5}$	0.056
2mC ₅	$3.91 \cdot 10^{-5}$	0.051

Notes: The coefficients are calculated at 473 K and 5bar for the composition shown in Table 9.

shown below.

$$D_k = \frac{d_{\text{pore}}}{3} \sqrt{\frac{8RT}{\pi M}} \quad (299)$$

In Equation (299), d_{pore} is the pore diameter, R is the universal gas constant, T is the temperature and M is the molar mass of the component. The values of dispersion coefficients (D) and mass transfer coefficients (k) for 2mC₄ and 2mC₅ at 473K and 5bar total pressure are shown in Table 10.

Pure component adsorption isotherms are modelled using single site Langmuir isotherms. The parameters (q^{sat}) and (b) obtained from fitting the Langmuir isotherm to the adsorption loading data are shown in Table 11. The adsorption loadings for the pure components are obtained using grand-canonical Monte Carlo (GCMC) simulations [83].

Figure 13 shows the comparison between the breakthrough curves at the column exit for the mixture of 2mC₅ and 2mC₄

Table 11. Pure component adsorption isotherm parameters.

	$q^{\text{sat}} / [\text{mol}/(\text{kg framework})]$	$b / [\text{Pa}^{-1}]$
2mC ₄	$0.717 \pm 4 \cdot 10^{-3}$	$2.835 \cdot 10^{-5} \pm 7 \cdot 10^{-7}$
2mC ₅	$0.699 \pm 2 \cdot 10^{-3}$	$1.271 \cdot 10^{-4} \pm 3 \cdot 10^{-7}$

Notes: Single-site Langmuir isotherms are used to fit the pure component adsorption loading data obtained using GCMC simulations at 473 K. q^{sat} is the saturation loading and b is the equilibrium constant.

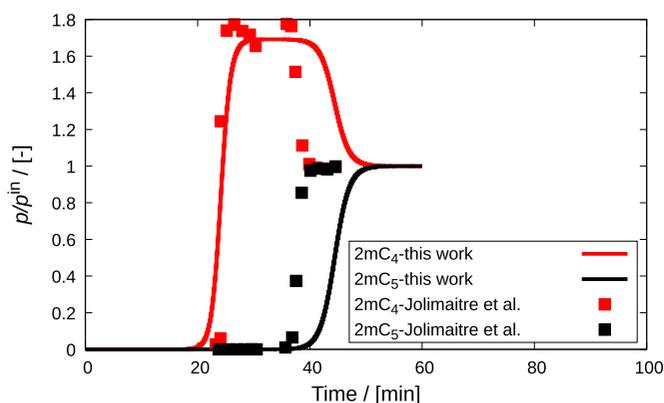


Figure 13. (Colour online) Validation of the breakthrough curve model with the experimental results of Jolimaitre et al. [233]. This figure shows the separation of 2mC₄ and 2mC₅ in MFI-type zeolite at 473K and 5bar. The coloured squares represent the experimental data and the solid lines represent the results from our simulations.

obtained from our simulation and the experiment performed by Jolimaitre et al. [233]. The breakthrough curves from the simulation and experiment follow similar trends. The discrepancies between the experimental and simulated fronts can occur because of several reasons such as errors in the pure component isotherm data, assumptions involved in IAST/ SIAST model for equilibrium calculations, inaccurate estimation of the dispersion or/and diffusion coefficients, use of the LDF model, etc. Further, errors in conducting experiments and quality of the adsorbent and fluid phase sample can also cause these deviations.

The adsorption of 2mC₄ is weaker compared to 2mC₅. Therefore, 2mC₄ is the first component to exit the column and shows a roll-up behaviour. The roll-up refers to the hump that occurs in the breakthrough curve of the weakly adsorbing component before the strongly adsorbing component starts to breakthrough. This behaviour occurs because the gas phase concentration of the strongly adsorbing component is continuously decreasing due to its adsorption. As a result, the partial pressure of the weakly adsorbing component increases and at certain time, it exceeds the inlet partial pressure (i.e. $p_i/p_i^{\text{in}} > 1$) [187]. The roll-up falls back to the inlet partial pressure, once the strongly adsorbing component starts to breakthrough and eventually reaches equilibrium.

4.10. Case study

In this section, we present a case study consisting of fitting of pure component loading data, mixture isotherm prediction, and breakthrough curve simulations. Here, we consider the case of adsorption of CO₂ and C₃H₈ mixture in MOR-type zeolite at 300 K from Ref. [31]. Fitting of pure component loading data and estimation of mixture isotherms, and simulations of breakthrough curves were performed using RUP-TURA. The pure component loading data were obtained using the RASPA software [21,22]. In this study, we also compare the influence of different mixture isotherm prediction models on the adsorption isotherms, and the breakthrough curves.

Figure 14(a) shows pure component isotherms (dual-site Langmuir) fitted to the adsorbed loadings obtained using Grand-Canonical Monte Carlo (GCMC) simulations. The unary isotherms show dual-site behaviour because MOR-type zeolite has two types of adsorption sites (pockets) [29,31]. Dual-site Langmuir isotherms have two pairs of fitted parameters (equilibrium constant and saturation loading) which are shown in Table 12. The MOR-type zeolite has a slightly higher loading of CO₂ compared to C₃H₈. This indicates that the affinity of the structure with CO₂ is higher than that of C₃H₈ and the preference for CO₂ is energetic in nature in this regime. At higher pressure, entropy (packing) effects come into play. Here we see that also these effects are in favour of CO₂ since CO₂ shows a higher adsorption and higher saturation loading in the pure component isotherms.

We can examine what happens when CO₂ and C₃H₈ compete with each other by doing explicit grand-canonical Monte Carlo mixture simulations. Indeed, as shown in Figure 14(b), at low loading, CO₂ is adsorbed significantly more than C₃H₈. At high pressures, we note that competition can increase

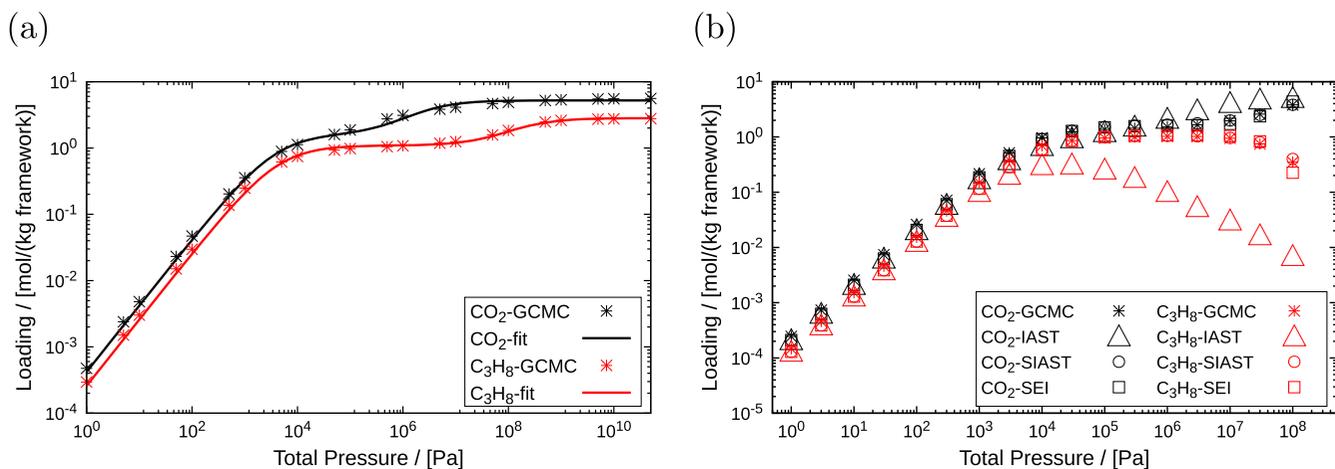


Figure 14. (Colour online) Adsorption isotherms for CO₂ and C₃H₈ in MOR-type zeolite at 300 K. (a) Unary isotherms (dual-site Langmuir) which are fitted to the pure component loading data obtained using RASPA, (b) comparison between mixture isotherms for equimolar composition of CO₂ and C₃H₈ computed using IAST, SIAST and SEI.

Table 12. Fitted parameters for the adsorption of pure CO₂ and C₃ in MOR-type zeolite at 300 K.

	b_1 [1/Pa]	q_1^{sat} [mol/(kg framework)]	b_2 [1/Pa]	q_2^{sat} [mol/(kg framework)]
CO ₂	$2.617 \cdot 10^{-4}$ $\pm 3 \cdot 10^{-5}$	1.60 $\pm 5 \cdot 10^{-2}$	$4.859 \cdot 10^{-7}$ $\pm 3 \cdot 10^{-8}$	3.62 $\pm 5 \cdot 10^{-2}$
C ₃	$6.506 \cdot 10^{-9}$ $\pm 3 \cdot 10^{-10}$	1.73 $\pm 6 \cdot 10^{-3}$	$2.376 \cdot 10^{-4}$ $\pm 8 \cdot 10^{-6}$	1.09 $\pm 4 \cdot 10^{-3}$

Notes: Adsorbed loadings obtained from the GCMC simulations for the pressure range ($10^0 - 5 \cdot 10^{10}$) Pa are fitted using the dual-site Langmuir isotherm.

the loading of one species at the expense of another. Thus, in a mixture, the loading of a component can go down with pressure, something that can not happen in single-component isotherms (when the framework is kept rigid). In most scenarios, IAST does an excellent job predicting the mixture. However, the CO₂ and C₃H₈ in MOR-type zeolite system is an exception caused by segregation effects. In Figure 14(b), we compare the mixture isotherms computed using IAST, SIAST, and SEI models for an equimolar mixture of CO₂ and C₃H₈ inside MOR-type zeolite. For this system, IAST shows significant deviations from the GCMC data whereas SIAST and SEI are in excellent agreement with these data. IAST underpredicts the adsorbed loadings for C₃H₈ and overpredicts for CO₂ adsorption. The reason for the failure in this system, is that IAST assumes a uniform adsorbent but MOR-type zeolite has two distinct types of adsorption sites with CO₂ and C₃H₈ have very different affinities for the two types of sites [29]. Consequently, the competition due to adsorption will not be identical in both of these sites. IAST fails to capture this effect and leads to incorrect predictions of adsorbed loadings.

The segregation effect has a huge influence on the behaviour of the breakthrough curves. Figure 15 shows the breakthrough curves for CO₂, and C₃H₈ inside MOR-type zeolite comparing the IAST, SIAST and SEI mixture predictions. The simulations parameters are: column length (L) = 0.3 m, particle density (ρ_p) = 1711.06 kg/m³, bed void fraction (ε_b) = 0.4, inlet velocity (v^{in}) = 0.1 m/s, total pressure

(p_T) = 1 bar, and the mass transfer coefficients (k) for CO₂, and C₃H₈ in MOR-type zeolite are taken as 0.06 s⁻¹. The difference in breakthrough behaviour between IAST and SIAST is striking. Note that the prediction is based on the same pure component isotherm models, but that the IAST and SIAST differ in the adsorption physics. This example serves as an example that mixture prediction should be validated by explicit grand-canonical Monte Carlo simulations to verify the correct choice of the mixture prediction model. Note that SIAST and SEI lead to almost identical breakthrough curves. SEI is the non-iterative version, and hence has advantages in terms of speed and stability.

RUPTURA provides various options (IAST, SIAST, EI, and SEI) to estimate the mixture equilibrium loadings. One has to know apriori whether the adsorbent is heterogeneous and the adsorbing components prefer certain types of adsorption sites over the others. Knowledge of such information is essential in choosing the right mixture isotherm prediction model. If the adsorbent has distinct adsorption sites, then one should use SIAST [29], or SEI [31]. For uniform adsorbents, one can use IAST or EI. Also, it is important to note that for adsorbents with single type of adsorption sites, SIAST, and IAST are identical. Similarly, SEI, and EI are identical for uniform adsorbents. One should also be aware that EI and SEI can only be used if the pure component isotherms are Langmuir type.

Another important factor to consider is the effect of the number of grid points. A grid independence test is vital to determine the adequate number of grid points necessary for the breakthrough simulation. Here, we present a grid independence test for this case study. Three simulations are performed for this mixture with a different number of spatial grid points ($N_{\text{grid}} = 20, 50, \text{ and } 100$). In Figure 16, we can observe that the breakthrough curves generated using $N_{\text{grid}} = 20$ are slightly different from those using $N_{\text{grid}} = 50$. The differences in the breakthrough curves becomes smaller for $N_{\text{grid}} = 50$, and 100. This indicates that the breakthrough curves undergo changes with increasing N_{grid} to a certain limit. Beyond this point, these curves are invariant to an increase in the number of grid points.

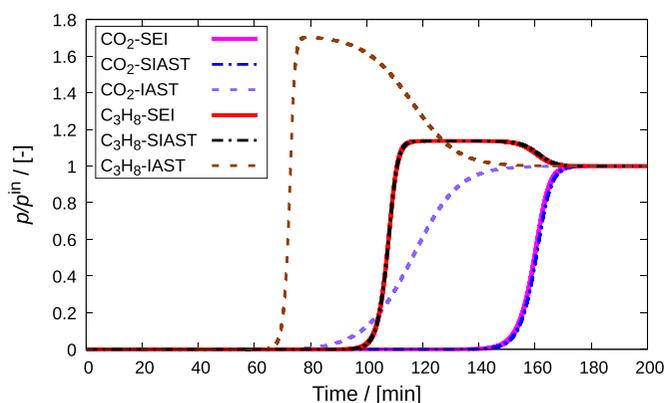


Figure 15. (Colour online) Comparison between breakthrough curves obtained on implementing IAST, SIAST, and SEI to the breakthrough curve model. A mixture of CO_2 and C_3H_8 in MOR-type zeolite at 300 K and 10^5 Pa is considered. Each of these components constitutes 10% of the gas phase. Helium is used as the carrier gas. The adsorption column is operated in isothermal and isobaric conditions.

5. Isotherm fitting

5.1. Introduction

Curve fitting methods play an important role in many fields that involve system modelling and prediction techniques. Fitting is frequently used when it is necessary to match a complex model with (experimental) data [234,235]. The determination of a suitable set of parameters for an analytical model (the parametric function) can reveal insights into the underlying physical phenomena. The aim of this work is to accurately fit the pure component isotherm models (as described in Section 2) to isotherm data obtained from experiments or grand-canonical Monte Carlo simulations. The most common procedure in the literature is the use of analytical functions for model representation. It is also possible to interpolate data in a model-agnostic manner using e.g. cubic splines [236]. Simon et al. provided an interesting discussion on this topic [77]. Both simulation and experimental data have inherent noise, and when using numerical quadrature, there is always the danger

of missing some physical information in an analytical model owing to over-fitting or over-interpreting the physical behaviour that is actually caused by errors in the data. Recently, Anderson and Gómez-Gualdrón [237] designed a method to predict the single-component adsorption of various small adsorbates (Xe , Kr , CH_4 , CH_6 , and N_2) using machine learning techniques ('multipurpose' multilayer perceptron (MLP)). Using this method, these authors were able to predict thousands of mixing isotherms using a hybrid implementation of MLP-IAST. In RUPTURA, we developed our own implementation of a fitting tool for the isotherm models listed in Table 1.

5.2. Fitting methods

5.2.1. Linear fitting methods

A widely used technique to fit models to isotherm data is to carry out linear transformations on the isotherm data and then perform linear regression. Some isotherm models, such as Langmuir and Freundlich, can be estimated from linear regression, since these models can be linearised. Four linear transformations can be applied to the Langmuir isotherm ($\frac{q}{q^{\text{sat}}} = \frac{bp}{1 + bp}$):

- (1) Double Reciprocal or Lineweaver-Burk transformation [238] ($\frac{1}{q}$ vs. $\frac{1}{p}$ plot, and $\frac{1}{q} = \frac{1}{q^{\text{sat}}} + \frac{1}{q^{\text{sat}}bp}$ transformation): It is strongly biased towards fitting the data in the low concentration range.
- (2) Reciprocal or Langmuir transformation [239] ($\frac{p}{q}$ vs. p plot, $\frac{p}{q} = \frac{1}{bq^{\text{sat}}} + \frac{1}{bp}$) tends to amplify the deviations from the fitted equation, highlighting outliers.
- (3) Eadie-Hofstee transformation [240,241] (q vs. $\frac{q}{p}$ plot, $q = q^{\text{sat}} - \frac{q}{bp}$ transformation). It has some bias toward fitting the data in the low concentration range.
- (4) Distribution Coefficient or Scatchard transformation [242] ($\frac{q}{p}$ vs. p plot, $\frac{q}{p} = bq^{\text{sat}} - bq$). It is biased toward fitting the data in the high concentration range.

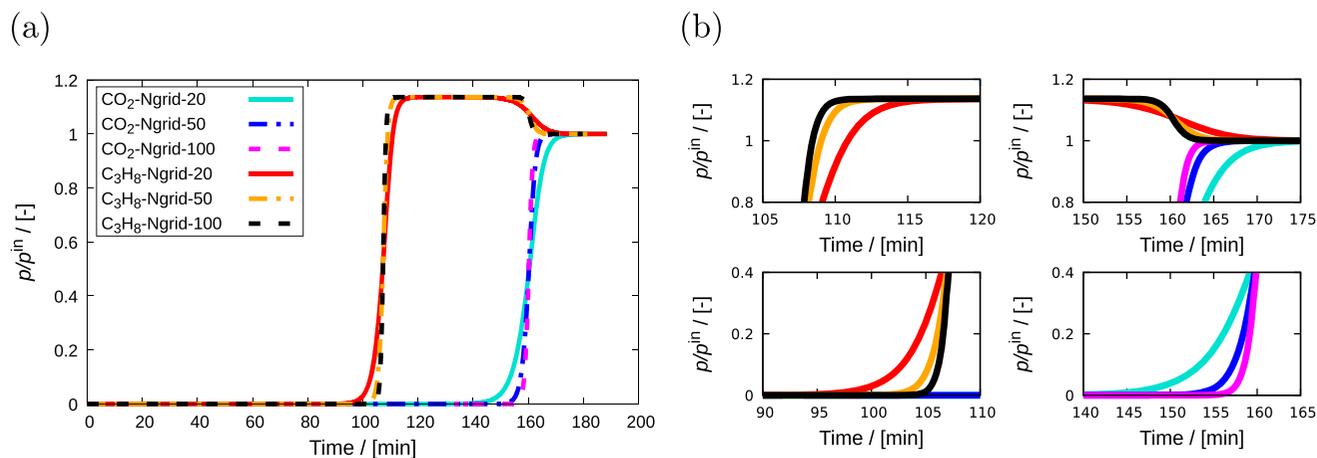


Figure 16. (Colour online) Grid independence test on simulation of breakthrough curves for a mixture of CO_2 and C_3H_8 in MOR-type zeolite at 300 K and 10^5 Pa is performed. (a) Breakthrough curves simulated at different spatial grid points ($N_{\text{grid}} = 20, 50,$ and 100), (b) certain zoomed in parts of the curves showing discrepancies due to the use of a different number of grid points. Each of these components constitutes 10% of the gas phase. Helium is used as the carrier gas. The adsorption column is operated in isothermal and isobaric conditions. With increasing the number of grid points, the breakthrough curves slightly changes. The variation becomes smaller between $N_{\text{grid}} = 50$ and 100 .

Because the error distribution is modified and the weight of each point in the fit is transformation dependent, the result of the fit will depend on the choice of the linearisation method [243]. For this reason, the best fit is not the one with the highest correlation coefficient, but the one that predicts an error distribution that corresponds to the original data. Single Langmuir behaviour is rare, and in most cases multiple-site isotherm models are needed. A more general approach is to use nonlinear regression [235].

5.2.2. Nonlinear least-squares (NLLS) fitting methods

In nonlinear regression problems, the aim is to find a parametric function

$$y = f(x; \{a_k\}_{k=1}^M) \quad (300)$$

which best fits a certain reference data set of points $(x_i, y_i)_{i=1}^N$ by minimising an error measure in the fitting. A widely used approach is to use the sum of squared residuals. The problem is thus mathematically defined as follows:

$$\begin{aligned} \text{WSSE} &= \sum_{i=1}^N r_i(x; \{a_k\}_{k=1}^M) \\ &= \sum_{i=1}^N w_i (y_i - f(x_i; \{a_k\}_{k=1}^M))^2 \end{aligned} \quad (301)$$

$$\phi = \arg_{\{a_k\}_{k=1}^M} \min_{x \in \mathcal{X}} (\text{WSSE}) \quad (302)$$

where WSSE stands for Weighted Sum of the Squared Error (or cost function), ϕ is the value in the minimisation process, r_i are the residual functions, and w_i are the weights associated with each (x_i, y_i) -point. When the parametric function f is unknown, we have to choose a suitable model with a convenient set of M parameters (a_k) , and the error ϕ is minimised in an iterative way.

Gauss–Newton algorithm (GNA) [244]: In the Gauss–Newton method, the sum of squared errors is reduced by assuming that the least squares function is locally quadratic, and the minimum of the quadratic is obtained. The method is based on Newton’s method to follow the curvature to the minimum, but does not use the Hessian of the residual function (which is computationally expensive), but the Jacobian of the residual functions, $r(\{a_k\}_{k=1}^M)$.

Steepest descent algorithm (SDA) [244]: In this method, also known as Gradient Descent, the sum of the squared errors is reduced by updating the parameters in the steepest-descent direction. This direction is calculated using the gradient, $-\nabla r(\{a_k\}_{k=1}^M)$, and is therefore computationally cheap.

Marquardt–Levenberg algorithm (MLA) [245–249]: Developed by Levenberg, Girard, Wynne, Morrison, Marquardt. This method is actually a combination of two other NLLS fitting methods (GNA and SDA): It acts more like a SDA method when the parameters are far from their optimal value, and acts more like the GNA method when the parameters are close to their optimal values. This is the method used by the Gnuplot program, among others. An updated version of this method, which solves the problem of stacked solutions in local minimum, is the Trust Region Reflective method [250].

There are other widely used gradient-, Jacobian-, or Hessian-based algorithms to follow a path to find the minimum

(whose computational efficiencies depend on the nature of the problem to be optimised): The Conjugate Gradient (CG) method [251], Broyden–Fletcher–Goldfarb–Shanno (BFGS) algorithm [252–255], and updates (e.g. Limited-memory BFGS [256]), the rational function optimisation algorithm (RFO), etc. In general, NLLS fitting is not guaranteed to converge to the global optimum from scratch (the solution with the smallest sum of squared residuals, SSR), and often gets stuck in a local minimum.

5.2.3. Heuristic fitting methods

Heuristic Search methods (Non-Math Optimisation algorithms) are not based on finding optimal analytic paths, based on gradients, Jacobians or Hessians, but explore the search space stochastically, keeping track of the ‘best’ points along the way. Two example approaches are discussed: the Nelder–Mead algorithm and genetic algorithm.

The Nelder–Mead algorithm (NMA) [117,257] is also called the downhill simplex method and was first introduced by Spendley et al. [257]. It is a heuristic search method based on the construction of a hypertetrahedron in M dimensions (a simplex) and how it adapts itself iteratively (by minimising the WSSE value) to the local landscape of the M -dimensional surface for the $\{a_k\}_{k=1}^M$ parameters. Each vertex $\mathbf{a}_{j=1}^{M+1}$ of this simplex is a vector with as many dimensions as there are parameters of the function f , i.e. $\mathbf{a}_j = (a_{1,j}, a_{2,j}, \dots, a_{M,j})$. This is a local method and does not require derivatives.

The Genetic Algorithm (GA) [258,259] is a type of parallel heuristic search method. This method was described for the first time by De Jong [258] and Holland et al. [259]. The GA belongs to Evolutionary Algorithms (EA), a family of algorithms for global optimisation inspired by biological evolution, and uses biological operators inspired by biological evolution, such as reproduction, mutation, recombination, and selection. It is based on the generation of a population of individuals (each individual is a candidate for the optimisation solution) that are ordered according to their fitness. During the process, the population of solutions remains constant, and the worst solutions are replaced (by ranking its goodness-of-fit) by other solutions that are either mutation or recombination of better solutions. Some EA are as follows: Genetic Programming [260,261], Evolution Strategies [262], or Evolutionary Programming [263]. Other nature-inspired algorithms (but not part of the EA family) are: Particle Swarm Optimization (PSO) [264,265], Ant Colony Optimization (ACO) [266], Cuckoo Search (CS) [267], Grey Wolf Optimization (GWO) and updates [268,269], or Elephant Herd Optimization (EHO) [270,271].

GA is the most popular type of EA. In particular, GA represents each individual of the GA population as a string of numbers, usually a binary string called ‘‘genotype’’. Modifications in the genotype imply changes in the fitness. For some problems, it is convenient to use non-binary representations of the genotype.

5.3. Evaluating isotherm goodness-of-fit

In RUPTURA, we have used two standard measures for evaluating the goodness-of-fit: the Residual Root Mean Square Error (RMSE), and the correlation coefficient (r). We defined

the RMSE as:

$$\text{RMSE} = \left(\frac{\text{WSSE}}{N - M} \right)^{\frac{1}{2}} \quad (303)$$

where WSSE is the Weighted Sum of the Squared Error (Equation (301)), and N and M are the number of data points and the number of parameters of the model, respectively. The correlation coefficient r (usually r^2) is defined as:

$$r = \frac{\sum_{i=1}^N (w_i y_i - \bar{y})(w_i f(x_i) - \bar{f})}{\sqrt{\sum_{i=1}^N (w_i y_i - \bar{y})^2 \sum_{i=1}^N (w_i f(x_i) - \bar{f})^2}} \quad (304)$$

For each optimisation iteration, RUPTURA monitors both values.

5.4. Software for isotherm fitting

Here we list some software proposed in the literature for isotherm fitting, as well as other general fitting software used for this purpose:

- (1) ISOTHERM and FIT programs [243,272,273]:
This program is developed by Kinniburgh [272]. To the best of our knowledge, ISOTHERM appears in the literature as one of the first publicly available programs for isotherm fitting. Unfortunately, we have not been able to locate the code to test it.
- (2) ISOFIT [274]:
ISOFIT was developed by Matott and Rabideau [274]. It is a program (executables available for Linux and Windows) that utilises a hybrid optimisation procedure combining Particle Swarm Optimization with Levenberg-Marquardt nonlinear regression. Many tools are available to check the quality of the fit. ISOFIT includes a wide collection of isotherm models (BET, Freundlich, Freundlich with Linear Partitioning, Langmuir-Freundlich, Langmuir, Langmuir with Linear Partitioning, Linear, Polanyi, Polanyi with Linear Partitioning, and Toth isotherms). However, it does not support fitting multisite isotherm models.
- (3) GAIASST [120]:
GAIASST is developed by Balestra et al. [120]. Written in Fortran code (standard 2003), it has a module for isotherm fitting. The fitting module is coded using a constrained hybrid global optimisation procedure (NMA and GA). GA uses a single-precision floating-point format (binary32) to code the genotype. It presents a wide variety of isotherm models, from one to three adsorption sites, as well as some isobar models.
- (4) IAST++ [121]:
IAST++ is developed by Lee et al. [121]. It is a Windows user-friendly executable program with a graphical user interface. It contains a module for suggesting isotherm models (among Langmuir, Langmuir-Freundlich, Langmuir Dual Site, Langmuir Freundlich Dual Site, BET, Quadratic, and Henry) based on the isotherm data entered, as well as visualisation of the fitting procedure.

If the module does not find an acceptable isotherm model (based on goodness-of-fit) it suggests a quadratic interpolation. In practise, this module requires a fine-tuned selection of ranges in the generation of initial parameter values in order not to get stuck into local minima. This is particularly important for the Langmuir dual-site and Langmuir-Freundlich dual-site models.

(5) Non-dedicated software:

There is a large variety of open source tools, codes, and libraries for general purposes with which non-linear fits can be performed using different techniques. To mention a few of these: the SciPy Python Library [275] or the GNU Scientific Library (GSL) [276], or widely-used programs like Gnuplot [277], Octave [278]/ MATLAB [208], Origin [279] for NLLS methods, and the PIKAIA software [280] for GA methods.

5.5. Implementation of the GA-NMA hybrid method

In RUPTURA, we have implemented a constrained GA-NMA hybrid optimisation procedure that combines the GA (for an initial global search for the minimum), with the NMA method (to refine the founded best solutions). We employ the hybrid global optimisation method that was also used in the GAIASST code, but we have made significant improvements in speed and efficiency. RUPTURA uses hashing tables to map the genes, while GAIASST works with strings comparisons.

5.5.1. GA stage

We have used a concatenation of the 64-bit binary representation (double-precision floating-point format or just binary64) of the M parameters of the Equation (300) to codified the genotype. There is a one-to-one relationship between the genotype and the sequence of parameters $\{a_j\}_{j=1}^M$ that is called the "phenotype". The parameter values of the isotherm models are constrained to a range of values to prevent nonphysical isotherm parameters (e.g. negative values for the saturation loading are not allowed). These constraints are hard-coded for each isotherm model.

The initial population is based on randomly generated isotherms from a range of initial values for each specified parameter. For example, the saturation values, q^{sat} , are generated between 0.0 to 10.0 [mol/(kg framework)], the b parameter between 1×10^{-10} to $1 \times 10^{+10}$ [Pa $^{-1}$], and the heterogeneity parameter, ν , anywhere between 0.1 to 2.1 [–]. If the isotherm parameters specified in the input files are non-zero, a refitting process is performed starting from these values.

In each optimisation step, k , we sort the population of individuals (called "citizens") according to its fitness and apply five biological operators on their genotype: elitism, crossover, mutation, replacement, and nuclear disaster. These GA operators are shown schematically in Figure 17.

- (1) Elitism: We allow the best individuals ($\sim 5\%$) of the current generation, k , to pass on unchanged to the next generation. In this way, we ensure that the best individual does not lose fitness in the optimisation process.

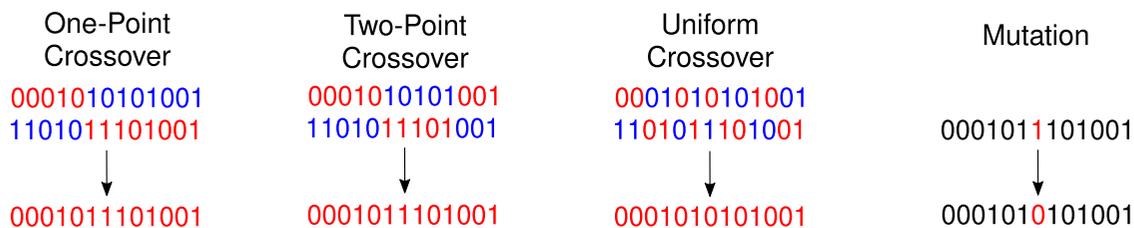


Figure 17. (Colour online) Schematic representation of GA operators crossover, and mutation. The crossover operator is analogous to the crossover that happens during sexual reproduction in biology, and it combines the genotype of two parents to generate new offspring. We implemented three types of crossover operator: with one- and two points, and the uniform crossover. The mutation operator is activated before the children are added to the next generation.

- (2) Replacement: The worst ($\sim 5\%$) individuals are replaced by new individuals.
- (3) Crossover: We mate the population of the current generation (parents) to generate the next generation of individuals (children). We have implemented one-point, two-point, and uniform crossover, but using only the first one is sufficient to converge to a high-quality result. We perform a controlled mating between parents. Two types of crossover were carried out: between elitists (the group that ensures the goodness-of-fit) and between elitists and non-elitists (which provides the global character of the optimisation method).
- (4) Mutation: Some of the children, depending on the mutation rate value, do not pass unaltered to the next generation: We apply small changes in their genotype (see Figure 17).
- (5) Nuclear disaster: Only elitists are passed on to the next generation. The rest of the individuals are replaced by new individuals. This operator operates at a very low rate and is designed to escape from local minima. When this operator is activated, we break the cycle of operators and jump directly to the next generation, $j + 1$.

At the end of the operator cycle, we update the children to become parents and move on to the next generation, $j + 1$. During the optimisation process, RUPTURA prints the values of the genotype, phenotype (parameters), as well as the RMSE and the squared correlation coefficient, r^2 , on the screen. As an example, for a step $j = 114$ of a Langmuir-Freundlich isotherm model fitting, it would look like:

```

mol: 0 step: 114 Fitness: 0.061057
R^2: 0.990488 Similarity: 2191/4096
Finishing: 80/100
number of parameters: 3
genotype:
0011111111110011000000000000000000000000-
0000000000000000000101100 parameter:
1.1875
genotype:
00111110111111111111111111111111111111-
111111111111111111111111111111111111 parameter:
3.05176e-05
genotype:

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```

0011111111110110000110110010000110011011-
001110111001110001010000 parameter:
1.38162

```

When the GA reached an optimal genotype ($r^2 \rightarrow 1$ and $\text{RMSE} \rightarrow 0$ or RUPTURA has reached the maximum number of steps allowed), the candidate for the global minimum is refined during the NMA stage.

5.5.2. NMA (simplex) stage

We start with the parameter values corresponding to the phenotype of the best individual in the GA population. At each iteration k , the $M + 1$ vertices of the simplex, Δ_k , are converging to the minimum, and we sort and label the vertices according to Equation (302), such that:

$$\phi(\mathbf{a}_1) \leq \phi(\mathbf{a}_2) \leq \dots \leq \phi(\mathbf{a}_{M+1}), \quad (305)$$

being \mathbf{a}_1 the best, and \mathbf{a}_{M+1} the worst. In addition, we also calculate the centroid of the best M vertices, i.e. avoiding the worst:

$$\bar{\mathbf{a}} = \sum_{i=1}^M \frac{\mathbf{a}_i}{M} \quad (306)$$

Following the version of Lagarias et al. [281] of the Nelder-Mead algorithm, we updated the vertices by performing four possible operations: reflection, expansion, contraction, and shrinkage. Each of these operations are determined by a scalar: $\alpha = 1$, $\beta = 2$, $\gamma = \frac{1}{2}$, and $\delta = \frac{1}{2}$, respectively. We have used a version in which these scalars are constant, but there are modern implementations in which these parameters are adaptable [282]. In Figure 18 we show the algorithm of a single iteration step. In more detail, the four operations are

- (1) Reflection: Once we have ordered the vertices according to Equation (305), and we have calculated the centroid of Equation (306), we proceed to calculate the reflected point, \mathbf{a}_r :

$$\mathbf{a}_r = \bar{\mathbf{a}} + \alpha(\bar{\mathbf{a}} + \mathbf{a}_{M+1}) \quad (307)$$

We evaluate this point, $\phi(\mathbf{a}_r)$. If $\phi(\mathbf{a}_r) \leq \phi(\mathbf{a}_1) < \phi(\mathbf{a}_M)$, then we accept the reflection point: $\mathbf{a}_{M+1} = \mathbf{a}_r$.

- (2) Expansion: If $\phi(\mathbf{a}_r) \leq \phi(\mathbf{a}_1)$ then we calculate the expansion point, \mathbf{a}_e :

$$\mathbf{a}_e = \bar{\mathbf{a}} + \beta(\mathbf{a}_r - \bar{\mathbf{a}}) \quad (308)$$

We evaluate this expansion point, $\phi(\mathbf{a}_e)$. If $\phi(\mathbf{a}_e) < \phi(\mathbf{a}_r)$

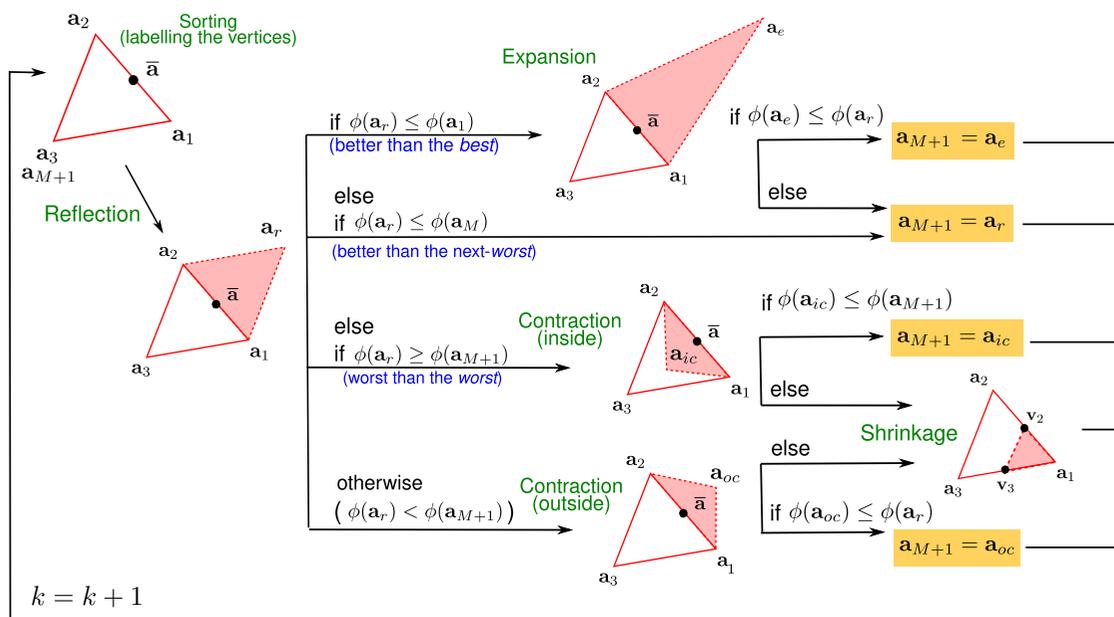


Figure 18. (Colour online) Flowchart of one step, k , in the Nelder-Mead algorithm [117] for a parametric function, f , with two parameters. In this way, the simplex is a triangle, and the visualisation is easier. The four operations and the sorting stage are in green labels.

then we accept $\mathbf{a}_{M+1} = \mathbf{a}_e$, otherwise we accept the reflection point: $\mathbf{a}_{M+1} = \mathbf{a}_r$.

(3) Contraction.

- (a) Outside: If $\phi(\mathbf{a}_M) \leq \phi(\mathbf{a}_r) < \phi(\mathbf{a}_{M+1})$ we perform an outside contraction:

$$\mathbf{a}_{oc} = \bar{\mathbf{a}} + \gamma(\mathbf{a}_r - \bar{\mathbf{a}}) \quad (309)$$

and we evaluate the new point, $\phi(\mathbf{a}_{oc})$. If $\phi(\mathbf{a}_{oc}) \leq \phi(\mathbf{a}_r)$ then we accept the outside contraction point: $\mathbf{a}_{M+1} = \mathbf{a}_{oc}$, else we perform a shrinkage operation.

- (b) Inside: If $\phi(\mathbf{a}_r) \geq \phi(\mathbf{a}_{M+1})$ we perform an inside contraction:

$$\mathbf{a}_{ic} = \bar{\mathbf{a}} - \gamma(\mathbf{a}_r - \bar{\mathbf{a}}) \quad (310)$$

and we evaluate the new point, $\phi(\mathbf{a}_{ic})$. If $\phi(\mathbf{a}_{ic}) \leq \phi(\mathbf{a}_{M+1})$ then we accept the inside contraction point: $\mathbf{a}_{M+1} = \mathbf{a}_{ic}$, else we perform a shrinkage operation.

- (4) Shrinkage: We generate the new vertices:

$$\begin{aligned} < p > \mathbf{v}_i = \mathbf{a}_1 + \delta(\mathbf{a}_i - \mathbf{a}_1), \\ \forall i = 2, \dots, M + 1. \end{aligned} \quad (311)$$

These will be the new vertices, $\mathbf{a}_{i=1}^{M+1}$, in the next iteration.

5.6. Validation

To validate the RUPTURA fitting function and compare it with other widely used codes (ISOFIT, IAST++, pyIAST, GAIASST, and Gnuplot; see Subsection 5.4) we fit the adsorption isotherms of $n\text{-C}_7$ in BEA zeolite at 552 K. The isotherm exhibits a behaviour that can be modelled by many kinds of models: Langmuir, Langmuir-Freundlich, Sips, Toth, etc. We have chosen the Toth model of a single adsorption site (three parameters: q^{sat} , b , and ν). For this relatively simple isotherm shape, all codes are able to accurately fit the isotherm

model to the data, as shown in Figure 19. The obtained goodness-of-fits were $r^2 > 0.998$, and $\text{RMSE} < 0.025$ [mol/(kg framework)], even from scratch. ISOFIT++ does not have incorporated the Toth model. The fitting of the isotherm using the Langmuir model using the IAST++ code gave reasonable results ($\text{RMSE} = 0.025$ [mol/(kg framework)]). RUPTURA takes 1.1 s to do this fit using a single core Intel Core i7-10700K CPU at 3.80 GHz.

A much more challenging case is the adsorption isotherm of o -xylene in MAF-X8 at 300 K. The isotherm shows, see Figure 20, two steep slopes at 1×10^{-6} and 10 Pa around an inflection ('kink'). By adding a third site to the model, it fits well to a third bend of the isotherm. Adding a fourth site does not qualitatively improve the model. We have modelled the isotherm using the Langmuir-Freundlich model with two adsorption sites. The dual-site Langmuir-Freundlich model has six parameters (q_1^{sat} , b_1 , ν_1 , q_2^{sat} , b_2 , and ν_2). In general, for an increased number of model parameters, it is more likely that local minima will appear, and global optimisation algorithms become necessary.

GAIASST and RUPTURA predict equivalent values (the fitting algorithms are very similar), but RUPTURA is much more optimised and performs the same fitting in ten times less time, with goodness-of-fit values of $\text{RMSE} \leq 0.066$ [mol/(kg framework)] and $r^2 = 0.998$. However, the optimisations from scratch using pyIAST (not shown in the Figure), Gnuplot (from scratch), or IAST++, with $\text{RMSE} \geq 0.312$ [mol/(kg framework)] were unable to accurately fit the model. That is, the error is too large for the model to represent the isotherm data well and to be used in IAST or breakthrough calculations). Only if the starting values are chosen close to the solution is Gnuplot able to generate models with high goodness of fit (see Table 13). RUPTURA takes 2.6 s to do this fit, and GAIASST, 26 s. If we consider a Langmuir-Freundlich with three sites (nine parameters) for the model in the fitting procedure, RUPTURA takes 6.279

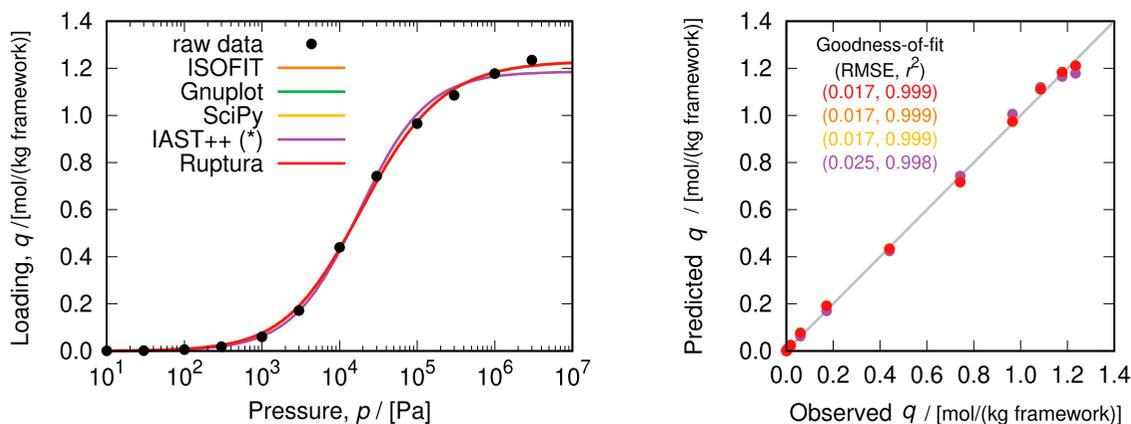


Figure 19. (Colour online) (Left) Adsorption of n -C₇ in BEA zeolite at 552 K and some fitted models using ISOFIT, Gnuplot, IAST++, and RUPTURA for a Toth model of a single adsorption site. (Right) Predicted loading value vs. observed loading values. The goodness-of-fit in colours (same code colour of the Left panel) for each code. The RMSE values are in [mol/(kg framework)] units.

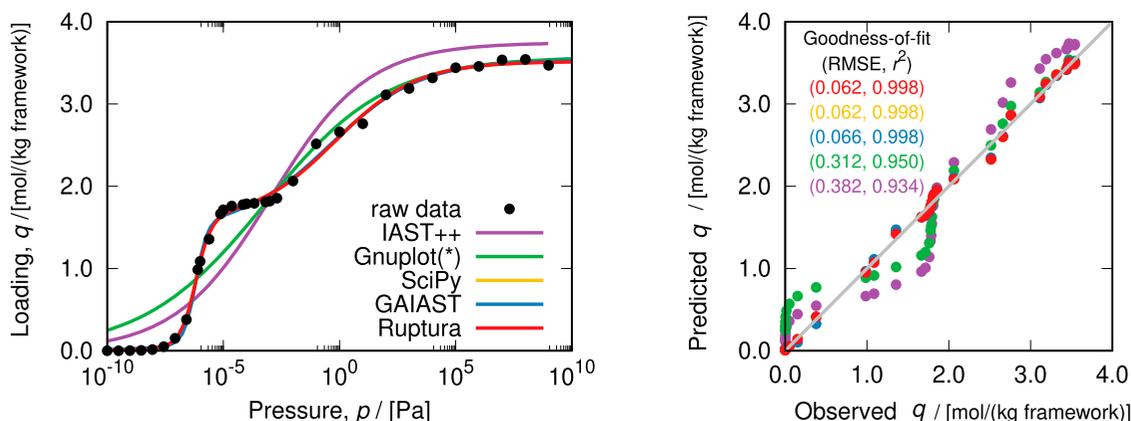


Figure 20. (Colour online) (Left) Adsorption of o -xylene in MAF-X8 zeolite at 300 K and some fitted models using IAST++, Gnuplot (from scratch), GAIAS, and RUPTURA for a dual-site Langmuir-Freundlich model. (Right) Predicted loading value vs. observed loading values. The goodness-of-fit for each code in colours defined in the left panel. The RMSE values are in [mol/(kg framework)] units.

Table 13. Fitted parameters for the adsorption isotherm (dual-site Langmuir-Freundlich) of o -xylene in MAF-x8-P1 zeolite at 433 K using different methods.

$q_1^{\text{sat}}/$	$b_1/$	$\nu_1/$	$q_2^{\text{sat}}/$	$b_2/$	$\nu_2/$	RMSE/	
	[mol/(kg framework)]	[Pa ⁻¹]	[-]	[mol/(kg framework)]	[Pa ⁻¹]	[-]	[mol/(kg framework)]
RUPTURA	1.9377	1.1132	0.2476	1.5793	1.0485×10^8	1.2963	0.062
SciPy	1.9583	1.1334	0.2439	1.5617	2.8218×10^8	1.3654	0.062
Gnuplot	1.9554	1.1305	0.2438	1.5642	2.4394×10^8	1.3553	0.064
GAIAS	2.0059	1.1785	0.2337	1.5215	3.2212×10^9	1.5360	0.066

Notes: In this table, unlike in Figure 20, the Gnuplot fit has been performed using initial values close to the final solution, to avoid being stuck in a local minimum.

s, obtaining RMSE = 0.0385 [mol/(kg framework)], and $r^2 = 0.9993$. However, erroneous results could be obtained by overfitting a simple isotherm with an unnecessary complex model. Regardless of this issue, RUPTURA is able to quickly optimise difficult isotherms (with multiple minima) as shown in Figure 21.

A particularly difficult test case is alkane C6 isomers in MAF-6 at 298 K with a relatively small amount of points, but with small error bars. Figure 22 shows that RUPTURA produces excellent fits using dual- and triple-site Langmuir-Freundlich models. The shape of the isotherms, combined with smooth and sharply rising slopes over many orders of magnitude of pressure, poses a challenge for the fit. Note that using a small amount of points over a large

pressure range (equally distributed in log-scale) is a very common scenario to explore the overall shape of the isotherms.

Lastly, we used Python SciPy Library to test the RUPTURA code (see Listing 1). Scipy (scipy.optimize.curve_fit) uses the Trust Region Reflective (TRR) method for constrained problems [283,284]. The TRR method is an evolution of the Levenberg-Marquardt algorithm, but with global convergence. In Figures 19 and 20, as well as Table 13, you can see that RUPTURA gives goodness-of-fit comparable to TRR.

Listing 1. Python script used to fit isotherms with Toth and dual-site Langmuir-Freundlich models using the SciPy Library.]

```

import pandas as pd
import numpy as np
import matplotlib.pyplot as plt
from scipy.optimize import curve_fit

def Toth(P, q, b, n):
    return q * b * P / pow(1 + pow(b * P, n), (1.0/n))

def DSLangmuirFreundlich(P, q1, b1, n1, q2, b2, n2):
    return q1 * b1 * pow(P, n1) / (1 + b1 * pow(P, n1)) +
           q2 * b2 * pow(P, n2) / (1 + b2 * pow(P, n2))

df = pd.read_csv('Results.dat-MAF-x8-P1-Repeat-433K-o-xylene', sep=' ')
popt, pcov = curve_fit(DSLangmuirFreundlich,
                       df['P'].values, df['L'].values,
                       p0=(1.0, 1.0, 1.0, 1.0, 1.0, 1.0),
                       bounds=([0, 1.0E-20, 0.1, 0, 1.0E-20, 0.1],
                               [100, 1.0E+20, 10.0, 100, 1.0E+20, 10.0]))

print(*popt)

```

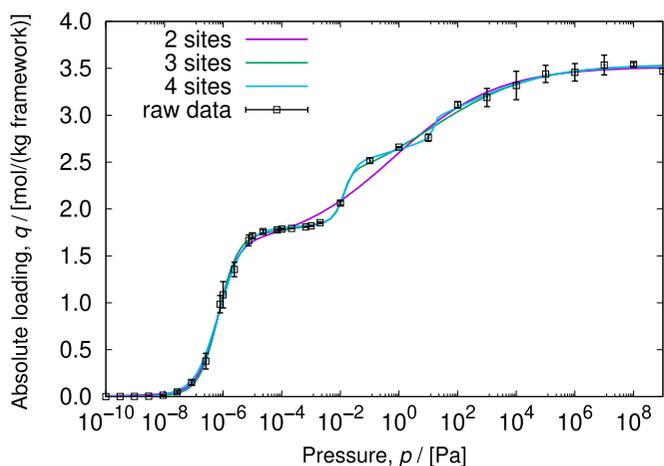


Figure 21. (Colour online) The adsorption isotherm prediction for two, three, and four sites Langmuir-Freundlich isotherm models for *o*-xylene in MAF-X8. Without the experimental error information for the loading data is difficult to establish what kind of model is more realistic.

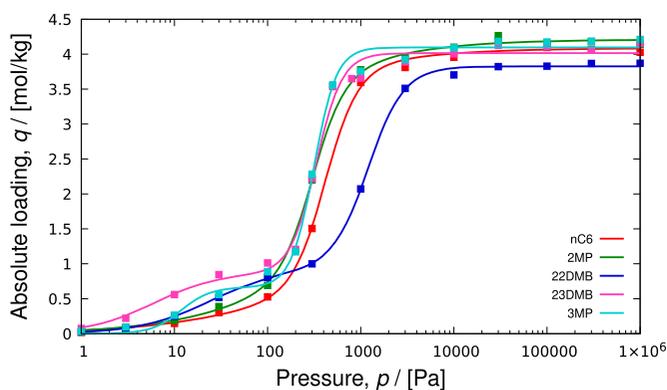


Figure 22. (Colour online) The C_6 -alkane-isomers adsorption isotherms in MAF-6 computed from grand-canonical Monte Carlo simulations fitted with dual- and triple site Langmuir-Freundlich isotherm models. The peculiar shape of these isotherms in the low-pressure region makes this system challenging to perform reliable fitting.

6. RUPTURA installation

For the basic functionality, only a c++11 compiler is needed. However, automatic picture generation is based on gnuplot [277], and automatic movie generation is based on gnuplot and ffmpeg [285]. FFmpeg needs to have support for HEVC/H.265 and/or H.264 video encoding.

The default colour scheme of gnuplot has several issues: the sequence of colours is hard to see for colour-blind people and yellow is hardly visible against a white background. We therefore use the colour scheme published in the book ‘Gnuplot in action’, stylesheet listing 12.7 [286]. All the required software tools are available as open source software.

6.1. Mac

Some additional software tools need to be installed. First, the Xcode Command Line Tools need to be installed. The easiest way to install Xcode Command Line Tools is by installing Homebrew, the popular package manager for macOS. When you install Homebrew, you will be offered the option of installing Xcode Command Line Tools. Go to the website <https://brew.sh> and copy and paste the installation command into a terminal. The command line tools include `git`, a version control system. Using homebrew, we can also install `gnuplot` and `ffmpeg`.

```

brew install gnuplot
brew install ffmpeg

```

Next, download RUPTURA using `git` and compile the code

```

git clone https://github.com/iraspa/ruptura
cd ruptura
cd src
make

```

6.2. Linux

Some additional software tools need to be installed. For Ubuntu-based systems

```
sudo apt install git build-essential gnu-
plot ffmpeg
```

Next, download RUPTURA using git and compile the code

```
git clone https://github.com/iraspa/
ruptura
cd ruptura
cd src
make
```

6.3. Windows

Some additional software tools need to be installed.

- **git**
The most official build is available for download on the Git website. Just go to <https://git-scm.com/download/win> and the download will start automatically.
- **gnuplot**
Go to <https://sourceforge.net/projects/gnuplot/files/gnuplot/> to download gnuplot, and install it via the binary installer. Preferably install gnuplot in C:\Program Files\gnuplot, or alternatively add the directory C:\Program Files\gnuplot\bin to the PATH variable.
- **ffmpeg**
Go to <https://github.com/BtbN/FFmpeg-Builds/releases>, and download ffmpeg-master-latest-win64-gpl.zip. Unzip, and preferably install ffmpeg in C:\Program Files\ffmpeg-master-latest-win64-gpl, or alternatively add the directory C:\Program Files\ffmpeg-master-latest-win64-gpl\bin to the PATH environment variable.

Next, download RUPTURA using git

```
git clone https://github.com/iraspa/
ruptura
```

A binary executable src/ruptura.exe for windows is already provided.

7. RUPTURA input description

7.1. General

All input is case-insensitive and white space does not matter. Font keyword means the literal text, [a|b] means the input of either a or b, [real] means the expected number is a floating point value, [int] means an integer is expected, and [string] means a string is expected. Strings are not allowed to contain spaces (replaces these by dashes or underscores). Numbering of indices starts at zero.

7.2. Simulation types

- **SimulationType** [MixturePrediction | Breakthrough | Fitting]
Selects the type of the simulation. MixturePrediction selects the computation of a mixture based on pure component isotherms, the pressure-range, and the fluid-phase mole fractions. Breakthrough selects the

computation of a mixture adsorbing in a fixed-bed adsorber. Fitting selects the computation of the best fit of an analytic isotherm model to raw adsorption data.

7.3. Component information

- **Component** [int] **MoleculeName** [string]
The index of the component and the name of the component. The component name is used in the automatically generated plot-files and movies.
- **Filename** [string]
The name of a file associated with this component. Used in fitting to specify the raw data of the isotherm.
- **CarrierGas** [yes|no]
Specifies whether this component is the carrier-gas in a breakthrough simulation. There can be only one carrier-gas and a breakthrough simulation *must* contain a carrier gas. For the carrier gas there is no need to specify an isotherm model (the carrier gas is assumed to not adsorb).
- **GasPhaseMolFraction** [real]
The dimensionless gas-phase mole fraction of the component. The values of all the components should sum up to unity, but if not, the code gives a warning and continues with the explicitly normalised mole fractions.
- **MassTransferCoefficient** [real]
The mass-transfer coefficient of this component used in the Linear Driving Force (LDF) model. Units: 1/s.
- **AxialDispersionCoefficient** [real]
The coefficient of axial mixing attribute to a diffusion-like process. Units: m²/s.
- **NumberOfIsothermSites** [int]
The number of isotherm sites associated with this component. This keyword is followed by a list of isotherm models and parameters chosen from (See Table 1 for definition of the models):
Langmuir [real] [real]
 b_0 in mol kg⁻¹, b_1 in Pa⁻¹.
Anti-Langmuir [real] [real]
 b_0 in mol kg⁻¹ Pa⁻¹, parameter b_1 in Pa⁻¹.
BET [real] [real] [real]
 b_0 in mol kg⁻¹, b_1 dimensionless, b_2 dimensionless.
Henry [real]
 b_0 in mol kg⁻¹ Pa⁻¹.
Freundlich [real] [real]
 b_0 in mol kg⁻¹ Pa⁻¹, b_1 dimensionless.
Sips [real] [real] [real]
 b_0 in mol kg⁻¹, b_1 in Pa⁻¹.
Langmuir-Freundlich [real] [real] [real]
 b_0 in mol kg⁻¹, b_1 in Pa⁻¹, b_2 dimensionless.
Redlich-Peterson [real] [real] [real]
Parameter b_0 in mol kg⁻¹ Pa⁻¹, parameter b_1 in Pa⁻¹, b_2 dimensionless.
Toth [real] [real] [real]
Parameter b_0 in mol kg⁻¹, parameter b_1 in Pa⁻¹, b_2 dimensionless.
Unilan [real] [real] [real]
Parameter b_0 in mol kg⁻¹, parameter b_1 in Pa⁻¹, parameter b_2 dimensionless.

O'Brien&Myers [real] [real] [real]
Parameter b_0 in mol kg⁻¹, parameter b_1 in Pa⁻¹, parameter b_2 dimensionless.

Quadratic [real] [real] [real]
Parameter b_0 in mol kg⁻¹, parameter b_1 in Pa⁻¹, parameter b_2 in Pa⁻².

Temkin [real] [real] [real]
Parameter b_0 in mol kg⁻¹, parameter b_1 in Pa⁻¹, parameter b_2 dimensionless.

Bingel&Walton [real] [real] [real]
Parameter b_0 in mol kg⁻¹, parameter b_1 in Pa⁻¹, parameter b_2 in Pa⁻¹.

7.4. Mixture prediction

The mixture prediction module predicts, using various possible theoretical models, the adsorbed phase mole fractions based on pure component isotherms only.

- MixturePredictionMethod [IAST | SIAST | EI | SEI]

The method used to predict the mixture adsorption based on pure component isotherm information. IAST denotes the Ideal Adsorption Solution Theory (IAST) [28], and SIAST is segregated IAST where IAST is applied to sites individually [29]. EI is the explicit isotherm model (not iterative and hence very fast) that is applicable to Langmuir models only [30,31]. SEI is the segregated explicit isotherm model. These models are explained in Sections 3.4 and 3.5 Default: IAST.

- IASTMethod [FastIAS | Bisection]
The method used to compute the IAST mixture prediction. Default: FastIAS.
- PressureStart [real]
The lowest pressure of the range of pressures to be evaluated. Must be smaller than PressureEnd. Units: Pa.
- PressureEnd [real]
The highest pressure of the range of pressures to be evaluated. Must be larger than PressureStart. Units: Pa.
- NumberOfPressurePoints [int]
The number of points equally spaced in log-scale or linear scale.
- PressureScale [log|linear]
The scale of the range of pressures, either logarithmic scale (log) or linear (linear).

7.5. Breakthrough

The breakthrough module allows the computation and evaluation of the performance of a fixed bed adsorber. A fixed bed packed with particles containing a porous material is pressurised and purged with a carrier gas. A (mixture-) fluid is added to the carrier gas, resulting in a step-wise change of the inlet concentration. In chromatographic separation processes, a pulse-wise change of the inlet concentrations is used. The change of the component concentrations along the column and at the outlet of the fixed bed are recorded.

7.6. Simulation duration

- BreakthroughType [step|pulse]
Selects a step breakthrough initial condition at the inlet, or a pulse condition as explained in Sections 4.7 and 4.8
- Pulselength [real]
The length in time of the pulse condition at the inlet. Units: s, default: 10.0.
- NumberOfTimeSteps [int|auto]
Explicitly set the the number of time steps of the breakthrough computation or (only for step-breakthrough) let the program determine when the breakthrough computation is converged (auto).
- TimeStep [real]
The time step used in the numerical integration scheme. Units: s, default: 0.0005.
- PrintEvery [int]
How frequently to write status information to the screen. Default: 10,000.
- WriteEvery [int]
How frequently to write data to the output files. Default: 10,000.

7.7. Column properties

- DisplayName [string]
The name of the column, or material, that will be displayed in the output files (plots and movies).
- ColumnVoidFraction [real]
The typical value of the fixed-bed porosity or bulk void fraction is $\epsilon_b=0.38-0.40$. Units: -, default: 0.4.
- ParticleDensity [real]
The particle density ρ_p (density of the adsorbent grain) includes the inner porosity, but excludes the void fraction of the bed. Units: kg/m³, default 1000.0.
- TotalPressure [real]
The total pressure at which to compute the breakthrough. Units: Pa, default: 1e6.
- PressureGradient [real]
The gradient of the pressure along the column. Units: Pa/m, default: 0.
- ColumnEntranceVelocity [real]
The interstitial velocity of the fluid at the entrance of the column. Units: m/s, default: 0.1.
- ColumnLength [real]
The length of the column. Units: m, default: 0.3.

7.8. Integration settings

- NumberOfGridPoints [int]
The number of grid points used in the spatial discretisation of the column. Default: 100.

7.9. Fitting

The fitting module allows the fitting of isotherm models on raw, computed or measured adsorption isotherms.

- `ColumnPressure` [int]
The index of the column in the raw-data file containing the information on the pressure.
- `ColumnLoading` [int]
The index of the column in the raw-data file containing the information on the absolute adsorption amount.

8. RUPTURA tutorial

8.1. Introduction

```

SimulationType          Breakthrough
// Column settings
DisplayName              Silicalite
Temperature              313.0      // [ K]
ColumnVoidFraction      0.4        // [ -]
ParticleDensity         1144.03    // [ kg/m^3]
TotalPressure           2.5e6      // [ Pa]
PressureGradient        0.0        // [ Pa/m]
ColumnEntranceVelocity  0.1        // [ m/s]
ColumnLength            0.3        // [ m]

// Run settings
NumberOfTimeSteps       auto
PrintEvery              1000
WriteEvery              200
TimeStep                0.01      // [ s]
NumberOfGridPoints      30
MixturePredictionMethod ExplicitIsotherm

Component 0 MoleculeName      Helium
             GasPhaseMolFraction 0.9          // [ -]
             CarrierGas          yes

Component 1 MoleculeName      CO2
             GasPhaseMolFraction 0.05          // [ -]
             MassTransferCoefficient 0.06        // [ 1/s]
             AxialDispersionCoefficient 0.0        // [ m^2/s]
             NumberOfIsothermSites 1
             Langmuir            2.858 1.089e-5 // [ mol/(kg framework)] [ 1/Pa]

Component 2 MoleculeName      N2
             GasPhaseMolFraction 0.05          // [ -]
             MassTransferCoefficient 0.06        // [ 1/s]
             AxialDispersionCoefficient 0.0        // [ m^2/s]
             NumberOfIsothermSites 1
             Langmuir            2.094 0.111e-5 // [ mol/(kg framework)] [ 1/Pa]

```

The tutorial examples are designed to be fast. The binary mixture breakthrough example of CO₂/N₂ in silicalite runs in a matter of seconds. This allows interactive computations for

teaching purposes, where students can easily play around with the column properties and investigate how the separation would be influenced by the gas-phase mole fractions, the bed-void fraction, the length of the column, axial dispersion and mass-transfer coefficients, etc. The second example of C₆-isomers in BEA-type zeolite is more advanced, but still runs in one or two minutes. Both examples make use of the explicit isotherm model developed by Van Assche et al. [30] (Section 3.4.6) for the prediction of the mixture isotherms.

8.2. Breakthrough of CO₂/N₂ in silicalite

The directory `tutorial/Silicalite-CO2-N2/breakthrough` contains the input file `simulation.input`:

The simulation-type is set to `breakthrough`, the column properties and run settings are specified, and lastly the information on all the components. The component

information starts with the keyword `Component` followed by the component index (starting from zero) and the name of the component. The properties set after this line refer to the component denoted by the `Component` keyword. A component requires isotherm information except for the carrier gas. There must be a component labeled as carrier-gas and there can be only one. The isotherm information for the carrier has is implicitly a Langmuir isotherm with affinity parameter set to zero. For a component that is not the carrier gas, the number of isotherm sites need to be specified, followed by a list of isotherm models along with its parameters. A component also needs a gas-phase mol-fraction and mass-transfer coefficient, while the axial dispersion coefficient is optional.

The code is executed on mac/linux by typing in the terminal

```
./run
```

On windows you can run it from the windows console using the `run.bat` batch script, or by double-clicking on it. After a few seconds, the program is finished and many new files have been created

```
column.data          make_movie_Pnorm
component_0_Helium.data  make_movie_Pt
component_1_CO2.data    make_movie_Q
component_2_N2.data     make_movie_Qeq
make_graphs           make_movie_V
make_movie_Dpdt       make_movies
make_movie_Dqdt       plot_column_Dpdt
make_movie_P           plot_column_Dqdt
```

The `column.data` and `component` files are the files with the actual simulation data. `make_movies` creates movies to visualise the variation of different quantities along the length of the column. `Dpdt` and `Dqdt` represent time derivatives of the partial pressures and the adsorbed loadings of each component respectively. Movies are also created for the variation of the partial pressures (`P`), normalised pressure (ratio of partial pressure at the column exit to that at the inlet: `Pnorm`), total pressure (`Pt`), adsorbed loadings (`Q`), equilibrium loading (`Qeq`), and interstitial velocity (`V`) along the length of the fixed bed column. The `plot_column` files are used by the movie scripts to create figures for these measured quantities (using `gnuplot`). On windows, the `make_movies` and `make_graphs` scripts have the `bat` extension. By running these two scripts, the figures (`breakthrough.pdf` and `breakthrough_dimensionless.pdf`) and movies (files with `.mp4` extension and file names starting with `column_movie`) will be created:

```
breakthrough.pdf          column_movie_Pnorm.mp4
breakthrough_dimensionless.pdf  column_movie_Pt.mp4
column_movie_Dpdt.mp4    column_movie_Q.mp4
column_movie_Dqdt.mp4    column_movie_Qeq.mp4
column_movie_P.mp4       column_movie_V.mp4
```

You could also run the individual make-movie scripts if you are interested only in some of them. The figures are in pdf files, the movies are in h265 format for mac/linux and h264 on windows, with resolution 1200x800 by default. On mac/linux, command line options can be specified to modify the defaults

```
./make_movies -e 5 -w 1600 -h 1200 -q 18 -l
```

The `-e` option stands for 'every' and allows a periodic sampling only using every 5 data -points in the example case. The `-w` and `-h` changes the width and height of the movie, while `-q` determines the quality of the movies. The quality range is 0–51, where 0 is lossless and 51 is worst quality possible. The default in RUPTURA is 18 which is visually nearly lossless. The `-l` option stands for legacy and changes the movie-format h265 to the older h264. On windows, these options can be specified in the windows console as

```
make_movies 5 1600 1200 18
```

Note the fixed order of the options, and the format on windows is h264 as h265 is not supported out-of-the-box under windows.

```
plot_column_P
plot_column_Pnorm
plot_column_Pt
plot_column_Q
plot_column_Qeq
plot_column_V
plot_breakthrough
```

The output figures are shown in [Figure 23\(a\)](#). The breakthrough graph plots the normalised concentration at the exit of the column as a function of time. Two versions of the plots are available: (1) as a function of time in seconds, (2) as a function of dimensionless time. [Figure 23\(b\)](#) shows a single frame of the movie, here the loading of the components adsorbed in the crystallites along the column.

8.3. Mixture prediction of C₆-isomers in BEA-type zeolite

For the C₆-isomers in BEA-type zeolite example, we can test how well the explicit Langmuir models mixture adsorption in comparison with IAST. The directory `tutorial/BEA-C6/mixture_prediction` contains the input file `simulation.input`:

```

SimulationType           MixturePrediction
ColumnName               BEA
Temperature              552.0           // [ K]
PressureStart            1e3             // lowest pressure
PressureEnd              1e7             // highest pressure
NumberOfPressurePoints   100          // number of points equally spaced
PressureScale            log              // [ log, or linear]
MixturePredictionMethod  ExplicitLangmuir // [ IAST, SIAST, or ExplicitLangmuir]

Component 0 MoleculeName      Helium
              GasPhaseMolFraction  0.96           // [ -]
              CarrierGas           yes
Component 1 MoleculeName      nC6
              GasPhaseMolFraction  0.01           // [ -]
              NumberOfIsothermSites 1
              Langmuir              1.393 3.307e-05 // [ mol/(kg framework)] [ 1/Pa]
Component 2 MoleculeName      C5m3
              GasPhaseMolFraction  0.01           // [ -]
              NumberOfIsothermSites 1
              Langmuir              1.559 1.809e-05 // [ mol/(kg framework)] [ 1/Pa]
Component 3 MoleculeName      C4m2m2
              GasPhaseMolFraction  0.01           // [ -]
              NumberOfIsothermSites 1
              Langmuir              1.714 5.451e-06 // [ mol/(kg framework)] [ 1/Pa]
Component 4 MoleculeName      C4m2m3
              GasPhaseMolFraction  0.01           // [ -]
              NumberOfIsothermSites 1
              Langmuir              1.678 1.522e-05 // [ mol/(kg framework)] [ 1/Pa]

```

Note the input is very similar in structure. The major difference is that the simulation-type is set to MixturePrediction. Using the option MixturePredictionMethod we can control the specific method used in the mixture prediction. Minor difference are that the mass-trans-

fer and axial dispersion coefficients are not needed. To compute the mixture isotherm some info on the pressure range, i.e. begin and end-pressure and the number of pressure points is required. These points can be spread equi-distant in normal or in log-scale.

```

component_0_Helium.data      component_4_C4m2m3.data  plot_mixture_mol_fractions
component_1_nC6.data        plot_mixture             plot_pure_components
component_2_C5m3.data       component_3_C4m2m2.data  make_graphs

```

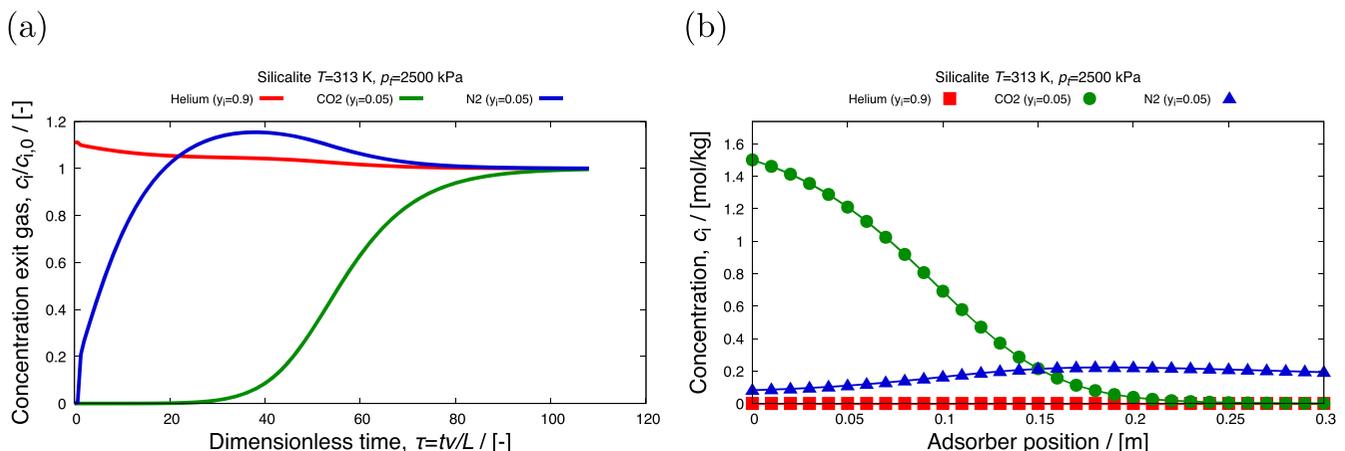


Figure 23. (Colour online) Breakthrough predictions of an equimolar mixture of CO₂-N₂ in silicalite at 313 K and 2.5 · 10⁶ Pa: (a) breakthrough curve plot (file `breakthrough_dimensionless.pdf`) (b) movie frame of the loading inside the column (file `column_movie_Q.mp4`).

After running, the output directory contains the following plot-files.

Files with `.data` extension and file names starting with component consists of equilibrium loading data for the specified temperature, and the range of pressure. In windows, the script `make_graphs` has the `bat` extension. After running that script we obtain the plots in pdf format

```
mixture_prediction.pdf
mixture_prediction_mol_fractions.pdf
pure_component_isotherms.pdf
mixture_prediction.pdf file consists of the plots
of mixture adsorption isotherms for all the components pre-
```

plots in the form of mole fractions. `pure_component_isotherms.pdf` shows the plots for the isotherms for the pure components. In Figure 24, we can compare the pure components isotherms with the mixture isotherm predictions. In the mixture, we can see the effect of competitive adsorption.

8.4. Isotherm fitting

To obtain the isotherm model parameters we can use the fitting module. The directory `tutorial/MAF-X8-xylenes` contains the input file `simulation.input`:

```
SimulationType      Fitting
DisplayName         MAF-X8
ColumnPressure     3
ColumnLoading      8
PressureScale      log

Component 0 MoleculeName      p-xylene
              FileName         Results.dat-MAF-x8-P1-Repeat-433K-p-xylene
              NumberOfIsothermSites 2
              Langmuir-Freundlich 0.0 0.0 0.0
              Langmuir-Freundlich 0.0 0.0 0.0
```

The result of the fit is printed at the end of the output.

```
number of isotherm sites: 2
Langmuir-Freundlich isotherm
  q_sat: 1.71616          // [ mol / (kg framework) ]
  b:      3.54859e+09    // [ 1 / Pa ]
  nu:     1.47094       // [ - ]
Langmuir-Freundlich isotherm
  q_sat: 1.63797          // [ mol / (kg framework) ]
  b:      12.3201        // [ 1 / Pa ]
  nu:     0.515807      // [ - ]
```

sent in the mixture in the same unit specified for saturation loadings (q_{sat}) in the input file. `mixture_prediction_mol_fractions.pdf` file consists of the same

File names starting with `Results.dat` consists of the equilibrium loading data computed using grand-canonical Monte Carlo simulations.

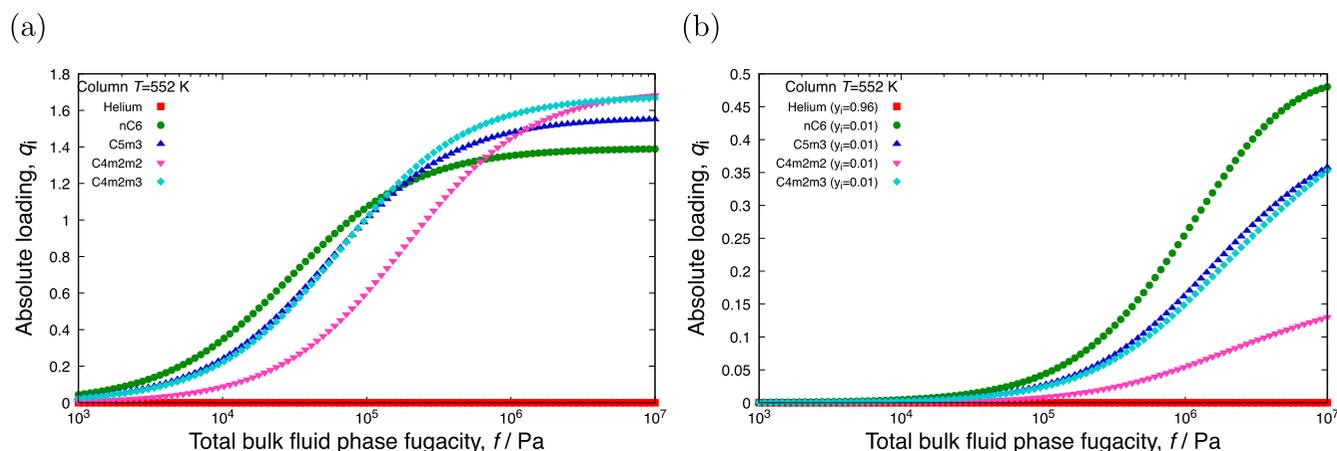


Figure 24. (Colour online) Mixture predictions of a C_6 isomer mixture in BEA-type zeolite at 552K using explicit isotherm model developed by Van Assche et al [30]: (a) pure components (file `pure_component_isotherms.pdf`), (b) mixture prediction (file `mixture_prediction.pdf`).

```

Results.dat-MAF-x8-P1-Repeat-433K-benzene
Results.dat-MAF-x8-P1-Repeat-433K-ethylbenzene
Results.dat-MAF-x8-P1-Repeat-433K-m-xylene
Results.dat-MAF-x8-P1-Repeat-433K-o-xylene
Results.dat-MAF-x8-P1-Repeat-433K-p-xylene
Results.dat-MAF-x8-P1-Repeat-433K-toluene
make_graphs
plot_fit_component_0_p-xylene

```

Again, using the `make_graphs` script, we can create the pdfs of the figures, e.g.

```
isotherms_fit_p-xylene.pdf
```

The result is plotted in Figure 25. It shows the initial random starting isotherm, and the final fit result after GA optimisation for adsorption of p-xylene in MAF-X8- type zeolite at 433 K.

8.5. Examples

RUPTURA comes with many examples included. These examples have three parts: (1) fitting the pure component isotherm data with different isotherm models to obtain isotherm parameters (e.g. equilibrium constant (b), saturation loading, etc), (2) prediction of mixture isotherms with the fitted

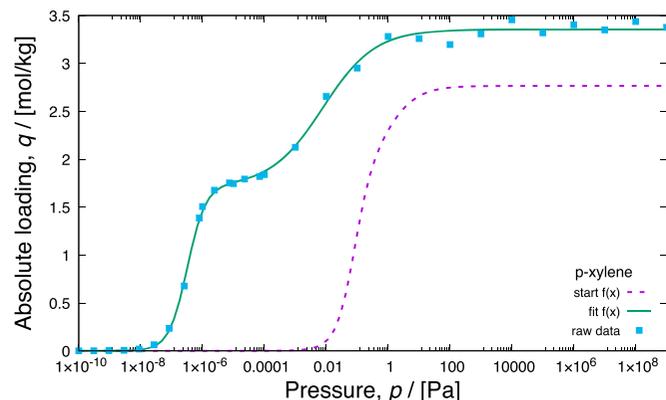


Figure 25. (Colour online) Fitting a dual site Langmuir isotherm model to the pure component isotherm data for the adsorption of p-xylene in MAF-X8- type zeolite at 433 K. The pure component adsorbed loadings are computed using grand-canonical Monte Carlo simulations. The fitting is performed using genetic algorithm optimisation which is shown in the file `isotherms_fit_p - xylene.pdf`.

parameters as input, (3) breakthrough curve simulations with the fitted parameters as input. The examples range from a simple binary mixture up to a 15-component C_5 - C_6 - C_7 alkane mixture. The xylene-examples have been selecting for displaying qualitatively different adsorption behaviour.

The examples are listed in Table 14 along with typical run times for breakthrough simulations, here on a mac-studio using an M1-chip. Most examples run in a few minutes. However, keep in mind that run-times depend on the total pressure. Increasing the pressure shifts the breakthrough to shorter dimensionless times, decreasing the pressure shifts the breakthrough to longer dimensionless times. Also, for lower pressure or stiff systems, a smaller time-step might be in order. This could significantly increase the computational time needed for the breakthrough computation. Other factors that influence the run times are the details of the isotherm models and isotherm shapes.

9. RUPTURA troubleshooting

9.1. The curve fitting does not visually match well to the isotherm data

Run the fitting several times to make sure the solution is stable. If the problem remains, then it is the isotherm model and/or the number of isotherm sites. Increase the number of sites if inflections are not represented well.

9.2. Breakthrough error: pressure gradient is too large (negative outlet pressure)

The given pressure and pressure gradient result in negative pressure further down the column. This is nonphysical and indicates that the pressure gradient is chosen too high, and/or the pressure is too low.

Table 14. List of mixture prediction, breakthrough, and fitting examples provided with RUPTURA.

structure	mixture	N_c	N_{grid}	Δt [s]	p_i [kPa]	$\tau = tv/L$ [-]	time	p_i [kPa]	$\tau = tv/L$ [-]	time
MOR	CO_2 - C_3H_8	2	100	0.0005	125.0	270.8	1m36	1250.0	53.2	0m25
JUC-77	xylenes	4	100	0.0005	25.0	201.8	4m02	250.0	43.5	0m58
MIL-125-NH2	xylenes	4	100	0.0005	25.0	355.5	7m34	250.0	77.2	2m07
CoBDP	xylenes	4	100	0.0005	25.0	395.3	8m08	250.0	68.5	1m50
MFI	xylenes	4	100	0.0005	25.0	1025.2	10m13	250.0	162.5	2m08
MIL-47	xylenes	4	100	0.0005	25.0	504.5	11m18	250.0	95.0	2m37
MAF-X8	xylenes	4	100	0.0005	25.0	643.2	13m28	250.0	99.0	2m37
CoBDP	alkanes- C_6	5	100	0.0005	20.0	489.3	13m33	200.0	86.2	2m51
BEA	alkanes- C_7	5	100	0.0005	1.2	873.24	17m10	12.0	331.7	6m57
fe2bdp3	alkanes- C_6	5	100	0.0005	20.0	3520.0	105m58	200.0	376.7	12m41
ZIF-77	alkanes- C_5 - C_6 - C_7	15	100	0.0005	20.0	269.3	28m03	200.0	52.8	5m44

Notes: For breakthrough simulations, in addition to the N_c -components, there is a carrier-gas component present. The timings are done on a mac-studio using an M1-chip.

9.3. Instability or erratic breakthrough curves

The time step might be too high, reduce the time step and check for improvement. Check the values of mass transfer and axial dispersion coefficients for physical validity. Check whether using the reference IAS method using bisection (IASTMethod Bisection) makes a difference. Try this first in a mixture prediction calculation, since this is fast. If you find a difference, then there is a numerical instability in the implemented FastIAS method.

9.4. Breakthrough curves with sharp transitions or spikes

Use more grid points in the spatial discretisation of the column.

9.5. The breakthrough curve depends on the time-step and number of grid points

The breakthrough curves are correct in the limit of a very small time-step and a large number of grid points. Generally, you will have to choose the time-step and number of grid points such that a further decrease in time-step or increase in number of grid points will not (visually) change the breakthrough curves anymore. Note that always using a very small time-step and a large amount of grid points is computationally expensive.

9.6. No convergence or hangs

Use recommended units, like mol/kg for loading, and Pascal for pressure. Other units could lead to very small or very large numbers.

10. Conclusions

We presented the RUPTURA code (<https://github.com/iraspa/ruptura>), which is a freely available, open-source package for the computation of breakthrough curves, mixture adsorption, and fitting of isotherm models to raw adsorption data. RUPTURA contains three modules of workflow encountered in this field: (1) the computation of step/pulse breakthrough, (2) the prediction of mixture adsorption (used in the breakthrough equations) based on pure component isotherms, and (3) the fitting of isotherm models on raw (computed or measured) isotherm data. We included isotherm models like Langmuir, BET, Henry, Freundlich, Sips, Langmuir-Freundlich, Redlich-Peterson, Toth, Unilan, O'Brian & Myers, Asymptotic Temkin, and Bingel & Walton including their multi-site versions or combinations of that. The mixture prediction methods implemented include Ideal Adsorption Solution Theory (IAST), segregated IAST, and explicit Langmuir methods. IAST is computed fast and at machine precision. The breakthrough simulations include axial dispersion and the Linear Driving Force (LDF) model for mass-transfer, and have excellent numerical stability through the use of Strong-Stability Preserving Runge-Kutta (SSP-RK) integrators. RUPTURA is freely available (MIT license) and

should be viewed as a demonstration 'code' that could be useful for researchers working in the field and for teaching in chemistry and chemical engineering classes. For future versions of RUPTURA, we envision to include support for non-ideal gas behaviour, liquid phase conditions, and chemical reactions. Non-isothermal operation is an important aspect that needs to be considered. Variation in temperature along the column can be significant for certain cases such as adsorption of CO₂. Therefore, in the next version of RUPTURA, we plan to include non-isothermal operation. Also, the code will be modified for simulating adsorption columns with more than one type of adsorbent. This will be useful in separating multiple components inside the column.

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