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**DOI**

[10.3390/s19153337](https://doi.org/10.3390/s19153337)

**Publication date**

2019

**Document Version**

Final published version

**Published in**

Sensors (Switzerland)

**Citation (APA)**

Hong, H., Sun, J., Wu, C., & Liu, Z. (2019). High performance mixed potential type  $\text{No}_2$  gas sensor based on porous YSZ layer formed with graphite doping. *Sensors (Switzerland)*, 19(15), 1-14. Article 3337. <https://doi.org/10.3390/s19153337>

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## Article

# High Performance Mixed Potential Type NO<sub>2</sub> Gas Sensor Based on Porous YSZ Layer Formed with Graphite Doping

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Received: 28 June 2019; Accepted: 26 July 2019; Published: 30 July 2019



**Abstract:** High performance mixed potential type NO<sub>2</sub> sensors using porous yttria-stabilized zirconia (YSZ) layers doped with different concentration graphite as solid electrolyte and LaFeO<sub>3</sub> as sensing electrode were fabricated and characterized. LaFeO<sub>3</sub> was prepared by a typical citrate sol–gel method and characterized using XRD. The surface morphology and porosity of porous YSZ layers were characterized by field emission scanning electron microscope (FESEM). The sensor doped with 3 wt% graphite shows the highest response (−76.4 mV to 80 ppm NO<sub>2</sub>) and the response is linearly dependent on the logarithm of NO<sub>2</sub> concentration in the range of 10–200 ppm. The sensor measurement results also present good repeatability and cross-sensitivity.

**Keywords:** mixed potential; NO<sub>2</sub>; porous YSZ layers; graphite

## 1. Introduction

With the accelerated development of automobiles and industry, gas emission has caused serious environmental disasters and human diseases. Among the emitted gas, nitrogen dioxide (NO<sub>2</sub>) is the most dangerous [1–3]. In order to detect and monitor the NO<sub>2</sub> precisely, high-performance NO<sub>2</sub> sensors are in high demand [4–6].

Since Fleming first observed non-Nernst behavior in 1977, the mixed potential theory has been proposed consequently [7]. Mixed potential type gas sensors consist of a high-temperature stable electrolyte, a porous sensitive electrode (SE), and a reference electrode (RE). It could be used to detect various target gases if the sensitive material used properly [8]. Currently, the most suited electrolyte for those sensors is yttria-stabilized zirconia (YSZ) due to its excellent chemical and thermal stability at high temperatures. Comparing to the metal oxide semiconductor, catalytic combustion and surface acoustic wave (SAW) gas sensors, the mixed type potential sensor has many advantages including better mechanical properties, chemical stability and thermal stability at high temperatures [9], which make mixed potential sensor work well in the harsh environment such as the automobile exhaust gas after-treatment system [8,10–13]. Recently, to further improve the performance of the mixed potential sensor effectively, many groups have turned their attention to finding more sensitive materials including single metal oxides, composite perovskite and spinel-type oxides, and also made some good results [14,15]. Researchers used In<sub>2</sub>O<sub>3</sub> as SE had reached a NO<sub>2</sub> response of 126 mV to 100 ppm at 700 °C [16]. Liu et al. reported a mixed potential sensor based on Pt/YSZ/CoTa<sub>2</sub>O<sub>6</sub> displays segmentally linear relationship to the logarithm of NO<sub>2</sub> concentration in the ranges of 0.5–5 ppm and 5–500 ppm, with sensitivities of 12 and 80 mV/decade at 650 °C, respectively [17]. These sensors exhibit high

response and good sensitivity to  $\text{NO}_2$ . It demonstrates the used materials' good catalytic properties to  $\text{NO}_2$ . However, the operating temperature of the proposed sensor is above  $600\text{ }^\circ\text{C}$ , which may not match the low-temperature region of an exhaust pipe. However, according to the mixed potential type sensing mechanism, the performance of the mixed potential sensor is not only related to the catalytic ability of the sensitive material, but also the structure of the triple-phase boundary (TPB) and a larger TPB means more active sites for the electrochemical reaction. In recent years, research works are focused on increasing the TPB by constructing YSZ substrates such as hydrofluoric acid corrosion, sand blasting, laser fabrication and ion beam etching, and mixing YSZ with sensitive material to obtain the larger TPB [18–22]. Due to these proposed technologies, the TPB increases effectively. However, some of those methods like mixing YSZ with sensitive material, which causes the covering of the electrochemical reaction sites and resulting in a low response. Other methods such as using high-cost ion beam etching need complex processes and make the experiment difficult to be repeated. Moreover, most of the mixed potential sensors usually work at  $300\text{--}800\text{ }^\circ\text{C}$ , while it is also desirable for a high-performance sensor with low operating temperatures such as the vehicle exhaust pipe ( $200\text{--}300\text{ }^\circ\text{C}$ ). Those sensors may not work properly or result in low performance at this temperature. A  $\text{NO}_2$  sensor located downstream of the exhaust pipe should operate at a similar temperature as the exhaust gases ( $200\text{--}300\text{ }^\circ\text{C}$ ). Otherwise, an additional heating unit may be necessary and it would take more power assumption and cost.

In this work, we report a high performance mixed potential type  $\text{NO}_2$  sensor using the porous YSZ layer. The porous YSZ layer was prepared by adding graphite to YSZ paste, and screen-printing to the initial YSZ substrate. To the best of our knowledge, there are no reports about this low-cost and facile method. Due to the larger TPB and uniform porous layer, the fabricated sensor response to  $\text{NO}_2$  improves. The presented mixed potential  $\text{NO}_2$  sensor doped with 3 wt% graphite exhibits the highest performance and response to 80 ppm  $\text{NO}_2$  is  $-76.4\text{ mV}$ . Moreover, the sensor also exhibits excellent repeatability during continuous five cycles' measurement and good cross-sensitivity compared with acetone, CO and  $\text{CH}_4$ . Additionally, the fabricated sensor optimum operating temperature is  $250\text{ }^\circ\text{C}$ . Comparing to existing publications [16–18], the working temperature of the presented sensor is lower than most of the publications. This high performance mixed potential type  $\text{NO}_2$  sensor could be installed on an exhaust pipe without extra heating units and could monitor the  $\text{NO}_2$  emission in the low-temperature region. In the following session, the experiment on sensor material preparation, device fabrication and the detailed investigation of the properties of the fabricated sensor are presented.

## 2. Experiment

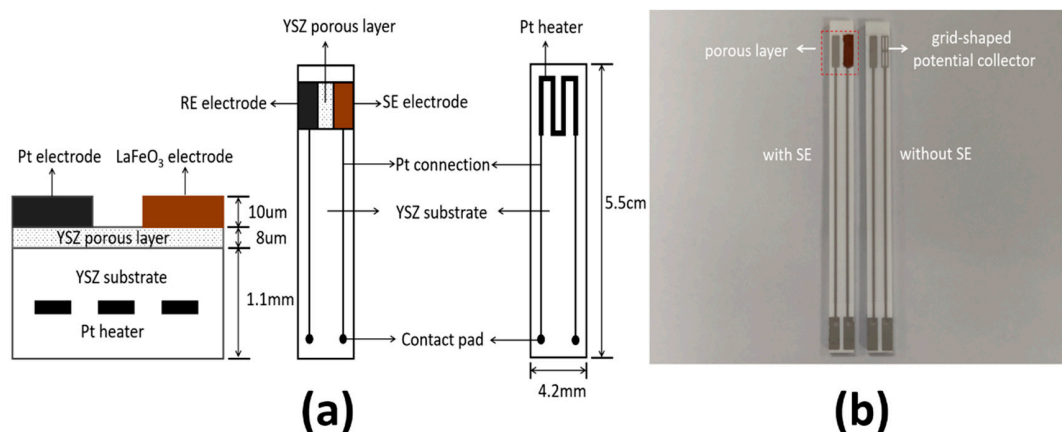
### 2.1. Material

The  $\text{LaFeO}_3$  powder was prepared by a typical citrate sol–gel method, and all the raw materials were of analytic grade. At first, appropriate  $\text{La}(\text{NO}_3)_3 \cdot 6\text{H}_2\text{O}$ ,  $\text{Fe}(\text{NO}_3)_3 \cdot 9\text{H}_2\text{O}$ , citric acid and ethylene glycol were dissolved in deionized water with molar ratios of 1:1:2:6. Then the solution was stirred for 4 h at  $80\text{ }^\circ\text{C}$  to obtain the sol precursor. The sol precursor was dried for 24 h at  $120\text{ }^\circ\text{C}$  and then we got a gel precursor, after that the gel precursor was pre-calcined at  $400\text{ }^\circ\text{C}$  to gain  $\text{LaFeO}_3$  precursor powder. Finally, the precursor was ground with an agate mortar and then calcined for 2 h at  $700\text{ }^\circ\text{C}$  to acquire the  $\text{LaFeO}_3$  powder.

Porous YSZ paste was fabricated by a simple stirring method. At first, different concentration graphite (0 wt%, 3 wt%, 10 wt%, 15 wt%) was added to the YSZ powder (8 mol  $\text{Y}_2\text{O}_3$ -doped). Then the mixture was dissolved in the colloid adhesive, which was prepared by mixing  $\alpha$ -terpineol, cellulose dispersant, leveling agent and defoamer. In the next step the vibration tumbling machine was used to stir the obtained precursor paste to acquire the porous YSZ paste. Finally, porous YSZ paste was deposited on the initial YSZ substrate by the screen-printing method, after calcination the porous YSZ layer was formed.

## 2.2. Fabrication of the Sensor

As shown in Figure 1, the mixed potential planar sensor with the configuration of  $\text{LaFeO}_3/\text{YSZ}/\text{Pt}$  was fabricated by the screen-printing method. Firstly, the Pt heater was printed in the initial YSZ substrate ( $5.5 \text{ cm} \times 4.2 \text{ mm} \times 1.1 \text{ mm}$ ), after calcination, the porous YSZ paste was printed on the initial YSZ substrate mentioned before and then calcination. Graphite was oxidized to  $\text{CO}_2$  at  $750^\circ\text{C}$  in this process. After that a stripe-shaped and a grid-shaped Pt electrode ( $5 \text{ mm} \times 1 \text{ mm}$ ) were performed on the two sides of the porous YSZ layer using commercial Pt paste (Pt-JC, electroplating engineers of Japan, Ltd., Hiratsuka, Japan) as the RE and potential collector. At the same time the Pt connection was also printed on the substrate. After calcination, the SE paste was obtained by mixing  $\text{LaFeO}_3$  powder with the appropriate colloid adhesive. Then the obtained paste was deposited on the grid-shaped Pt electrode. The distance between the two electrodes was 1 mm. Finally, the sensor was sintered again at the temperature of  $1200^\circ\text{C}$  to get a dense structure. The fabricated sensors using the porous YSZ layers with different concentration graphite (0 wt%, 3 wt%, 10 wt%, 15 wt%) were labeled as Sensor A, Sensor B, Sensor C and Sensor D.



**Figure 1.** (a) Schematic structure and (b) the top view of the sensor.

## 2.3. Measurement of the Sensor

X-ray (Rigaku SmartLab., Tokyo, Japan) diffraction with  $\text{Cu-K}\alpha$  radiation was used for analyzing the crystalline structure of the  $\text{LaFeO}_3$  powder. The surface morphology and porosity of the porous YSZ layers were characterized by field emission scanning electron microscope (FESEM; FEI Company, Brno, Czech Republic). The gas sensing performance of the sensor was measured by a conventional static method. The gas sensing experiment was carried out in a clean room with humidity of 56% and environment temperature of  $26^\circ\text{C}$ , with an oxygen concentration of 20.8% in a standard atmosphere. The heating voltage was provided by a DC power supply (6 V- $250^\circ\text{C}$ , 7 V- $300^\circ\text{C}$ , 8 V- $350^\circ\text{C}$ , 9 V- $400^\circ\text{C}$  and 10 V- $450^\circ\text{C}$ ) and an infrared thermometer was used to monitor the surface of the device in real time. The potential response was measured by a digital multimeter (Keithley 2400). The sample gas with 10–200 ppm  $\text{NO}_2$  was prepared by diluting 2000 ppm  $\text{NO}_2$  standard gas by air. The gases for cross-sensitivity measurement including CO,  $\text{CH}_4$  were prepared by diluting 4000 ppm CO,  $\text{CH}_4$  standard gas by air and acetone was diluting with volume ratio. According to the mixed potential theory, other carrier gases were unnecessary. The detailed gas sensing measurement was as follows. At first, the sensor was placed in an airtight chamber with a volume of 500 mL. Next the gas in the chamber was pumped out and then fresh air was pumped in. Before injecting the target gas into the chamber, using DC power to supply voltage when the sensor's temperature was stable. Then turning off the pump and a certain amount of gas was injected into the chamber via the different sizes of needles (5 mL, 10 mL and 50 mL) in a few seconds. After 400 s, when the response magnitude was almost unchanged, turning on the pump for another 400 s, the rest of the gas was pumped out and the pure air filled the chamber. That was one cycle measurement.



### 3. Result and Discussion

Figure 2 shows the X-ray diffraction (XRD) pattern of the  $\text{LaFeO}_3$  powder prepared by a typical citrate sol–gel method, the result demonstrated that all diffraction peaks of the  $\text{LaFeO}_3$  powder were in correspondence with the standard  $\text{LaFeO}_3$  patterns of JCPDS card No.37-1493, No other diffraction peaks of the sensitive material were observed, which indicates the high purity of the  $\text{LaFeO}_3$ . The surface morphology and porosity of sensors were characterized by FESEM. Figure 3 are the SEM images of porous YSZ layer fabricated with 0 wt%, 3 wt%, 10 wt% and 15 wt% graphite. It could be clearly seen that few cavities were found on the YSZ layer without any graphite (Figure 3a). However, there was a large number of holes on the surface when the graphite doping in. With the increase of the graphite concentration, more holes could be found on the porous layer and the size of holes was becoming larger in Figure 3b–d, averagely  $2.2\ \mu\text{m}$ , as shown in Figure 3d.

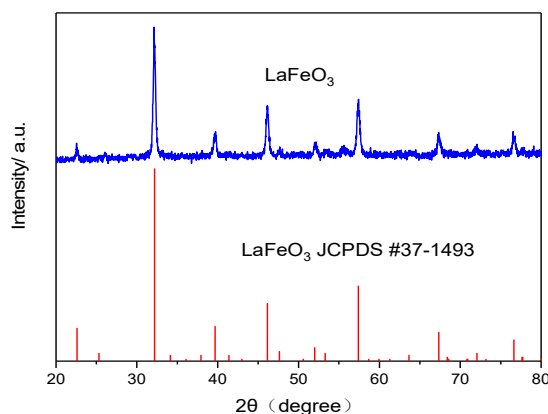


Figure 2. XRD patterns of  $\text{LaFeO}_3$  sensing electrode material.

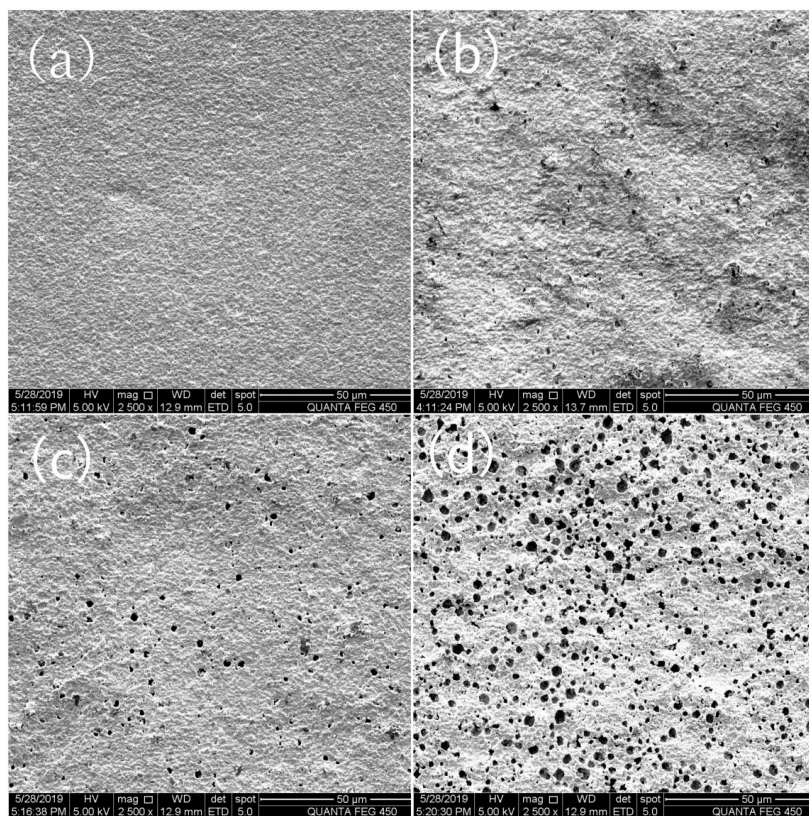
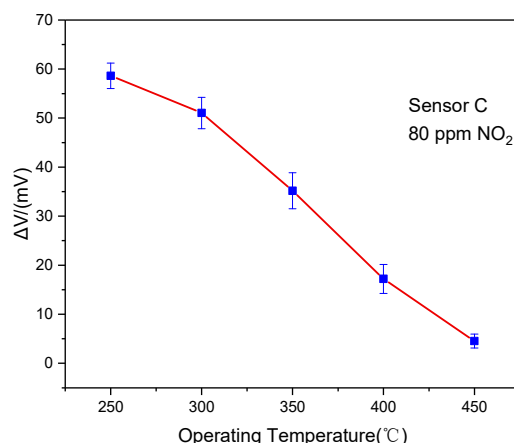


Figure 3. Field emission scanning electron microscope (FESEM) graph of the fabricated yttria-stabilized zirconia (YSZ) porous layer with different doping (a) 0 wt%, (b) 3 wt%, (c) 10 wt% and (d) 15 wt%.

It is known that the performance of the mixed potential sensor relies on the operating temperature. In order to investigate the optimum operating temperature, the response of Sensor C was measured in the temperature at the range of 250–450 °C. As demonstrated in Figure 4, it was apparent that the response decreased with the increasing operating temperature. It was found the maximum response to 80 ppm NO<sub>2</sub> was −58.6 mV at 250 °C. The reason for this phenomenon might be explained as follows. The definite activation energy was a necessary condition for the electrochemical reaction in TPB. However, the desorption process of NO<sub>2</sub> became dominant at above 250 °C, and the amount of NO<sub>2</sub> adsorbed on LaFeO<sub>3</sub> was less along with the increasing temperature. Hence, the response of the sensor to NO<sub>2</sub> decreased with further increasing temperature [19,23–25].



**Figure 4.** Response changes of the sensor to 80 ppm NO<sub>2</sub> at a different operating temperature.

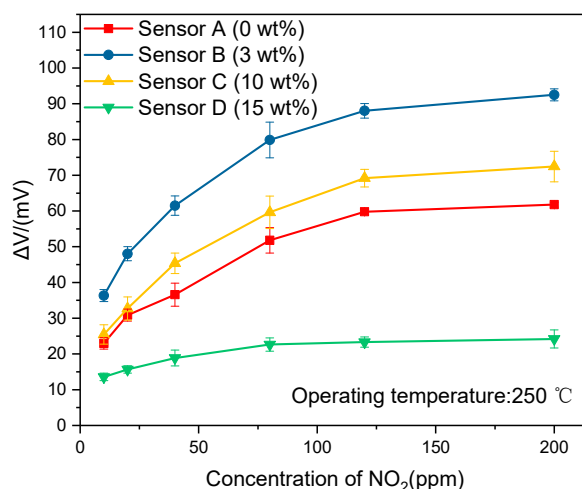
Table 1 shows a comparison of the mixed potential type NO<sub>2</sub> sensor's operating temperature with different materials and configurations. The operating temperature of the presented sensor was the lowest. Due to catalytic properties of the LaFeO<sub>3</sub>, comparing with other sensitive materials including single and spinel oxides, the sensor with LaFeO<sub>3</sub>/YSZ/Pt exhibited a lower operating temperature. On account of the uniform porous YSZ layer, the fabricated sensor with LaFeO<sub>3</sub>/YSZ/Pt worked at a lower temperature than the sensors with the same sensitive material and configuration. It indicated a low power assumption of the presented sensor.

**Table 1.** Comparison of the mixed potential NO<sub>2</sub> type sensors operating temperature.

Sensor Structure	Conc (ppm)	Response (mV)	Temp (°C)	Ref.
NiO/YSZ/Pt	100	106	850	[18]
Nb <sub>2</sub> O <sub>5</sub> /YSZ/Pt	400	35	800	[26]
In <sub>2</sub> O <sub>3</sub> /YSZ/Pt	100	126	700	[16]
CoTaO <sub>6</sub> /YSZ/Pt	100	93	650	[17]
LaFeO <sub>3</sub> /YSZ/Pt	60	45	550	[27]
LaFeO <sub>3</sub> /YSZ/Pt	100	9	550	[28]
Bi <sub>2</sub> W <sub>2</sub> O <sub>9</sub> /YSZ/Pt	100	20	500	[29]
La <sub>0.65</sub> Sr <sub>0.35</sub> MnO <sub>3</sub> /YSZ/Pt	100	48	500	[30]
LaFeO <sub>3</sub> /YSZ/Pt	100	60	450	[31]
SmFeO <sub>3</sub> /YSZ/Pt	90	130	400	[32]
LaFeO <sub>3</sub> /YSZ/Pt	100	164	300	[33]
LaFeO <sub>3</sub> /YSZ/Pt	100	81	250	This work

Figure 5 shows the response of the sensors doped with different concentration graphite, which means the different sizes and density of holes on the porous layer exposure to 10–200 ppm of the test gas. It was found that the Sensor B doped with 3% graphite exhibited the highest value and the response to 80 ppm NO<sub>2</sub> was −76.4 mV. It proved the function of the YSZ porous layer, which increased

the contact area between SE and YSZ substrate effectively. That could be understood there were more active sites for the electrochemical reaction and then the output potential of sensor increased. However, overfull graphite made the YSZ porous layer lower adhesion. Hence the YSZ porous layer could not combine both with SE and RE well, which caused an increase in interface resistance, and resulted in the lower response. The result also means the existing of an optimizing doping concentration. In order to investigate the detailed relationship between  $\text{NO}_2$  concentration and the response, transient response and recovery characteristics of Sensor C to different concentration of  $\text{NO}_2$  were researched.



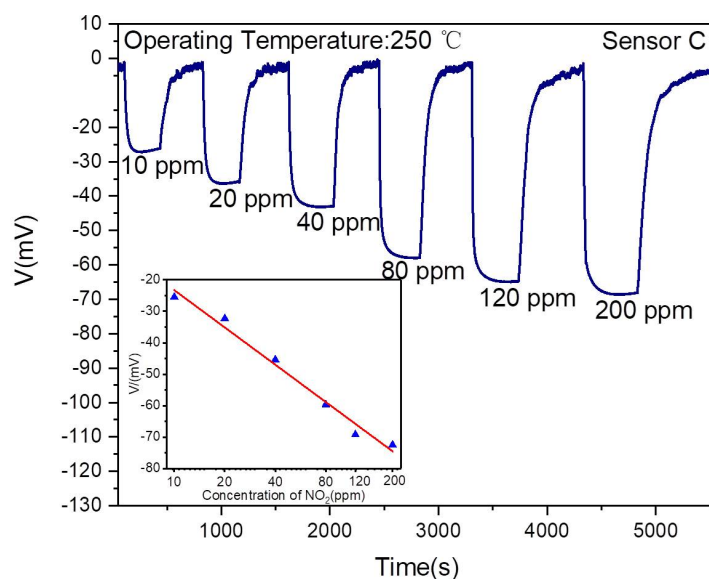
**Figure 5.** Response of the sensors doped with 0 wt%, 3 wt%, 10 wt% and 15 wt% to 10–200 ppm  $\text{NO}_2$  at 250 °C.

As illustrated in Figure 6. It was found that the response increased with the  $\text{NO}_2$  concentration increasing. It could be understood that the response of the fabricated sensor was determined by the number of  $\text{NO}_2$  molecules in TPB. When the  $\text{NO}_2$  concentration increases, there would be more  $\text{NO}_2$  arriving at TPB to participate in the electrochemical catalytic reaction and resulting in a higher response. From this figure, the response was linearly dependent on the logarithm of  $\text{NO}_2$  concentration in the range of 10–200 ppm, which was following the sensing mechanism according to the mixed potential theory. It could also be explained by Equation (1), which clearly shows the response of the sensor linearly varies with the  $\text{NO}_2$  concentration [34].

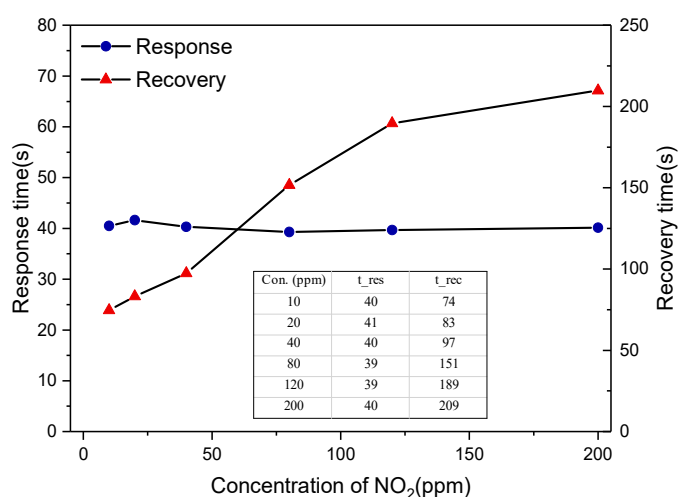
$$V = A - B \ln C_{\text{NO}_2}, \quad (1)$$

where  $V$  is the response,  $A$  and  $B$  are constants and  $C_{\text{NO}_2}$  is the concentration of  $\text{NO}_2$ . The increase of the sensor response to 80–200 ppm  $\text{NO}_2$  is lower than that of 10–80 ppm, which could also be demonstrated in Figure 5. It can be speculated that when the number of adsorbed molecules increases, desorption of the molecules also enhances. Finally, the rates of the two processes were equal and the electrochemical reactions of the fabricated sensors reached saturation slowly, which is similar to the phenomena described in Langmuir's theory [35]. The response and recovery time were studied in the next part.

Deriving from the experiment evidence based on Figure 6, Figure 7 gives an insight into the response and recovery time. It exhibits that the response time was basically stable at 40 s and recovery time increased with the increasing of  $\text{NO}_2$  concentration, and the recovery time to 200 ppm  $\text{NO}_2$  was 209 s. It could be explained that it would take more time for the process of desorption because of the increasing  $\text{NO}_2$  concentration, lower temperature. Another reason was the slow pumping speed in the experiment, while that in the automobile exhaust pipe was very fast. The presented sensor could be a potential candidate for practical automobile exhaust application.



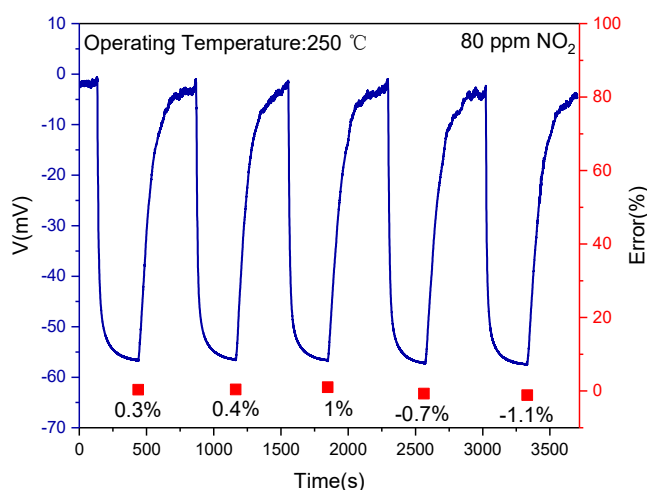
**Figure 6.** Transient response and recovery characteristics of Sensor C to different concentrations of  $\text{NO}_2$  at  $250\text{ }^\circ\text{C}$ .



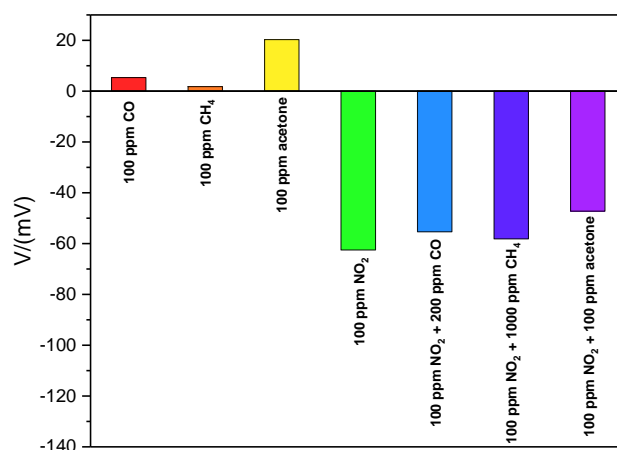
**Figure 7.** Response and recovery time of Sensor C to different concentrations of  $\text{NO}_2$ .

To study the error in the response of the fabricated sensor, Figure 8 shows the continuous five cycles' measurement of Sensor C to 80 ppm  $\text{NO}_2$  gas at  $250\text{ }^\circ\text{C}$ . The error of response is denoted by  $(V - V_0)/V_0 \times 100\%$ , where  $V$  and  $V_0$  represent the sensor response and the average of the five responses, respectively. It is seen that the response and recovery characteristics of the presented sensor held good consistency during the continuous five cycles' measurement and the maximum error of the response to 80 ppm  $\text{NO}_2$  was  $-1.1\%$ , which demonstrated good repeatability of the sensor. Cross-sensitivity for Sensor C to 100 ppm of various gases including  $\text{CH}_4$ ,  $\text{CO}$ , and acetone was tested. As illustrated in Figure 9, the sensor response to 100 ppm  $\text{NO}_2$  exhibited the highest value compared with other single interfering gas. It was also clearly seen that a slight change in response was observed to the mixture gases of  $\text{NO}_2$ ,  $\text{CO}$  and  $\text{CH}_4$ , which were mixed in different concentration ratios. However, compared with  $\text{CO}$  and  $\text{CH}_4$ , the sensor response was affected much by the acetone. Actually, as reported in other literature [36,37],  $\text{LaFeO}_3$  was also sensitive to acetone. However, the concentration of acetone in automobile exhaust was lower than  $\text{NO}_2$ . The result proved that the presented sensor had good cross-sensitivity to  $\text{NO}_2$ .



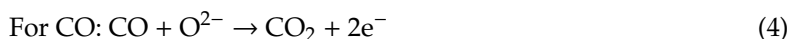
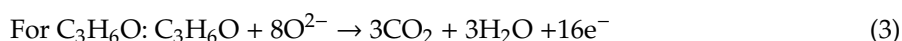
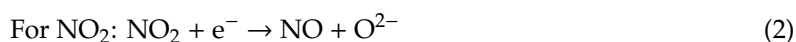


**Figure 8.** Continuous five times response–recovery transient characteristics of Sensor C to 80 ppm NO<sub>2</sub> at 250 °C.



**Figure 9.** Cross-sensitivity measurement for Sensor C to 100 ppm various gases at 250 °C.

As the gas sensing mechanism, it could be explained by the mixed potential theory. When the mixed potential sensor Pt/YSZ/LaFeO<sub>3</sub> exposes to target gases, the electrochemical reactions can occur simultaneously in the TPB. It can be described by the following reactions:



The exchange of ionic ( $\text{O}^{2-}$ ) and electronic ( $\text{e}^-$ ) could form the electrochemical potentials at the two electrodes of the sensor. The dissimilar catalytic activities, disparate gas adsorption and different electrochemical reactions in the YSZ/LaFeO<sub>3</sub> and the YSZ/Pt interfaces caused different potentials between SE and RE. The electric potential difference between SE and RE was the response  $V$ . The potential magnitude of the sensor depended on the catalytic properties between reducing/oxidizing gases and adsorbed gases at the two interfaces. From the equations, it can be easily understood the response to NO<sub>2</sub> was opposite to that of other interfering gases.

#### 4. Conclusions

In this article, the mixed potential NO<sub>2</sub> sensors based on the porous YSZ layers doped with different concentration graphite were fabricated. The sensor using the porous YSZ layer fabricated by 3 wt% graphite exhibited the highest response (−76.4 mV to 80 ppm NO<sub>2</sub>) at a low operating temperature (250 °C). The sensor also showed good sensitivity to 10–200 ppm NO<sub>2</sub> and also exhibited superior repeatability and cross-sensitivity. It could be believed this method had a promising prospect because of low-cost, simple process, high sensor response and low power assumption of sensor, which is very attractive for NO<sub>2</sub> sensing in automobile and industry applications.

**Author Contributions:** In this article, the original draft, experiments, analysis were done by H.H. with measurements and inspiration from J.S. The review and editing were done by C.W. and Z.L.

**Funding:** This research was funded by the National Key R&D Program of China (Grant No.2018YFB2002800) and the Institute of Microelectronics, Tsinghua university.

**Conflicts of Interest:** The authors declare no conflict of interest.

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