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# Advanced NO<sub>2</sub> Gas Sensor Fabrication through UV Laser-Induced Selective Reduction Laser Sintering

Shaogang Wang <sup>†‡</sup>, Qihang Zong<sup>‡</sup>, Huiru Yang<sup>‡</sup>, Qianming Huang<sup>‡</sup>, Huaiyu Ye<sup>†‡</sup>, Paddy French<sup>†\*</sup>

<sup>†</sup>Email: s.wang-10@tudelft.nl yehy@sustech.edu.cn p.j.french@tudelft.nl <sup>†</sup>The Faculty of EEMCS, Delft University of Technology, Delft, Netherlands

<sup>‡</sup>The School of Microelectronic, Southern University of Science and Technology, Shenzhen, China

*Abstract*—This study introduces an innovative approach for fabricating flexible nitrogen dioxide (NO<sub>2</sub>) gas sensors based on In2O3 nanoparticles (NPs) using selective reduction laser sintering (SRLS) technology. The SRLS technology enables specific chemical reduction reactions during the sintering process, achieving fabrication and control of oxygen vacancy defects and the porous structure in the In<sub>2</sub>O<sub>3</sub> sintering region. The sensor exhibits exceptionally high sensitivity, fast response/recovery times, and superior selectivity for NO<sub>2</sub> gas detection, particularly at room temperature. Compared with traditional NO<sub>2</sub> gas sensor fabrication methods, this technology not only provides a potential way to fabricate highperformance NO<sub>2</sub> gas sensors but also further expands the application potential of laser direct writing (LDW) technology in the fields of advanced materials and sensor fabrication.

# Keywords—Flexible gas sensor, NO<sub>2</sub> detection, Indium oxide nanoparticles, Selective reduction laser sintering.

#### I. INTRODUCTION

The rapid progress of wearable technology has extensively promoted the innovation of advanced flexible sensors, enabling them to become an essential tool for personal health monitoring, assessment, and intervention [1]. Nitrogen dioxide (NO<sub>2</sub>), a byproduct of fossil fuel combustion, is critical to monitoring the environment and public health. NO<sub>2</sub> gas is not only destructive in terms of acid rain, photochemical smog, and thinning of the ozone layer but may also pose a threat to human health when its concentration exceeds 3 ppm [2]. Therefore, it is vital to develop sensors that can quickly detect NO2. Indium oxide (In<sub>2</sub>O<sub>3</sub>) based sensors have attracted attention for their excellent sensitivity and fast response, and performance enhancement has been achieved through innovative approaches such as heterostructures, doping technology, and metal catalysis [3]. However, the limitations of these sensors in terms of selectivity, operating temperature, and humidity sensitivity remain challenges that need to be addressed [4]. Laser direct writing (LDW) technology, particularly selective laser sintering (SLS), offers a new solution to these challenges through its ability to process materials and devices with precision and customization.

In this study, we report a novel flexible gas sensor fabricated using selective reduction laser sintering (SRLS) technology, designed to detect NO<sub>2</sub> at room temperature. This technology achieves the selective reduction of PVP-coated In<sub>2</sub>O<sub>3</sub> nanoparticles (NPs) by controlling the critical parameters of UV pulse laser, thereby achieving precise modification of materials and rapid fabrication of devices. Due to the synergistic effect of oxygen vacancy defects and porous structure in the sintering region, the sensor exhibits high sensitivity (442.24), fast response/recovery times (30/570 s), and superior selectivity to NO<sub>2</sub> gas at room temperature.

#### II. RESULTS AND DISCUSSION

#### A. Mechanism of Selective Reduction Laser Sintering

Unlike traditional selective laser sintering (SLS), which directly irradiates laser light onto the material surface to achieve high-temperature solid phase conversion, selective reduction laser sintering (SRLS) achieves material sintering by finely regulating the temperature distribution along the edge of the laser scanning path. The flexible NO2 gas sensor fabrication using this technology contains four primary steps, as shown in Fig. 1(a). First, the In<sub>2</sub>O<sub>3</sub> NPs paste was uniformly coated on the PET (Polyethylene terephthalate) substrate using a combination of four-sided scraper and doctor blade method. Next, after the solvent was evaporated entirely at room temperature, the In2O3 layer was finely linearly laser-sintered using a computer-controlled ultraviolet (UV) laser system. Subsequently, the PET substrate was carefully cleaned with deionized water to remove the remaining unsintered In<sub>2</sub>O<sub>3</sub> NPs paste. Finally, the silver electrodes for the sensor were printed on the PET substrate using screen printing technology.



Fig. 1. (a) Schematic flow diagram of the flexible NO<sub>2</sub> gas sensor fabrication process. (b) Schematic diagrams of the overall and localized surface of In<sub>2</sub>O<sub>3</sub> nanoparticles (NPs) in the laser sintering and laser ablation regions after the sintering and printing processes. (c) Comparison images of flexible gas sensors in different deformation states.

In the SRLS process, In<sub>2</sub>O<sub>3</sub> NPs are not only the critical material of flexible gas sensors but also the primary coating that triggers photothermal effects. It is widely recognized that PET has a relatively low absorption coefficient for ultraviolet (UV) laser. Therefore, when the laser is irradiated vertically onto the PET film, most of the laser energy will pass through the PET without causing any apparent physical or chemical reaction to the PET [5]. However, when the PET surface is coated with In<sub>2</sub>O<sub>3</sub> NPs, the In<sub>2</sub>O<sub>3</sub> layer absorbs the UV laser energy and rapidly converts it into thermal energy.

This photothermal conversion action produces a significant photothermal effect on the PET surface, which is essential for achieving a precise sintering process. Under UV laser irradiation, the high laser energy density causes slight ablation of the PET substrate underneath the In2O3 layer. At the same time, the high-temperature gradient generated by this laser ablation region promotes the thermal sintering of In<sub>2</sub>O<sub>3</sub> at the edges of the laser scanning path. As a result, the In2O3 NPs melt and aggregate, forming a unique laser sintering region. On the contrary, unsintered In<sub>2</sub>O<sub>3</sub> NPs can be easily removed by cleaning with deionized water, as shown in Fig. 1(b). It is worth noting that the benefit from the fast laser scanning speed (10 mm/s) and small laser radius (6.5  $\mu$ m), this technology significantly reduces the impact on the substrate compared to conventional hightemperature sintering and hot-press sintering processes. As a result, the SRLS technology can be easily realized even on 250  $\mu$ m PET films, enabling the fabrication of gas sensors with a variety of patterns. The fabricated flexible gas sensor can maintain stable mechanical properties under various deformation states, such as finger twisting and curling, as shown in Fig. 1(c).

### B. Characterization of Oxygen Vacancy Defects



Fig. 2. (a) Overall and (b) localized X-ray diffraction (XRD) patterns of  $In_2O_3$  NPs paste before and after the SRLS treatment at different scanning intervals. (c) Electron paramagnetic resonance (EPR) spectra of  $In_2O_3$  NPs paste before and after the SRLS treatment. (d) Scanning electron microscope (SEM) images of the sensing region of the sensor.

To investigate the effect of different laser scanning intervals on the crystal structure and phase transformation of In<sub>2</sub>O<sub>3</sub> NPs paste during the selective reduction laser sintering (SRLS) process, we characterized the untreated and 50  $\mu$ m, 70  $\mu$ m, and 90  $\mu$ m scanning intervals of the samples by using X-ray diffraction (XRD) and analyzed their XRD patterns, as shown in Fig. 2(a). The XRD pattern of the In<sub>2</sub>O<sub>3</sub> NPs untreated by the SRLS process predominantly indicates characteristic peaks of the In<sub>2</sub>O<sub>3</sub> phase located at 30.6°, 35.5°, 51.0°, and 60.7°, corresponding to the (222), (400), (440), and (622) crystal planes (PDF#06-0416). However, the In<sub>2</sub>O<sub>3</sub> NPs treated with the SRLS process at different scanning intervals, in addition to characterizing the peaks of In<sub>2</sub>O<sub>3</sub>, also exhibits XRD characteristic peaks of metallic indium, located at 32.9°, 36.3°, 39.2°, and 54.4°, respectively (PDF#70-2888). Comparing the overall intensity of the XRD peaks, it is evident that the transition from In<sub>2</sub>O<sub>3</sub> to metallic indium is relatively slight.

Further, especially in the diffraction angle range of  $30^{\circ}$  to  $40^{\circ}$ , the intensity of the metallic indium characteristic peaks near the (321) and (400) crystal planes of In<sub>2</sub>O<sub>3</sub> increases significantly as the laser scanning interval decreases, as shown in Fig. 2(b). Meanwhile, the XRD pattern reveals that as the average sintering temperature increases due to the reduction of the laser scanning interval, the XRD diffraction peak near the In<sub>2</sub>O<sub>3</sub> (321) crystal plane moves to a higher 20 diffraction angle [6, 7]. This transformation indicates a decrease in the lattice constant of In<sub>2</sub>O<sub>3</sub>, resulting in a more compact lattice structure. It also shows that the indium ions in In<sub>2</sub>O<sub>3</sub> are reduced to lower valence states or even reduced to metallic indium, and implies the formation of oxygen vacancy defects [8].

Additionally, the electron spin resonance (EPR) results further demonstrate the significant signal at a g value of 2.0 for In<sub>2</sub>O<sub>3</sub> nanoparticles after the SRLS treatment, as shown in Fig. 2(c). During the SRLS process, the reducing macromolecules generated by the decomposition of the main chain of PVP reduce In<sub>2</sub>O<sub>3</sub> to metallic indium while forming oxygen vacancy defects. These oxygen vacancy defects trap the electrons, resulting in the formation of a distinct signal in the EPR spectrum. This result further proves the existence of oxygen vacancy defects after the SRLS treatment [9].

Fig. 2(d) shows the scanning electron microscope (SEM) images of the sensing region of the flexible gas sensor. Interestingly, the ablation of the PET substrate during the SRLS process results in sputtering at the edges of the sintering region, leading to the formation of a porous structure. This not only enhances the adhesion between the In<sub>2</sub>O<sub>3</sub> NPs and the PET substrate in the sintering region but also increases the specific surface area of the sensing region to some extent. As a result, the In<sub>2</sub>O<sub>3</sub> NPs sensing material with oxygen vacancy defects is able to capture more target gases, which in turn improves the sensitivity of the sensor.

#### C. Performance of Flexible Gas Sensors



Fig. 3. (a) The response curves of the gas sensors based on  $In_2O_3$  NPs for 10 ppm NO<sub>2</sub> at different scanning intervals. (b) The response curves of the gas sensors based on  $In_2O_3$  NPs for 10 ppm NO<sub>2</sub> at different scanning intervals. (c) Dynamic response curve of the gas sensor to NO<sub>2</sub> from 2 to 10 ppm at room temperature. (d) Radar plot of gas sensor selectivity test for NO<sub>2</sub> relative to other interfering gases (C<sub>2</sub>H<sub>3</sub>OH, CO<sub>2</sub>, C<sub>3</sub>H<sub>6</sub>O, NH<sub>3</sub>, CH<sub>4</sub>, and H<sub>2</sub>S).

During the SRLS process, the difference in sintering temperature induced by the laser scanning interval is highly critical to the performance of N-type chemoresistive gas sensors based on In<sub>2</sub>O<sub>3</sub> NPs. To fully evaluate this effect, the sensor was exposed to a specific concentration of NO<sub>2</sub> gas at room temperature (25°C) for 30 seconds. The evaluation equation for the sensor sensitivity was defined as  $S=\Delta R/R_a=(R_g-R_a)/R_a$  with a bias voltage of 1.0 V, where  $R_a$ and  $R_g$  represent the stabilized resistance values of the sensor in air and in the target gas environment, respectively. Response time ( $\tau_{resp}$ ) and recovery time ( $\tau_{reco}$ ) were determined by the time required for the sensor resistance value to reach a 90% change after exposure to NO<sub>2</sub> and upon subsequent re-exposure to air, respectively [10].

Test results show a rapid increase in resistance when the sensor is placed in 10 ppm NO<sub>2</sub> gas, followed by a gradual fall back in the air environment, as shown in Fig. 3(a). It is noteworthy that the average sintering temperature of the In<sub>2</sub>O<sub>3</sub> NPs sensing region decreases as the laser scanning interval increases. Nevertheless, the sensor sensitivity to NO2 gas shows an increasing trend, reaching values of 18.27, 19.69, 442.24, 802.16, and 967.62, respectively. In fact, the stabilized resistance value (Ra) of the sensor in the air shows an increasing trend as the laser scanning interval increases. Although intuitively, an increase in R<sub>a</sub> would seem to decrease sensitivity (due to an increase in the denominator), sensor sensitivity actually shows an upward trend as the laser scan interval expands. This indicates that the creation of oxygen vacancy defects plays a decisive role in enhancing the sensitivity of the sensor. In other words, even though the increase in initial sensor resistance may not be favorable to the improvement of sensitivity, the increase in oxygen vacancy defects still plays a crucial role in improving the sensitivity of the device [11]. In detail, the increase in oxygen vacancy defects provides both more adsorption sites for target gas molecules and increases the number of free electrons in the conduction band. This further reduces the difficulty of electron capture by the target gas molecules. As a result, the resistance of the sensor increases significantly during operation, reflecting its sensitive response to the NO<sub>2</sub> gas.

However, the increase in the density of oxygen vacancy defects, while enhancing the adsorption of the NO<sub>2</sub> gas on the sensor surface, also affects the rapid recovery capability of the sensor. Furthermore, the increase in the laser scanning interval led to a decrease in the average sintering temperature, which in turn weakened the adhesion between the In<sub>2</sub>O<sub>3</sub> nanoparticles and the PET substrate. As a result, the quality of the sintered structure decreases, which poses a challenge to the stability and reliability of the sensor. In order to strike a balance between performance and stability, subsequent studies will focus on the selection of In<sub>2</sub>O<sub>3</sub> NPs based sensors with a scanning interval of 70  $\mu$ m for performance evaluation. The fast response and recovery times of this sensor for 10 ppm NO<sub>2</sub> at room temperature are 30 and 660 s, respectively, as shown in Fig. 3(b).

In addition, the response of the sensor increased from 9.8 to 460.9 when the NO<sub>2</sub> gas concentration increased from 2 ppm to 10 ppm, demonstrating its excellent dynamic response and recovery capability, as shown in Fig. 3(c). Significantly, the sensor responds much better to 10 ppm NO<sub>2</sub> than to 100 ppm concentrations of interfering gases, including  $C_2H_5OH$ ,  $CO_2$ ,  $C_3H_6O$ , NH<sub>3</sub>, CH<sub>4</sub>, and H<sub>2</sub>S, demonstrating its excellent selectivity, as shown in Fig.3 (d).

As a result, gas sensors fabricated using SRLS technology and based on  $In_2O_3$  NPs exhibit high sensitivity, fast response/recovery, and excellent selectivity. This method has obvious advantages over the conventional fabrication method of  $In_2O_3$ -based gas sensors.

#### D. Performance of Flexible Gas Sensors

The primary sensing mechanism of the  $NO_2$  gas sensor based on  $In_2O_3$  NPs fabricated using the SRLS technology at room temperature mainly relies on the conductivity changes triggered by the adsorption and desorption of gas molecules on the surface of the sensing region [12]. In particular, oxygen vacancy defects on the  $In_2O_3$  surface play a crucial role in this process. They promote the transition of electrons from the valence band to the conduction band, which significantly increases the concentration of free electrons in the conduction band, leading to a decrease in the sensor resistance.



Fig. 4. The schematic diagram of the NO<sub>2</sub> surface sensing mechanism of a flexible gas sensor based on  $In_2O_3$  NPs fabricated using the SRLS technology. (E<sub>c</sub>: conduction band; E<sub>F</sub>: fermi energy; E<sub>V</sub>: valence band).

In the air atmosphere, oxygen molecules  $(O_2)$  are adsorbed to the surface of  $In_2O_3$  NPs and capture free electrons from the conduction band of  $In_2O_3$  to from  $O_{2(ads)}^{-1}$  ions with higher chemical activity [13], as detailed in the reaction equations (1) and (2) [14]. Meanwhile, this process reduces the carrier concentration on the surface of the  $In_2O_3$ , causing the energy band to bend upward and forming a surface electron depletion layer, as shown in Fig. 4.

$$O_{2(gas)} \leftrightarrow O_{2(ads)}$$
 (1)

$$O_{2(ads)} + e^{-} \rightarrow O_{2(ads)}^{-}$$
<sup>(2)</sup>

When the sensor is exposed to the NO<sub>2</sub> gas environment, the NO<sub>2</sub> molecules directly interact with the electrons in the conduction band of the In<sub>2</sub>O<sub>3</sub> to form NO<sub>2</sub><sup>-</sup> ions due to their high electron affinity [13]. In addition, the NO<sub>2</sub> molecules can also interact directly with already existing O<sub>2(ads)</sub><sup>-</sup> ions to form NO<sub>3</sub><sup>-</sup> ions, as detailed in the reaction equations (3) and (4) [15]. Meanwhile, this process further increases the depth of the electron depletion layer on the surface of the In<sub>2</sub>O<sub>3</sub>, resulting in a further upward bending of the energy band and a significant increase in the resistance of the material.

$$NO_{2(ads)} + e^{-} \rightarrow NO_{2(ads)}^{-}$$
 (3)

$$O_{2(ads)} + 2NO_{2(ads)} \rightarrow 2NO_{3(ads)}$$
(4)

Both of these effects lead to a reduction in the conduction band electrons of  $In_2O_3$  NPs, which in turn increases the thickness of the electron depletion layer and the potential barrier. However, due to the strong oxidizing nature of NO<sub>2</sub>, it dominates at room temperature, significantly increasing the sensor resistance. The subsequent desorption process works in reverse and further reduces the resistance of the sensor. Therefore, the excellent performance of the NO<sub>2</sub> gas sensor based on  $In_2O_3$  NPs fabricated by SRLS technology at room temperature is mainly attributed to the synergistic effect of oxygen vacancy defects and surface porous structure.

#### **III.** CONCLUSION

In summary, we have successfully demonstrated a new method of fabricating flexible gas sensors using selective reduction laser sintering (SRLS) technology to detect nitrogen dioxide (NO2) at room temperature. The SRLS technology utilizes a UV-pulsed laser that enables the selective reduction of PVP-coated In2O3 NPs on a PET substrate, resulting in the fabrication of oxygen vacancy defects and porous structures in the sensing region. The sensors designed by this technology exhibit excellent performance, such as high sensitivity (442.24), fast response/recovery time (30/570 s), and high selectivity for NO2. This technology provides a new solution to the challenges of In2O3-based gas sensors in terms of selectivity and operating temperature and expands the potential of laser direct writing (LDW) technology for advanced materials and sensor fabrication applications.

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