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Combining Photonic Crystal and Metasurface Architectures for Advanced Lightsails**

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Broadband, High-Reflectivity Dielectric Mirrors at Wafer Scale: Combining Photonic Crystal and Metasurface Architectures for Advanced Lightsails

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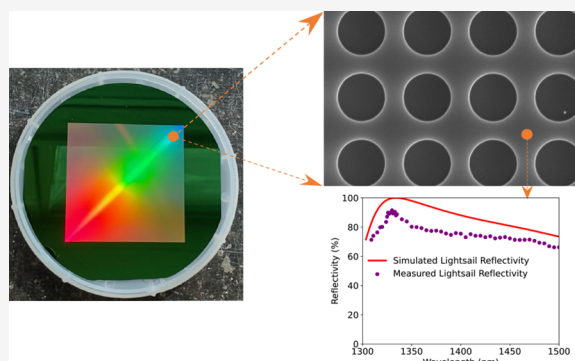
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Supporting Information

ABSTRACT: Highly ambitious initiatives aspire to propel a miniature spacecraft to a neighboring star within a human generation, leveraging the radiation pressure of lasers for propulsion. One major challenge for this enormous feat is to build a meter-scale, ultralow mass lightsail with broadband reflectivity. In this work, we present the design and fabrication of a lightsail composed of two distinct dielectric layers with photonic crystal/metasurface structure covering a 4" wafer. We achieved broadband reflection of >70% spanning over the full Doppler-shifted laser wavelength range during spacecraft acceleration with a low total mass in the range of a few grams when scaled up to meter size. Furthermore, we find new paths to reliably fabricate these subwavelength structures over macroscopic areas and then systematically characterize their optical performance, confirming their suitability for future lightsail applications. Our innovative device and precise nanofabrication approaches represent a significant leap toward interstellar exploration.

KEYWORDS: *Lightsail, Photonic Crystal, Metasurface, Dielectric Mirrors, Broadband Reflection, Interstellar Exploration.*



In the quest for interstellar exploration, the dream of propelling spacecraft to neighboring star systems has remained captivating for decades.^{1–4} Within this ambitious pursuit, the Starshot Breakthrough Initiative has emerged as a leading forum to bring together scientists and engineers from many distinct fields and is driven by the goal of sending a spacecraft to Proxima Centauri, our nearest stellar neighbor, within the span of a human lifetime.⁵ At the heart of this mission lies the core concept—a laser-driven lightsail. Once achieved, such lightsail technology would also enable many other ground-breaking space exploration missions, such as exploring our own solar system within days rather than months or years, as well as harnessing the extraordinary imaging capabilities of the Solar Gravitational Lens (SGL).^{6,7} Here, a lightsail is indispensable due to the SGL's optimal focal point being located over 548 astronomical units (AU) away from Earth. This vast distance necessitates a lightsail for delivering a camera to the SGL's focal point and precise positioning, enabling the capture of high-resolution images of exoplanets at 30 parsecs with a 10-km-scale surface resolution—unattainable with conventional spacecraft propulsion methods.⁸ The fundamental challenge confronting this endeavor requires the development of a lightweight spacecraft, which can be propelled by laser beams to extraordinary velocities, up to 20% the speed of light.^{9,10} Unlike conventional propulsion systems,¹¹ laser-driven lightsails rely on the radiation pressure

force to achieve the immense speeds and acceleration required for interstellar space travel, which require the lightsail device to feature a large area, low mass, and broadband reflection. Several other crucial material requirements for designing a practical lightsail were thoroughly explored in previous work,¹² showing that the lightsail must have extreme optical, mechanical, and thermal properties to meet the constraints on mass and sail shape.

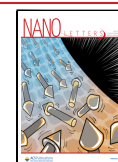
Previous works have simulated possible solutions with the practical constraints of making a lightsail. For example, it was demonstrated that by using inverse design and large-scale optimization, a lightweight broadband reflector for relativistic lightsail propulsion based on stacked photonic crystal slabs shows a potential improvement in acceleration distance performance.¹³ Similarly, it was also shown that optimized multilayer structures can enable ultralight spacecraft to sustain high acceleration while striking a balance between efficiency and weight.¹⁴ The choice of materials for these layers is crucial,

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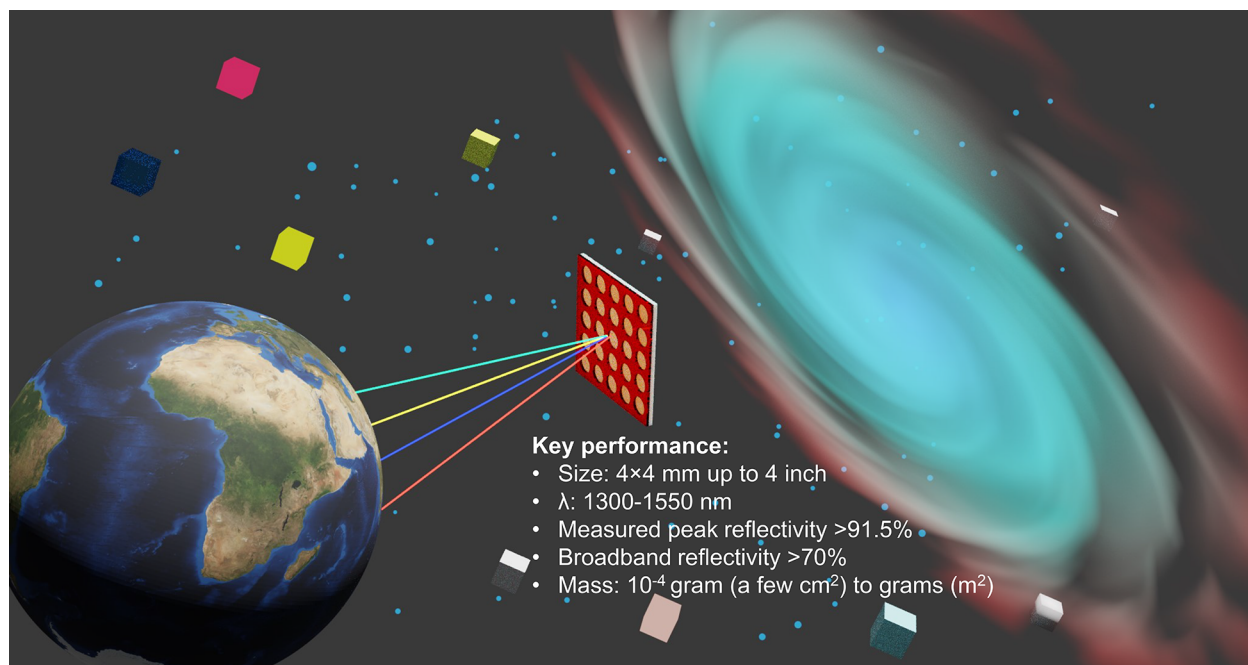


Figure 1. Illustration of the lightsail concept and the main performance parameters of the device realized in this work, including size, working wavelengths, reflection performance, and mass. The source image used to create the planet is adapted with permission from ref. 19. Copyright 2024, NASA.

ensuring high reflectance in the Doppler-shifted laser wavelength range. Although different works have carefully analyzed the design,¹⁵ stability,^{16,17} and acceleration properties of a lightsail,¹⁸ no experimental realization of such a lightsail has been demonstrated to date, to the best of our knowledge.

One of the key challenges for a feasible lightsail design lies in constructing a broad-band reflector capable of covering the Doppler-shifted laser wavelength spectrum during the spacecraft's high-velocity acceleration phase. Earlier efforts to develop such a broadband reflector involved an InP 2D photonic crystal and Fano resonator.^{20,21} However, these attempts were constrained to very small areas without complete substrate release. Moreover, in the later work, the added SiO₂ layer inevitably filled in the holes of the photonic crystal layer, resulting in a degraded reflection performance. For a more detailed discussion, we refer to.²² In this work, we approach the material and design challenges associated with laser-driven lightsails, by pioneering a bilayer membrane structure using a silicon nitride photonic crystal atop a flat silicon layer, drawing inspiration from the high reflectivity exhibited by conventional photonic crystal devices^{23,24} and the enhanced functionality and tunability offered by metasurface devices.^{25,26} Our novel approach encompasses the incorporation of a high refractive index layer beneath the photonic crystal membrane, resulting in a significant expansion of the reflectance spectrum. The bilayer configuration accomplishes broadband reflectivity (exceeding 70%) spanning from 1300 to nearly 1550 nm, whereas a conventional single-layer photonic crystal only allows a reflectivity within the range of a few tens of nanometers. Furthermore, we establish a complete fabrication flow using silicon nitride on silicon-on-insulator (SOI) wafers, with new nanofabrication protocols that will allow scaling these structures from 4" wafers to the square-meter sizes required for future interstellar exploration. The artistic depiction of the lightsail and its key performance characteristics are illustrated in Figure 1.

In the following section, we would like to elaborate on the detailed design and simulation results of four different types of lightsail architectures and highlight the exceptional performance of our bilayer membrane-based lightsails and their important role in advancing the frontiers of interstellar exploration. To design and simulate the reflection properties exhibited by distinct dielectric structures, we employ the electromagnetic field simulation software (CST Studio Suite). The refractive indices of our specific silicon (Si) and high-stress silicon nitride (SiN) films were first determined through ellipsometry measurements, with $n_{\text{Si}} = 3.4$ and $n_{\text{SiN}} = 2.0$.

We first calculate the properties of a canonical single-layer photonic crystal periodic structure,^{27,28} visually represented in Figure 2a. Within this configuration, SiN serves as the dielectric material, with photonic crystal parameters $p_1 = 1200$ nm for the lattice constant, a thickness $h_1 = 200$ nm, and a hole radius $r_1 = 500$ nm. Using the finite-difference time-domain (FDTD) method, we conduct simulations with the electromagnetic waves incident along the z-direction, and electric field polarization along the x-direction, while imposing periodic boundary conditions. The simulation results, shown in Figure 2e as the blue curve, reveal that the reflectivity exceeds 99% at its peak wavelength. As expected for this type of photonic crystal, we observe its reflectivity to exceed 70% between 1330 and 1380 nm, corresponding to a bandwidth of 50 nm.

Due to their resonant character, photonic crystals are however inherently limited in their reflection bandwidth.²⁸ To boost the reflection bandwidth and through inspiration by recent metasurface devices,²⁶ we introduce a silicon optical impedance matching layer beneath the SiN. As a first step, we simulate how this affects the broadband reflection characteristics with both layers as simple continuous dielectric films (as shown in Figure 2b). The fabrication of such a structure is much simpler than a photonic crystal design and already allows us to see that the reflectivity exceeds 70% within the

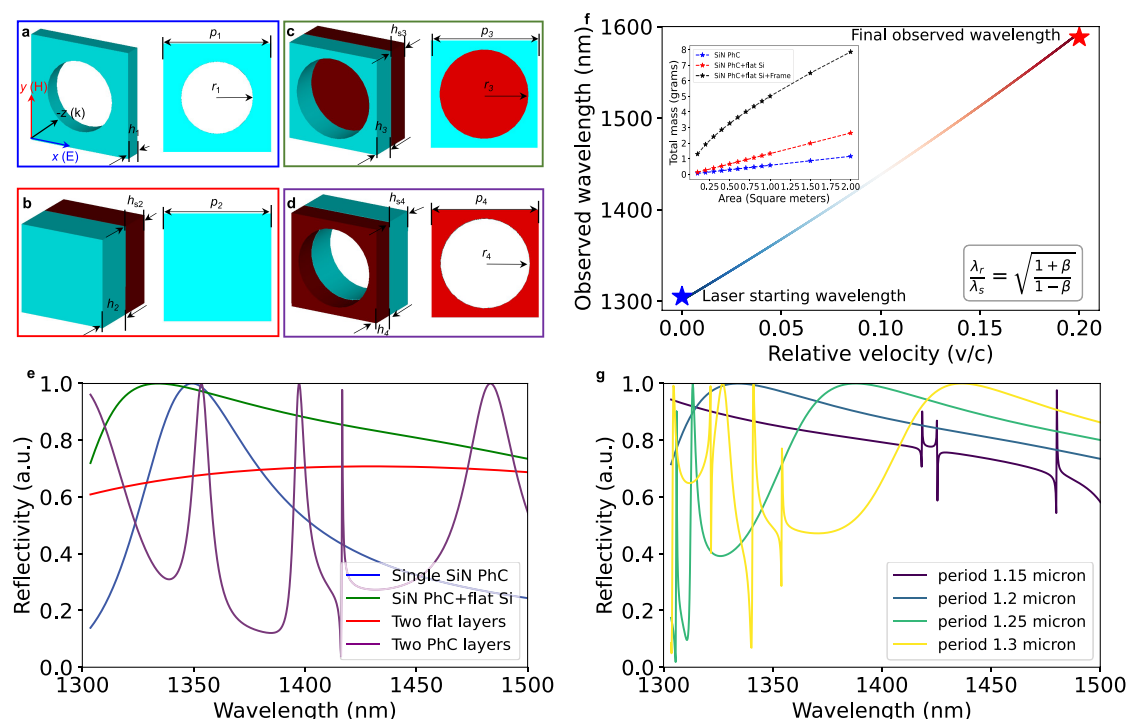


Figure 2. Simulated optical performance of different lightsail structures, and the Doppler effect for a fast-moving spacecraft. Panels (a)–(d) depict the side/top view of the single SiN photonic crystal, SiN/Si double flat layer membrane, SiN PhC/Si bilayer membrane, and SiN/Si double PhC structure, respectively. In panel (e) we compare each design's reflectivity and (f) the Doppler effect of a moving lightsail from low speed up to 20% of the speed of light. The figure inserted in the top-left illustrates the size-weight relationship of the single-layer PhC device, MPhC device, and MPhC device with silicon frame for enhanced structure intensity. Panel (g) shows a parameter sweep of the photonic crystal period values from 1.15 to 1.3 μm in the SiN PhC/Si bilayer membrane architecture to show how such design's reflectivity peak position can be flexibly engineered through modifications of the PhC layer parameter.

wavelength range of 1385 to 1475 nm using the same lattice constant (red curve in Figure 2e). While the overall peak reflectivity is much lower compared to the one-layer PhC and the overall mass is greater, this approach points to a significant increase in the reflection bandwidth.

By combining the photonic crystal layer with a second high-refractive-index material underneath, we can now create a novel structure as illustrated in Figure 2c, which we call a *meta-photonic crystal* (MPhC). The matching layer beneath the SiN, fabricated from silicon (depicted in red), is described by its thickness $h_3 = 321$ nm, given by the specific SOI wafer we chose for this work. The new photonic crystal layer is now described by parameters $p_3 = 1200$ nm, $h_3 = 400$ nm, and $r_3 = 500$ nm. Using the same methodology, we simulate the MPhC's reflectivity, which surpasses 70% for the entire 1300 to 1500 nm wavelength interval, with a peak reflectivity greater than 99% (green curve in Figure 2e). This remarkable enhancement of the reflection bandwidth to around 200 nm, nearly quadrupling the bandwidth compared to the original structure while still maintaining an overall high reflectivity, holds significant promise for applications with broadband reflection requirements.

Finally, for completeness, we also study the design where a photonic crystal is fully etched through both layers, as shown in Figure 2d. The resulting reflectivity is plotted as the purple curves in Figure 2e. This design exhibits multiple resonance peaks in the 1300–1500 nm range, and we thus do not pursue it further as a design in our fabrication process.

The new design of the meta-photonic crystal allows us to realize a broad-band reflector that seamlessly covers the entire

wavelength range of a Doppler-shifted laser during the acceleration phase of the lightsail, while still maintaining its very low mass. The top-left figure in Figure 2f illustrates the size-weight relationship of different devices: single-layer PhC device (blue), MPhC device (red), and MPhC device with a Si frame (black). The frame, anticipated to be made of Si with a thickness of 200 μm and a width of 2 mm on each edge of the MPhC, is designed to endure high intensities. It is evident that even with the Si frame, the total weight of a 2-square-meter MPhC device remains below 8 g, meeting the weight constraints for lightsails. Besides, for detailed materials' property, for example, optical absorption and mechanical deformation, we refer to refs. 12 and 29. To provide specific context, a laser with an initial wavelength of 1300 nm used to accelerate the lightsail to approximately 20% the speed of light will experience a substantial shift, transitioning from 1300 nm to approximately 1550 nm, as depicted in Figure 2f. The Doppler shift is calculated using the relativistic Doppler effect formula³⁰ (see formula in Figure 2f), where λ_r is the lightsail's observed wavelength during acceleration, λ_s is the laser wavelength on Earth, and $\beta = v/c$ is the speed of the lightsail normalized to the speed of light. It is worth mentioning that the MPhC lightsail's peak reflection position can be easily tuned by changing the photonic crystal layer's parameters, such as its periodicity. As shown in Figure 2g, the reflectivity peak changes from below 1300 nm to about 1420 nm by increasing the lattice constant from 1.15 to 1.3 μm . This offers high flexibility for designing a lightsail or other optical elements with adjustable optical responses, for example, meta-lenses,³¹ on-chip integrated photonics devices,³² or free space optics.³³

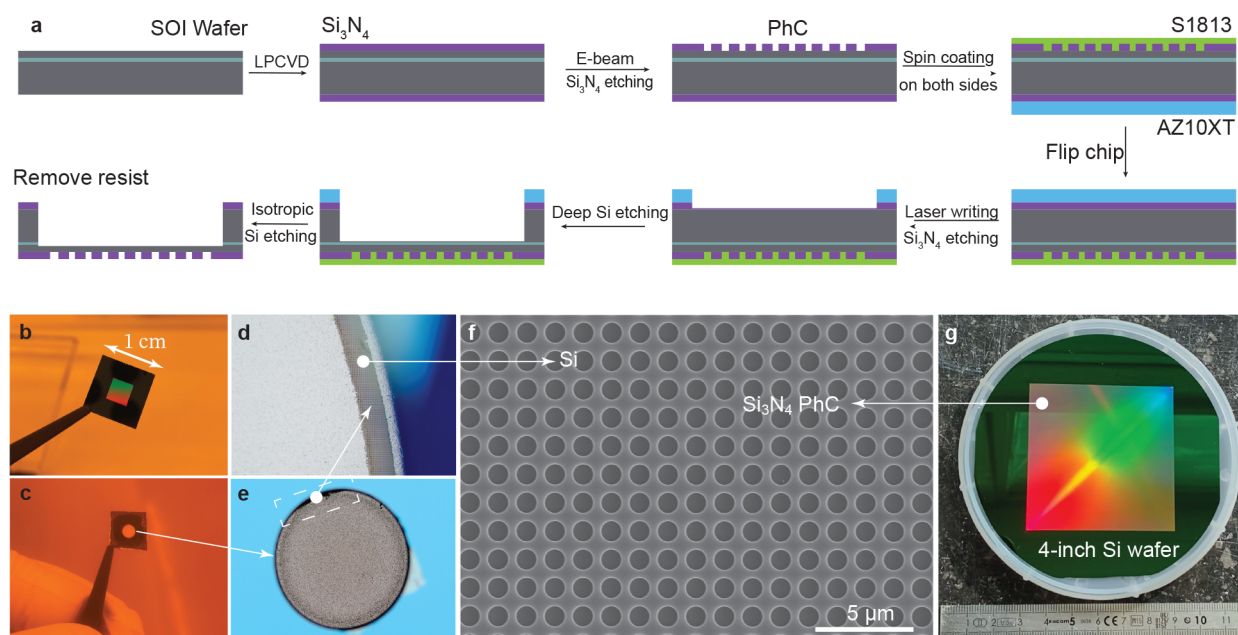


Figure 3. Fabrication flowchart of the lightsail starting from an SOI wafer and sample images at different fabrication steps. Panel (a) illustrates the detailed meta-photonic crystal fabrication process, panels (b)–(e) show the optical images of the lightsail during the fabrication flow. (f) Scanning electron microscopy (SEM) image of the lightsail device and (g) 4-in. size photonic crystal.

Fabrication of small-scale photonic crystals is well established, and we use a similar approach as previous work.²⁸ For a meta-photonic crystal device, as depicted in Figure 3a, the fabrication starts with a commercial SOI wafer with 321 nm thick silicon on a 394 nm thick buried oxide (BOX) layer, and a silicon handle wafer at the bottom, which is around 500 μm . A 400 nm high-stress stoichiometric silicon nitride (Si_3N_4) film is then deposited on both sides of the SOI wafer by low-pressure chemical vapor deposition (LPCVD) as described in ref. 34. The thickness of the silicon nitride layer and the silicon layer beneath are confirmed by ellipsometry measurements. After the LPCVD process, the 4-in. wafer is diced into 1×1 cm chips. We pick individual chips and spin-coat their front side (MPHC side) with a positive e-beam resists AR-P 6200 series (CSAR 62) followed by electron beam lithography using the Raith EBPG 5200 with a 100 kV acceleration voltage. After development (pentyl acetate for 1 min plus isopropyl alcohol for 1 min) and silicon nitride plasma etching using CHF_3/O_2 mixed gases,³⁴ the photonic crystal pattern, as simulated in the previous design and simulation section, is transferred to the silicon nitride layer. Then photoresist S1813 from Microresist is spin-coated on the chip front surface as a protection layer, and photoresist AZ10XT from MicroChemicals is spin-coated on the backside of the chip for next-step processing. The backside of the chip with the AZ10XT resist is then exposed in a Heidelberg Instruments Laserwriter (μMLA) and developed to make a circular opening with a diameter of about 3 mm. Here, we use a circular-shaped opening, as it leads to a higher survival rate of the final bilayer membrane by reducing the stress concentration at the edge.²⁸ The same plasma etch with CHF_3/O_2 mix gases is then used to first remove the 400 nm silicon nitride at the backside of the chip, and then a deep reactive ion silicon etching (Bosch process) is used to remove the 500 μm silicon handle layer. More details on this Bosch process are available in previous work.³⁵ When the silicon etching is finished, which can be confirmed by optical microscope

observation from the color contrast between the silicon and silicon dioxide (cf. Figure 3d, where the SiO_2 is lighter in color than the Si), isotropic silicon etching with SF_6 gas is finally used to remove the BOX layer. Then the chip is carefully removed from the silicon carrier wafer and cleaned in hot acetone and isopropyl alcohol, leaving a clean silicon nitride/silicon bilayer membrane device, as shown in Figure 3b. Significantly, the 400 nm high-stress silicon nitride and 321 nm silicon bilayer membrane exhibit notable mechanical resilience, resulting in a pronounced membrane survival rate during the whole fabrication process and upon final detachment from the silicon carrier wafer. Furthermore, the utilization of a thick and soft thermal compound adhesive between the chip and the silicon carrier wafer throughout the etching process, along with the prior application of spin-coated S1813 resist, ensures a high device yield.

To provide more details, we show a typical optical image of a 1×1 cm chip with 4×4 mm photonic crystal area (rainbow color) in Figure 3b. Similarly, Figure 3c shows the backside of the chip with a circular opening, which leads to higher device yield (exceeding 75%) compared to rectangular openings, since sharp corners of the back opening result in membrane damage in our first few fabrication rounds. As mentioned before, when the deep silicon etching is nearly finished, the front side photonic crystal structure becomes visible through the edges of the backside opening, which can be seen under an optical microscope (Figure 3d,e). We then stop the Bosch process and switch to an isotropic silicon etch using SF_6 gas to remove the 394 nm BOX layer. The periodic photonic crystal structure is confirmed by a scanning electron microscopy (SEM) image, as presented in Figure 3f.

The dedicated fabrication process developed in this work can not only be used to produce centimeter-scale lightsails, but more importantly, it can directly be extended to scale up to larger sizes, such as a 4-in. wafer-scale fabrication process, as shown in Figure 3g. The rainbow-colored area in the middle of the wafer is the e-beam patterned and plasma-etched photonic

crystal, where colors originate from scattered white light. To pattern such a large-area device with around 2.3×10^9 holes using e-beam lithography, we employ a custom-built program (called 'txl2gpf') to generate GTX files in the Raith EBPG pattern data format. These files include sequences of beam positions, allowing the creation of single-shaped, high-resolution circles (with a subfield resolution of 0.08 nm). This approach contrasts with forming circles using numerous beam step-size resolution rectangles (ranging from 2 to 5 nm), leading to improved circle quality and significantly reduced e-beam writing time. The total e-beam writing time of such a 4-in. wafer sample is around 5–7 h using a relatively large beam spot size of around 100 nm. We would like to note that a deep silicon etch is not performed on this sample, as dry etching introduces variation in the etch uniformity for such a large device. This challenge can, however, be easily overcome by employing wet-etching, e.g., through a potassium hydroxide (KOH) wet etching process³⁶ for both silicon and SiO₂ to get a large-scale lightsail device. In order to scale the fabrication further, larger scale wafers can be used or multiple 4-in. sized lightsail devices could be connected together to assemble a square-meter-sized lightsail, on which different sensors, receivers, and transmitters can be attached and then delivered to deep space through laser propulsion.

To test the fabricated samples and confirm our simulations through measurements, we use the setup depicted in Figure 4a.

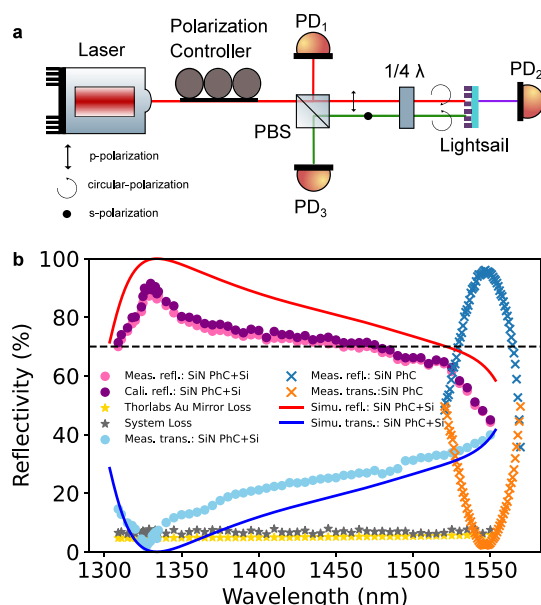


Figure 4. Characterization of the fabricated lightsail samples, including (a) optical measurement setup, and (b) measurements of both PhC and MPhC samples. See text for more details.

A tunable laser emitting light within the wavelength range of 1280–1600 nm serves as the source. Following the laser, a polarization controller (PC) is positioned, which we use to minimize the signal detected at photodetector 1 (PD₁) after the polarizing beamsplitter (PBS), ensuring the input light is linearly polarized (p-polarization). Subsequently, the transmitted light passes through a quarter wavelength wave plate, converting its polarization from linear to circular before reaching the lightsail sample. The light transmitted through the device is captured by PD₂ and recorded as P_{trans} . Conversely,

the reflected light is measured on PD₃ to obtain the reflected power P_{refl} .

The optical power detected at PD₁ is negligible (<0.5%) compared to the initial input power from the laser P_{in} . Thus, we compute the transmission and reflection of the lightsail samples using the ratios P_{trans}/P_{in} and P_{refl}/P_{in} , respectively. Due to small inherent losses in the optical setup, arising from factors such as misalignment of laser beams or imperfections in optical components, a small percentage of the total input laser power is lost. Consequently, $P_{refl} + P_{trans}$ is slightly lower than P_{in} . To quantify these losses, we calibrate the system using a commercial gold mirror.³⁷ Figure 4b illustrates the system loss (depicted by gray stars) between 1300 and 1550 nm when employing a gold mirror to measure the discrepancy between $P_{refl} + P_{trans}$ and P_{in} . The overall system losses range between 5% to 7%, which is in great part attributable to the gold mirror itself, for which we use the datasheet from the manufacturer (gold stars in Figure 4b).

Upon calibration, we evaluate the first batch of fabricated MPhC lightsail chips, each approximately 4×4 mm in size. As indicated by the pink dots in Figure 4b, the MPhC sample (denoted as “SiN PhC + Si”) achieves broadband reflection from 1300 to nearly 1550 nm (70% reflectivity threshold is indicated by the black dashed line). The peak reflectivity exceeds 90% at 1330 nm, with a bandwidth of nearly 200 nm. The corresponding transmission is denoted by the light-blue dots. Accounting for the aforementioned system losses, the calibrated reflectivity (depicted by purple dots) exhibits a similarly broad performance, reaching a peak reflectivity of over 91.5% at 1330 nm. The red and blue curves represent the simulated reflection and transmission of the lightsail, respectively. Discrepancies between simulations and measurements are attributed to fabrication deviations or imperfections in the measurement setup.

In comparison, the typical single-layer silicon nitride photonic crystal, referred to as “SiN PhC,” achieves >70% reflectivity only between 1525 and 1575 nm, with a narrow bandwidth of 50 nm. This bandwidth is significantly narrower than that of the bilayer lightsail design, highlighting the superior performance of the MPhC devices. For a detailed theoretical explanation of the reflection differences between single PhC and MPhC devices, please refer to the [Supporting Information](#).

It is worth mentioning that since the device contains identical circular holes with an equal lattice constant in the orthogonal x- and y-directions, the reflectivity is polarization-independent concerning the incident light. The measurement setup is similar to the one utilized in our previous work,²⁸ and by using a polarizing beamsplitter (PBS) followed by a quarter-wave plate, it allows separating the incoming light from the reflected beam on the PBS. Thus, it shows the reflector works for all polarizations, as the field impinging our device can be directly decomposed into horizontal and vertical polarizations. Furthermore, given that the reflection of the proposed structure is polarization-independent, it renders the device suitable for Gravitational Lens³⁸ and Solar Sails applications,³⁹ where sunlight inherently possesses broadband and unpolarized characteristics. Additionally, the development of a high-power laser system for lightsail propulsion remains an outstanding challenge in terms of both cost and engineering, which must be addressed for successful lightsail acceleration in the future.⁴⁰ Besides, several related technological challenges also need to be considered and solved, including but not

limited to lightsail thermal management⁴¹ and stabilization.⁴² For a detailed theoretical explanation of the reflection differences between single PhC and MPhC devices, please refer to the [Supporting Information](#).

In summary, our study pioneers the development of a photonic crystal/metasurface bilayer structure for laser-driven lightsails, overcoming critical challenges in the quest for interstellar travel. Our innovative design, featuring a silicon nitride photonic crystal with a thin silicon membrane, achieves outstanding experimentally demonstrated high (>91.5% at 1330 nm) and broadband reflectivity (exceeding 70% from 1300 to 1500 nm). This broad reflection spectrum is essential for accommodating Doppler-shifted laser wavelengths during lightsail acceleration. The dedicated fabrication process involves precise techniques, including wafer-scale nanophotonic structure patterning and deep silicon etching. Rigorous optical measurements and theoretical analyses confirm our lightsail's performance, marking a significant advancement in lightsail design and fabrication and verifying its capabilities for future interstellar exploration.

Looking ahead, the scope of lightsail research extends to larger dimensions on the meter scale, achievable through methods like wet chemical etching, to obtain large, free-standing reflective surfaces. Moreover, our study, while focusing on the SiN/Si bilayer structure, does not limit itself to this material system. Bilayers with a significant refractive index contrast, such as SiN/SiC or normal SiN/silicon-rich silicon nitride, can also be employed to design broadband reflectors, potentially minimizing any residual absorption. Additionally, this high-reflectivity, wideband reflection structure has the potential to also play a vital role in various other fields, including optoelectronic devices,^{43,44} integrated optics,^{45,46} and metamaterials and devices,^{47,48} opening up new possibilities for future applications.

■ ASSOCIATED CONTENT

Data Availability Statement

Source data for the figures will be made available on Zenodo.

Supporting Information

The Supporting Information is available free of charge at <https://pubs.acs.org/doi/10.1021/acs.nanolett.4c01374>.

Additional simulations and theoretical analysis of the broadband reflection behavior of the SiN PhC/Si bilayer membrane (PDF)

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Notes

The authors declare no competing financial interest.

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