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High-dynamic baseline determination for the Swarm constellation

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Abstract

Baseline determination for the European Space Agency Swarm magnetic field mission is investigated. Swarm consists of three identical satellites -A, -B and -C. The Swarm-A and -C form a pendulum formation whose baseline length varies between about 30 and 180 km. Swarm-B flies in a higher orbit, causing its orbital plane to slowly rotate with respect to those of Swarm-A and -C. This special geometry results in short periods when the Swarm-B satellite is adjacent to the other Swarm satellites. Ten 24-hr periods around such close encounters have been selected, with baseline lengths varying between 50 and 3500 km. All Swarm satellites carry high-quality, dual-frequency and identical Global Positioning System receivers not only allowing precise orbit determination of the single Swarm satellites, but also allowing a rigorous assessment of the capability of precise baseline determination between the three satellites. These baselines include the high-dynamic baselines between Swarm-B and the other two Swarm satellites.

For all orbit determinations, use was made of an Iterative Extended Kalman Filter approach, which could run in single-, dual-, and triple-satellite mode. Results showed that resolving the issue of half-cycle carrier phase ambiguities (present in original release of GPS RINEX data) and reducing the code observation noise by the German Space Operations Center converter improved the consistency of reduced-dynamic and kinematic baseline solutions for both the

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Swarm-A/C pendulum pair and other combinations of Swarm satellites. All modes led to comparable consistencies between the computed orbit solutions and satellite laser ranging observations at a level of 2 cm. In addition, the consistencies with single-satellite ambiguity fixed orbit solutions by the German Space Operations Center are at comparable levels for all the modes, with reduced-dynamic baseline consistency at a level of 1-3 mm for the pendulum Swarm-A/C formation and 3-5 mm for the high-dynamic Swarm-B/A and -B/C satellite pairs in different directions.

Keywords: Precise Baseline Determination, Precise Orbit Determination, Swarm, Ambiguity fixing, Half-cycle ambiguity

1. Introduction

Satellite formations and constellations have been increasingly utilized to fulfill various research objectives [1]. Data collected by their on-board instruments offer adequate information to satisfy complex scientific and operational tasks. For instance, two Low Earth Orbiting (LEO) satellites in close formation are used for observing the temporal and spatial variations of Earth's gravity field [2] or for producing digital elevation maps [3]. As a prerequisite for these state-of-the-art applications, satellite orbits and especially also baselines have to be precisely determined, the latter with (sub-)mm level precision. Precise baseline solutions are crucial for *e.g.* interferometric Synthetic Aperture Radar (SAR) missions [4] and have the potential benefit of supporting gravity field research [5].

Formation flying LEO satellites typically make use of high precision, dual-frequency multi-channel GPS receivers for Precise Orbit Determination (POD) [6]. By forming Double-Differenced (DD) carrier phase observations, common errors are strongly mitigated and so-called integer ambiguities can be resolved [7]. With the advent of the GRACE mission [2], it has been proved that Precise Baseline Determination (PBD) at 1-mm level is feasible by fixing DD carrier phase ambiguities [8]. Further improvements are obtained by making use of

20 relative dynamics constraints and GPS receiver antenna patterns. Nowadays,
 21 sub mm level baseline precision is achievable for in-line or along-track forma-
 22 tions like the Gravity Recovery and Climate Experiment (GRACE) mission
 23 [9, 10, 11]. For a more complex side-by-side or radial/cross-track formation such
 24 as the TanDEM-X/TerraSAR-X mission, it is claimed that a precision in each
 25 direction of 3-8 mm can be achieved [4]. On 22 November 2013, the European
 26 Space Agency (ESA) geomagnetic field mission Swarm was launched and soon
 27 the three Swarm satellites entered their preferred orbits by a series of dedicated
 28 maneuvers [12]. It is an unprecedented three-identical-satellite constellation
 29 equipped with the same space-borne instruments. All Swarm satellites fly in
 30 near-polar orbits, with Swarm-A/C in a pendulum formation and Swarm-B at
 31 a higher altitude [12]. The distance between the Swarm-A and -C satellites is
 32 varying between 30 and 180 km. When Swarm-B is in view of the other Swarm
 33 satellites, the distance can be as small as about 50 km. For the pendulum part
 34 of Swarm, PBD has already been studied in detail, showing that consistencies
 35 between reduced-dynamic and kinematic solutions under different in-flight envi-
 36 ronment can be achieved that are of the order of 5-40 mm in different directions
 37 [13, 14]. At present, no successful consistently high-precision high-dynamic PBD
 38 research has been done for such kind of constellation.

39 Obtaining very precise baseline solutions for LEO satellites that do not fly
 40 in stable formation is still an open issue. For example, the work described in
 41 [15] shows that it is not straightforward to achieve precise baseline solutions
 42 between the CHAMP and GRACE satellites when these satellites are in view
 43 of each other. The CHAMP-GRACE baselines grow easily from hundreds of
 44 kms to thousands of kms in one day and these are therefore referred to as high-
 45 dynamic baselines. The same applies to the Swarm-B satellite with respect to
 46 the Swarm-A and -C satellites. As the baseline - or distance - between two
 47 LEO satellites grows, the number of GPS satellites that are simultaneously in
 48 view of two GPS receivers drops, resulting in a smaller number of possible DD
 49 combinations. Moreover, LEO satellites experience different perturbing forces
 50 when at different altitudes, especially atmospheric drag due to different density

51 levels [16].

52 The three-identical-satellite Swarm constellation will be used as a test bed
53 for high dynamic baseline determination between LEO satellites. The results
54 in [15] are based on 24-hr orbital arcs that start and end at midnight, which
55 leads to significantly different CHAMP-GRACE orbital geometries for each arc.
56 Moreover, CHAMP and GRACE carry GPS BlackJack receivers with different
57 performance and also have different antenna installation geometries [17]. For
58 CHAMP and occasionally for GRACE, also so-called cross-talk signal interfer-
59 ence between the POD and radio occultation antenna's took place leading to
60 different multi-path patterns [18, 11]. For Swarm, this is not the case. Com-
61 pared to the work described in [15], a different approach is adopted for defining
62 the orbital arcs. A total of 10 days are identified in the period from mid-July
63 to mid-September in 2014 when the Swarm satellites are frequently in view of
64 each other. The time of closest approach is then determined and a 24-hr orbital
65 arc is defined starting 12 hr before and ending 12 hr after this time. This leads
66 to comparable and more stable geometries for each selected orbital arc.

67 The *RUAG Space* Swarm GPS receiver exhibits half- and full-cycle am-
68 biguities due to the tracking issue with its Numerically Controlled Oscillator
69 (NCO) [19, 14]. Systematic 180° phase rotation frequently happens during
70 the tracking process [20]. This makes carrier phase integer ambiguity fixing
71 more challenging. Fixing half-cycle ambiguities erroneously to full-cycle will
72 significantly downgrade the baseline solution precision for the lower pair [10].
73 This receiver characteristic has thus to be properly dealt with. The German
74 Space Operations Center (GSOC/DLR) has implemented an algorithm to
75 correct the half-cycles into full-cycles by checking a certain bit of each carrier
76 phase tracking record in the raw data [20]. In addition, a systematic GPS
77 RINEX converter software issue existed for code observations, leading to
78 larger code noise at the early stage of the Swarm mission and was fixed
79 by ESA on 11 April 2016 ([https://earth.esa.int/web/guest/missions/esa-](https://earth.esa.int/web/guest/missions/esa-operational-eo-missions/swarm/news/-/article/swarm-software-issue-in-rinex-converter-fixed)
80 [operational-eo-missions/swarm/news/-/article/swarm-software-issue-in-rinex-](https://earth.esa.int/web/guest/missions/esa-operational-eo-missions/swarm/news/-/article/swarm-software-issue-in-rinex-converter-fixed)
81 [converter-fixed](https://earth.esa.int/web/guest/missions/esa-operational-eo-missions/swarm/news/-/article/swarm-software-issue-in-rinex-converter-fixed), last accessed: 9 January 2019). ESA has been re-creating

82 these old Swarm RINEX files with both issues removed (the 8th Swarm
83 Data Quality Workshop, <https://earth.esa.int/web/guest/missions/esa->
84 eo-missions/swarm/activities/conferences/8th-data-quality-workshop, last
85 accessed: 9 January 2019). The resulting GPS data lead to significantly
86 more precise single-satellite POD [21] and dual-satellite PBD solutions for the
87 Swarm-A/C formation [14, 13]. Their impacts on the high-low satellite pairs
88 will be investigated in this research.

89 For the Swarm mission, it is not possible to validate PBD solutions by com-
90 parison with independent data coming from for example a K-band Radar Rang-
91 ing system as on board the GRACE twin satellites [22]. A quality check can
92 typically be done by assessing the consistency between kinematic and reduced-
93 dynamic baseline solutions [5, 10, 13]. Moreover, external POD and PBD solu-
94 tions are available and can be used for a quality assessment. An interesting de-
95 velopment is single receiver ambiguity fixing, leading to enhanced POD solutions
96 [23, 20]. [23] propose a scheme of ambiguity fixing based on the ionosphere-free
97 wide-lane model developed by [24], while [20] make use of the wide-lane phase
98 bias estimate products provided by [25]. Such single-satellite ambiguity fixed
99 POD solutions have been made kindly available by GSOC/DLR for Swarm and
100 will be used for assessing the quality of both POD and PBD orbit solutions in
101 this research [21]. Details of the single-satellite ambiguity fixed POD solutions
102 can be found in [20] for the Sentinel-3A satellite, which carries a GPS receiver
103 with similar characteristics when comparing with those flown by Swarm. An
104 external validation of the individual satellite orbit solutions is offered by the
105 availability of Satellite Laser Ranging (SLR) observations, which will form part
106 of the analysis and quality assessments [26].

107 The structure of this paper is as follows. Section 2 includes a description of
108 the Swarm constellation data selection and corresponding quality assessment.
109 Section 3 introduces the kinematic and reduced-dynamic POD and PBD al-
110 gorithms. Section 4 describes results and orbit comparisons for the Swarm
111 constellation. This paper is concluded by Section 5, which includes a summary
112 and outlook.

113 2. Observations

114 2.1. Data selection

115 Representative data have been selected to test PBD for all three Swarm
116 satellites. Table 1 includes three selected Keplerian orbital elements for Swarm
117 satellites at a representative epoch. The Swarm-A/C formation flies in two
118 almost identical polar orbits with only 1.5° difference in the right ascension of
119 the ascending node (RAAN). These two satellites form a so-called pendulum
120 formation. During the analyzed period the Swarm-B satellite flies about 50 km
121 higher, which slightly differs with the early designed orbit scheme [12, 27], and
122 the RAAN difference on average is about 10° . Baseline lengths of high-low
123 Swarm satellite pairs thus vary dramatically due to the different orbital planes
124 and altitudes. It is found that the period July-September 2014 includes days
125 for which the Swarm-A/B/C geometry is favorable, *i.e.* all three satellites are
126 in view of each other. During this period, the baseline lengths between the
127 Swarm-B satellite on the one hand and the Swarm-A and -C satellites on the
128 other hand reach a local minimum every 6.1 days.

129 To evaluate the PBD methods used in this research, a sliding 24-hr orbit arc
130 selection is done. Each selected orbit arc centers around the epoch of minimum
131 distance, see *e.g.* Figure 1. The Swarm-A/C formation baseline length varies
132 consistently between 30 and 180 km. For the Swarm-B/A and Swarm-B/C
133 pairs, the two satellites approach each other from an approximate 3500 km
134 to a minimum of around 50 km. Ten orbit arcs are selected and recorded in
135 Table 2. The used GPS ephemeris products are separate 24-hr GPS satellite
136 orbits and 5-sec clock biases files [28]. Before making use of them, a tool is used
137 to interpolate the adjacent three consecutive 24-hr GPS satellite orbits into 5
138 seconds and then a merged orbit and clock file is created. The influence of GPS
139 orbit and clock bias gaps crossing midnight is reduced.

140 Figure 2 shows that the Swarm-A/C pendulum formation has on average
141 > 7 common GPS satellites in view. This number is not yet influenced by the
142 antenna field of view modification and is approximately equal to the number of

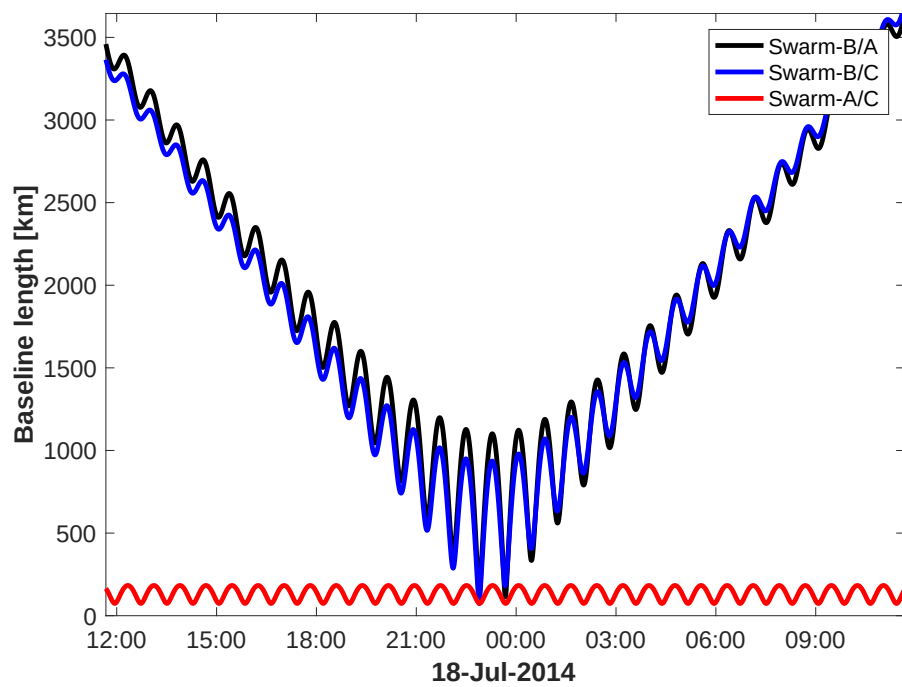


Figure 1: Length variations for each Swarm dual-satellite formation during one representative 24-hr orbit arc.

Table 1: The crucial Keplerian orbital elements determining the relation between Swarm orbital planes during mid-July to mid-September 2014. a represents the semi-major axis, i means the orbit inclination and Ω is the right ascension of the ascending node (Credit: satellite two line elements data is obtained from www.space-track.org).

Satellite	a (km)	i (deg)	Ω (deg)
Swarm-A	6842.06-6840.75	87.35-87.36	197.53-175.66
Swarm-C	6842.05-6840.75	87.35-87.36	198.70-177.03
Swarm-B	6890.98-6890.41	87.75-87.76	206.28-188.59

Table 2: Ten selected 24-hr orbit arcs for Swarm constellation. Please note that DOY specifies the day of the center of the arc. This DOY number will be used as orbit arc identifier in this research.

Date (YYYY-MM-DD)	DOY	Middle of the arc	Minimum distance (km)
2014-07-17	198	23:40:30	112.57
2014-07-24	205	02:50:40	85.69
2014-07-30	211	06:00:40	82.85
2014-08-05	217	08:23:30	120.39
2014-08-11	223	11:33:00	56.14
2014-08-17	229	13:55:10	51.84
2014-08-23	235	16:17:20	52.51
2014-08-29	241	18:39:10	70.62
2014-09-04	247	20:13:40	58.99
2014-09-10	253	21:47:50	64.91

GPS receiver tracking channels [13]. For the high-low Swarm satellite pairs, this number drops from 6-8 to 4-6 as the baselines become longer. A low number of common GPS satellites in view has a big impact on the achievable PBD precision, especially for kinematic solutions. For high-quality PBD, at least 5 GPS satellites are required to be simultaneously tracked by two GPS receivers [8]. If less than 5 GPS satellites are commonly in view, no kinematic PBD solution will be generated for the associated epochs. Reduced-dynamic baseline

solutions will then however still be available.

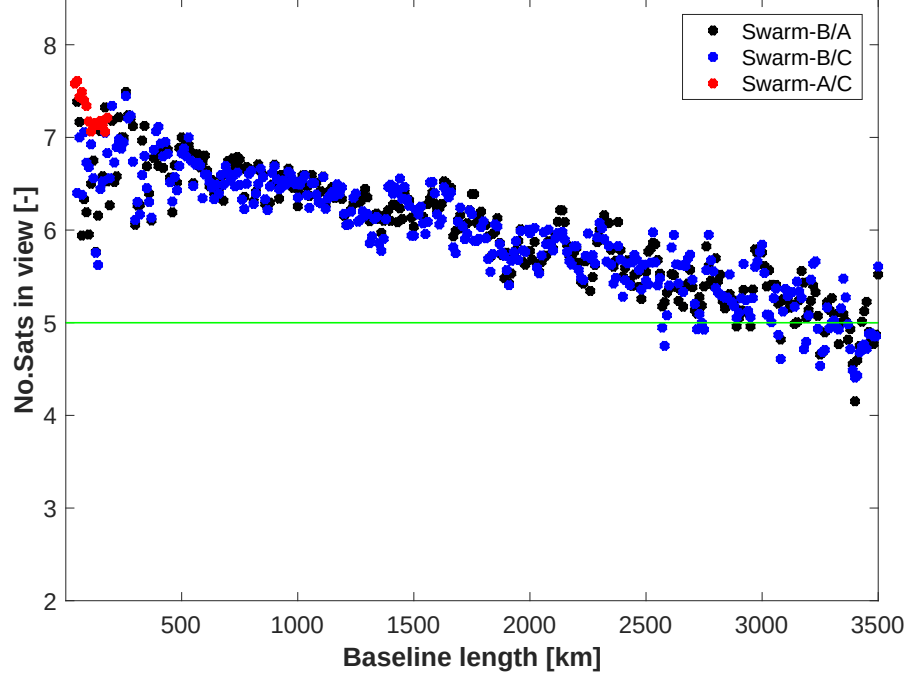


Figure 2: The number of GPS satellites simultaneously tracked by two GPS receivers as a function of distance (every 10 kms) for each Swarm dual-satellite formation (analysis for 10 24-hr orbit arcs).

2.2. Data quality assessment

GPS code and carrier phase observations are affected by several error sources, including thermal noise and multi-path. For the relevant Swarm data used in this research, the original GPS code observations suffer additionally from systematic errors due to sub optimal RINEX converter software leading to large noise levels. The code noise level has a clear impact on the ambiguity fixing success rate. The original carrier phase observations experience half-cycle ambiguity issues as mentioned above. A new version of Swarm GPS data was kindly provided by GSOC/DLR. For this version, the converter code error was removed and in addition the half-cycle carrier phase ambiguities were corrected to full-cycles.

162 The quality of in-flight GPS code observations can be assessed by analyzing
 163 their multi-path effects by using the multi-path evaluation models that are in-
 164 troduced in [18, 29]. Thus, the multi-path represents an independent evaluation
 165 of misfit caused by the systematic errors from the RINEX converter on the one
 166 hand and the code observation noise on the other hand. The Root-Mean-Square
 167 (RMS) of multi-path is displayed in Figure 3 for Swarm-A as a function of the
 168 elevation of the GPS satellites as seen from the GPS receiver antenna installed
 169 on the zenith surface of each Swarm satellite. The results displayed in Figure 3
 170 hold for 17 July 2014, when the Swarm-A GPS antenna had an antenna field of
 171 view of 80° (improved to 88° in October, 2014, [30]). The tracked GPS observa-
 172 tions below 10° antenna cut-off angle are obtained by the tracking performance
 173 of GPS receiver antenna in its aft direction, as reported by [30].

174 In general, the observation residual level drops with increasing elevation
 175 angle, which is in agreement with anticipated noise levels of GPS observations
 176 [18]. Modifications in the new version of data clearly reduce the code noise level.
 177 This analysis indicates a reduction from 0.34/0.37 m to 0.18/0.20 m in terms
 178 of global RMS for the L_1/L_2 frequencies. Code noise on the L_1 frequency is
 179 slightly smaller than on the L_2 frequency. It is anticipated that the ambiguity
 180 fixing will improve when using the new batch of data.

181 Research in [14, 13] confirms that the GPS observation correction process
 182 implemented by GSOC/DLR has a clear impact on the ambiguity fixing process,
 183 as also shown in Figure 4 in this research. This figure is representative for a
 184 triple-satellite PBD (see Section 3.1) and displays the ambiguity fixing success
 185 rate as a function of the number of iterations completed by the IEKF (with a
 186 maximum of 20). In the IEKF procedure, the ambiguities for the pendulum
 187 formation Swarm-A/C pair are fixed first (requiring around 6 iterations until
 188 convergence), after which as many as possible ambiguities are fixed for the
 189 Swarm-B/A and Swarm-B/C pairs. It can be observed that the ambiguity fixing
 190 is clearly enhanced by using the new version of the data. For the Swarm-A/C
 191 formation, the success rate for the first iteration is improved from 37% to 97%.
 192 The final fixing success rate increases from 88% to 98%. For the Swarm-B/A

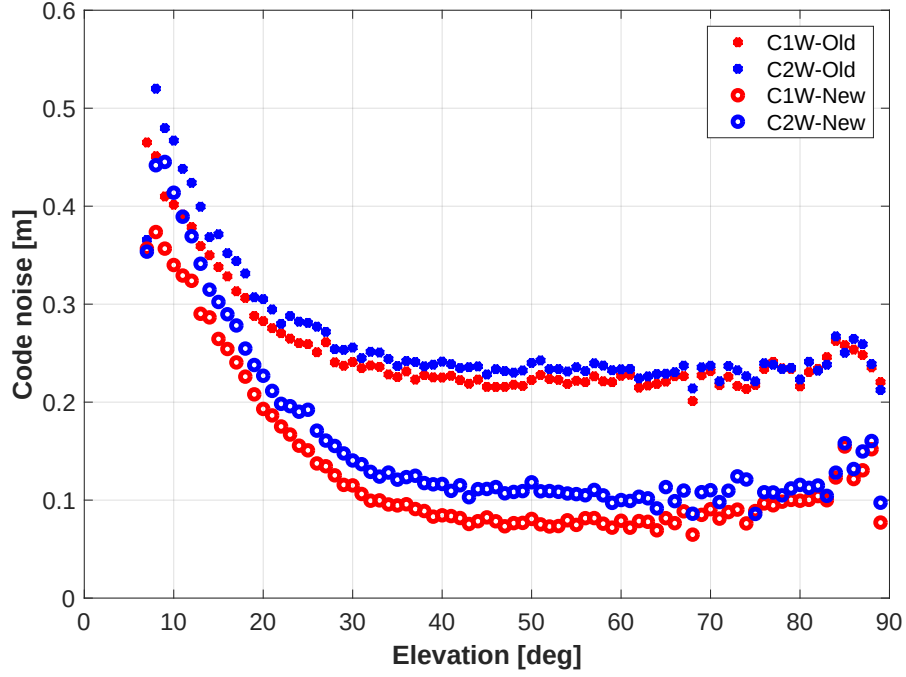


Figure 3: RMS of code multi-path as a function of elevation for the GPS L_1 and L_2 frequencies for two versions of Swarm-A GPS receiver RINEX data: *Old* indicates the ESA original file with RINEX converter software issues, *New* indicates the one corrected by GSOC/DLR and used in this research (selected day: DOY 198, 2014).

193 and Swarm-B/C combinations, fixing starts at iteration 8 for the old version of
 194 the data and iteration 7 for the new version of the data. It can also be clearly
 195 seen that for the starting iteration, the success rate improves from merely 9%
 196 and 8% to a much higher level of 64% and 64% for the Swarm-B/A and Swarm-
 197 B/C combinations, respectively. The final success rates reach about 97% and
 198 97%, respectively, which is much higher than 81% and 83% when using the old
 199 version of the data.

200 Swarm dual-satellite PBD (again, please see Section 3.1) is done to evalu-
 201 ate the influence of half-cycle *vs.* full-cycle inter ambiguity fixing. As shown in
 202 table 3, the ambiguity fixing success rate is improved by more than 10% when
 203 full-cycle ambiguities are to be fixed. The new version of the data also im-

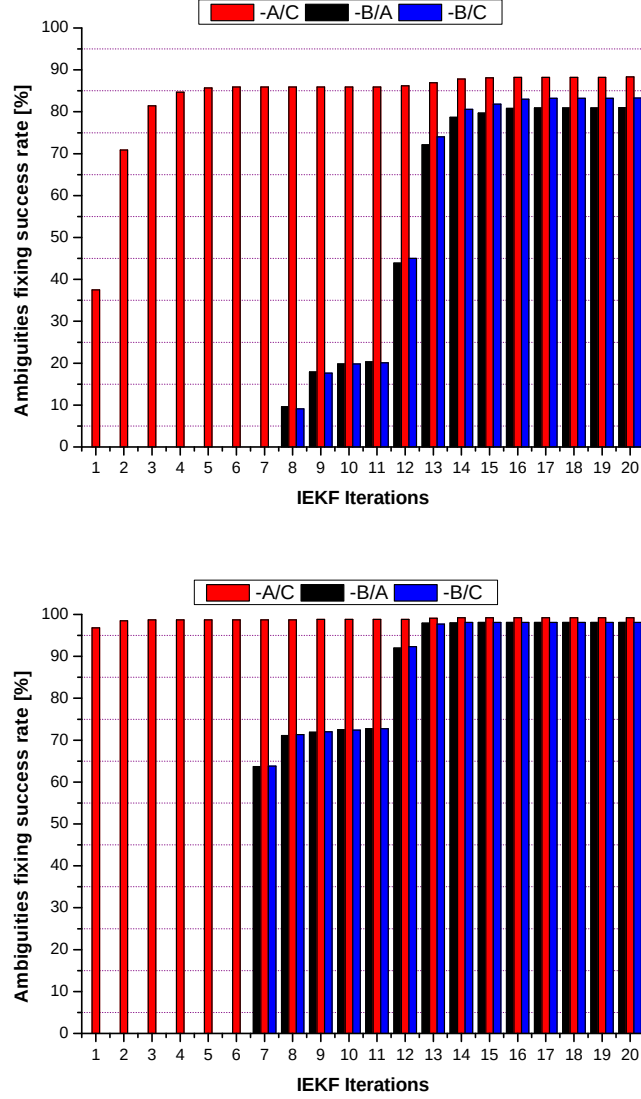


Figure 4: Integer ambiguity fixing success rate versus IEKF iterations for the triple-satellite Swarm PBD. Two sets of data, original version (top) and new version with corrections (bottom) are used (selected day: DOY 198, 2014).

204 proves the kinematic and reduced-dynamic baseline consistency, especially for
 205 two high-dynamic Swarm-B/A and Swarm-B/C satellite pairs. Therefore, for

206 the remainder of this paper, results will be based on the new version of the data
 207 (Section 4).

Table 3: Mean of daily RMS differences between kinematic and reduced-dynamic baseline solutions, and ambiguity fixing success rate for Swarm constellation (dual-satellite PBD solutions). Two sets of Swarm GPS RINEX data are used.

Solution	Radial	Along-track	Cross-track	Amb.fix.
	(mm)	(mm)	(mm)	(%)
Swarm-A/C				
Half-cycle	15.0	7.8	4.1	86.9
Full-cycle	12.4	5.5	3.6	98.1
Swarm-B/A				
Half-cycle	24.9	11.2	5.3	84.2
Full-cycle	22.9	9.8	5.6	97.3
Swarm-B/C				
Half-cycle	24.9	11.4	6.5	83.9
Full-cycle	22.6	10.4	5.7	97.5

208 3. Methodology

209 3.1. Single-, dual- and triple- POD/PBD

210 When solely using dual-frequency high-precision GPS tracking data and GPS
 211 satellite orbit/clock products, instantaneous satellite positions can be deter-
 212 mined at the observation epochs when a sufficient number of GPS satellites is
 213 in view. This approach is referred to as kinematic approach [31] and obviously
 214 leads to gaps in the position time series when there are gaps in the GPS ob-
 215 servation data or when not enough GPS satellites are in view. Dynamic and
 216 reduced-dynamic orbit determination, which include force models to solve equa-
 217 tions of motion, result in continuous time series of satellite positions [6]. Force

models are typically divided in (1) gravitational force models including the non-spherical gravity field, perturbations from 3rd bodies (Sun and the Moon), and solid-earth and ocean tides, and (2) non-gravitational force models including the Sun radiation pressure, the Earth albedo pressure, and atmospheric drag. However, the associated models are not perfect, and model errors can be absorbed by so-called empirical accelerations [17].

The Multiple Orbit Determination using Kalman filtering (MODK, [15]) tool is an in-house developed add-on tool to the GPS High Precision Orbit Determination Software Tools (GHOST) [32]. MODK has the capability to provide reduced-dynamic single-, dual- and triple-satellite orbit solutions, where for the dual- and triple-satellite mode ambiguity fixing as well as further kinematic baseline determination can be done. The core of the MODK tool is based on an Iterative Extended Kalman Filter (IEKF) process, where the GPS observations are used and modeled for each frequency, *i.e.* L_1 and L_2 [11]. A comprehensive description of the MODK tool and underlying method can be found in Chapter 3.3 of [15].

Compared to single-satellite POD, PBD in case of dual- and triple-satellite orbit determination includes the possibility to constrain differential empirical accelerations, which is especially relevant if two satellites fly in almost identical orbits (as is the case for Swarm-A and -C). This constraining proved to be very beneficial for estimating high-precision baselines for the GRACE tandem and for the Swarm-A/C pendulum formations [10, 13]. In this study the frequency-dependent antenna Phase Center Variation (PCV) maps created by so-called *residual approach* are included [33, 11]. Our proposed Code Residual Variation (CRV) maps are not modelled since the used GSOC/DLR processed data have lower noise levels than the original data. Besides, no significant signal interference exists for Swarm when comparing with GRACE as described in [11].

The MODK tool first computes reduced-dynamic orbit solutions, after which kinematic solutions are generated. The latter are based on the same modeled GPS observations, where use is made of the ambiguity fixing of the reduced-

dynamic solution. In order to minimize gaps in the kinematic satellite position time series, all available fixed integer ambiguities and otherwise float ambiguities are used. No kinematic solutions are computed for epochs for which less than 5 GPS satellites are simultaneously in view of each combination of two GPS receivers, or epochs for which the RMS of GPS observation phase residuals is above 5 cm. A Least Squares Method (LSM) is adopted for the kinematic PBD. More detailed information and the data flow chart regarding the kinematic and reduced-dynamic approaches can be found in [13]. The MODK tool includes the option to define a preferred baseline, *i.e.* a pair of satellites for which the ambiguity fixing is done first, after which the fixing is invoked for the other baselines. For the Swarm triple-satellite PBD, this option is used and the preferred baseline is the one for the pendulum Swarm-A/C satellite pair.

The DD ambiguities are resolved by the Least-squares Ambiguity De-correlation Adjustment (LAMBDA) algorithm [7]. It has been widely used for different satellite formations PBD [8, 10, 11]. To maximize the ambiguity fixing success rate, a subset fixing process is implemented. It allows for part of a set of integer ambiguities to be fixed while for the remaining the associated float values are used. This is not a conventional use of the LAMBDA algorithm, which nominally only accepts epochs when the entire set of ambiguities is fixed [8]. A strict ambiguity fixing validation scheme is adopted and integrated in the MODK tool [34, 11]. Moreover, an additional outlier detection check is included: if the absolute value of GPS carrier phase observation residuals (after fixing) is above 5 cm, the associated ambiguity will be kept at its float value and sent into IEKF for further fixing in the next iterations. It was found that this resulted in a reduced chance of wrongly fixed integer ambiguities and thus a more robust PBD by the IEKF as used by the MODK tool.

3.2. Parameter settings

Due to the different orbit altitudes for the Swarm satellites (Table 1), especially uncertainties in the modeling of non-gravitational accelerations can be different for Swarm-A and -C on the one hand and Swarm-B on the other hand.

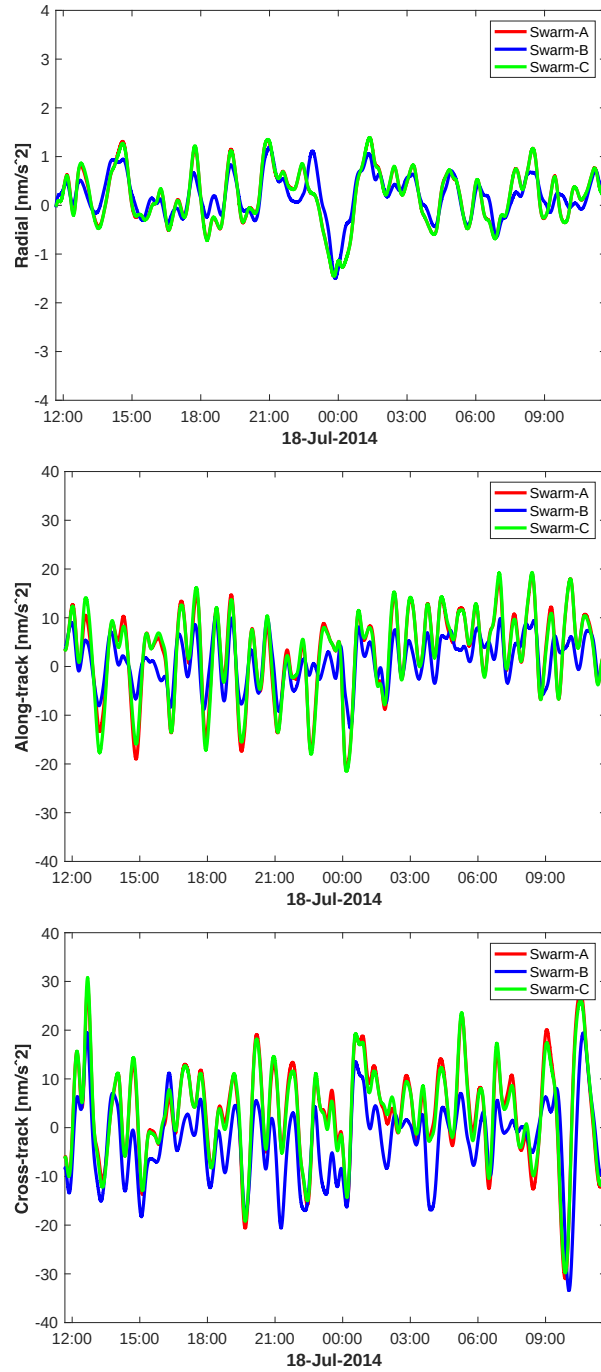


Figure 5: Time series of estimated empirical accelerations in the radial (top), along-track (middle) and cross-track (bottom) directions for each Swarm satellite based on triple-satellite PBD. Please note different scales are set for the vertical axes (DOY 198, 2014). Please note that the curves for Swarm-A and -C almost completely overlap.

279 This will lead to differences in the estimated empirical accelerations that are
 280 used to absorb modeling errors. Figure 5 shows typical levels of estimated em-
 281 pirical accelerations for the three Swarm satellites on a representative day. The
 282 statistics of them are shown in Table 4. The mean of estimates of empirical
 283 accelerations represents the level of constant correction to the adopted dynamic
 284 models in certain direction. Although for all three Swarm satellites, the val-
 285 ues seems to overlap to quite a significant extent, the empirical acceleration
 286 differences for the Swarm-A/C pair are significantly smaller than for the other
 287 pairs. It can be observed that the empirical accelerations (mean and RMS-
 288 about-mean) are larger in the along-track direction, which is the direction for
 289 which atmospheric drag is predominant, and the cross-track direction, which
 290 is the direction for which mis-modeling of solar radiation pressure forces is the
 291 largest (also due to the simplified canon ball satellite model that is used by the
 292 MODK tool, the scaling factors of the associated non-gravitational forces can
 293 not compensate the in-flight perturbations completely [13, 35]).

Table 4: Empirical acceleration estimate statistics for each Swarm satellite and satellite pair
 (mean and RMS-about-mean, DOY 198, 2014).

Sat/Pair	Radial	Along-track	Cross-track
	(nm/s^2)	(nm/s^2)	(nm/s^2)
Swarm-A	0.2 ± 0.6	2.9 ± 8.2	3.2 ± 9.8
Swarm-B	0.2 ± 0.4	1.2 ± 4.6	-2.6 ± 8.2
Swarm-C	0.2 ± 0.6	3.0 ± 8.3	3.2 ± 9.5
Swarm-A/C	0.0 ± 0.0	-0.0 ± 1.1	-0.0 ± 1.2
Swarm-B/A	0.0 ± 0.3	-1.7 ± 5.3	-5.8 ± 6.5
Swarm-B/C	0.0 ± 0.3	-1.7 ± 5.4	-5.8 ± 5.9

294 The correlation time (τ), STandard Deviation (STD) of a-priori values (σ_a)
 295 and process noise (σ_p) of empirical accelerations have been tuned to reflect the
 296 typical level for these parameters, both in an absolute and relative sense. The
 297 adopted values are included in Table 5. It can be seen that the values for the

298 STD for the difference between empirical accelerations is specified to be smaller
 299 for the Swarm-A/C pendulum satellite pair, reflecting their similarity of orbit
 300 (especially altitude).

301 Both GPS carrier phase and code observations are used by MODK to pro-
 302 duce orbit solutions. The carrier phase weight is set inversely proportional to
 303 its claimed noise level, which is 3 mm for each frequency in POD and 5 mm in
 304 PBD as in that case single-differences are used. The code observation weight
 305 is set as 0.3 m for each frequency in POD and 0.5 m in PBD. The same force
 306 models and standards are used as specified in [13].

Table 5: Empirical acceleration parameter settings in three directions (radial/along-track/cross-track) for each Swarm satellite and each pair of satellites in IEKF. The correlation time τ is equal to 600 s.

Sat/Pair	σ_a	σ_p
	(nm/s ²)	(nm/s ²)
Swarm-A	5/15/15	1/3/3
Swarm-B	5/15/15	1/3/3
Swarm-C	5/15/15	1/3/3
Swarm-A/C	2/5/5	0.2/1/1
Swarm-B/A	5/15/15	1/3/3
Swarm-B/C	5/15/15	1/3/3

307 4. Results and discussion

308 This section includes the results of the Swarm precise orbit and baseline
 309 determination for the selected 10 orbit arcs. The single-satellite ambiguity fixed
 310 GSOC/DLR kinematic and reduced-dynamic POD solutions serve as reference
 311 both for the absolute and baseline solutions, where the latter is referred to as
 312 the GSOC/DLR Differential POD or DPOD solution. Results for both dual-
 313 satellite (Section 4.2) and triple-satellite (Section 4.3) PBD will be provided

and discussed, followed by SLR validation (Section 4.4). However, this section starts with a brief result regarding the detection of GPS observation outliers.

4.1. GPS data outliers

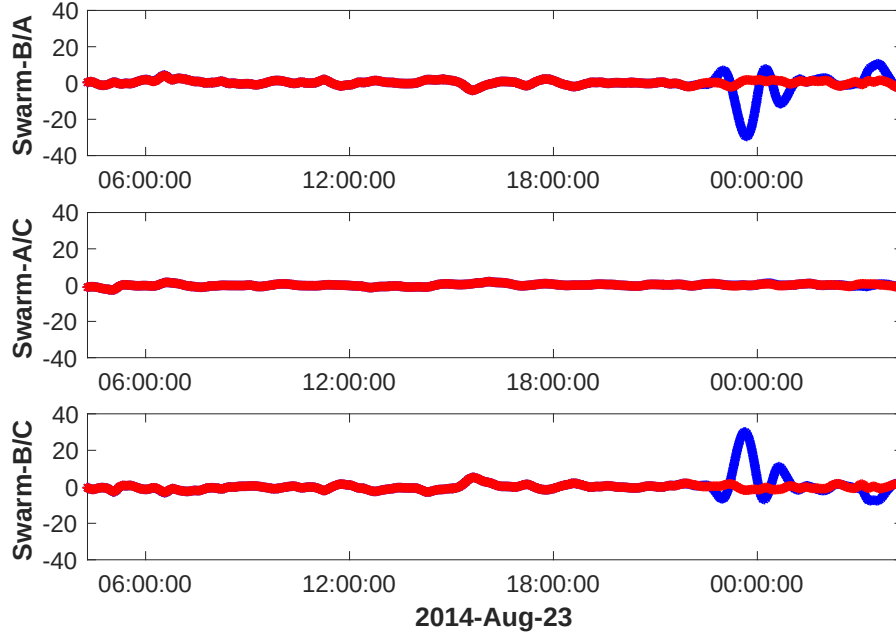


Figure 6: Consistency (unit:cm) between triple-satellite Swarm baseline solutions and baselines derived from the reference GSOC/DLR orbits in the along-track direction, both for including (blue) and excluding (red) the identified G04 outliers (22:50 to 23:50, on 23 August 2014). The consistency is included for the Swarm-B/A (top), Swarm-A/C (middle) and Swarm-B/C (bottom) satellite pairs.

GPS observation outliers are in principle detected automatically by the MODK tool (Section 2.2). It is important to report that for a few GPS satellite tracking passes very large observation residuals were obtained, *i.e.* after the automated outlier detection. This resulted in an unstable IEKF process. Therefore, these observations were excluded manually. To be precise, the following passes were eliminated: GPS Block IIA G04 for Swarm-B from 22:50 to 23:50 on 23 August 2014 (DOY 235) and GPS Block IIR-M G17 for Swarm-A from

23:50 on 04 September (DOY 247) to 00:50 on 05 September 2014. Block IIA GPS satellites are sometimes in eclipse affecting their yaw attitude motion [36]. The outliers for 23 August can be attributed to G04 being in eclipse. The cause for the outliers during the other pass might be the inconsistency of GPS satellite clock corrections spanning midnight. The impact of removing the outlying pass is shown for 23 August 2014 in Figure 6. It can be seen that the impact of the outlying pass reaches a level of 20 centimeters. The eliminated data accounts for less than 0.5% of all GPS available observations. It has to be noted that for PBD the relevant GPS tracking passes are excluded for all three satellites when forming DD combinations.

4.2. Dual-satellite PBD

Three dual-satellite PBD solutions can be obtained for Swarm. For each possible pair of Swarm satellites, selected parameter settings are included in Table 5. An ephemeris comparison is done for each satellite between its MODK dual-satellite PBD solution and external GSOC/DLR solutions (Table 6). As for reduced-dynamic POD, two edges of each orbit often show large inconsistency when comparing with adjacent orbits. These edge effects will be exaggerated by differentiating two GSOC/DLR orbits directly. Therefore two 15 min edges of each MODK or GSOC/DLR orbit are neglected for all baseline comparisons in this research, namely 23-hr baseline comparisons are done instead of 24-hr. An example is shown in Figure 7 for 5 August 2014 (DOY 217), which indicates that the edge effects cause clearly larger inconsistency between two solutions. Therefore these influence will be excluded for the following ephemeris comparisons.

In general the different reduced-dynamic orbit solutions show a good level of consistency: the RMS-about-mean of orbit differences is about 5-7 mm for the radial and cross-track directions. For the along-track direction, this is around 12 mm level, which corresponds to a larger dynamic modeling difference between two institutes. Moreover, the comparison shows mean orbit differences of about 2-5 mm in the radial and cross-track directions. They again indicate

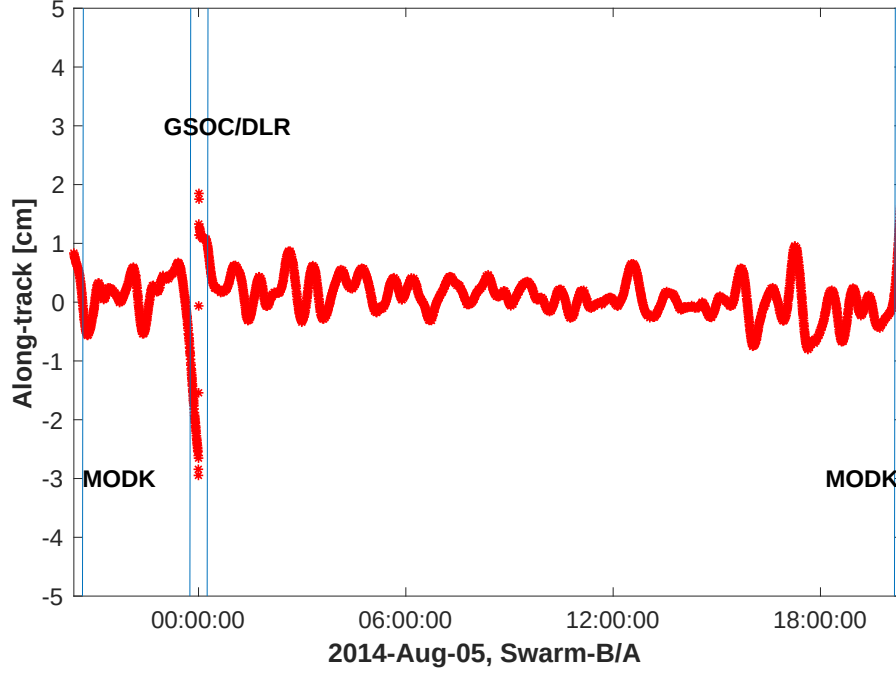


Figure 7: Ephemeris comparison between MODK reduced-dynamic solution and GSOC/DLR single receiver ambiguity fixed reduced-dynamic orbits in along-track direction for the Swarm-B/A baseline (DOY 217, 2014). The excluded edge effects of MODK solution and GSOC/DLR solution are indicated by the legends and blue vertical lines: for the MODK solution, the first and last 15 minutes of an orbit arc are excluded; for the GSOC/DLR solution, the 30 minutes around midnight of an orbit arc are excluded.

the differences between the satellite cannon-ball model used in this research and the panel box-wing macro-model used in [21]. The mean of differences in the radial direction can be attributed to the missing Earth albedo modeling in this research. More sophisticated dynamic modeling of satellite is beneficial for POD and PBD [35, 37], however it goes beyond the scope of this research.

Results of the ephemeris comparisons in terms of baseline are displayed in Table 7. It has to be noted that the GSOC/DLR solutions are provided from midnight to midnight, which differs with the 24-hr arc in this research. The comparisons have been done for both the reduced-dynamic and kinematic MODK baseline solutions. It can be observed that the mean of baseline differences is

Table 6: Ephemeris comparison between different dual-satellite reduced-dynamic MODK baseline solutions and GSOC/DLR single receiver ambiguity fixed reduced-dynamic orbits (mean and RMS-about-mean, 10 orbit arcs).

Satellite	PBD solution	Radial (mm)	Along-track (mm)	Cross-track (mm)
Swarm-A	Swarm-A/C	4.8 ± 6.0	-2.8 ± 12.8	1.4 ± 7.1
	Swarm-B/A	4.9 ± 6.0	-2.7 ± 12.4	3.1 ± 7.1
Swarm-B	Swarm-B/A	5.0 ± 5.3	-0.7 ± 11.1	3.3 ± 6.7
	Swarm-B/C	5.0 ± 5.4	-0.4 ± 11.5	3.2 ± 7.1
Swarm-C	Swarm-A/C	4.7 ± 5.9	-1.3 ± 12.8	1.3 ± 7.2
	Swarm-B/C	4.8 ± 5.7	-0.4 ± 12.1	2.9 ± 7.1

364 very small, typically below 1 mm for the radial and cross-track directions, and
 365 below 2.5 mm for the along-track direction. It is clear that common single-
 366 satellite orbit errors are canceled to a large extent when forming baselines, *cf.*
 367 Table 6. For the reduced-dynamic solutions, a 1-3 mm level consistency is ob-
 368 tained for the Swarm-A/C baseline. This is slightly worse than the level of
 369 consistency as reported in [13], in which only a comparison for the Swarm-A/C
 370 pair was done and the GSOC/DLR baselines were also DD ambiguity fixed so-
 371 lutions. [13] selected a more quiet ionospheric activity period (January 2016)
 372 for comparison. Stronger ionospheric activities bring more challenging issues for
 373 precise baseline determination [38]. For the other two reduced-dynamic base-
 374 lines, larger differences are obtained, which is due to the less favorable geometry
 375 between the associated two satellites.

376 For the kinematic baselines, the consistency between the MODK and the ref-
 377 erence GSOC/DLR orbit solutions is worse (Table 7). The consistency level is
 378 comparable to the consistency between the MODK reduced-dynamic and kine-
 379 matic orbit solutions (Table 3). The consistency for Swarm-A/C is better than
 380 for Swarm-B/A and Swarm-B/C, which can be attributed to the less favorable

geometry when these satellites are at larger distances. Kinematic solutions will not be computed when less than 5 GPS satellites are in view by two Swarm satellites, therefore the percentage of epochs with available kinematic solutions drops as the distance gets longer for satellite pairs. Another comparison is done between baselines derived from GSOC/DLR kinematic and reduced-dynamic DPOD solutions. It is interesting to observe that for the GSOC/DLR kinematic baseline comparison, a similar level of consistency is obtained for all three baselines, thus including Swarm-A/C. The MODK kinematic baselines display better consistency with the GSOC/DLR DPOD reduced-dynamic reference orbits than the associated GSOC/DLR DPOD kinematic orbits, even for Swarm-B/A and Swarm-B/C formations for which the lengths are varying up to 3500 km. This can be explained by considering that in single-satellite POD, no advantage can be taken of *e.g.* constraining relative dynamics, as are done for Swarm-A/C with the MODK tool. Nevertheless, the GSOC/DLR kinematic solutions for the high-dynamic satellite pairs have around 10% higher availability than the MODK solutions.

4.3. Triple-satellite PBD

When comparing the kinematic and reduced-dynamic baseline consistency obtained by dual-satellite and triple-satellite PBD, respectively, slightly downgraded consistency can be seen for the triple-satellite case in Table 8. Table 9 shows the direct comparison between satellite orbits computed using the triple-satellite PBD mode and the GSOC/DLR single-satellite reference orbit solutions. This in general also corresponds to the results in Table 6. The results indicate that by including a third Swarm satellite leading to high-dynamic baselines does not significantly degrade the baselines solution for the Swarm-A/C pendulum pair.

Table 10 shows the results of comparison between Swarm triple-satellite PBD solutions and baselines derived from the reference GSOC/DLR orbits. When comparing with dual-satellite mode, in general around 2.6% less kinematic solutions are created for Swarm-A/C baseline due to more data editing for three

Table 7: Comparison between different MODK baseline solutions (dual-satellite PBD) and baselines derived from the GSOC/DLR DPOD reduced-dynamic reference orbits (mean and RMS-about-mean, 10 orbit arcs), another comparison is done between the GSOC/DLR DPOD kinematic and reduced-dynamic reference orbits. The percentage of epochs with available kinematic solutions is also shown.

Solution	Radial (mm)	Along-track (mm)	Cross-track (mm)	Perc. (%)
MODK Reduced-dynamic				
Swarm-A/C	-0.0 ± 1.6	2.1 ± 2.9	-0.1 ± 1.4	100
Swarm-B/A	0.7 ± 4.7	1.6 ± 6.7	0.2 ± 3.5	100
Swarm-B/C	-0.2 ± 2.9	0.7 ± 4.3	-0.2 ± 3.0	100
MODK Kinematic				
Swarm-A/C	-0.1 ± 11.9	2.2 ± 5.7	-0.1 ± 3.5	97.7
Swarm-B/A	-0.2 ± 22.8	2.0 ± 12.0	0.4 ± 6.3	80.2
Swarm-B/C	0.9 ± 21.3	0.3 ± 10.0	-0.4 ± 5.9	81.3
DLR DPOD Kinematic				
Swarm-A/C	0.2 ± 21.2	0.1 ± 8.3	-0.1 ± 6.3	93.7
Swarm-B/A	-0.1 ± 25.0	1.0 ± 11.6	0.0 ± 7.6	91.7
Swarm-B/C	0.2 ± 25.4	-1.0 ± 11.6	-0.1 ± 7.6	91.8

satellites. Compared to the dual-satellite mode, more single-differenced combinations have to be established and pass the data editing because of the involvement of Swarm-B [15]. It is found that the single-differenced clock offset editing - highly determined by the relative ionospheric changes between two satellites - is the dominant impact factor which discards more than 1% data for each satellite. However for especially Swarm-B/A baseline a slight improvement of 1% is obtained, which can be attributed to more kinematic solutions passing the residual assessment. Dual-satellite PBD mode lacks constraint from the third satellite, therefore more solutions at larger distance will fail to pass this test. The baseline consistency between the MODK kinematic solutions and the

Table 8: Comparison between MODK kinematic and reduced-dynamic baseline solutions, and ambiguity fixing success rate for dual- and triple-satellite PBD (mean of RMS-about-mean statistics of 10 orbit arcs).

Solution	Radial (mm)	Along-track (mm)	Cross-track (mm)	Amb.fix. (%)
Swarm-A/C				
Dual-	12.4	5.5	3.6	98.1
Triple-	13.9	6.4	4.0	98.4
Swarm-B/A				
Dual-	22.9	9.8	5.6	97.3
Triple-	23.4	10.0	5.8	97.3
Swarm-B/C				
Dual-	22.6	10.4	5.7	97.5
Triple-	23.5	10.4	5.9	97.4

Table 9: Comparison between the Swarm triple-satellite reduced-dynamic PBD orbits of each satellite and the reference GSOC/DLR reduced-dynamic orbit (mean and RMS-about-mean, 10 orbit arcs).

Solution	Radial (mm)	Along-track (mm)	Cross-track (mm)
Swarm-A	4.8 ± 5.7	-2.7 ± 12.0	3.8 ± 7.2
Swarm-B	4.9 ± 5.4	-0.6 ± 11.6	3.9 ± 7.1
Swarm-C	4.7 ± 5.7	-0.5 ± 12.3	3.6 ± 7.3

reference solutions is similar compared to the result for dual-satellite PBD (Table 7), which corresponds to the results in Tables 8 and 9. Nevertheless, for the triple-satellite PBD, the reduced-dynamic baseline solutions, especially baselines involving Swarm-A, have slightly better agreement with the GSOC/DLR orbits.

425 For the Swarm-A/C pair an improvement from 1.6/2.9/1.4 to 1.5/2.6/1.4 mm
426 is obtained, for the Swarm-B/A pair 4.7/6.7/3.5 to 3.3/4.7/3.3 mm, and for the
427 Swarm-B/C pair a slight degradation from 2.9/4.3/3.0 to 3.1/4.6/3.1 mm. It
428 will be assessed in Section 4.4 if the absolute orbit solutions are influenced by
429 the triple-satellite PBD.

Table 10: Comparison between different MODK baseline solutions (triple-satellite PBD) and the baselines derived from the reduced-dynamic GSOC/DLR reference orbits (mean and RMS-about-mean, 10 days). The percentage of epochs with available kinematic solutions is also shown.

Solution	Radial (mm)	Along-track (mm)	Cross-track (mm)	Perc. (%)
MODK Reduced-dynamic				
Swarm-A/C	-0.1 ± 1.5	2.2 ± 2.6	-0.1 ± 1.4	100
Swarm-B/A	0.6 ± 3.3	1.5 ± 4.7	0.1 ± 3.3	100
Swarm-B/C	-0.2 ± 3.1	0.7 ± 4.6	-0.2 ± 3.1	100
MODK Kinematic				
Swarm-A/C	-0.0 ± 13.0	2.2 ± 6.2	-0.1 ± 3.8	95.1
Swarm-B/A	-0.6 ± 22.2	2.3 ± 10.0	0.5 ± 6.2	81.5
Swarm-B/C	1.1 ± 22.5	0.1 ± 10.8	-0.6 ± 6.3	81.2

430 Figure 8 depicts a one day comparison between two kinematic solutions and
431 the GSOC/DLR-derived reduced-dynamic baseline solution for three satellite
432 pairs. It shows periodic peaks, especially for the Swarm-A/C pair whose baseline
433 length is varying between 30 to 180 km. They fly simultaneously over two poles
434 with the smallest distance. However, they also experience the worst consistency
435 in the polar areas. [39, 13, 14] all report that ionospheric activities clearly
436 deteriorate the POD and PBD solutions above the geomagnetic poles. The
437 ionospheric activity became stronger as the 11-year solar cycle was approaching
438 its peak at the end of 2014.

439 Figure 9 takes one example and shows the baseline consistency between the

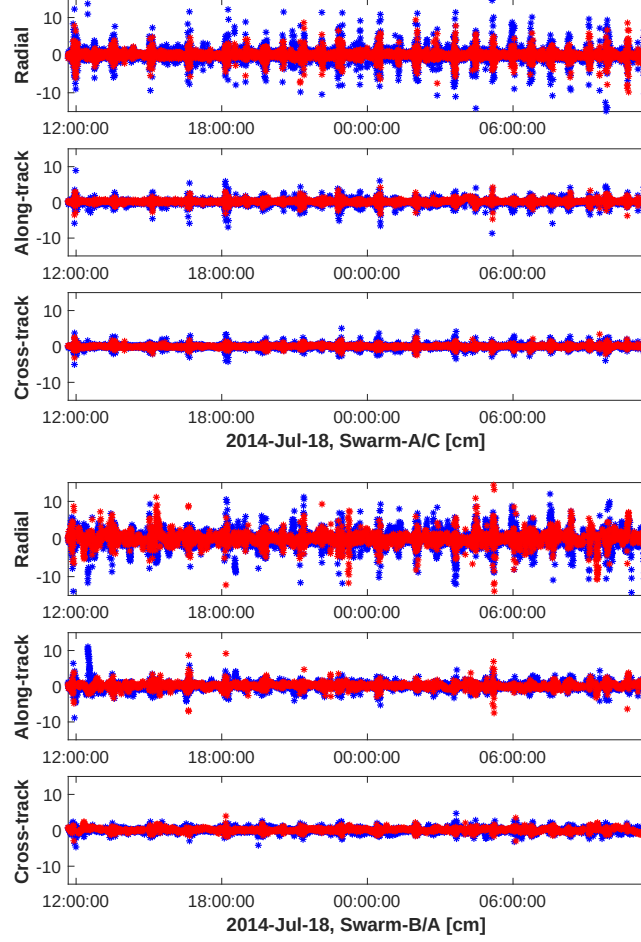


Figure 8: Ephemeris comparison (unit:cm) for the GSOC/DLR(blue) and MODK(red) kinematic baselines for the Swarm-A/C (top), Swarm-B/A(bottom) satellite pairs, the GSOC/DLR DPOD reduced-dynamic baselines are set as reference (DOY 198, 2014). The comparison for Swarm-B/C pair is similar with Swarm-B/A pair.

440 MODK kinematic and reduced-dynamic solutions as a function of the distance
 441 between two associated satellites for a representative day. This consistency
 442 is displayed for each individual direction, where the direction is defined by the
 443 local-horizontal, local-vertical reference frame (*i.e.* radial, along-track and cross-
 444 track direction) of a reference satellite (Swarm-A for Swarm-B/A and Swarm-

445 A/C formations, and Swarm-B for Swarm-B/C formation). Baseline consistency
 446 for the radial direction is the worst, which can be explained by geometry, *i.e.*
 447 the largest component of Geometric Dilution Of Precision (GDOP) is in this
 448 direction.

449 Figure 9 also shows that the availability of kinematic solutions drops when
 450 the distance between the two associated satellites increases. As shown in Fig-
 451 ure 2, the number of simultaneously tracked GPS satellites by two on-board
 452 GPS receivers drops when the distance increases. Eventually, there will not be
 453 sufficient satellites simultaneously in view to compute a kinematic baseline so-
 454 lution. Apparently the spatial geometry for the more dynamic Swarm-B/A and
 455 Swarm-B/C pairs deteriorates more quickly. In general the Swarm-B/A and
 456 Swarm-B/C satellite pairs have only 81.5% and 81.2% of epochs with kinematic
 457 solutions, respectively, compared to 95.1% for the Swarm-A/C satellite pair (see
 458 Table 10). It can be observed in Figure 9 that the consistency between kinematic
 459 and reduced-dynamic baselines solutions become slightly worse with increasing
 460 distance. The consistency statistics are shown in Table 10, which indicate that
 461 13.0/6.2/3.8 mm is achievable for the Swarm-A/C satellite pair in respectively
 462 the radial, along-track and cross-track directions. For the Swarm-B/A satellite
 463 pair, a degraded consistency level of 22.2/10.0/6.2 is obtained, similar to the
 464 Swarm-B/C satellite pair.

465 4.4. *Satellite Laser Ranging*

466 The availability of SLR observations for the Swarm constellation allows for
 467 an independent validation of orbit solutions in the line-of-sight direction between
 468 the SLR ground stations and each LEO satellite [40]. An editing threshold of
 469 30 cm is applied, which is more than an order of magnitude above the RMS of fit
 470 levels. In addition, observations below a 10° elevation cut-off angle are excluded
 471 to eliminate observations with relatively large atmospheric delay correction er-
 472 rors. An SLR retro-reflector correction map from the German Research Center
 473 for Geosciences (GFZ) is included [41]. Furthermore, four SLR stations (Are-
 474 quipa, Hartebeest, Kiev, Simeiz) with large mean offsets are excluded for the

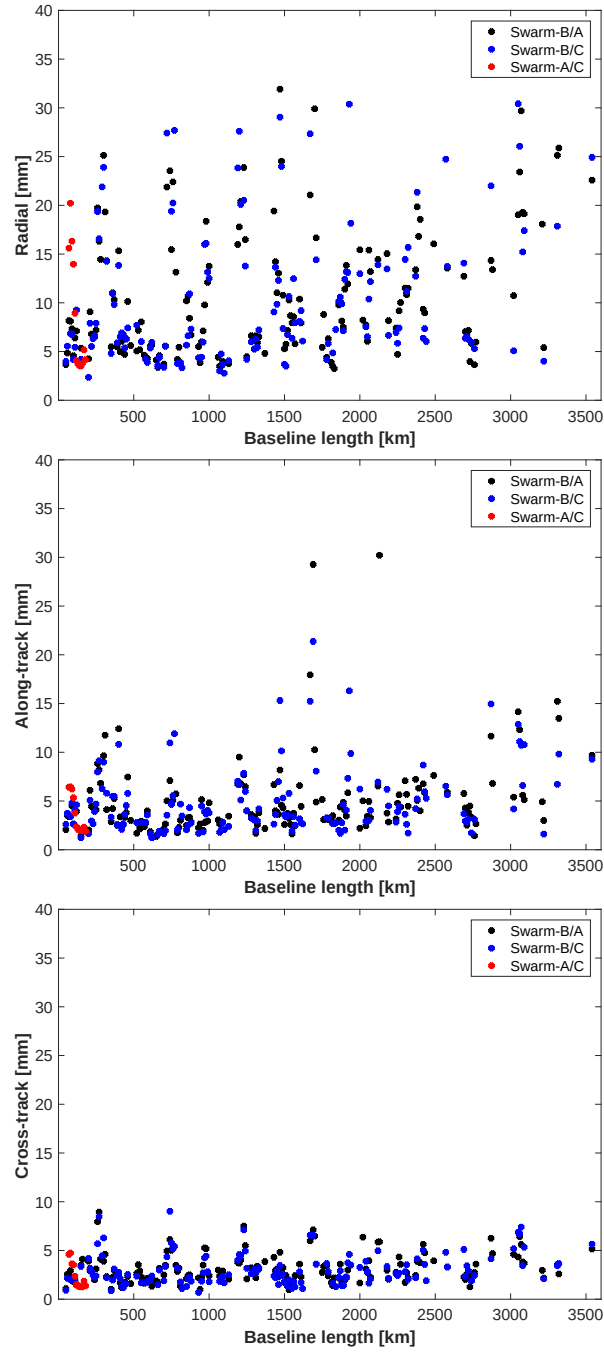


Figure 9: RMS of differences between kinematic and reduced-dynamic solutions as a function of distance (every 10 kms) in the radial (top), along-track (middle) and cross-track (bottom) directions for the three Swarm baselines (DOY 198, 2014).

Swarm SLR validations. Eventually 76.5%(649/848), 80.2%(1385/1726) and 75.3%(510/677) of the SLR observations are used for orbit validation of Swarm-A, -B and -C respectively (Table 11).

It can be observed that for the MODK POD single-satellite orbits the RMS-about-mean of fit of SLR validation is quite close to the reference ESA reduced-dynamic Precise Science Orbits (PSO) [39]. In general, a consistency level (RMS-about-mean) of around 20 mm is achieved for the three Swarm satellites. The best performance is obtained for Swarm-B, which flies at the highest altitude. The best accuracy is found for the GSOC/DLR single-receiver ambiguity fixed solutions. Similar to the analysis in [29, 15], the dual-satellite PBD results in slightly worse SLR consistency levels. Note that for the Swarm-B satellite, the consistency improves for the Swarm-B/C PBD, but not for the Swarm-B/A PBD solution. For the Swarm triple-satellite MODK PBD solution, similar levels are obtained. This indicates good consistency between dual-satellite and triple-satellite modes of MODK.

Table 11: Mean and RMS-about-mean of fit of SLR observations for different reduced-dynamic orbit solutions for the 10 selected orbit arcs.

Solution	Swarm-A (mm)	Swarm-B (mm)	Swarm-C (mm)
ESA	1.5 ± 18.4	-2.8 ± 14.7	1.9 ± 21.0
GSOC/DLR	1.1 ± 17.5	1.0 ± 11.1	1.6 ± 21.2
POD	-1.1 ± 20.8	-4.0 ± 14.1	0.8 ± 21.6
PBD Swarm-A/C	-0.7 ± 21.0	NA	0.7 ± 22.1
PBD Swarm-B/A	-0.8 ± 19.2	-2.2 ± 14.3	NA
PBD Swarm-B/C	NA	-3.7 ± 12.7	1.1 ± 22.3
PBD Swarm-A/B/C	-0.9 ± 19.7	-3.5 ± 12.9	1.3 ± 22.2
No.	649	1385	510

The Swarm-A/C satellites fly in formation with a baseline below 180 km. Therefore it is possible that an SLR station switches between these two Swarm

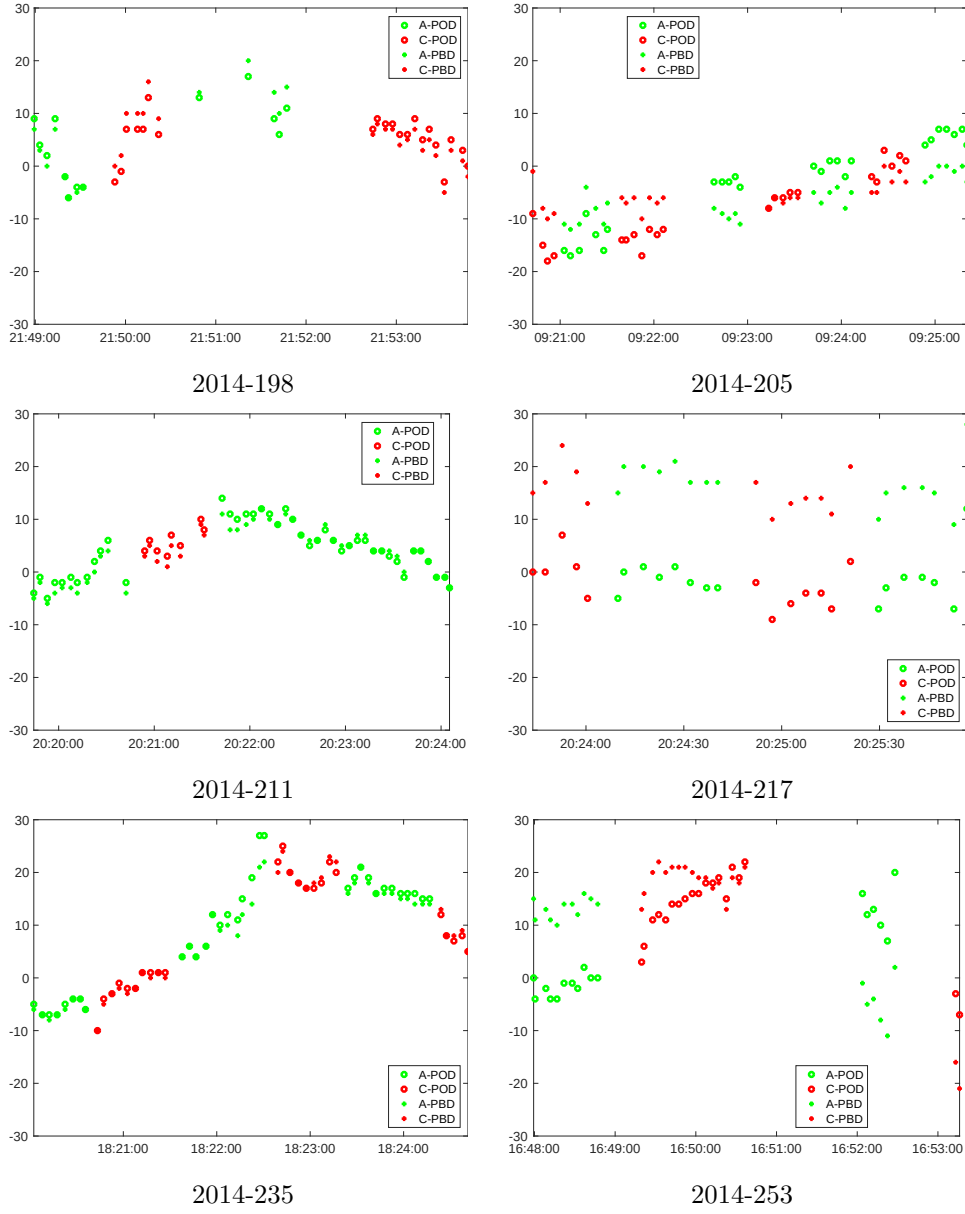


Figure 10: SLR residuals (unit:mm) for the Swarm-A/C single-satellite POD (reference) and dual-satellite PBD orbit solutions by using the well-performing Yarragadee station in Australia. Six tracking passes with more than 27 points are selected. For each pass the DOY in 2014 is indicated.

satellites during one overpass. This offers an additional opportunity to assess the consistency in terms of time series between the two different orbit solutions and the SLR observations. The Yarragadee station in Australia offers the largest number of such overpasses and is therefore selected for this analysis.

When tracking the Swarm-A and C satellites, normally the Yarragadee tracking switches happen 1 to 6 times during the satellite overpass, which typically has a duration of only a few minutes. Figure 10 shows that for DOY 205 in 2014, the SLR residuals are better aligned in time when using the Swarm-A/C dual-satellite PBD solution. For other passes displayed in Figure 10, consistency is at the same level for the PBD solutions as compared to the POD solutions. This result agrees well with results reported in [14] and also similar analysis for the TanDEM-X/TerraSAR-X formation as reported in [42].

Another assessment is done to check the alignment of Swarm-A and -C satellite orbits based on the Swarm-B/A and Swarm-B/C PBD on DOY 205 in 2014. The STDs of all Swarm-A and -C SLR residuals for a tracking pass are computed. A smaller STD means two satellite orbits align closer with the same reference SLR ground station, or in other words, it represents better alignment between two orbits. The STDs of Swarm-A and -C satellite SLR validation residuals for this orbit pass are 7.78, 3.36, 3.12 and 2.48 mm for the single-satellite POD, Swarm-A/C dual-satellite PBD, triple-satellite PBD and the Swarm-A/C baseline based on the Swarm-B/A and Swarm-B/C PBD, respectively. Clearly the alignments for the latter three solutions are very close and are better than the single-satellite POD orbits. The PBD seems to improve the SLR consistency between the Swarm-A and -C satellites for this day. This demonstrates the benefits of relative dynamics constraints between the higher Swarm-B and either of the lower Swarm satellites.

5. Conclusions and Recommendations

The three-satellite Swarm constellation has been used as test bed for Swarm dual- and triple-satellite orbit determination, where two of the satellites are fly-

ing in formation and the third one flies in a different orbit. Thus, in addition to
 relatively slowly varying baselines, also fast changing or high-dynamic baselines
 are included in the tests. Three different Swarm satellite pairs and thus baselines
 can be defined: the pendulum baseline (Swarm-A/C) and two high-low base-
 lines (Swarm-B/A and Swarm-B/C), where the high-low baselines can typically
 be formed during limited periods every 6.1 days. For the latter, the baseline
 varies from 50 km to 3500 km for orbital arcs with a duration of 24-hr centered
 around the time of closest approach. Precise Baseline Determination (PBD)
 for Swarm involving the Swarm-B satellite is challenging because of different
 levels of dynamic force modeling uncertainty, where it is expected that this is
 different for Swarm-A and -C. An Iterative Extended Kalman Filter (IEKF) in
 combination with subset ambiguity fixing is used to compute reduced-dynamic
 PBD solutions for Swarm. Kinematic PBD solutions are then obtained by using
 the fixed ambiguities obtained from the reduced-dynamic solutions.

Results show that the GPS receiver RINEX converter and half-cycle to full-
 cycle ambiguities corrections are very beneficial for PBD. The Swarm reduced-
 dynamic baseline comparisons with external orbits from the German Space Op-
 erations Center (GSOC/DLR) show good baseline consistency at a level of only
 1-3 mm for the pendulum Swarm-A/C satellite pair. For the other two pairs, a
 consistency at a level of 3-5 mm is achieved for different directions. The overall
 MODK kinematic baseline consistencies with its reduced-dynamic baseline are
 at a level of 13/6/4 mm for Swarm-A/C and a level of 23/11/7 mm for the
 other two pairs (radial/along-track/cross-track). They are better than the in-
 ternal consistencies between two GSOC/DLR solutions and again indicate the
 benefits of constraining relative dynamics and fixing Double-Difference (DD)
 carrier phase ambiguities. However it has to be noted that these consistencies
 deteriorate when baselines increase.

The research in this paper has shown that triple-satellite PBD including
 high-dynamic baselines leads to comparable performance in terms of kinematic/reduced-
 dynamic baseline consistencies and SLR observation fits as dual-satellite PBD.
 The inclusion of high-dynamic baselines does thus not degrade the quality of the

orbit solutions as was the case in *e.g.* [15]. Compared to single-satellite POD, it was shown that a better Swarm-A/C consistency can be obtained in the time series of SLR observation residuals.

It has also been shown that the consistency between kinematic and reduced-dynamic baseline solutions deteriorates with growing distance, which can be explained to a large extent by a less favorable geometry. A possibility for improvement might be to combine the single-satellite ambiguity fixed method with the PBD ambiguity fixing method used in this paper. This is a nice topic for future research. The single-satellite ambiguity fixed solutions lead to larger kinematic/reduced-dynamic consistency levels at short distance (Table 7), but might suffer less from a deteriorated geometry for longer distances.

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