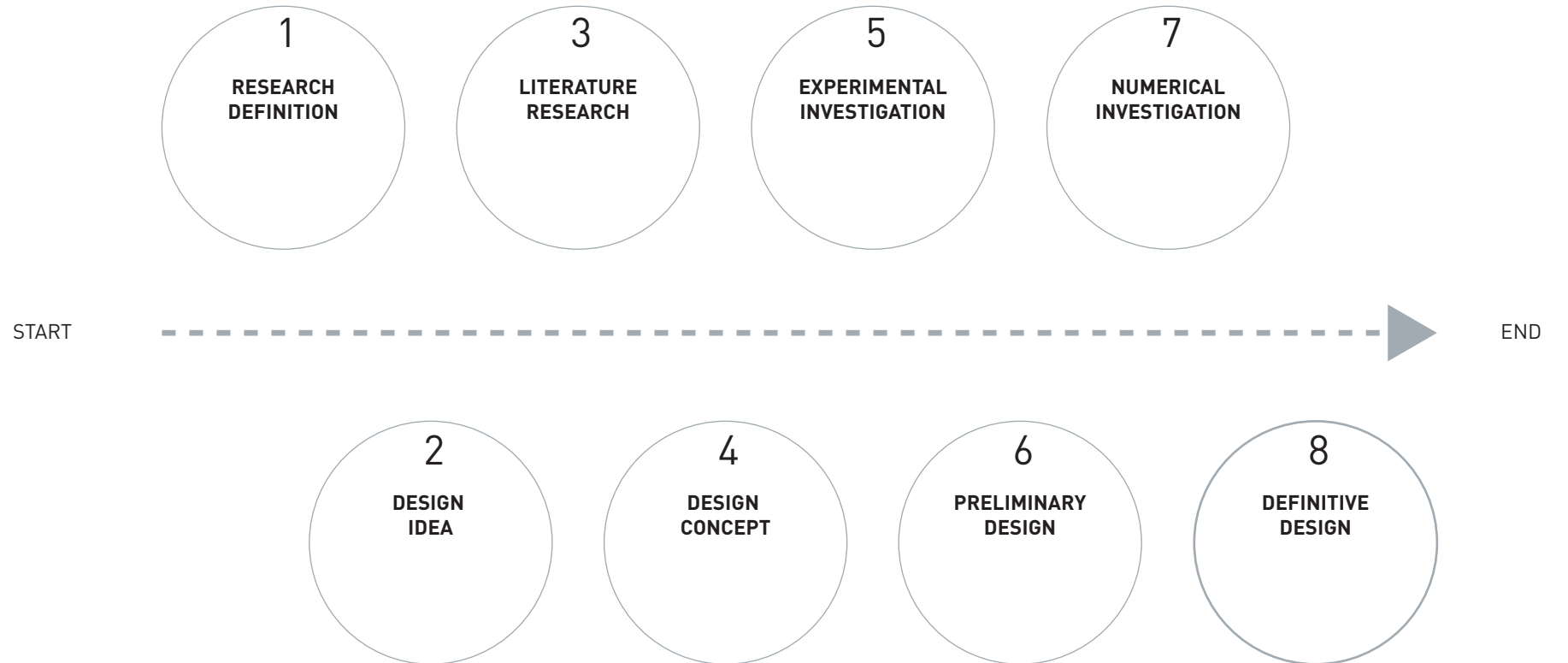


RENS OTTENS P5 PRESENTATION

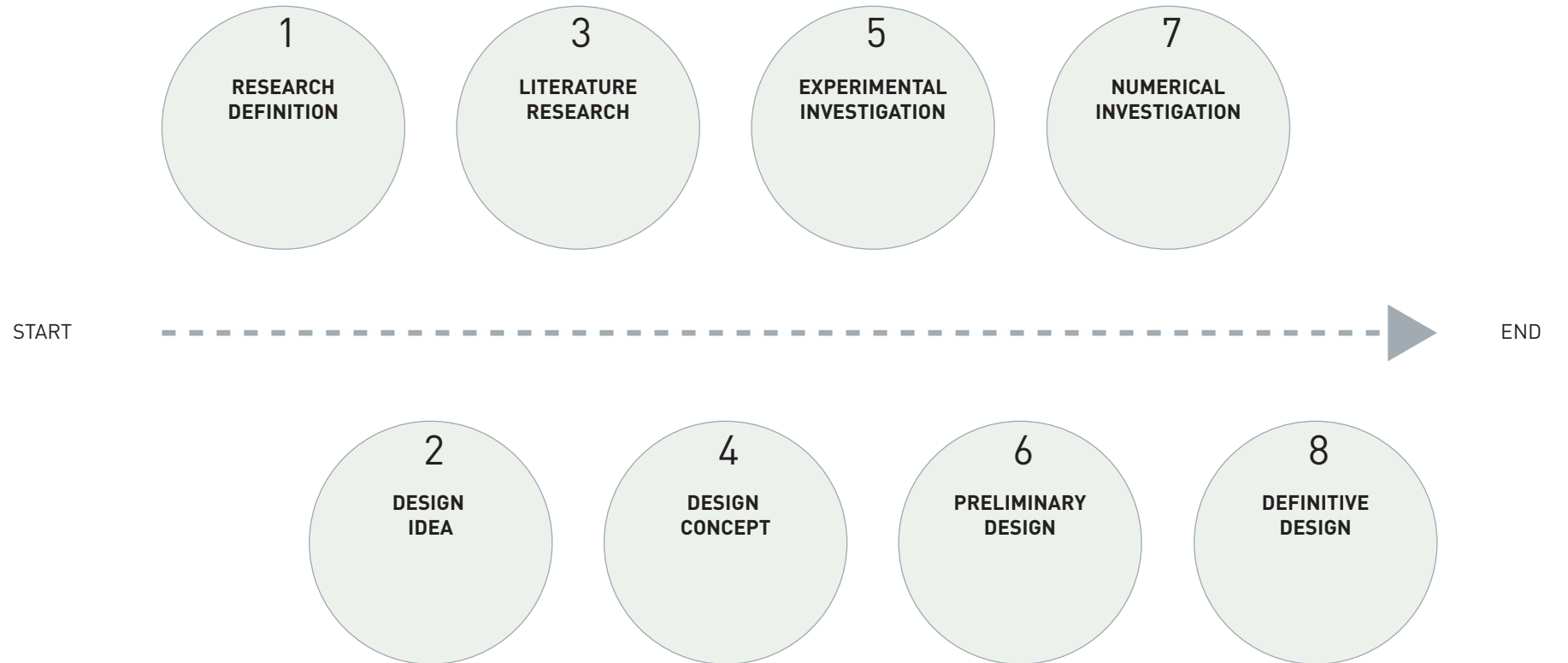
JANUARY 30TH, 2018

HIGH STRENGTH THIN GLASS AS STIFF STRUCTURAL FABRIC

CONTENT PRESENTATION



CONTENT PRESENTATION



INTRODUCTION

HIGH STRENGTH THIN GLASS *AS* **STIFF STRUCTURAL FABRIC**

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HIGH STRENGTH
THIN GLASS

POTENTIALS

KNOWLEDGE GAP

USED IN CONSUMER ELECTRONICS



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HIGH STRENGTH
THIN GLASS

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KNOWLEDGE GAP

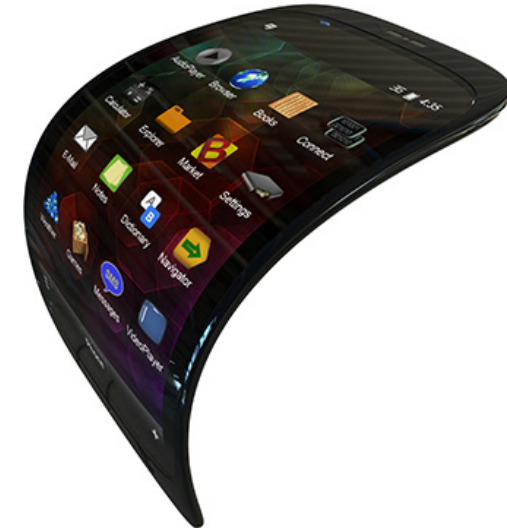
USED IN CONSUMER ELECTRONICS



Thinner



Stronger



Flexible

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USED IN CONSUMER ELECTRONICS



Thinner



Stronger



Flexible

Exceptional scratch resistance

Lightweight

Higher impact resistance

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USED IN CONSUMER ELECTRONICS



Thinner

Stronger



Flexible

Exceptional scratch resistance

Outstanding optical clarity

Superior touch sensitivity

Lightweight

Higher impact resistance

Durable

INTRODUCTION

MIGHT RESULT INTO MORE LIGHTWEIGHT, CURVED, TRANSPARENT STRUCTURES

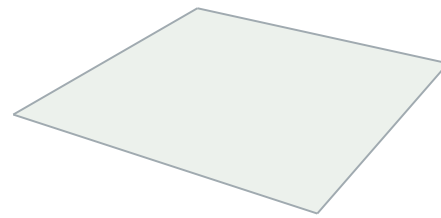
HIGH STRENGTH
THIN GLASS

POTENTIALS

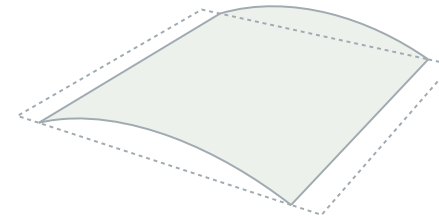
KNOWLEDGE GAP



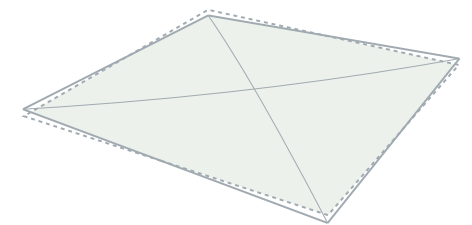
HIGH STRENGTH THIN GLASS SHAPES



1. Flat
*creating lightweight
facades*



2. Single curved
*creating curved
facades*



3. Double curved
*creating curved &
geometrical complex
facades*

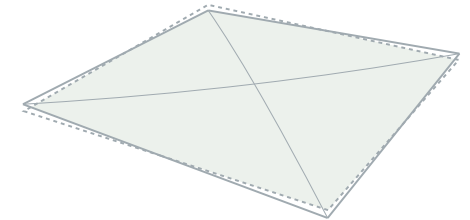
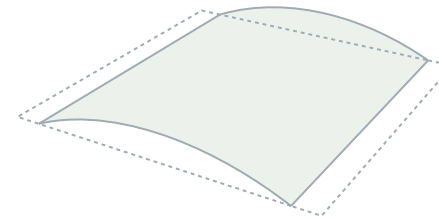
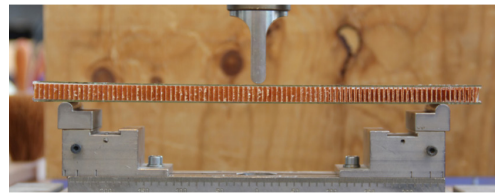
INTRODUCTION

HIGH STRENGTH THIN GLASS

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KNOWLEDGE GAP

EARLIER DONE RESEARCH HIGH STRENGTH THIN GLASS



1. Flat
*by I. van der weijde
(TU Delft, 2017)*

2. Single curved
*creating curved
facades*

3. Double curved
*creating curved &
geometrical complex
facades*

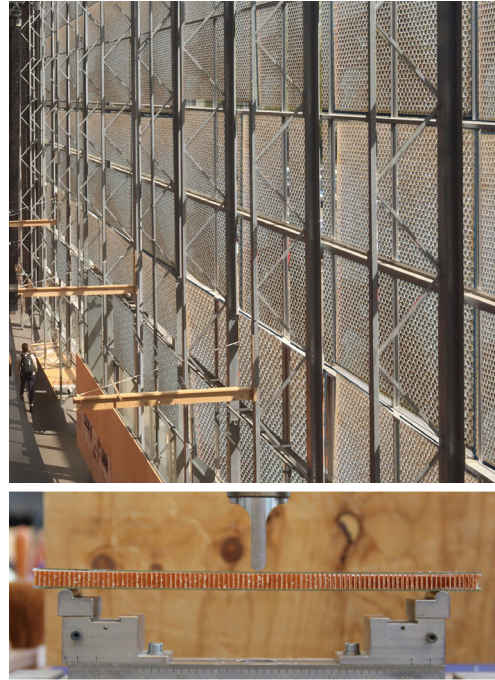
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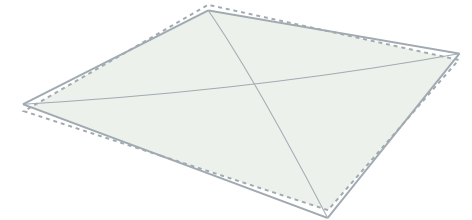
EARLIER DONE RESEARCH HIGH STRENGTH THIN GLASS



1. Flat
*by I. van der weijde
(TU Delft, 2017)*



2. Single curved
*by C. Simoen
(TU Delft, 2016)*



3. Double curved
*creating curved &
geometrical complex
facades*

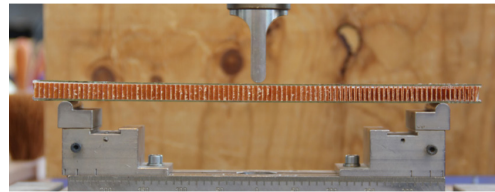
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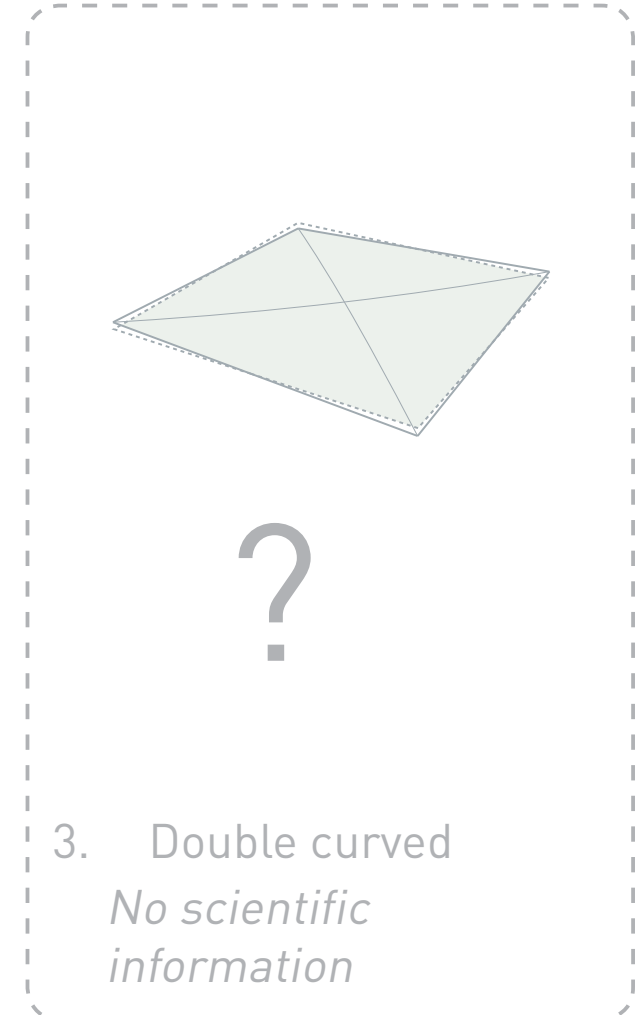
EARLIER DONE RESEARCH HIGH STRENGTH THIN GLASS



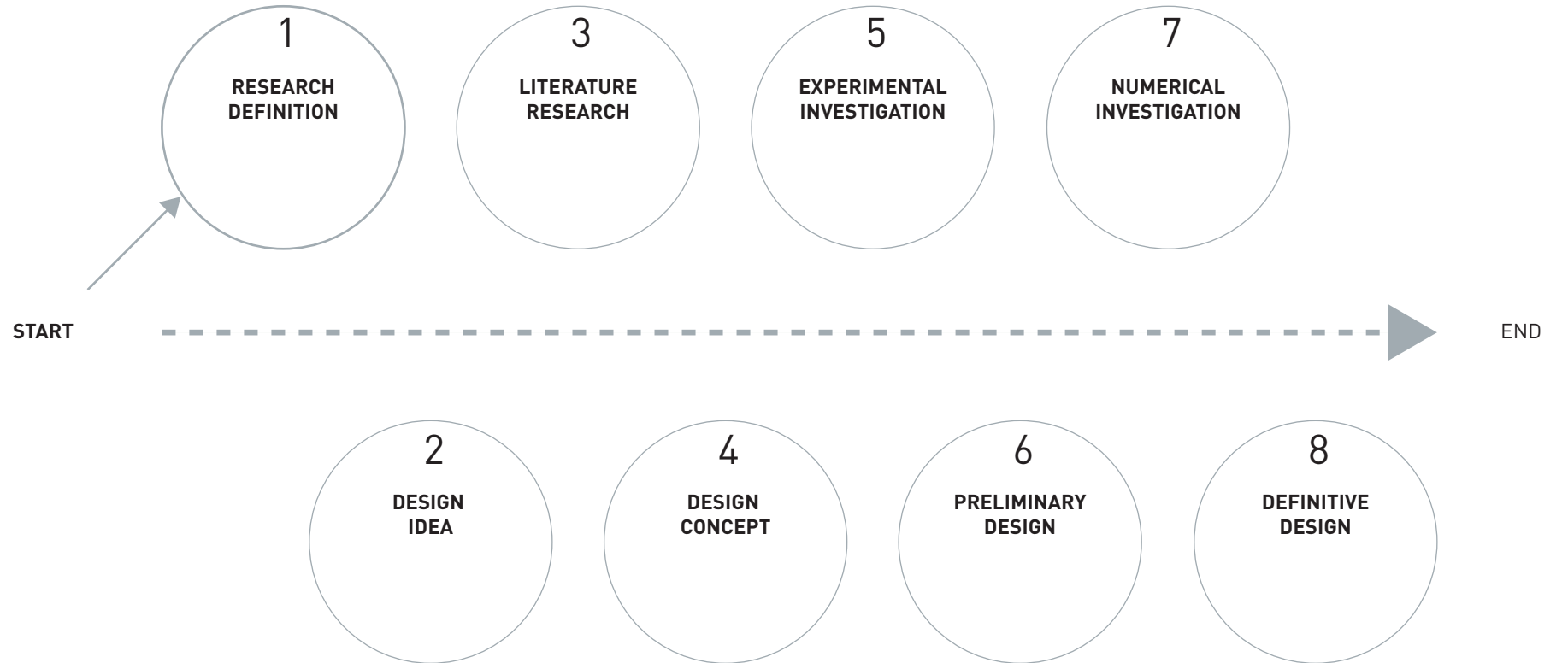
1. Flat
*by I. van der weijde
(TU Delft, 2017)*



2. Single curved
*by C. Simoen
(TU Delft, 2016)*

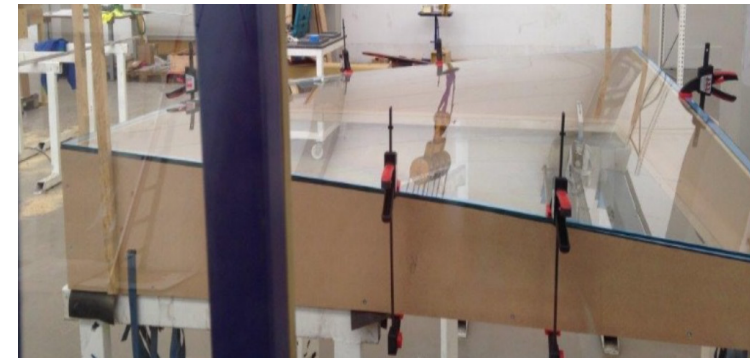
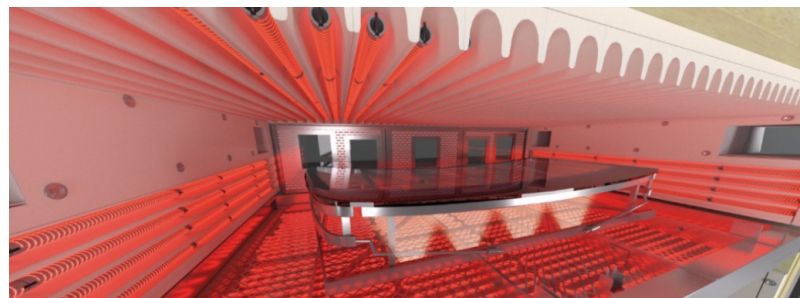


3. Double curved
*No scientific
information*



RESEARCH DEFINITION

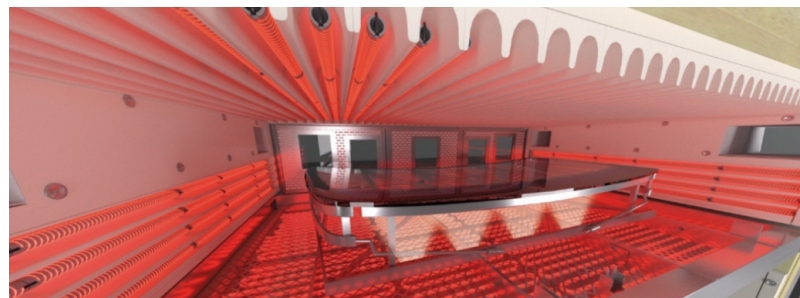
DOUBLE CURVED GLASS



1. Hot bent glass

2. Cold bent glass
*Can only be cold bent with
a curvature in the opposite way:
anticlastic*

DOUBLE CURVED GLASS



1. Hot bent glass



2. Cold bent glass
Research into anticlastic cold bent thin glass....

RESEARCH
DEFINITION

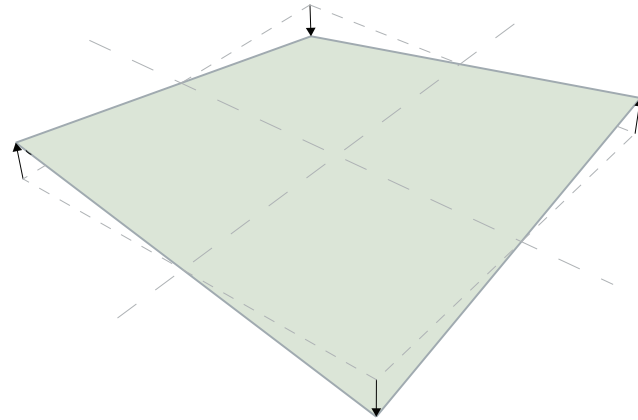
STATE-OF-THE-ART

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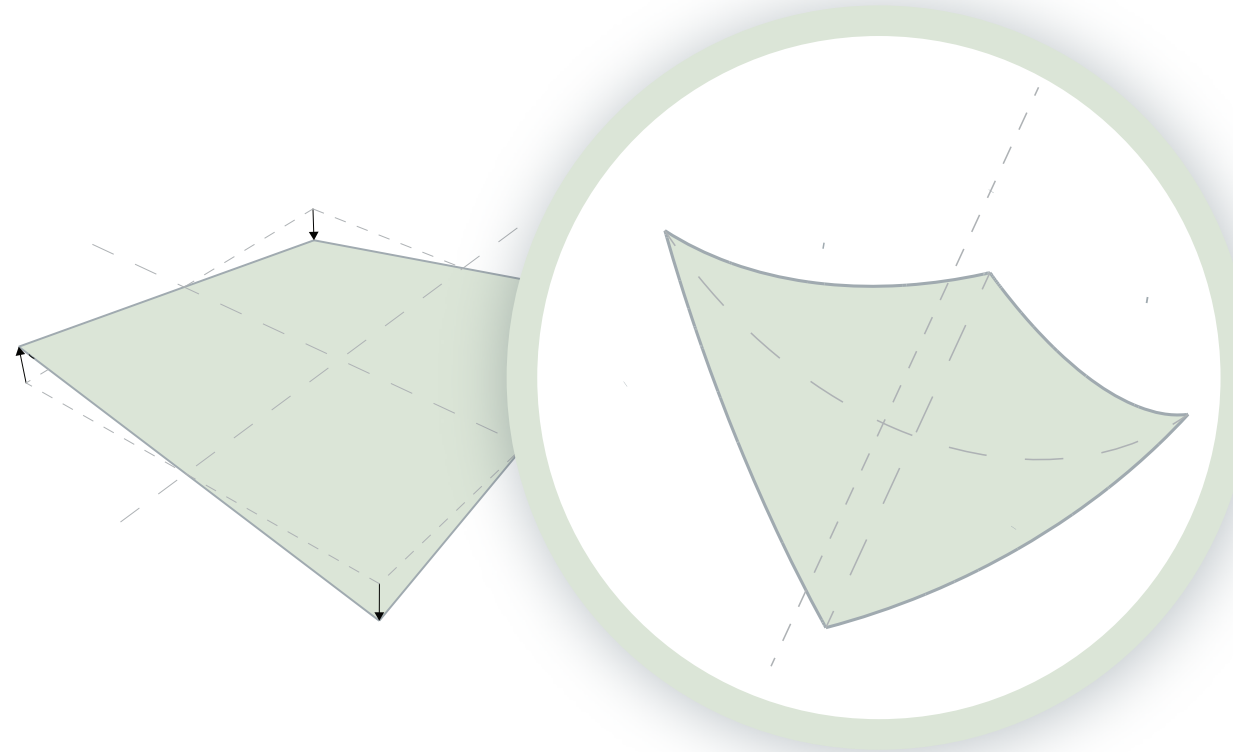
APPROACH

ANTICLASTIC COLD BENT THIN GLASS



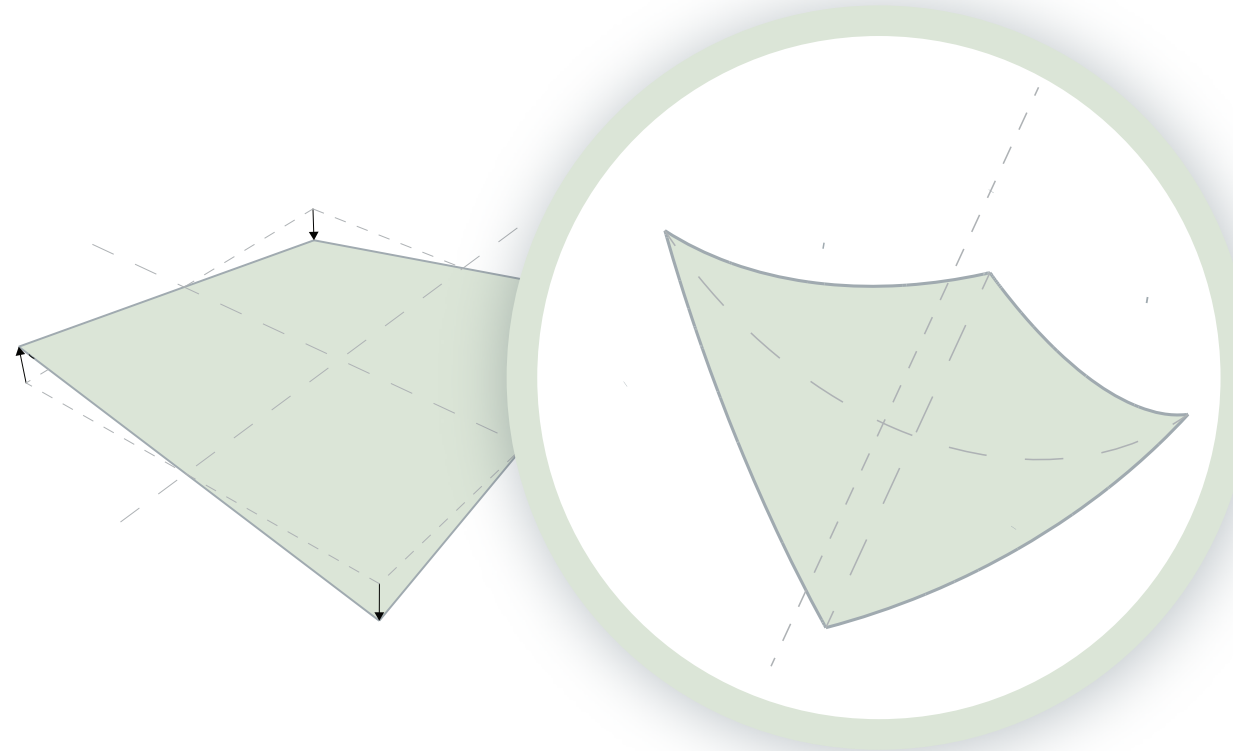
Although it is easier to bend...

DOUBLE COLD BENT THIN GLASS



Although it is easier to bend... **thin glass is more sensitive to buckling.**

DOUBLE COLD BENT THIN GLASS



Although it is easier to bend... **thin glass is more sensitive to buckling.**

*Because of lack of sustain any compressive normal forces: **membrane behaviour.***

*Thin glass probably never have the chance to come in a **metastable configuration.***

RESEARCH
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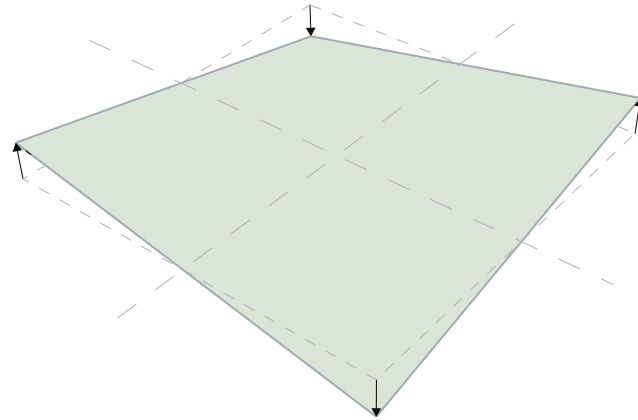
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BASED ON THE **HIGH STRENGTH & MEMBRANE BEHAVIOUR...**



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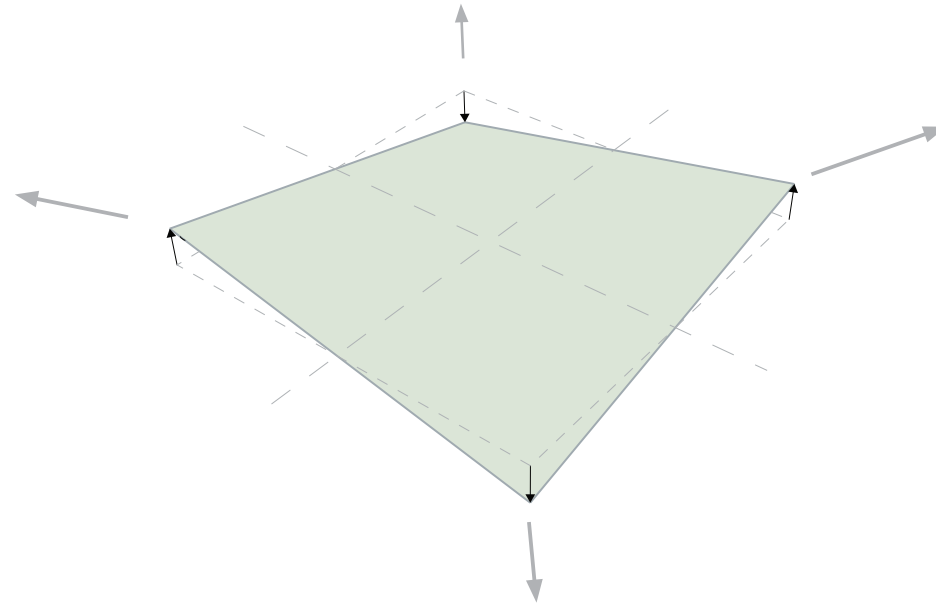
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BASED ON THE **HIGH TENSILE STRENGTH & MEMBRANE BEHAVIOUR...**



INDUCE THE TWISTING BY APPLYING (IN-PLANE) TENSION LOAD

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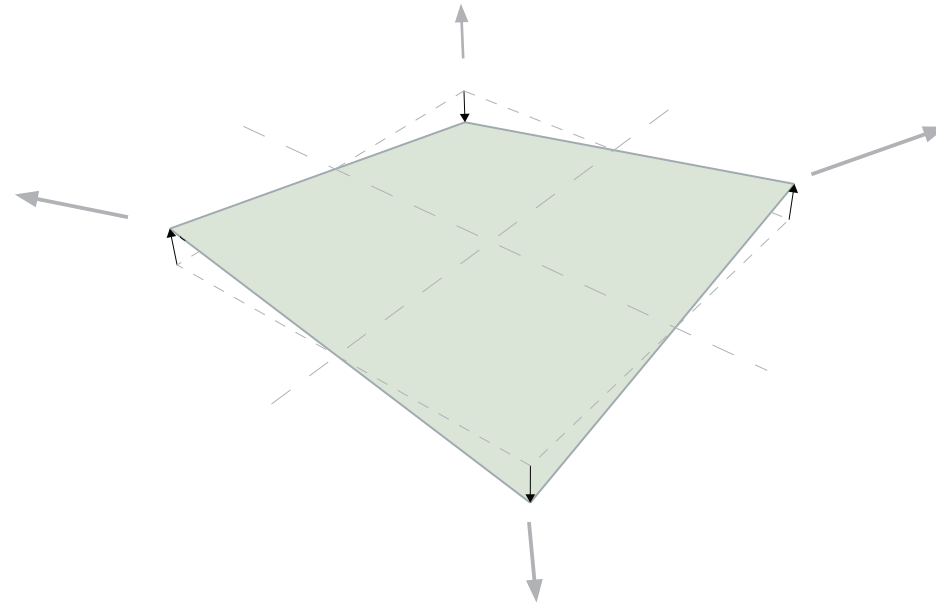
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“TO WHAT EXTENT IS IT POSSIBLE TO CURVE A FLAT SHEET OF THIN GLASS INTO A DOUBLE ANTICLASTIC BENT SURFACE BY ADDING TENSION TO THE CURRENTLY USED COLD TWISTING TECHNIQUE?”



RESEARCH
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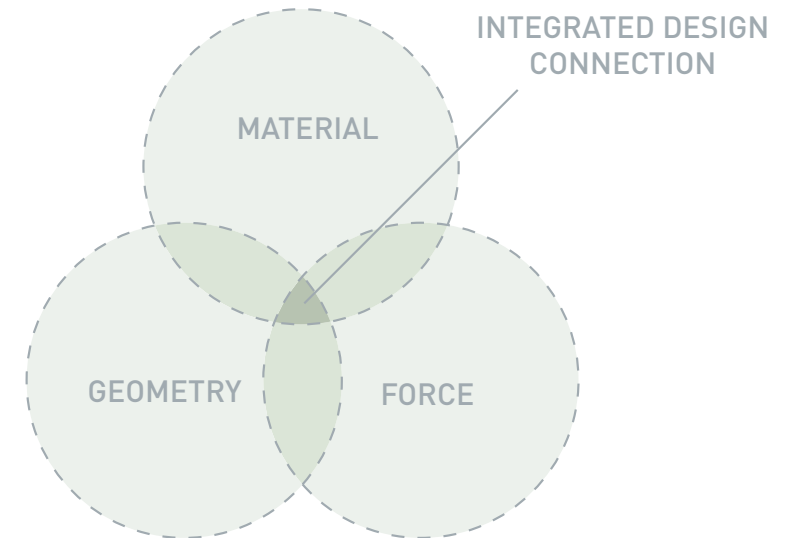
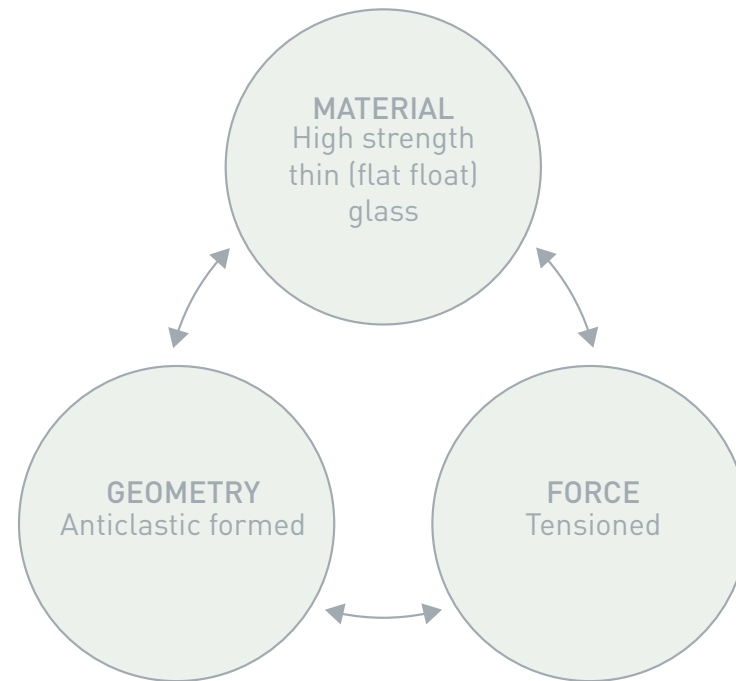
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FROM DESIGN IDEA TO DEFINITIVE DESIGN



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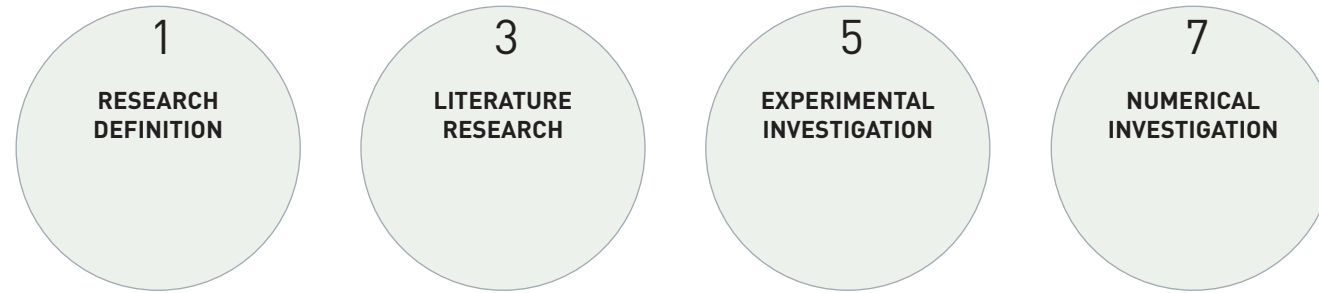
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DESIGN BY RESEARCH

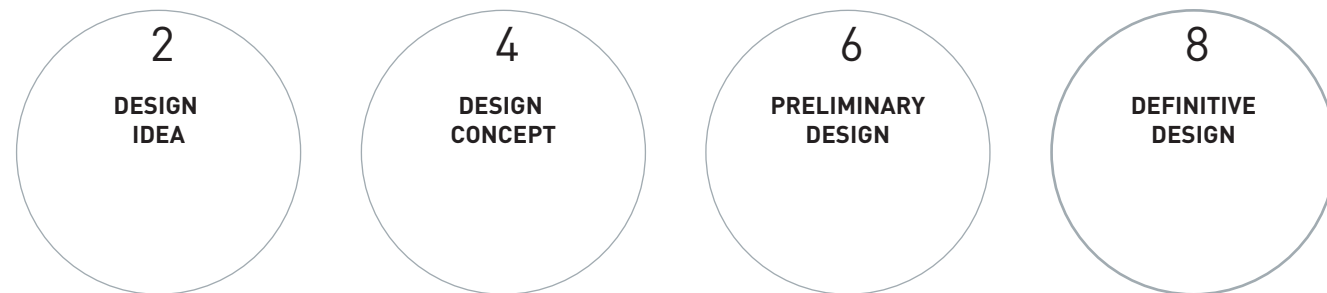
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START



END



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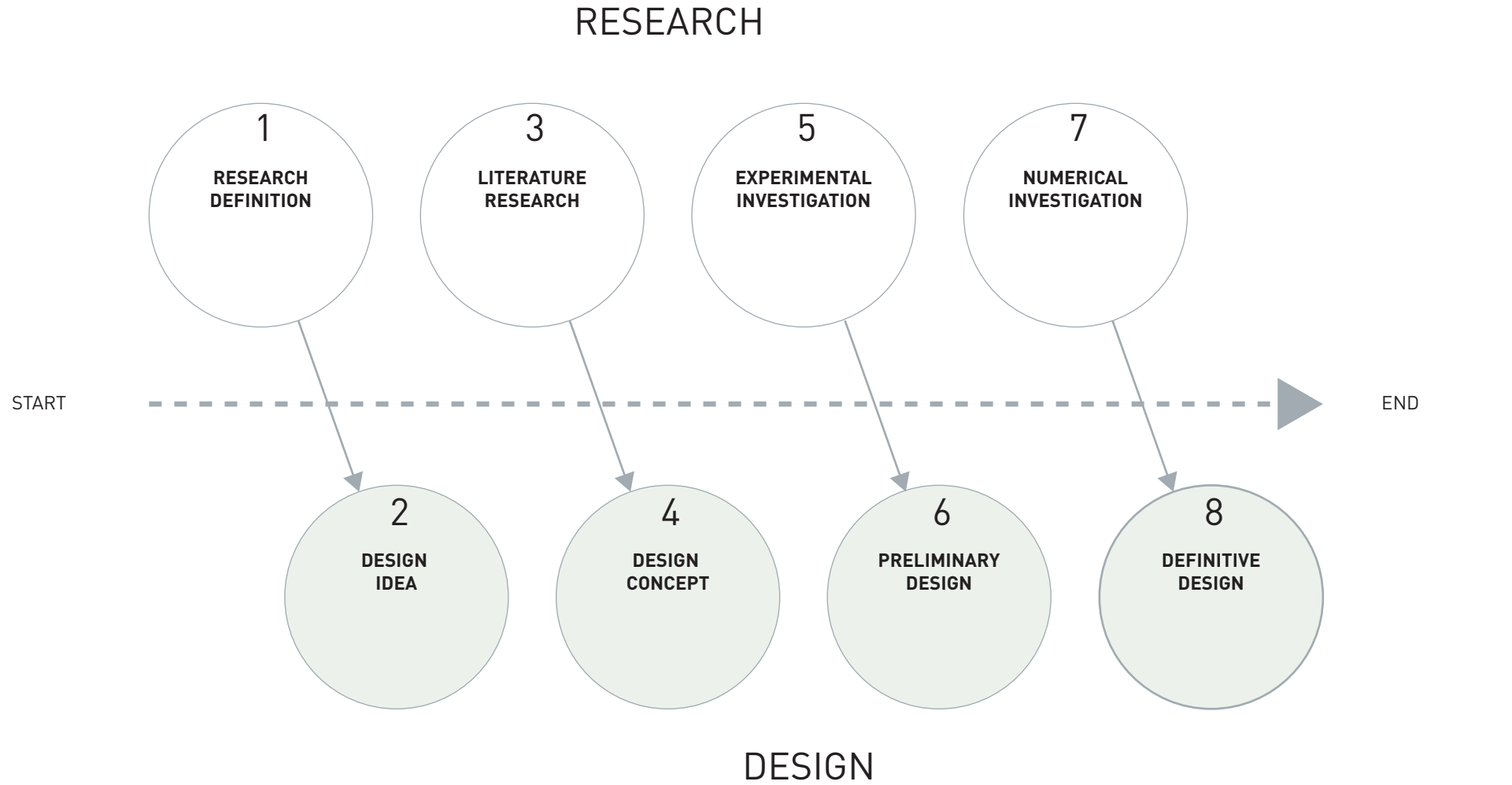
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DESIGN BY RESEARCH



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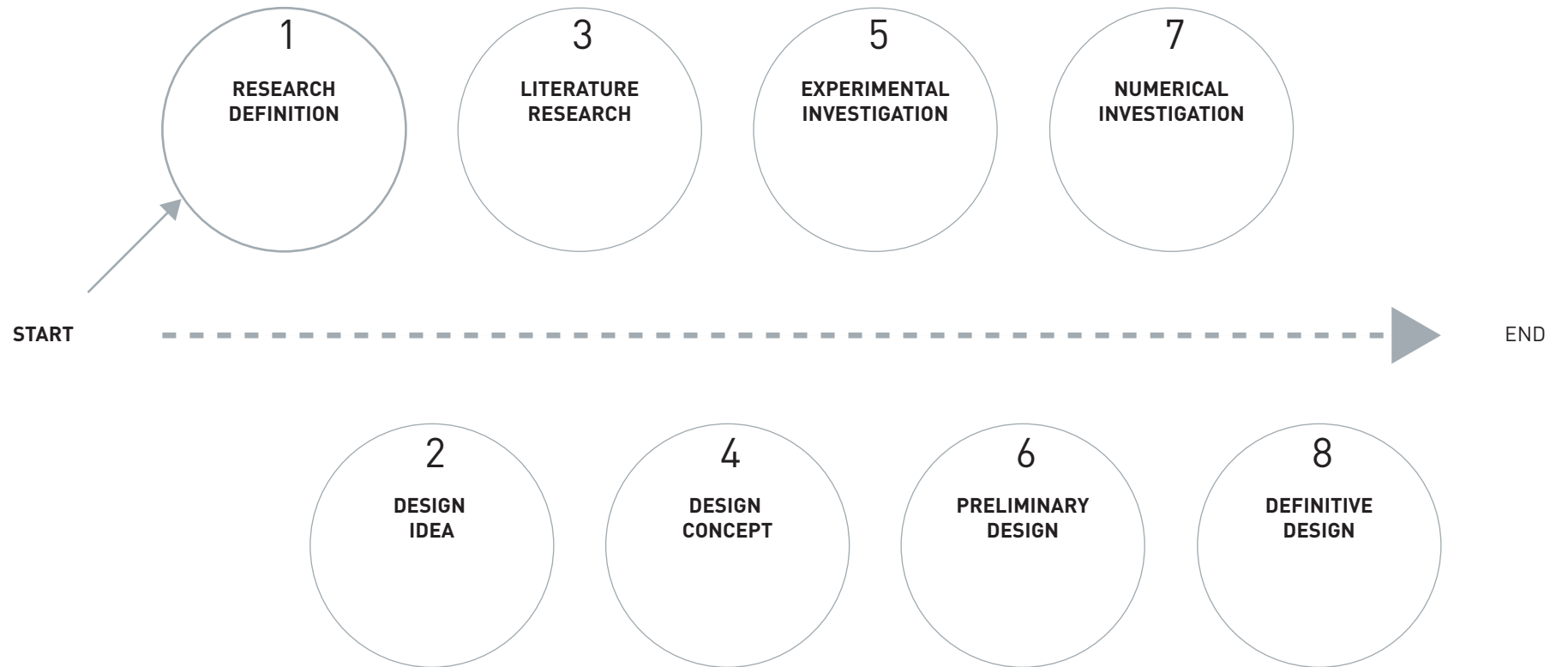
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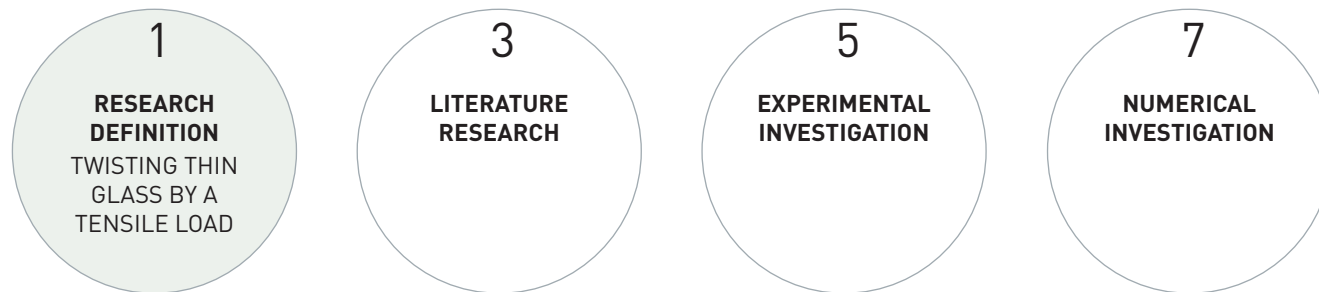
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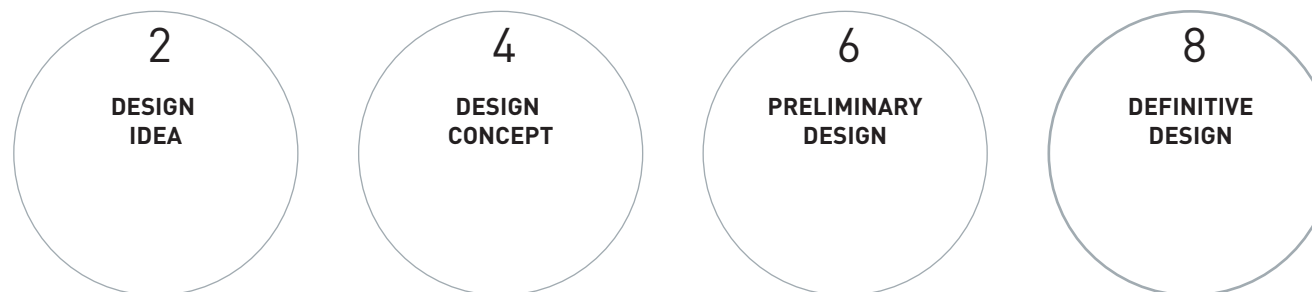


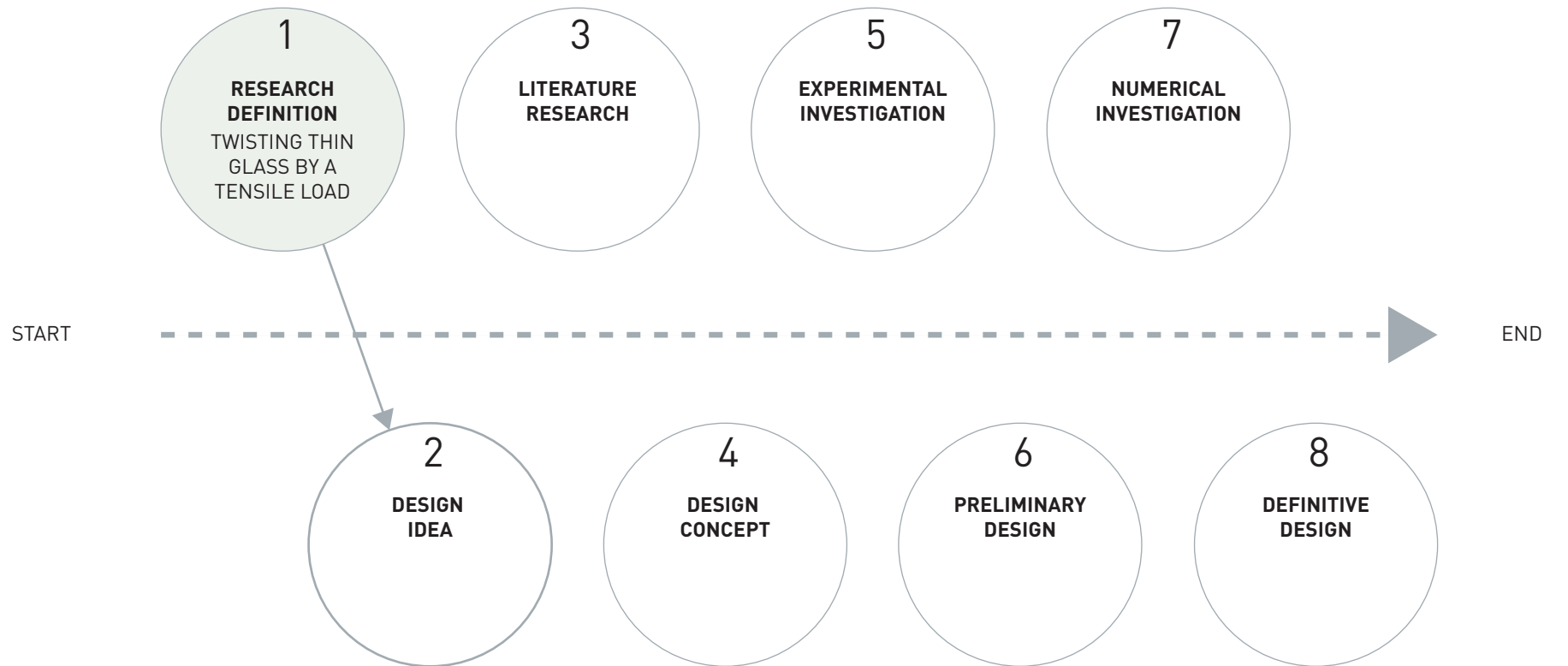


START



END





DESIGN IDEA



Four point fabric structure
design by Frei Otto
Kassel, 1955



Curved glass
demonstrated by Carlyn Simoen
Delft, 2016

IMAGINE TENT STRUCTURES **BUILT OUT OF GLASS**

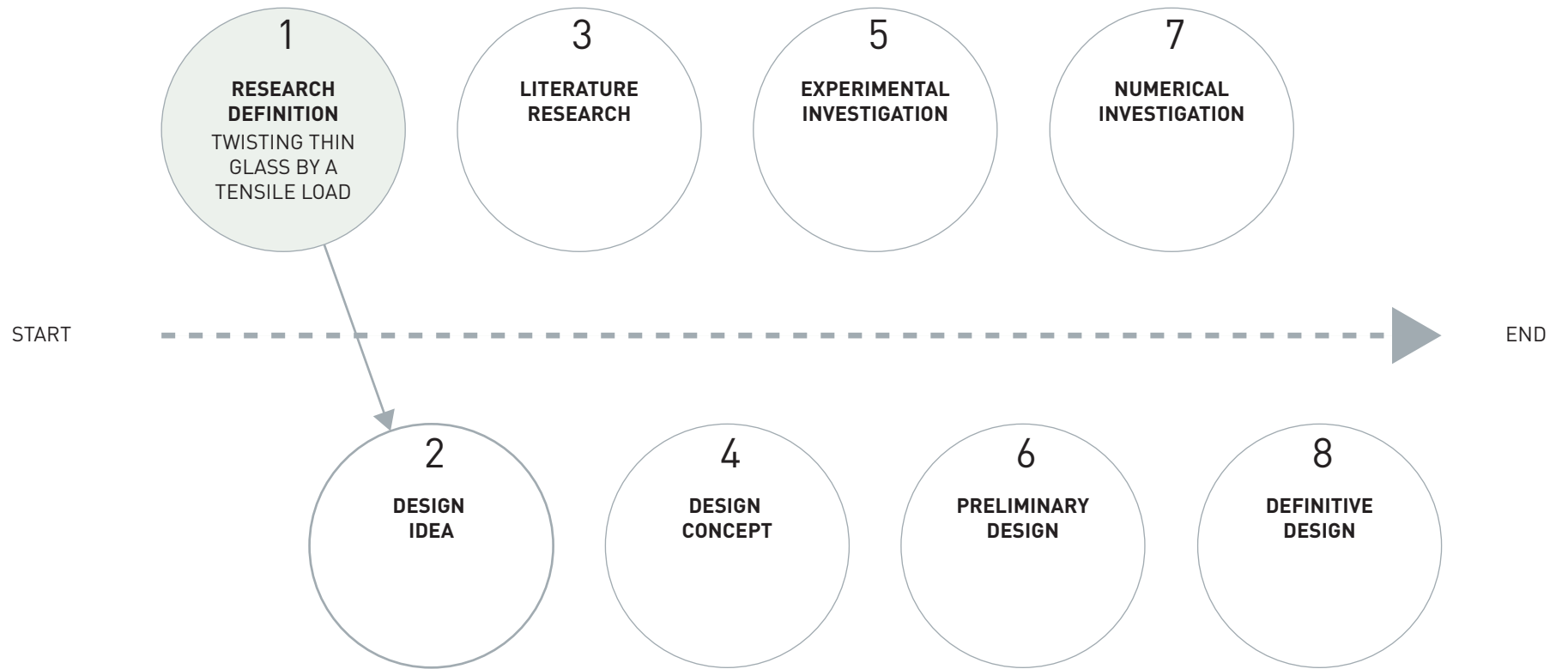


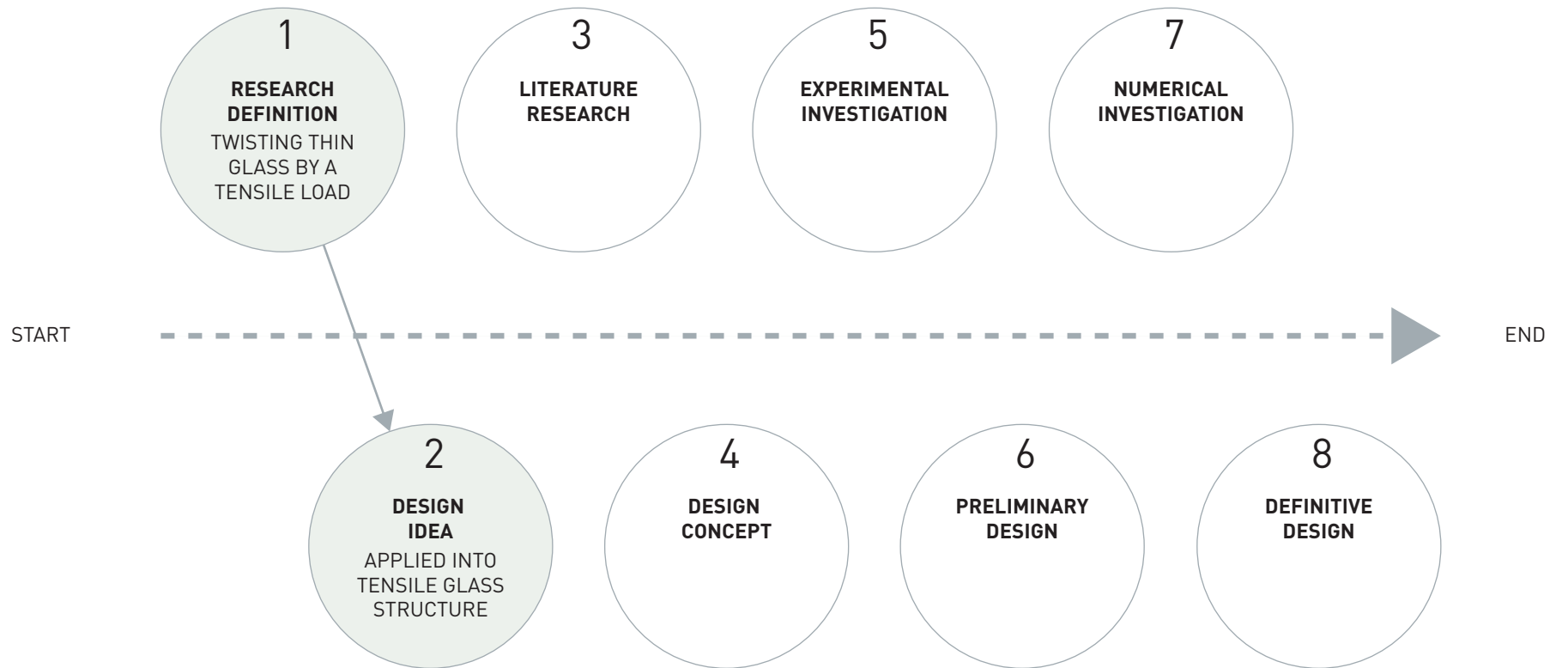
Four point fabric structure
design by Frei Otto
Kassel, 1955

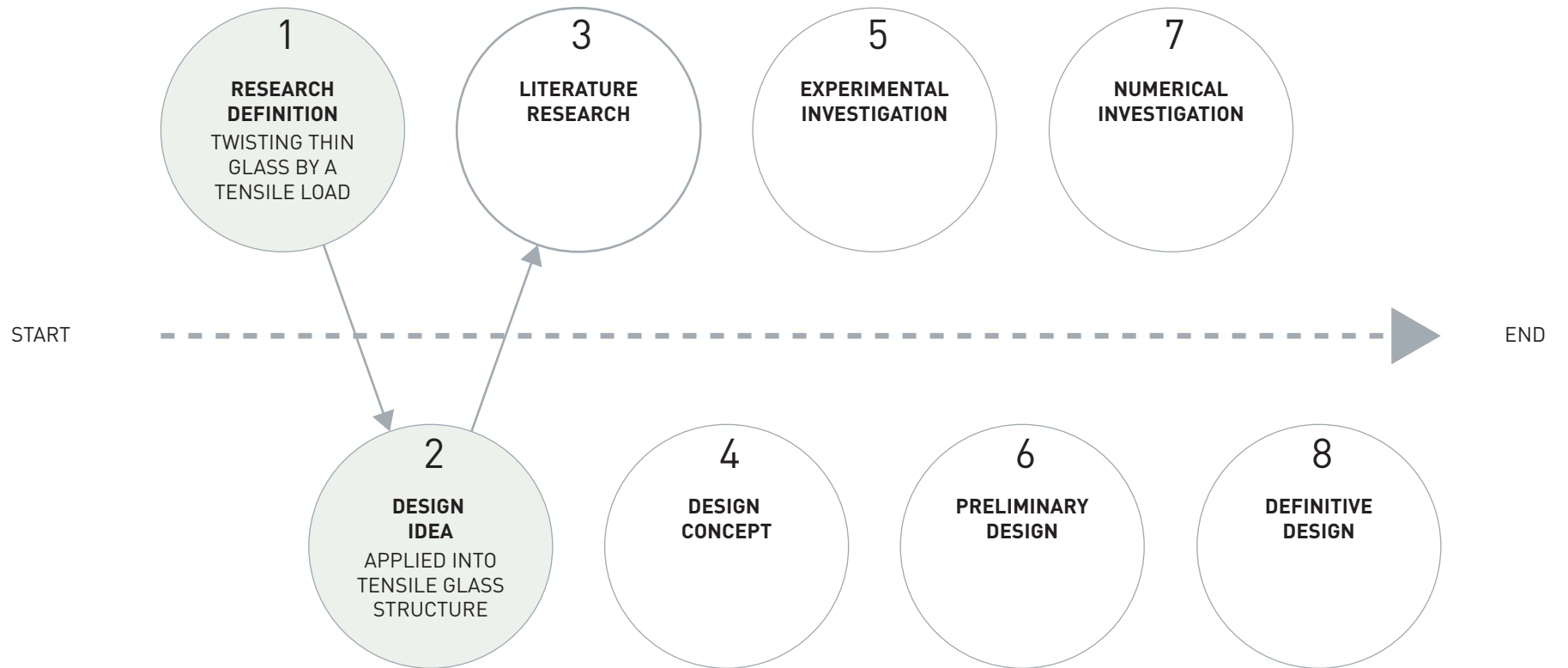


Curved glass
demonstrated by Carlyn Simoen
Delft, 2016

IMAGINE TENT STRUCTURES **BUILT OUT OF *HIGH STRENGTH THIN GLASS***







LITERATURE RESEARCH

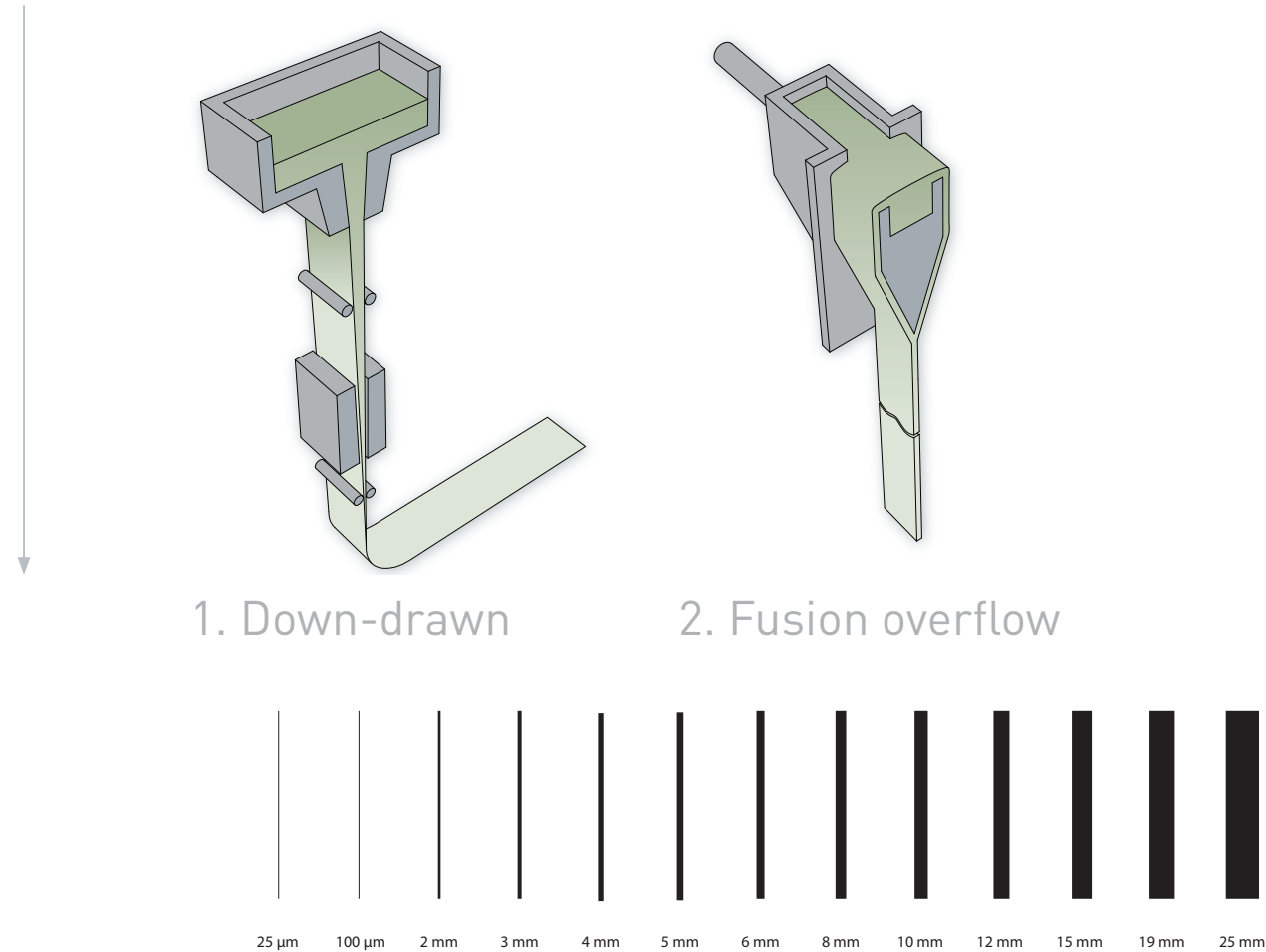
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GLASS AS
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SAFE
STIFF & STABLE
STRONG

VERTICAL PRODUCTION PROCESS FLAT GLASS



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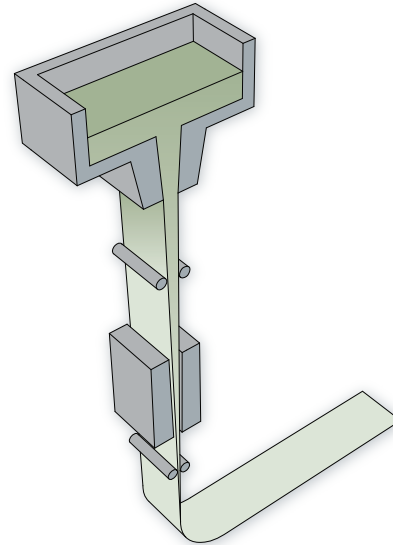
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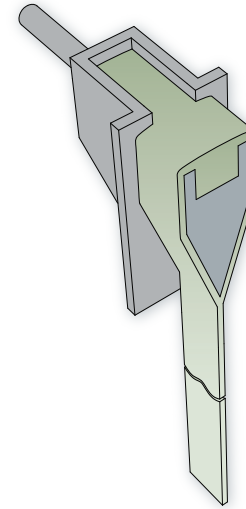
GLASS AS
CONSTRUCTION
MATERIAL

SAFE
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STRONG

VERTICAL PRODUCTION PROCESS (*ULTRA-*) THIN FLAT GLASS

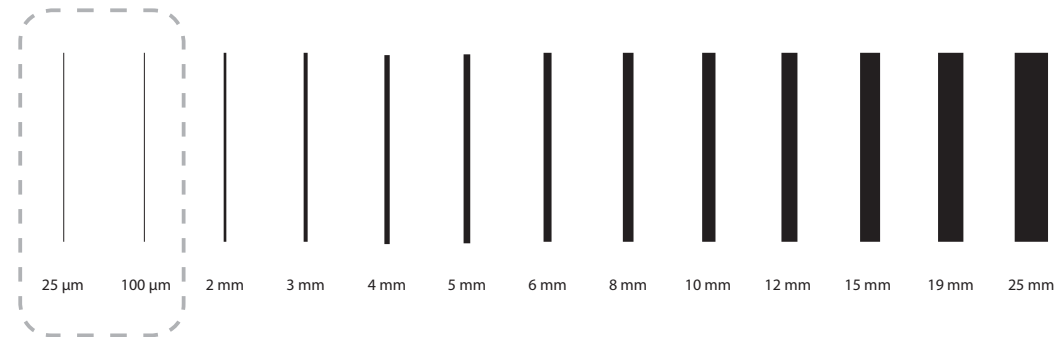


1. Down-drawn



2. Fusion overflow

Ultra-thin
glass



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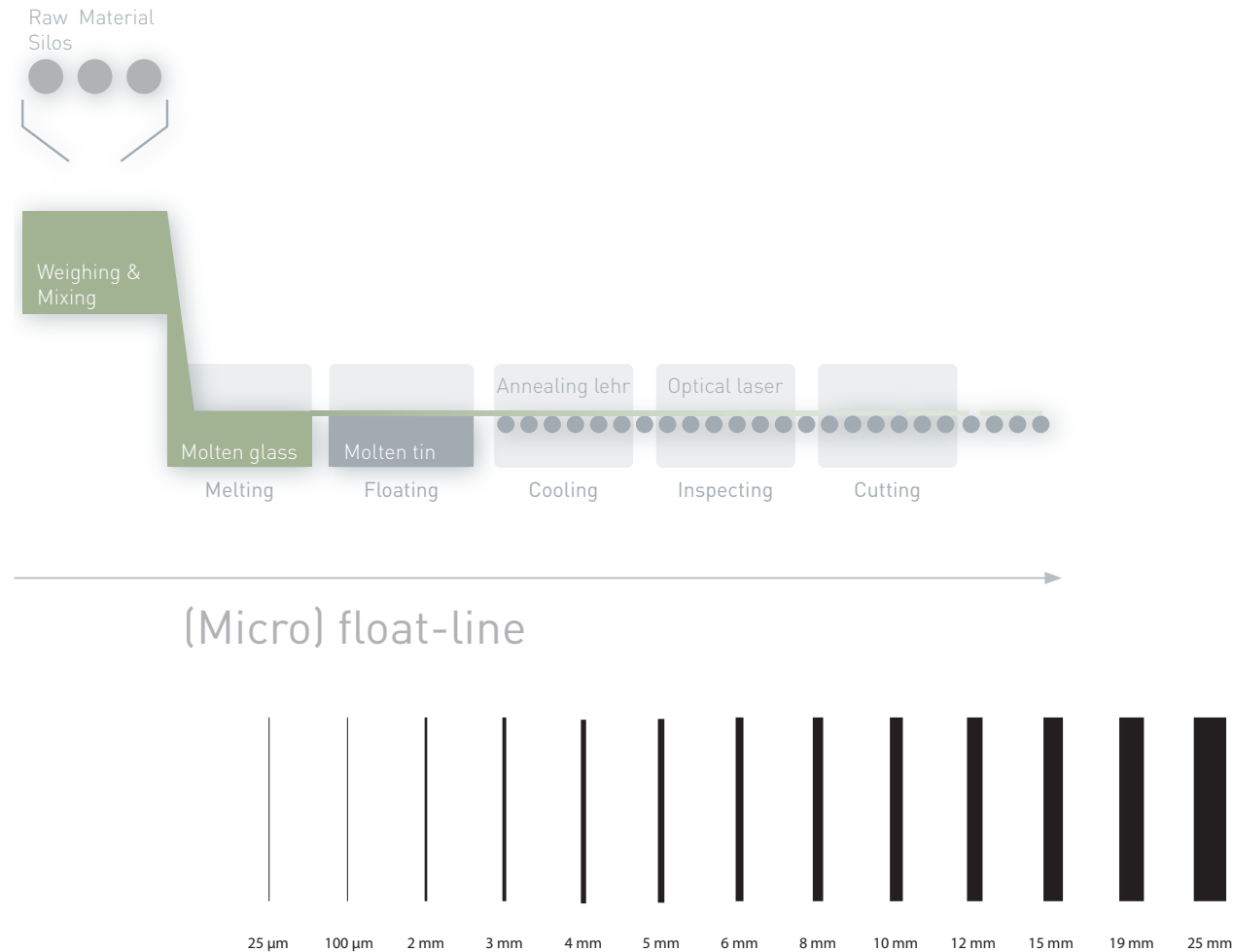
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HORIZONTAL PRODUCTION PROCESS FLAT GLASS



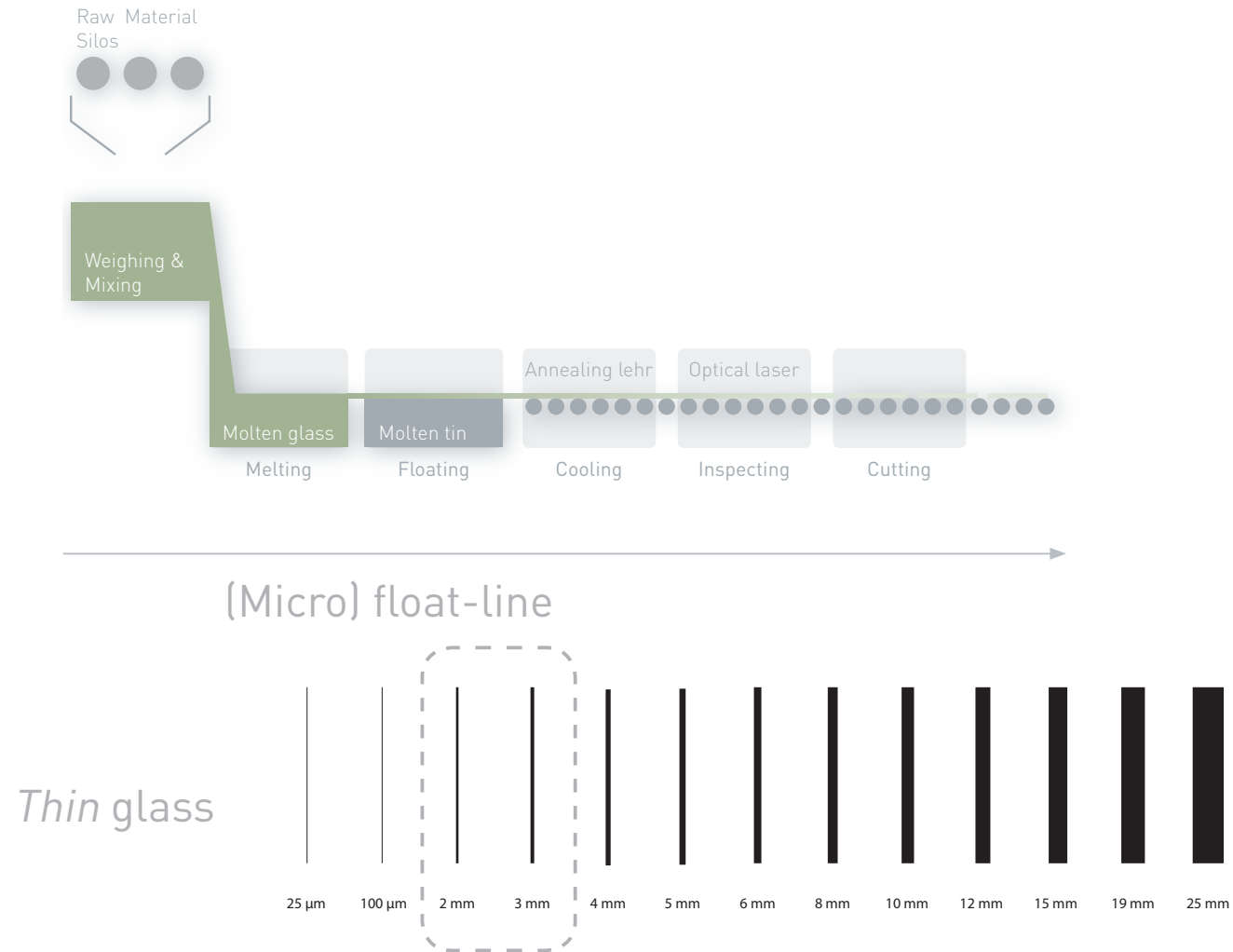
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HORIZONTAL PRODUCTION PROCESS *THIN* FLAT GLASS



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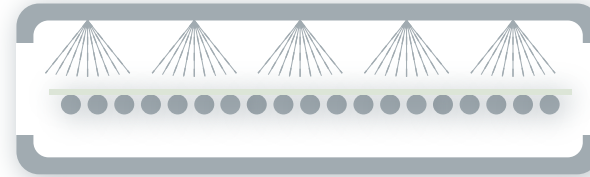
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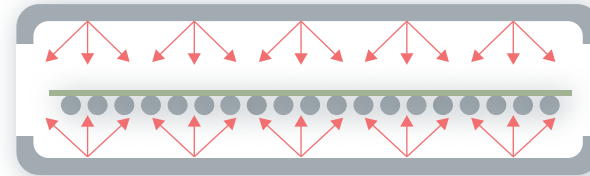
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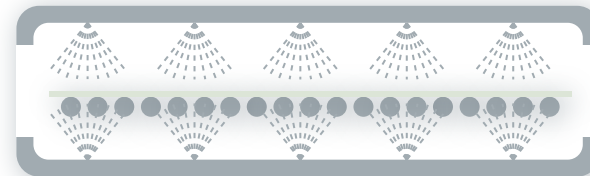
THERMAL TEMPERING



Cleaning



Heating



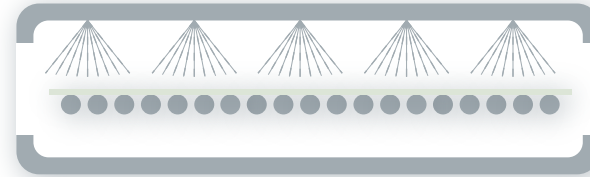
Quenching

In an oven
by temperature

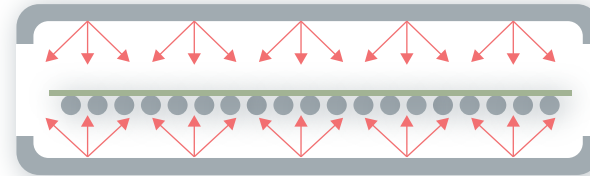
THERMAL TEMPERING

VS.

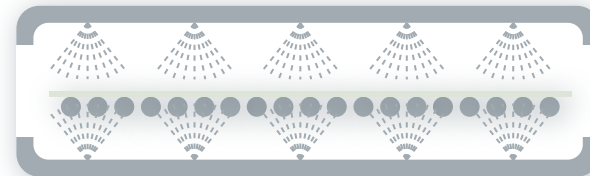
CHEMICAL STRENGTHENING



Cleaning

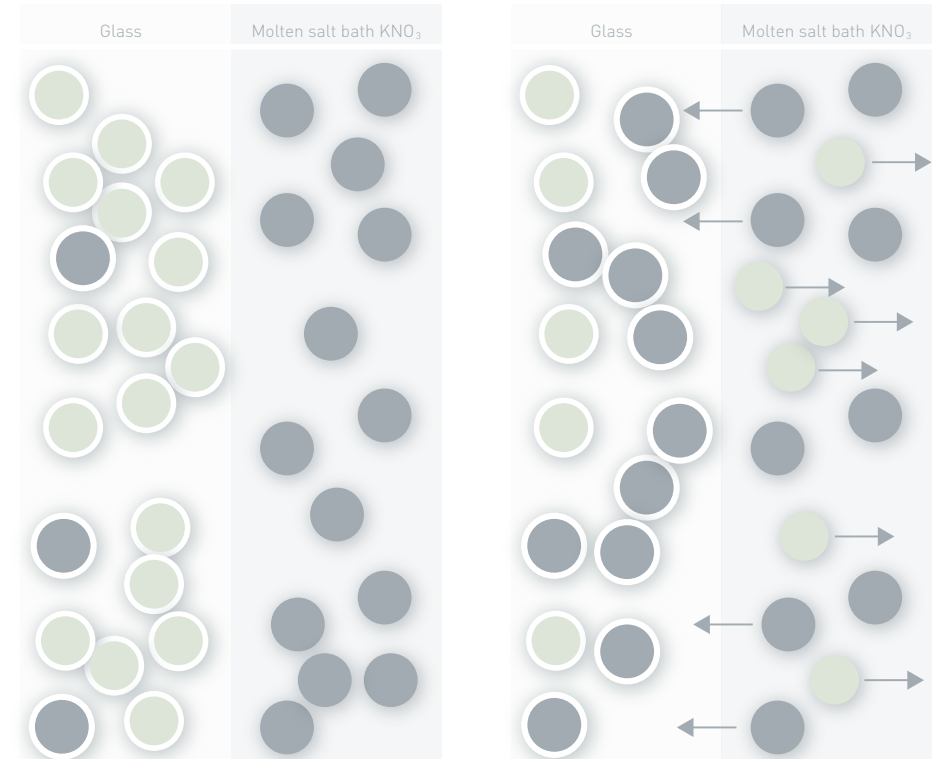


Heating



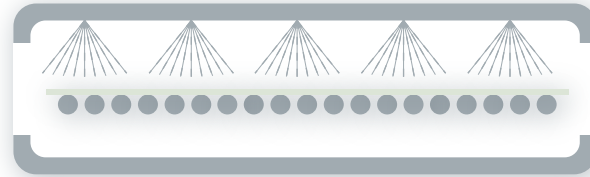
Quenching

In an oven
by temperature

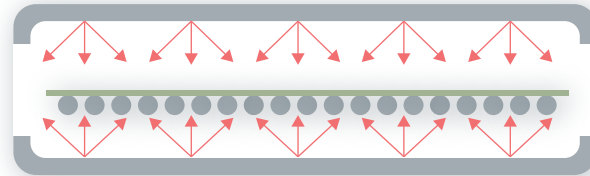


In a salt bath
by ion-exchange

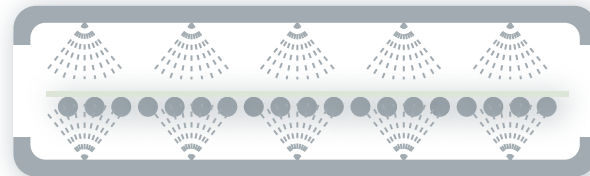
THERMAL TEMPERING



Cleaning



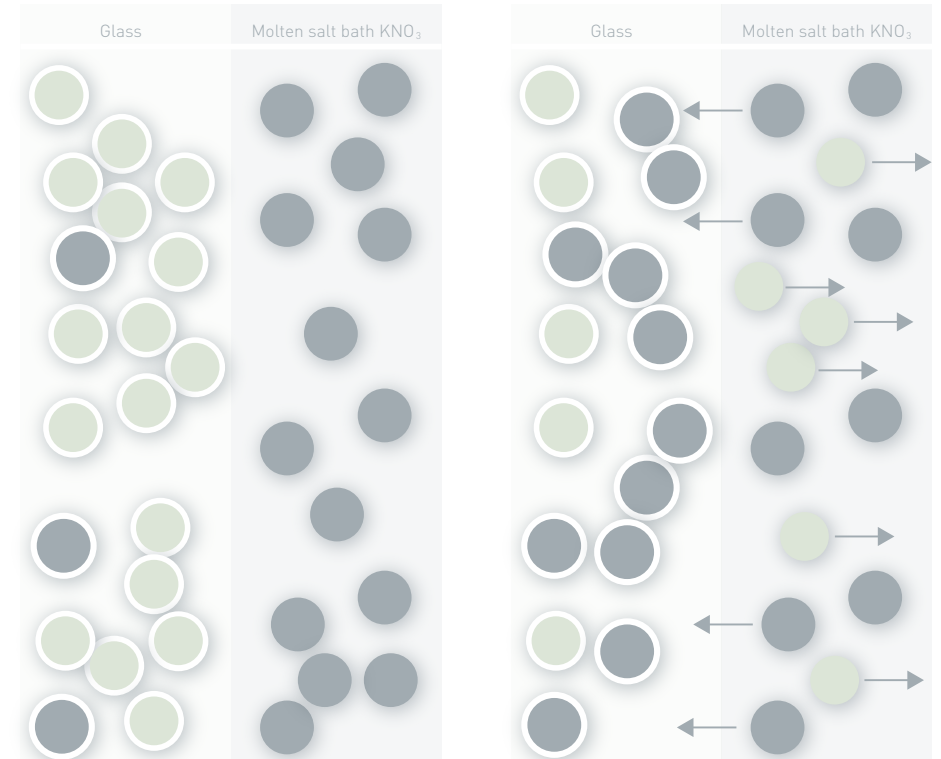
Heating



Quenching

In an oven
by temperature
thickness limited to 2.8mm
size is limited to 3m x 6m

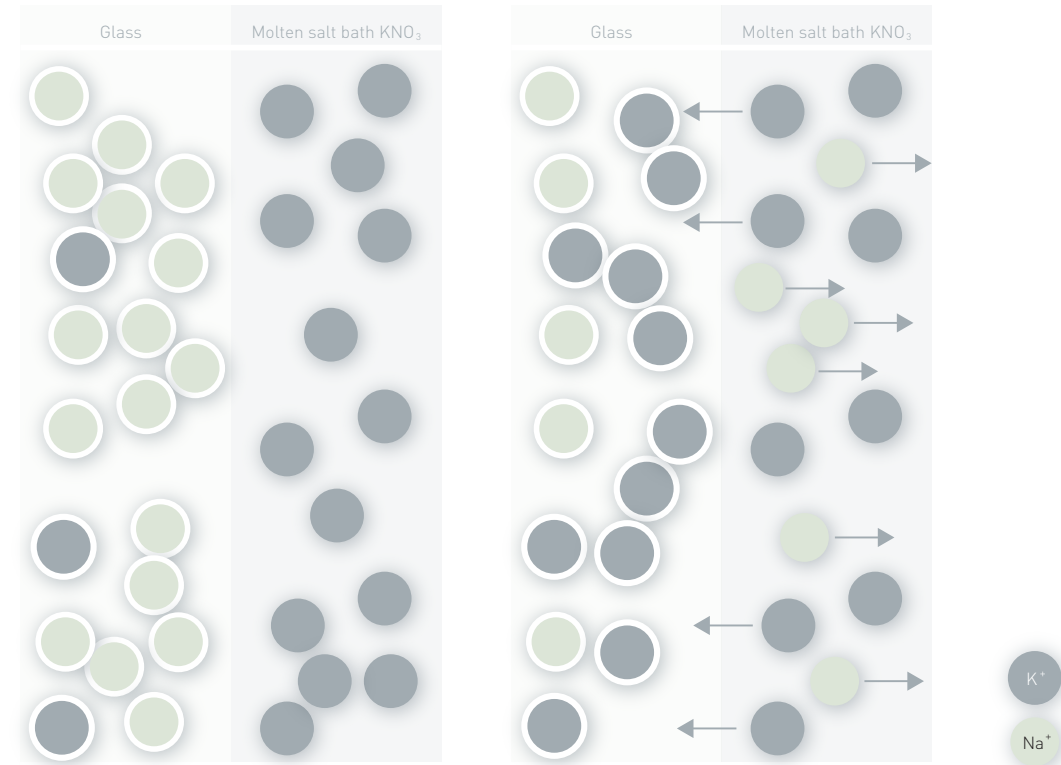
VS. CHEMICAL STRENGTHENING



In a salt bath
by ion-exchange
thickness not limited
size is limited to 1.5m x 1.5m

Thin glass is designated to

CHEMICAL STRENGTHENING



In a salt bath
by ion-exchange
thickness not limited
size is limited to 1.5m 1.5m

Chemical strengthening method is

8X
tougher

than thermal tempering method

Prestressing method	Value in MPa	[N/mm ²]
Annealed	45	
Heat-strengthened	70	
Fully tempered	120	
Chemically strengthened	750-1000*	

HIGH STRENGTH THIN GLASS

Chemical strengthening method is

8X
tougher

than thermal tempering method

Prestressing method	Value in MPa	[N/mm ²]
Annealed	45	
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STRONG

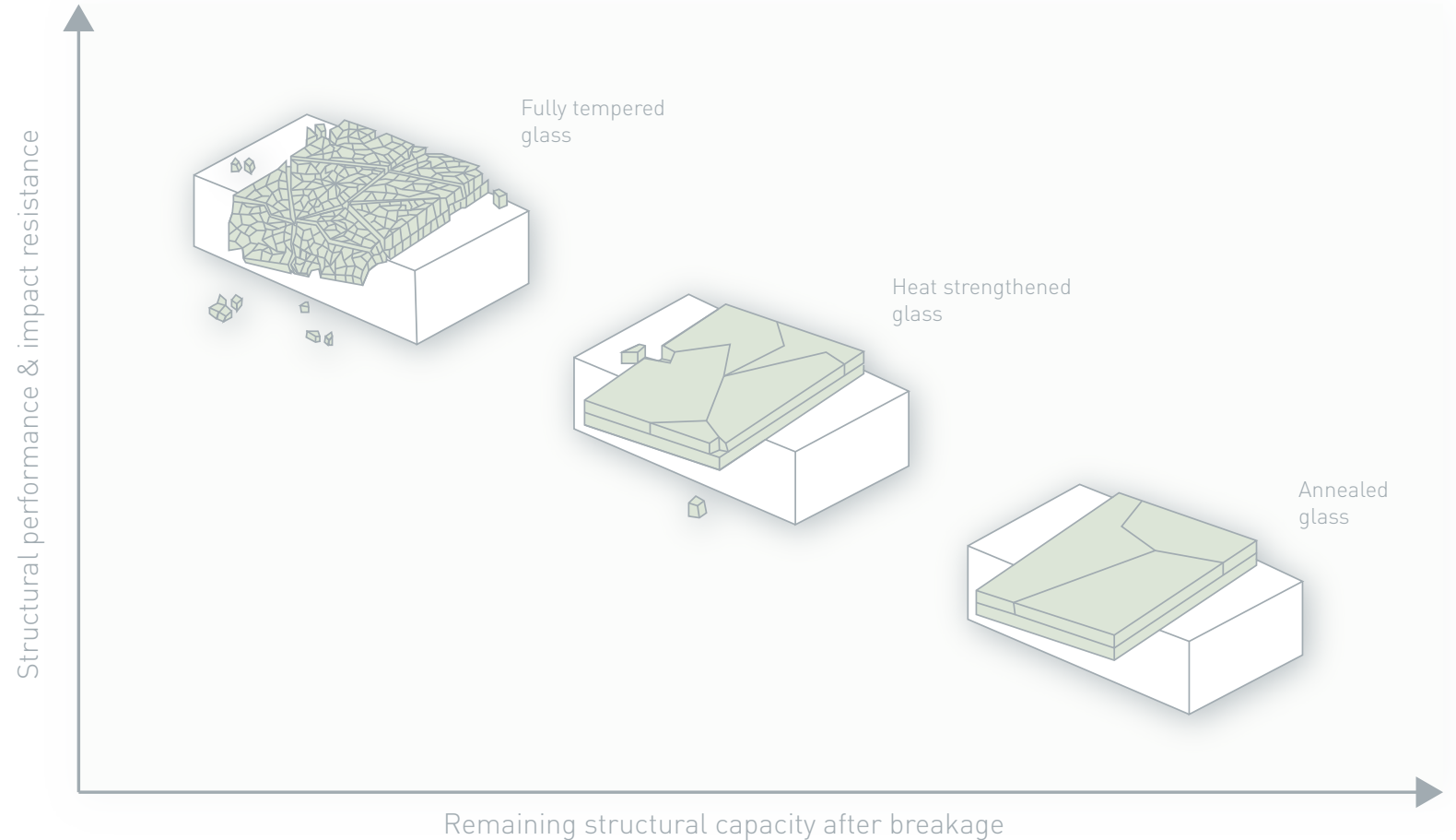
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+ SAFETY BY ENHANCED SAFETY MECHANISM: LAMINATION



Breakage behaviour depends on built up elastic energy stored in the pane

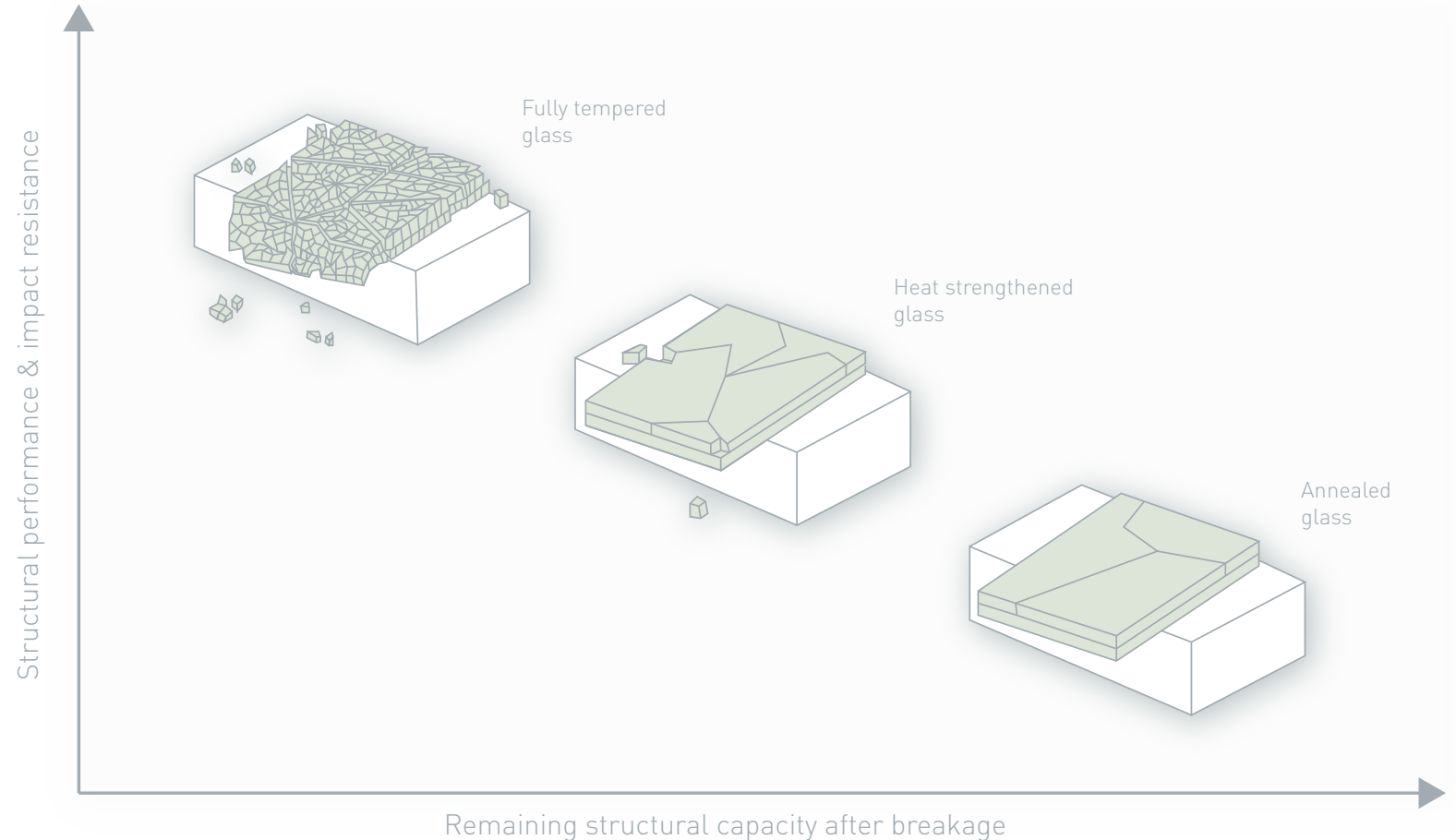
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WHERE CAN CHEMICALLY STRENGTHENED GLASS BE POSITIONED?



Breakage behaviour depends on built up elastic energy stored in the pane

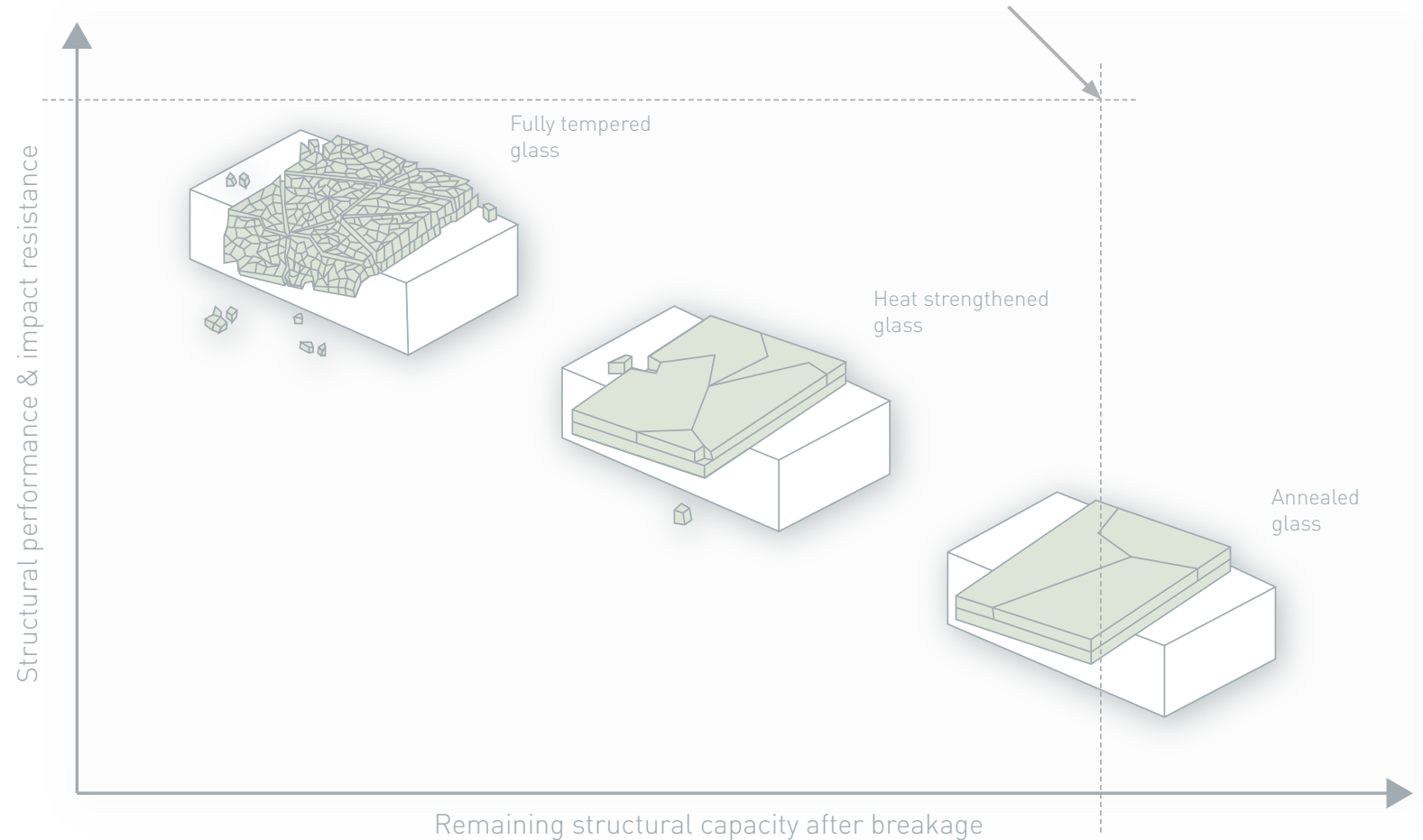
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WHERE CAN CHEMICALLY STRENGTHENED GLASS BE POSITIONED?



Breakage behaviour depends on built up elastic energy stored in the pane

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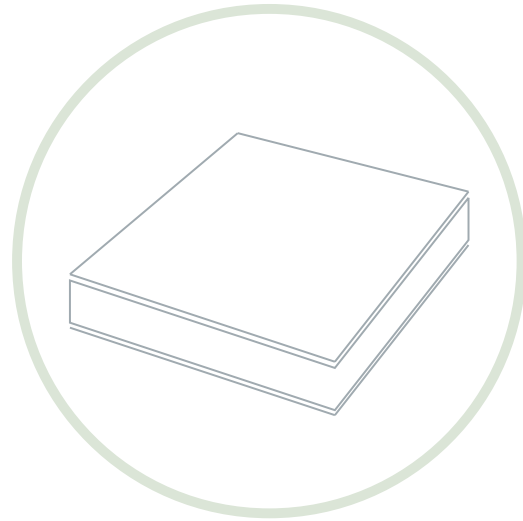
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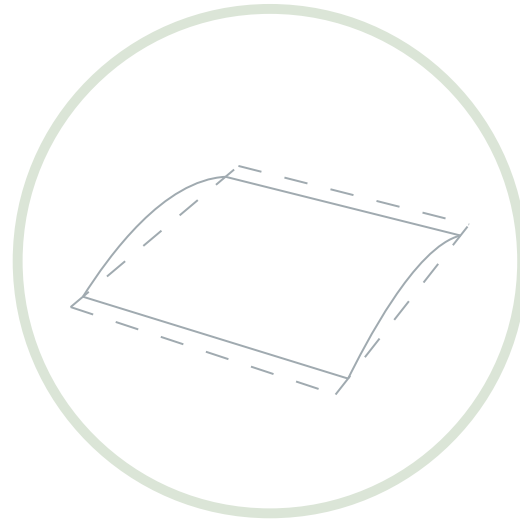
NUMERICAL
INVESTIGATION

DEFINITIVE
DESIGN

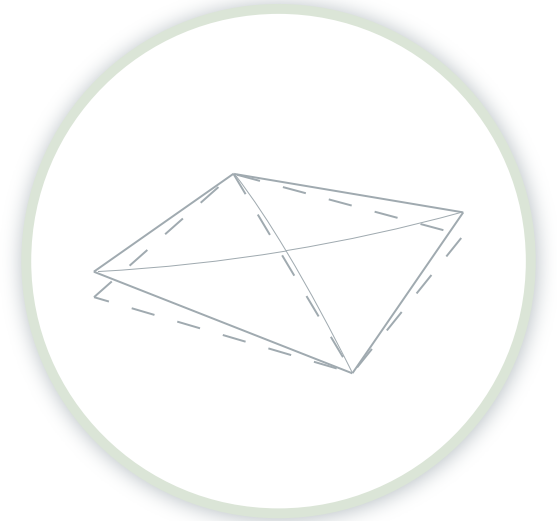
+ **STIFFNESS & STABILITY** BY *ADDING MATERIAL OR GEOMETRY*



1. Flat

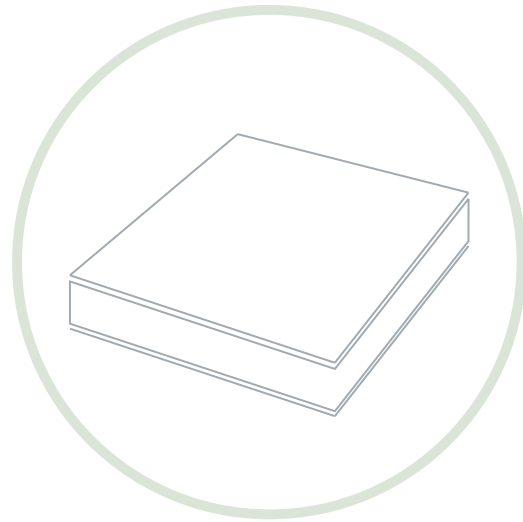


2. Single curved

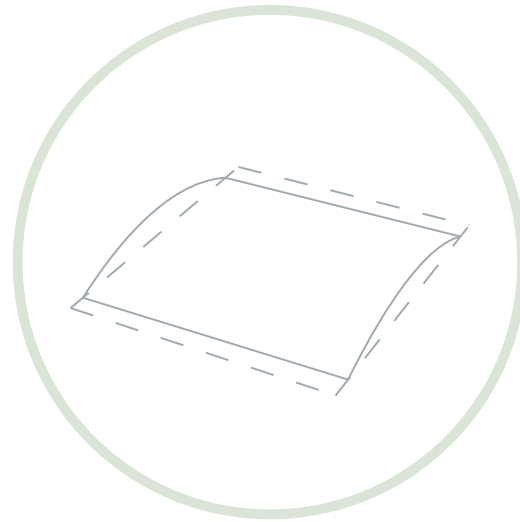


3. Double curved

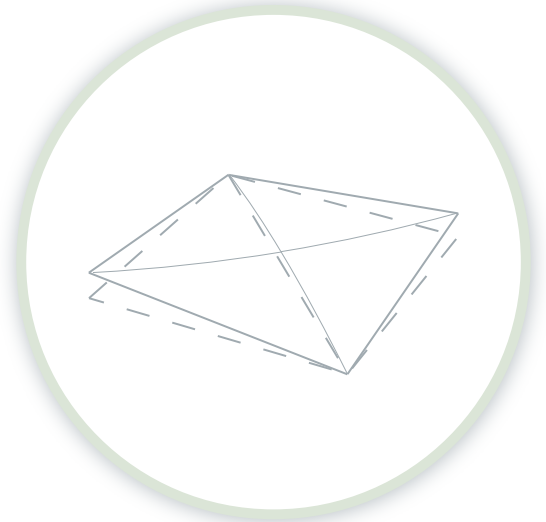
+ **STIFFNESS & STABILITY BY ADDING MATERIAL OR GEOMETRY**



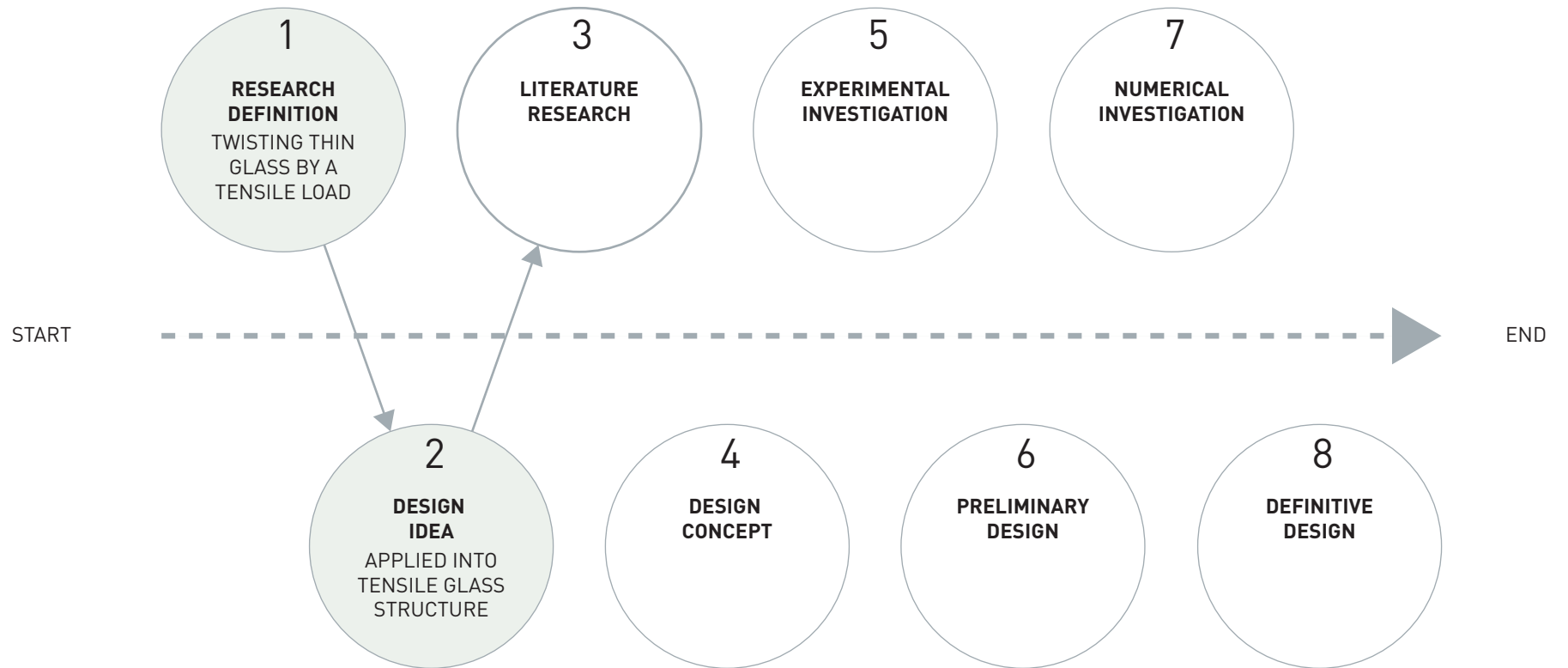
1. Flat
**By adding material
thickness.**

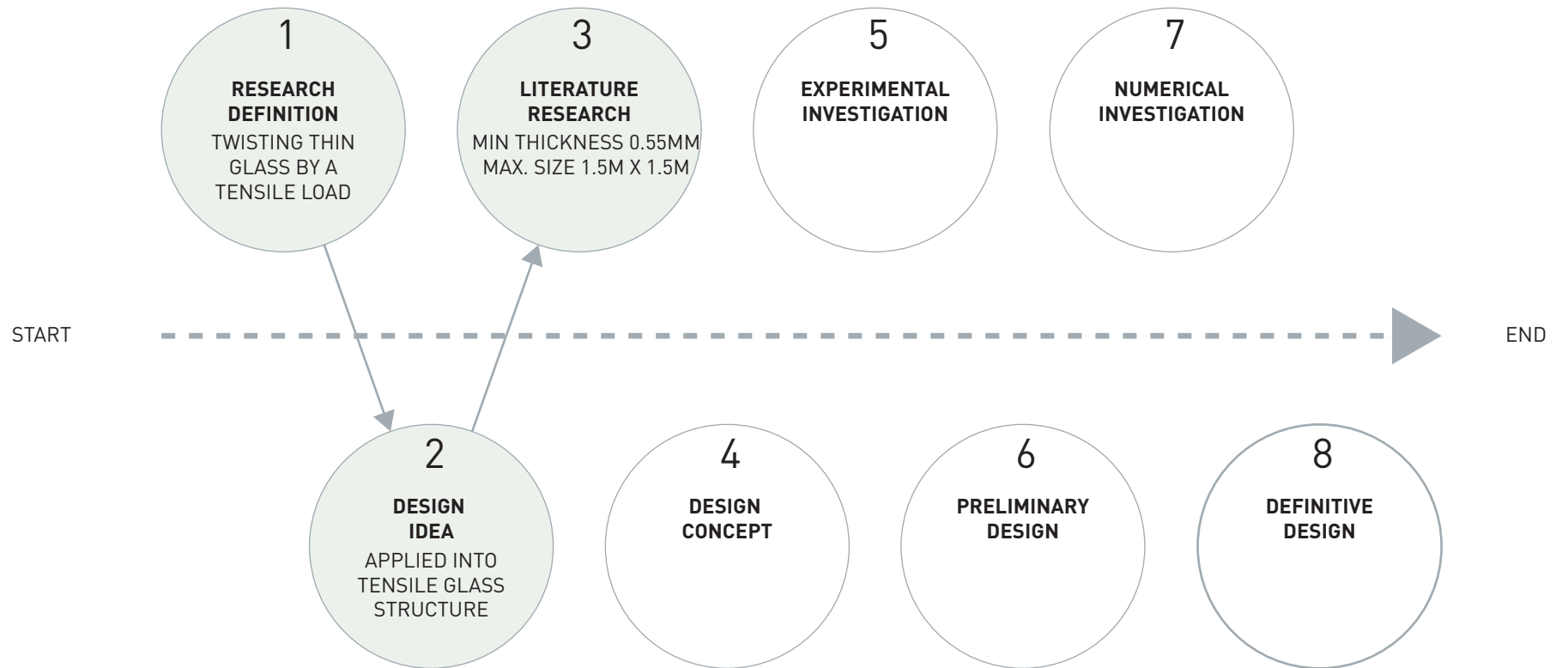


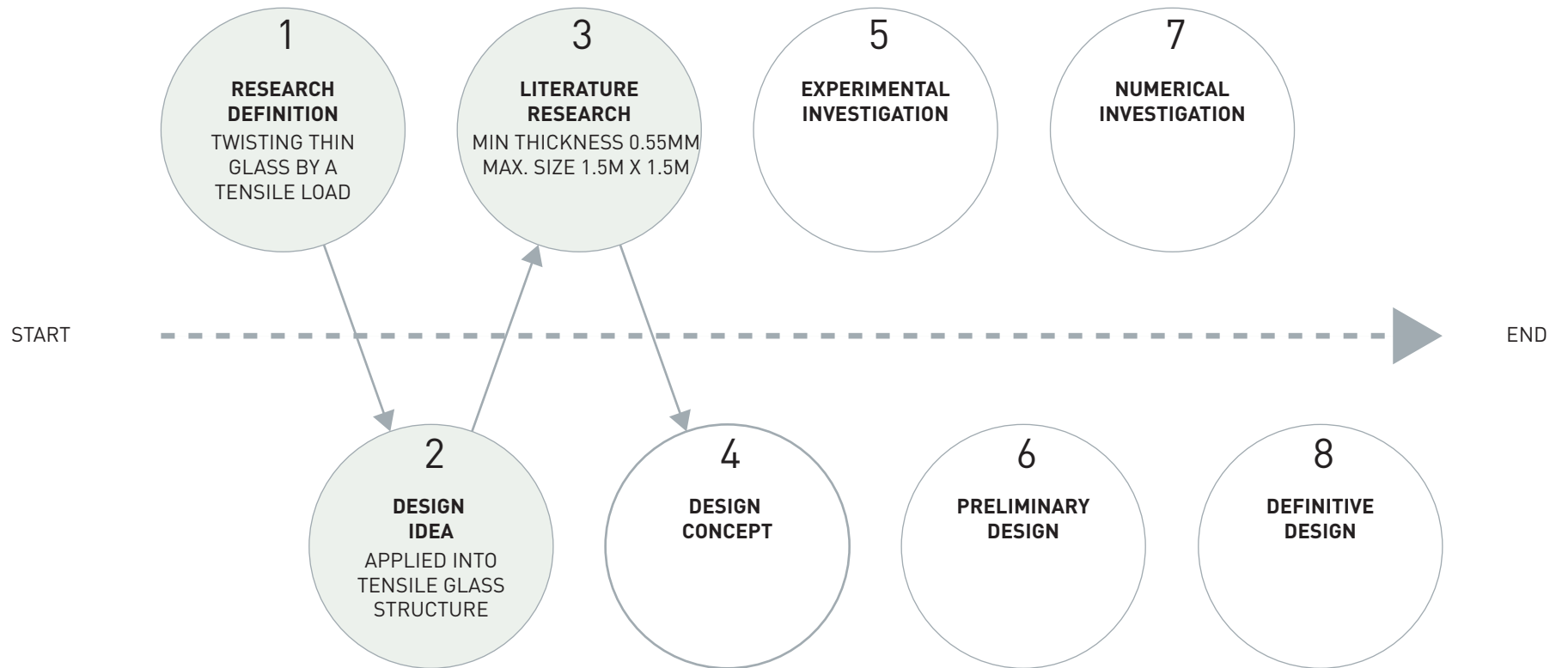
2. Single curved
**Through geometrical
form.**



3. Double curved
**Through geometrical
form.**

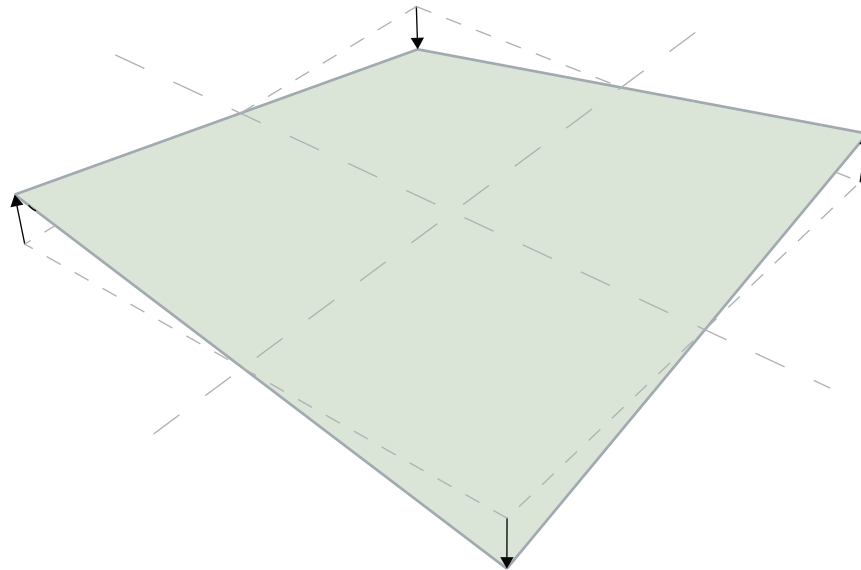






DESIGN CONCEPT

CONVENTIONAL TECHNOLOGY TO CREATE AN ANTICLASTIC SURFACE



Based on the idea that the pane can **resist COMPRESSION**, and a **little TENSION**

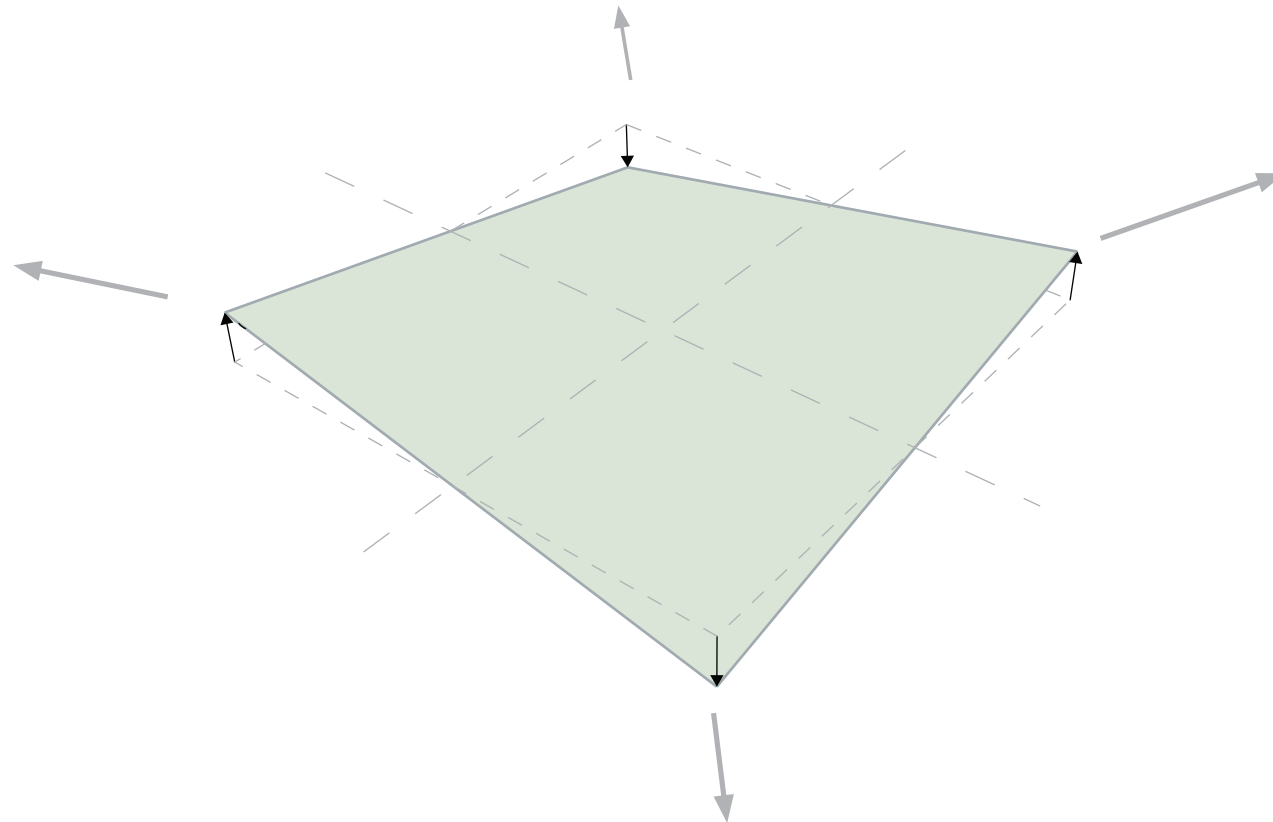
DESIGN
CONCEPT

CREATING A HYPAR
SURFACE

LIMITATIONS

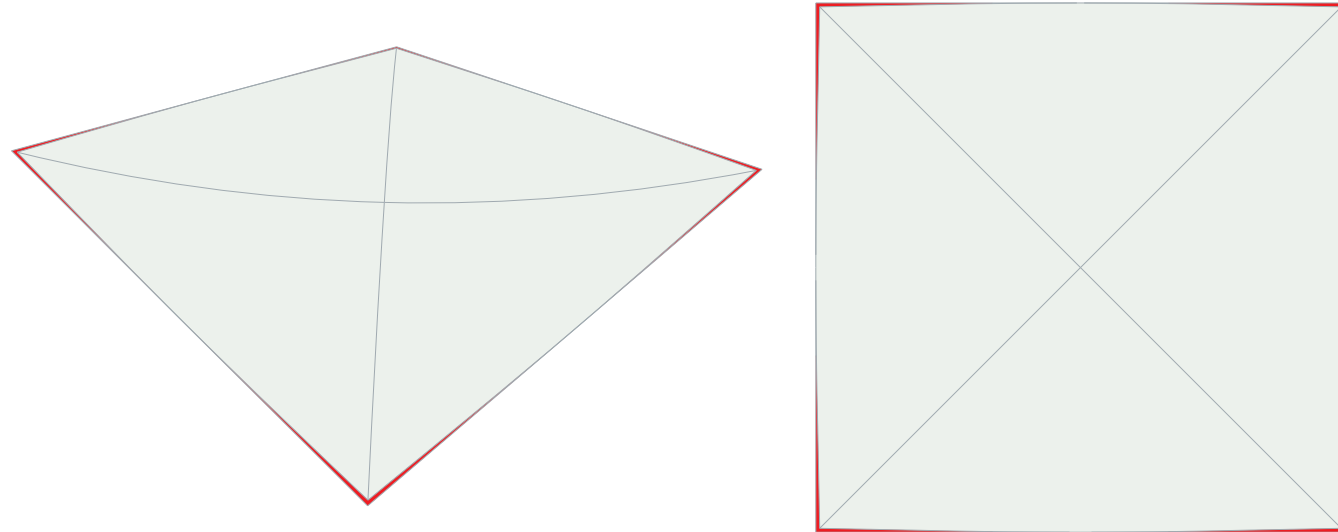
INTRODUCING
TENSION 2D

NEW TECHNIQUE TO CREATE AN ANTICLASTIC SURFACE

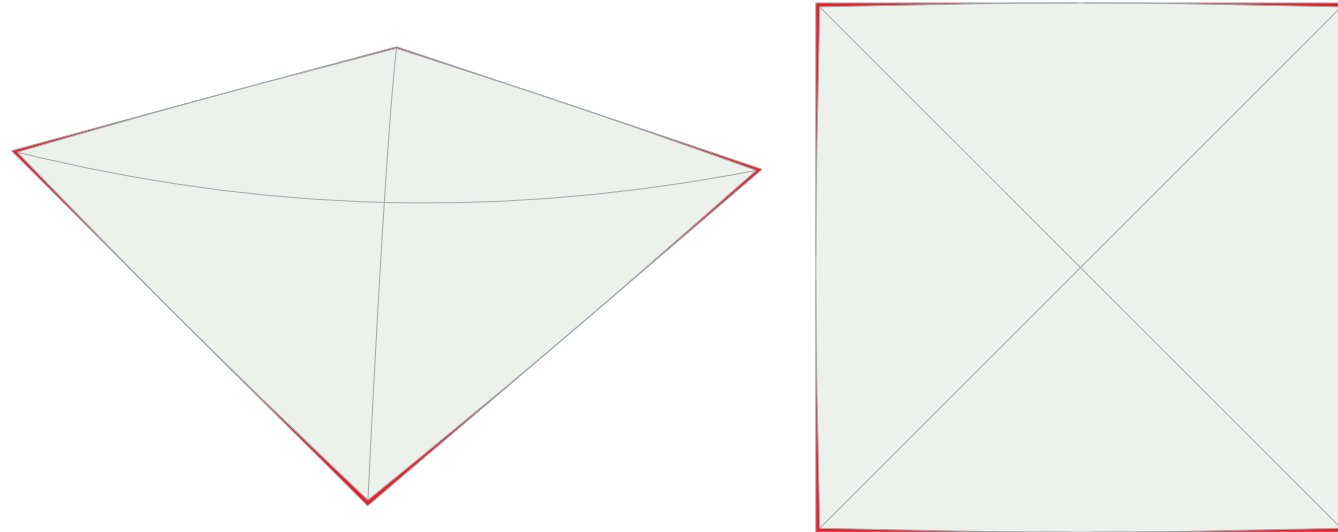


Based on the idea that the pane can **resist *TENSION***, and a **little *COMPRESSION***

CREATED GEOMETRY MAKES IT CHALLENGING *FOR A SUFFICIENT CONNECTION*

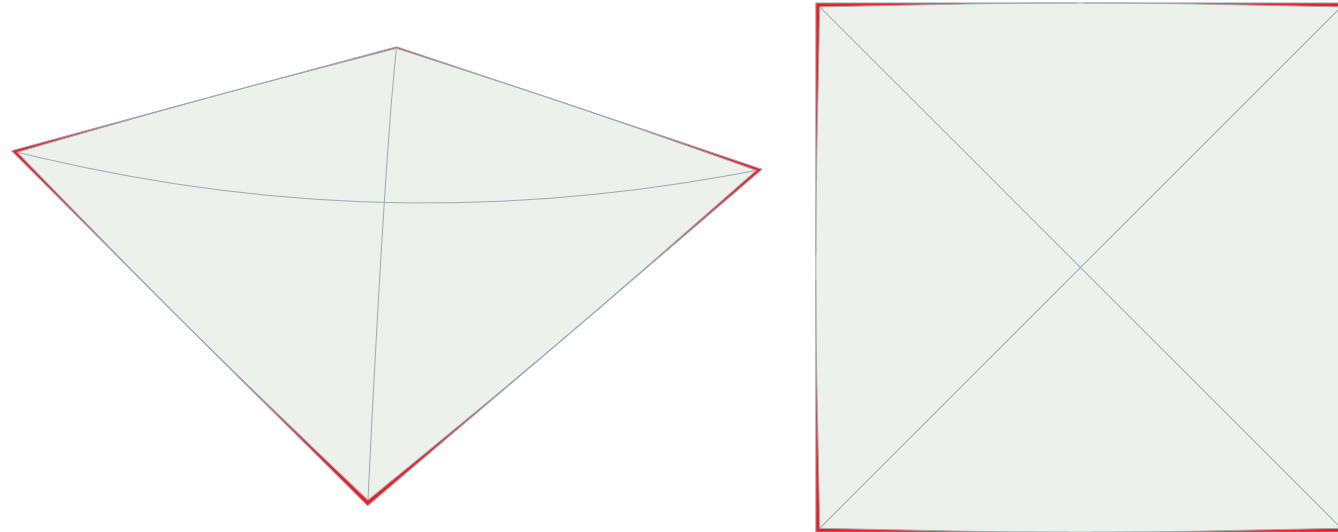


CREATED GEOMETRY MAKES IT DIFFICULT *FOR A SUFFICIENT CONNECTION*



How does the connection need to look like to double cold bend the glass?

CREATED GEOMETRY MAKES IT DIFFICULT *FOR A SUFFICIENT CONNECTION*



How does the connection need to look like to double cold bend the glass?

How do you grip?
Where do you grip?

DESIGN
CONCEPT

CREATING A HYPAR
SURFACE

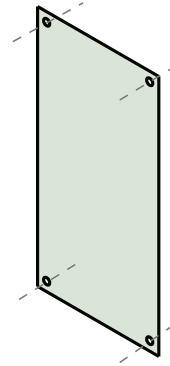
LIMITATIONS

INTRODUCING
TENSION 2D

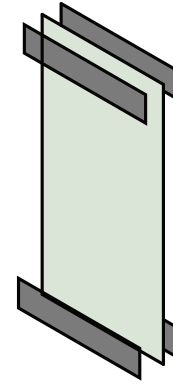
2D TENSIONING TO DETERMINE *STRENGTH*



2D TENSIONING TO DETERMINE *STRENGTH*



1. Holes

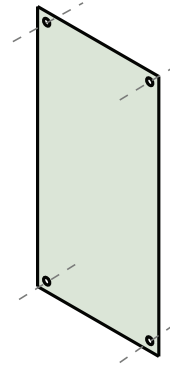


2. Clamping

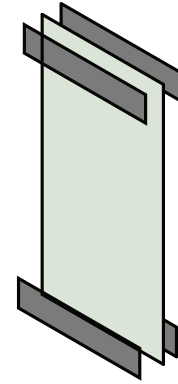


3. Adhesive

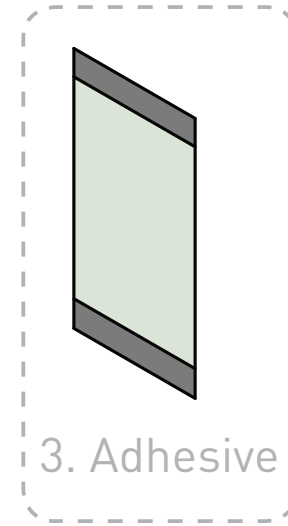
2D TENSIONING TO DETERMINE *STRENGTH*



1. Holes

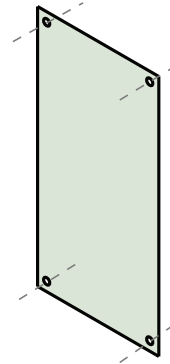


2. Clamping

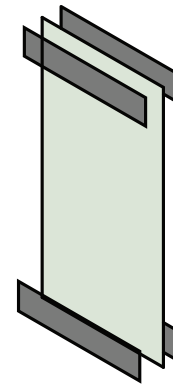


3. Adhesive

2D TENSIONING TO DETERMINE *STRENGTH*



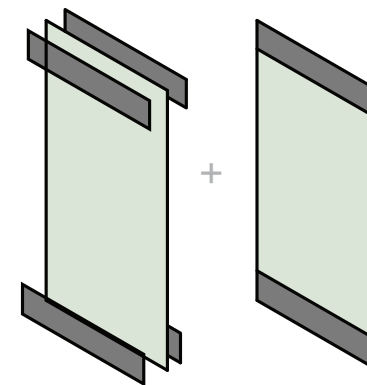
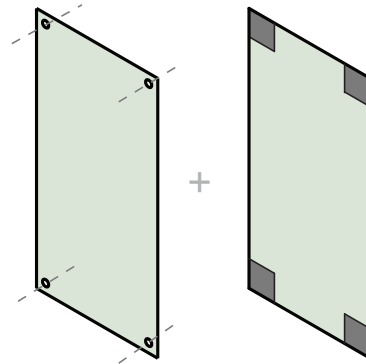
1. Holes



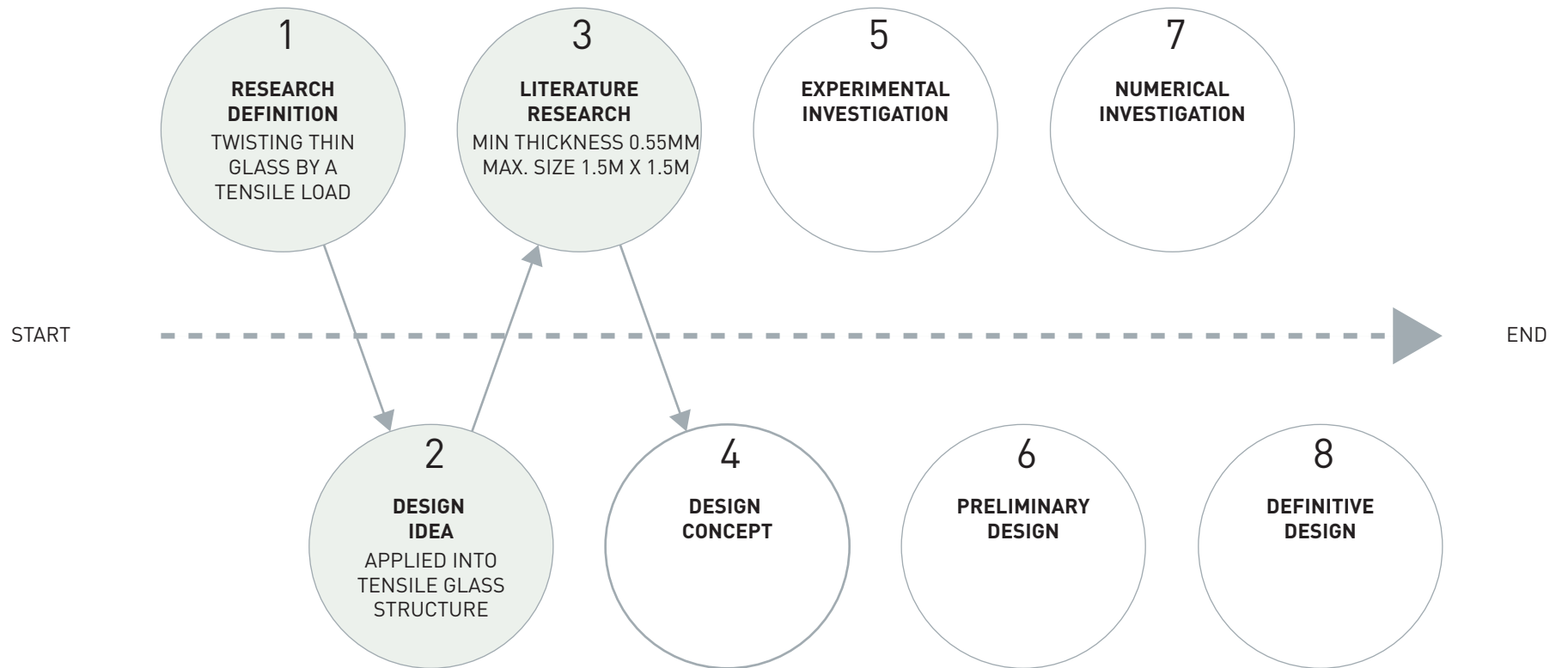
2. Clamping

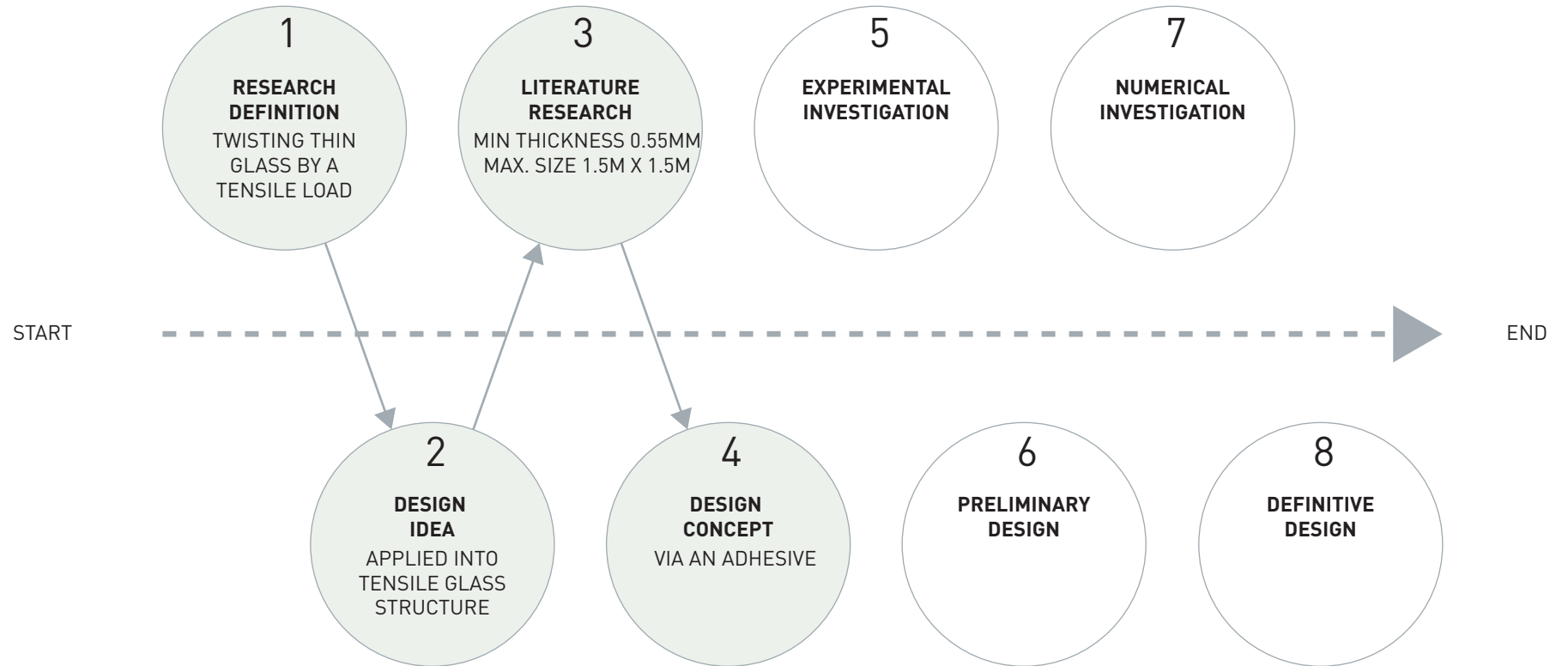


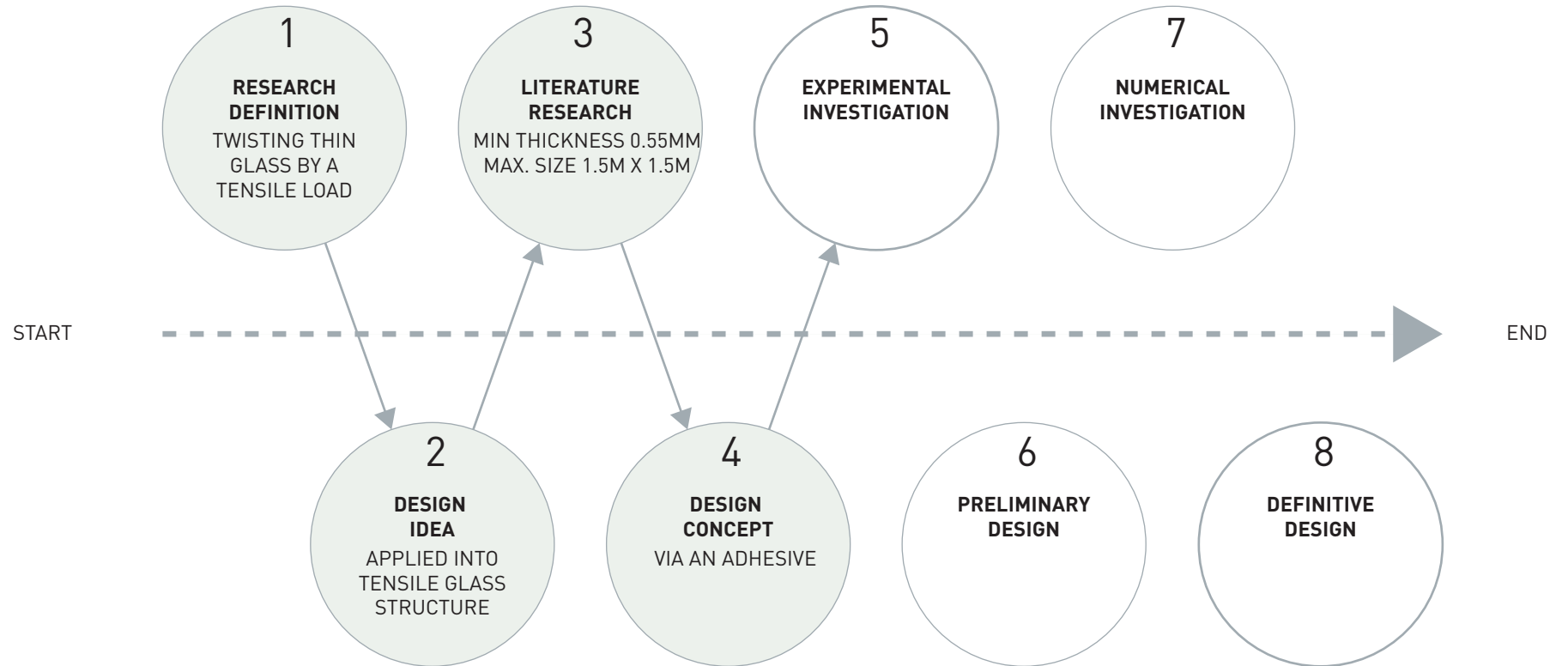
3. Adhesive



Combinations are also possible







EXPERIMENTAL INVESTIGATION

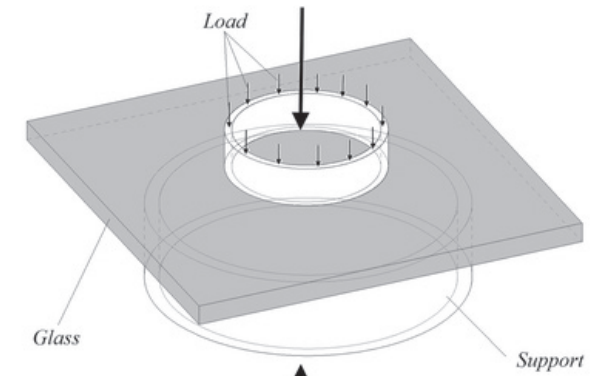
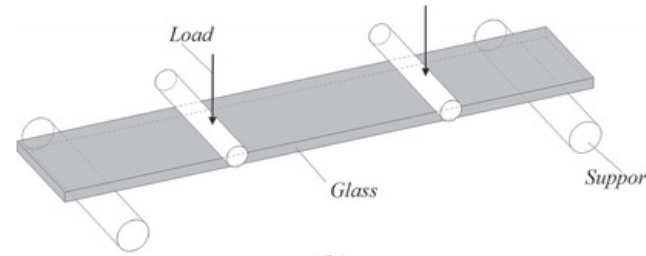
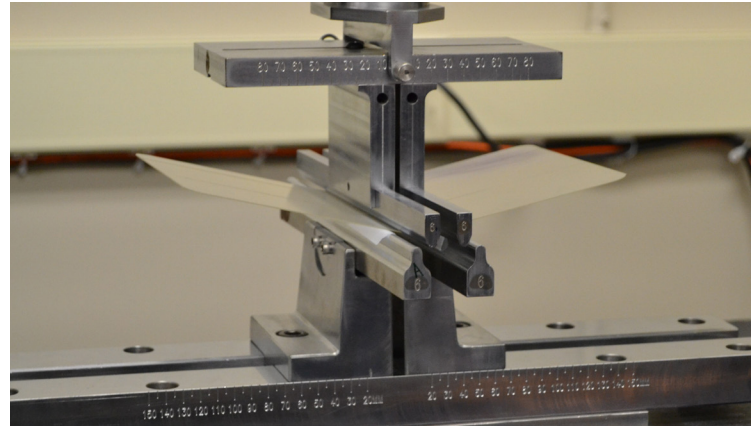
EXPERIMENTAL INVESTIGATION

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BRITTLE MATERIALS



1. **Flexural load** with 4-point bend test

2. **Flexural load** with Ring-on-ring test

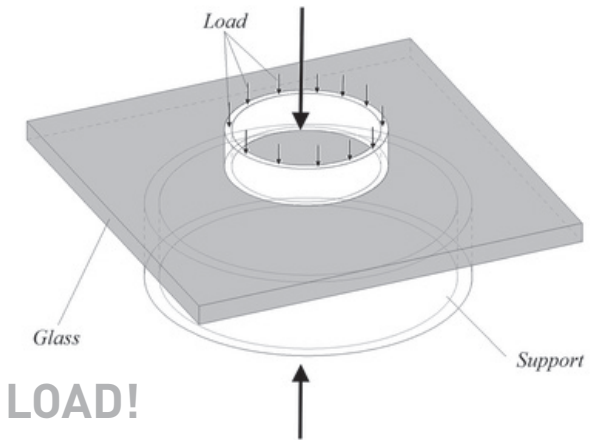
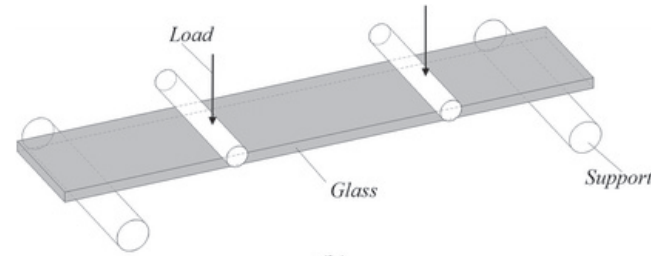
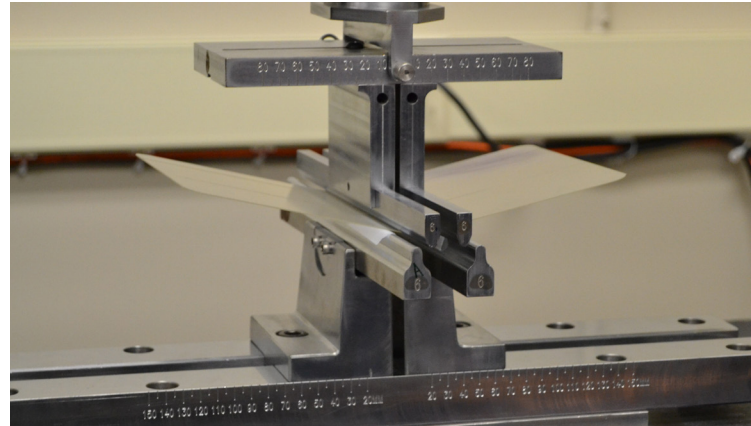
EXPERIMENTAL INVESTIGATION

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WE WANT TENSILE LOAD!

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**DESIGN A NON-STANDARD TEST METHOD
THAT FITS INTO THE PULL-OUT MACHINE**

WE WANT TENSILE LOAD!

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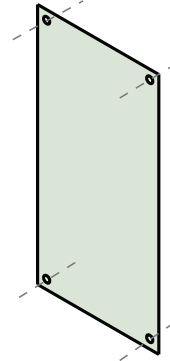
EXPERIMENTAL INVESTIGATION

STANDARD TEST METHODS

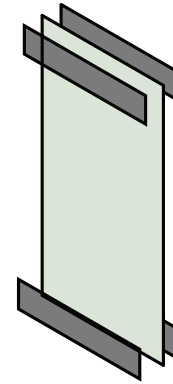
NON-STANDARD TEST METHOD

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2D TENSIONING TO DETERMINE *STRENGTH*



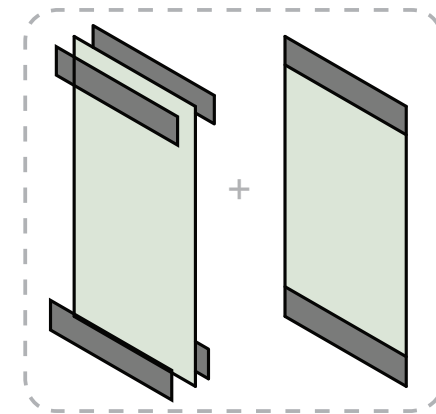
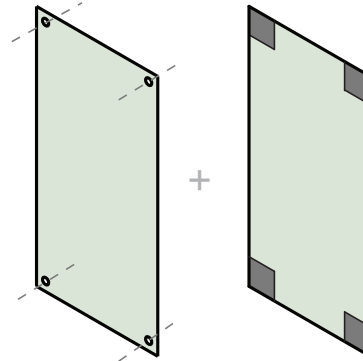
1. Holes



2. Clamping



3. Adhesive



Clamping & gluing for design test set-up

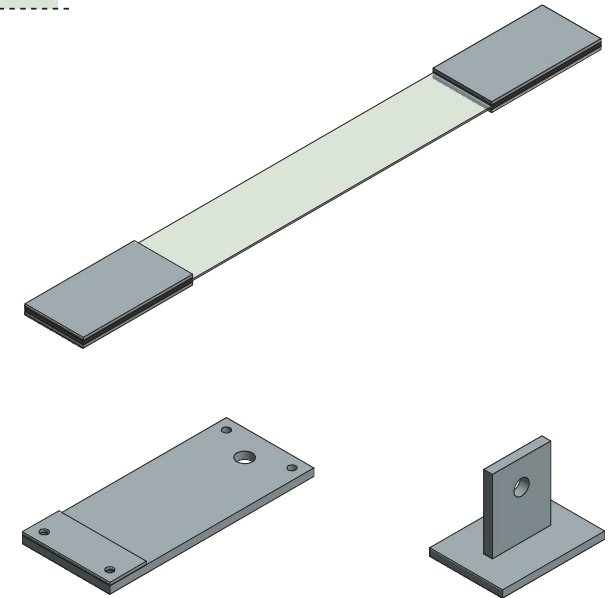
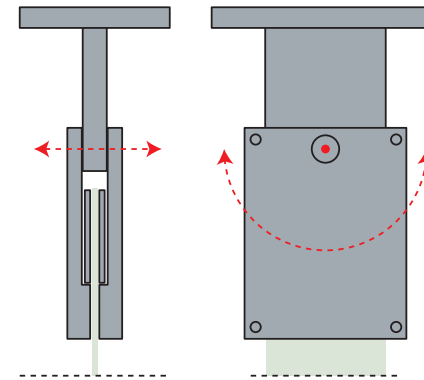
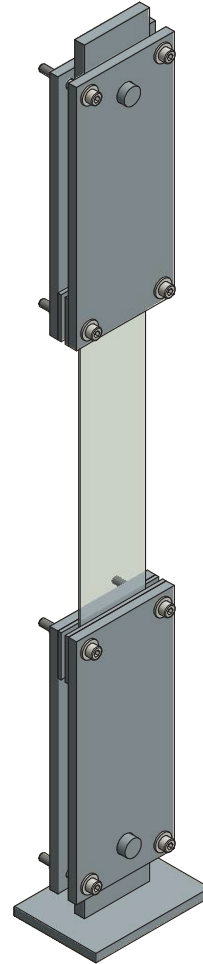
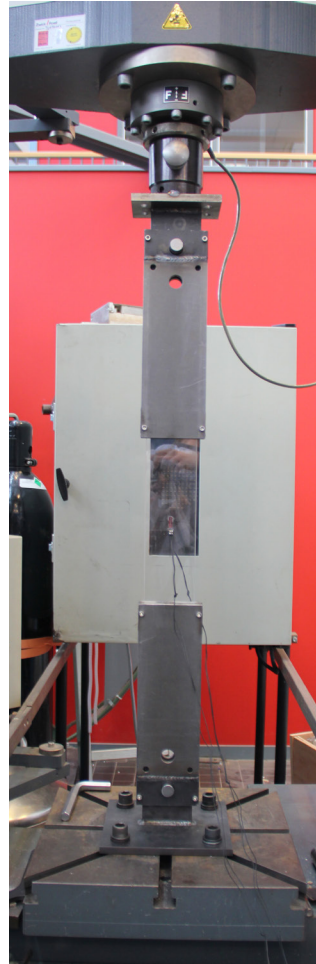
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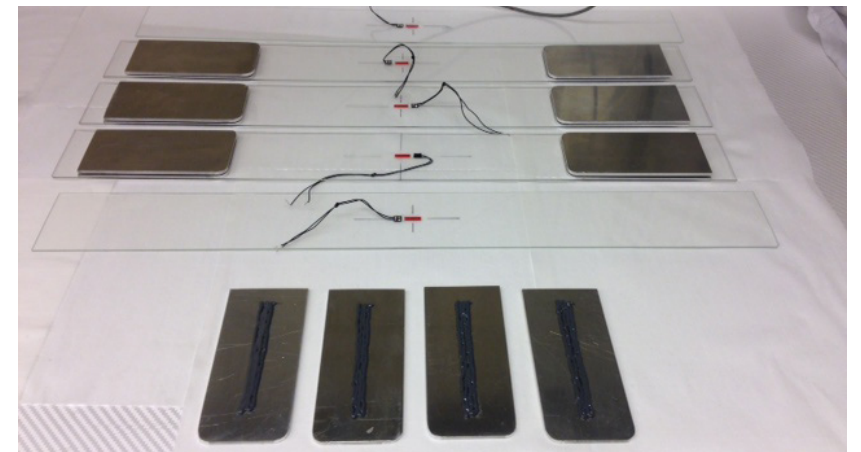
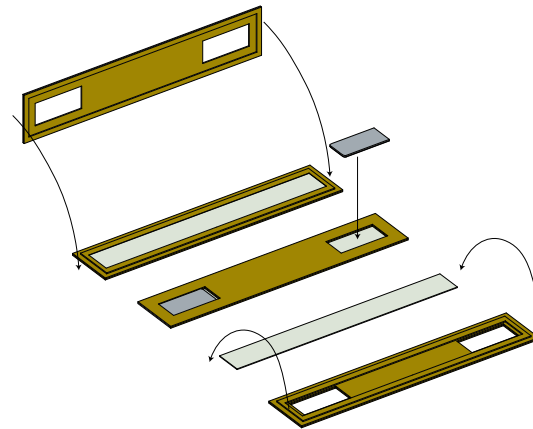
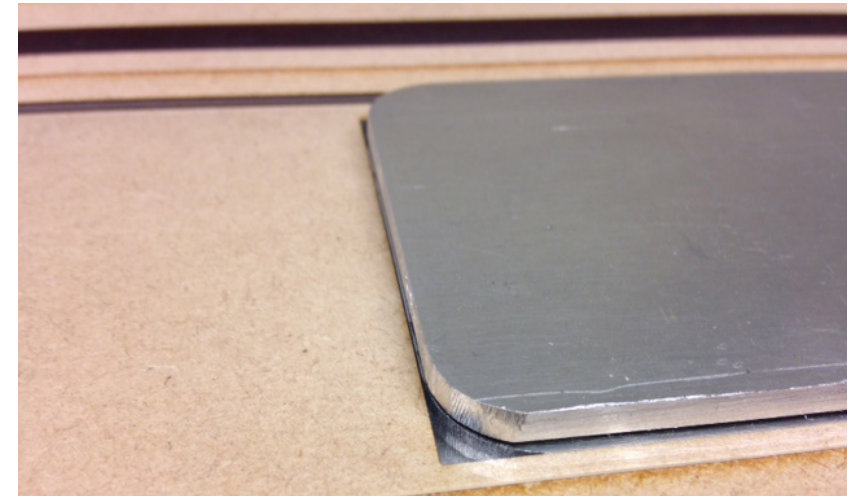
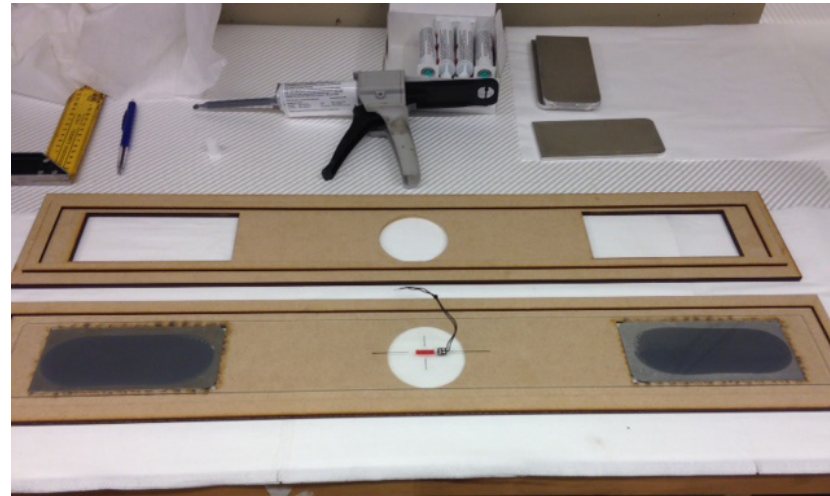
PULL-OUT TEST DESIGN

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PREPERATION SPECIMENS



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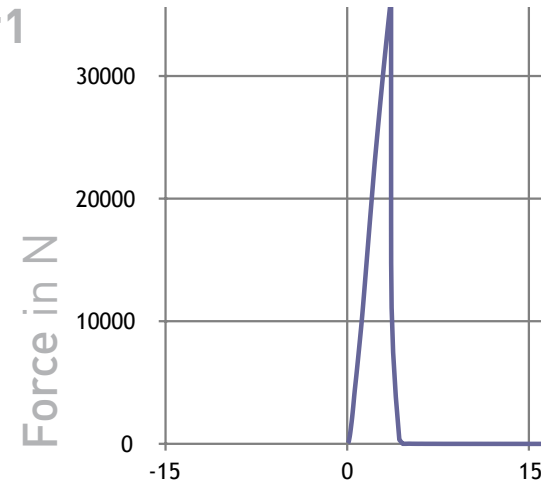
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RESULTS &
DISCUSSION

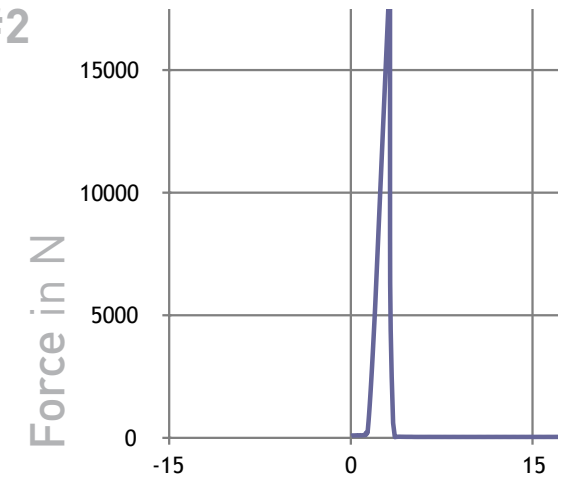
CONCLUSION

RESULTS SPECIMENS

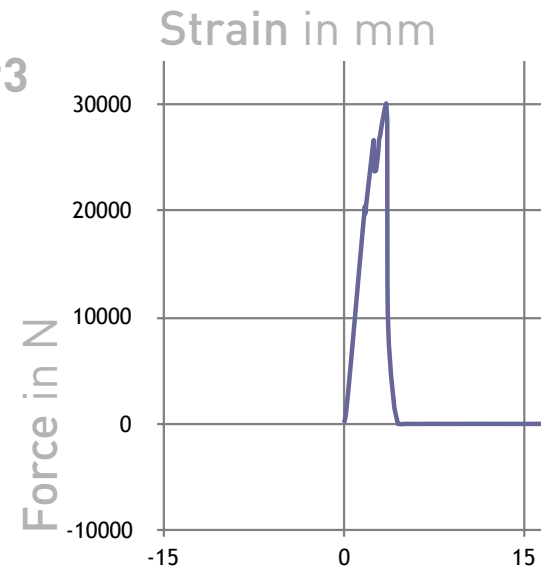
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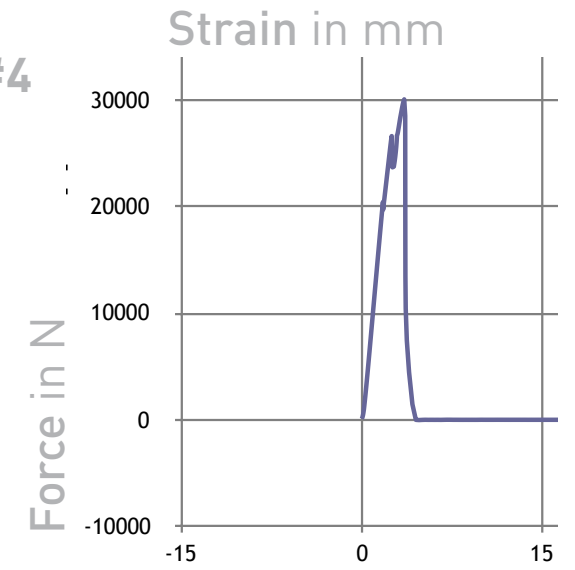
#2



#3



#4



EXPERIMENTAL INVESTIGATION

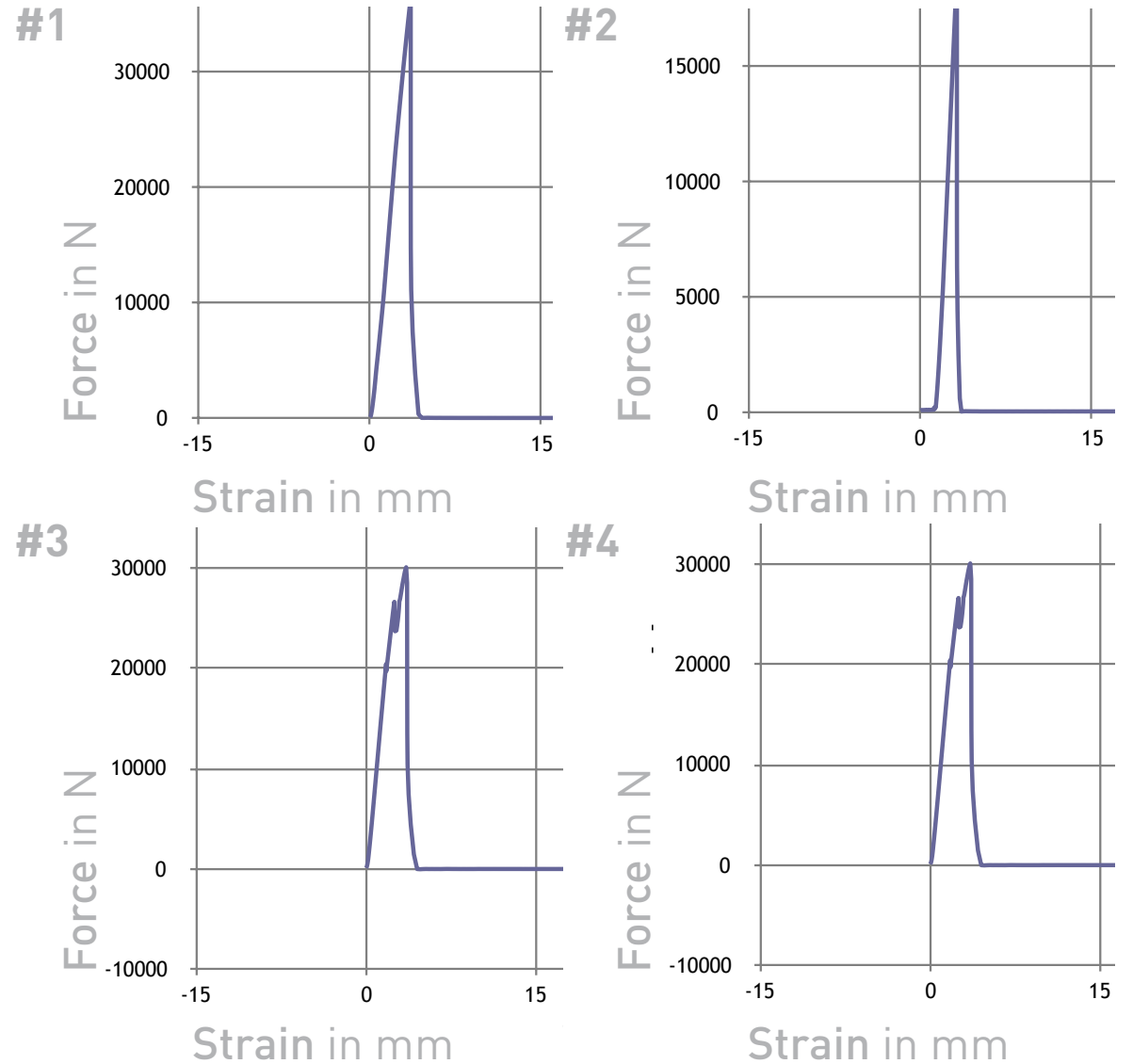
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RESULTS SPECIMENS

→ 3 of 4 above 30000N
circa 3000 kg



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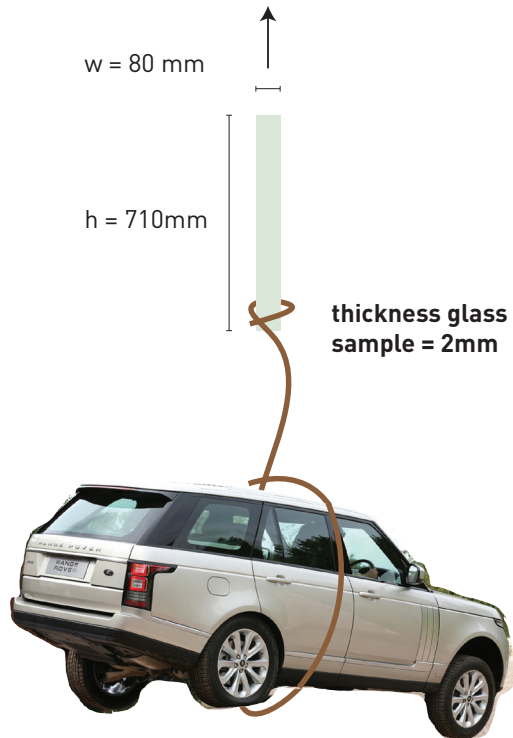
RESULTS & DISCUSSION

CONCLUSION

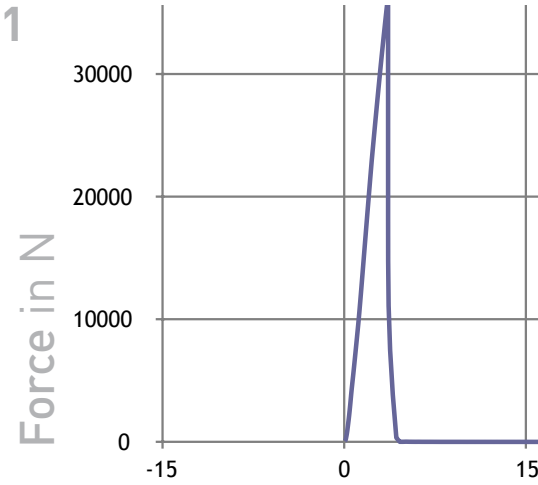
RESULTS SPECIMENS

→ 3 of 4 above 30000N

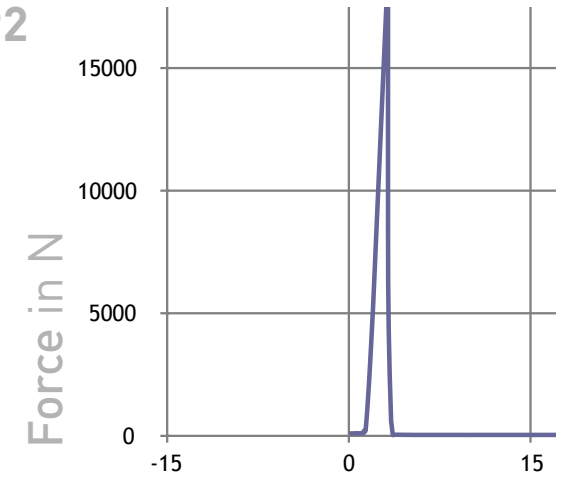
circa 3000 kg



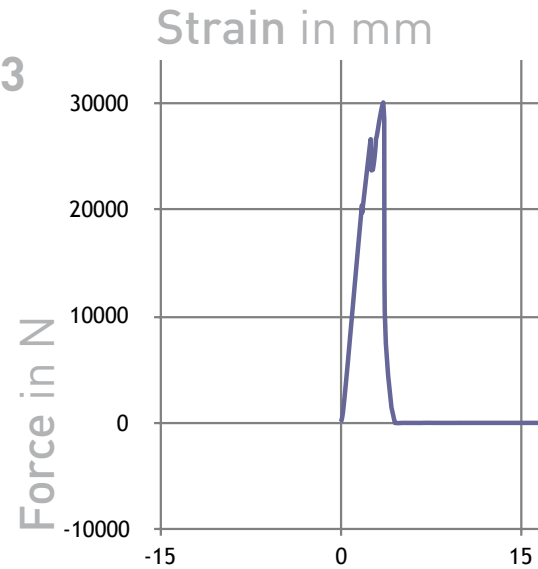
#1



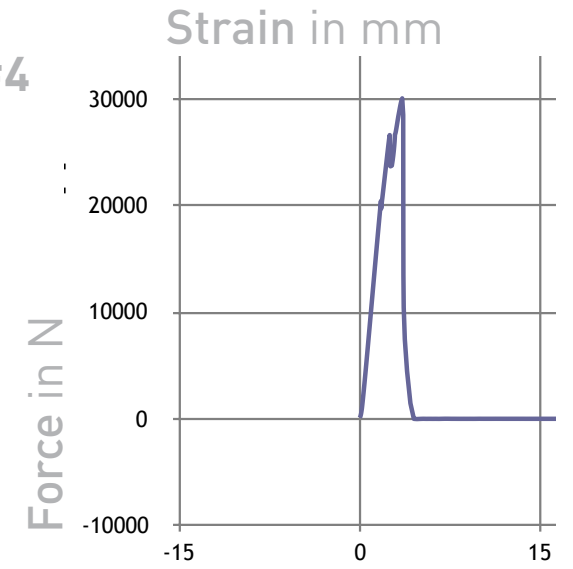
#2



#3



#4



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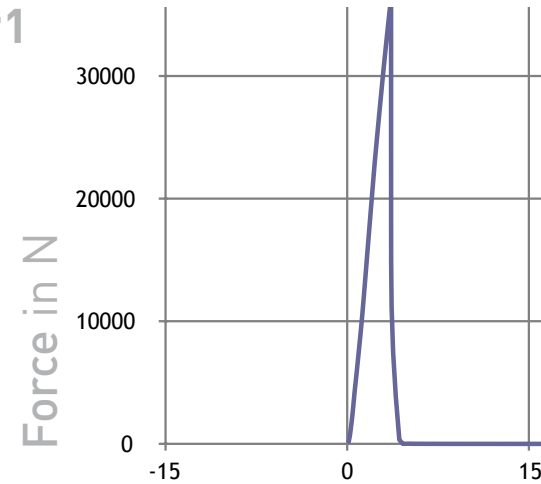
RESULTS SPECIMENS

→ 3 of 4 above 30000N

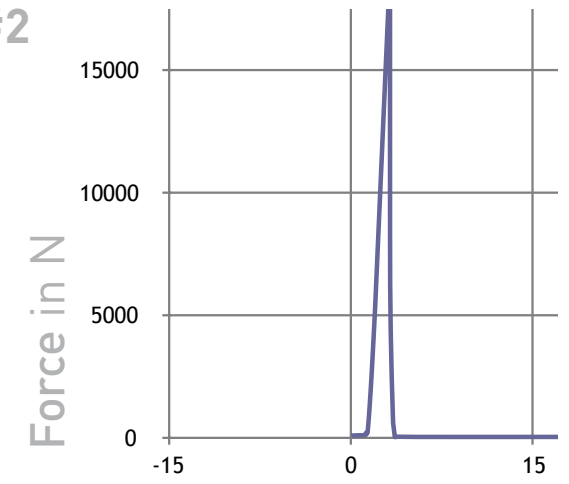
circa 3000 kg

→ 2 of 4 force/strain functions are not linear

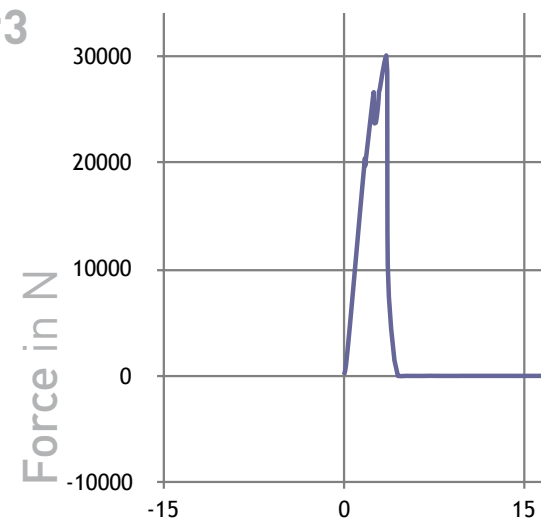
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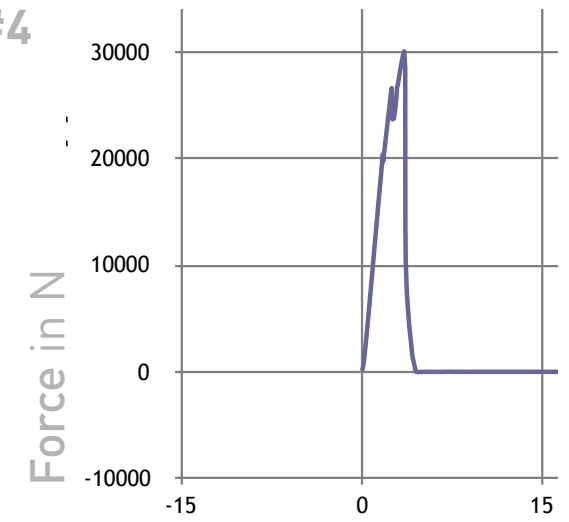
#2



#3



#4



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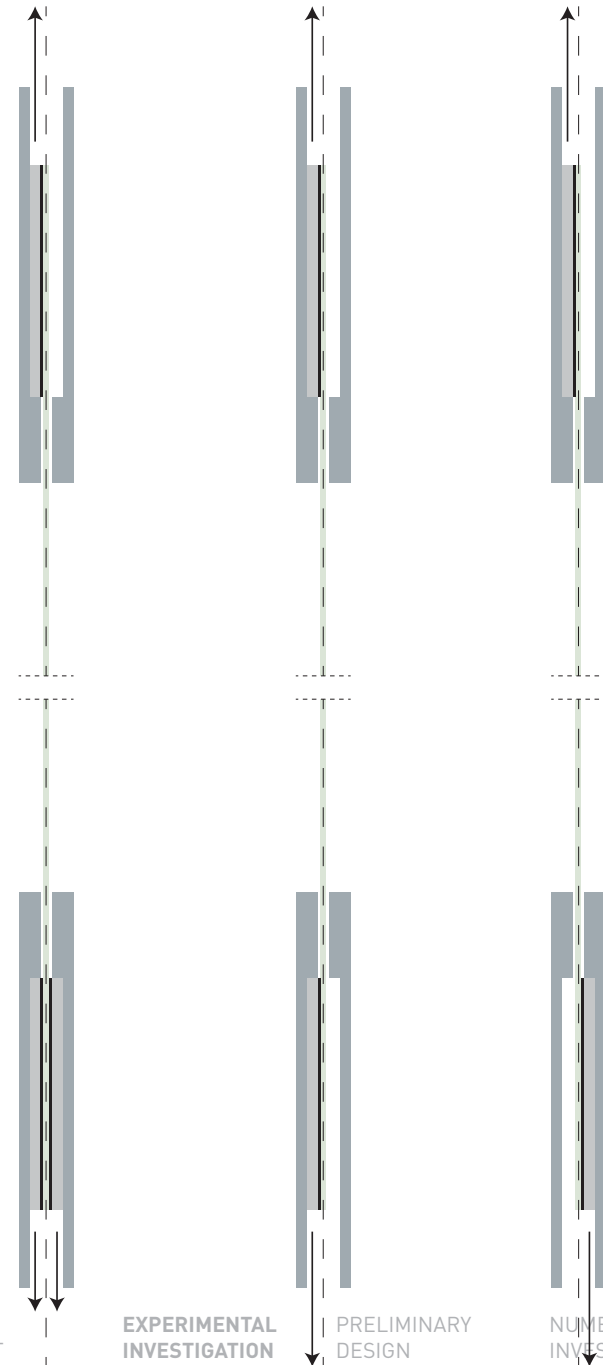
RESULTS SPECIMENS

→ 3 of 4 above 30000N

circa 3000 kg

→ 2 of 4 force/strain function is not linear

because of failure adhesive between glass and alumium plate



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TEST RESULT SPECIMEN #1



**Failure at
36 286 N
3.570 mm**

EXPERIMENTAL INVESTIGATION

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NON-STANDARD TEST METHOD

PULL-OUT TEST
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TEST RESULT SPECIMEN #2



**Failure at
19 038 N
3.184 mm**

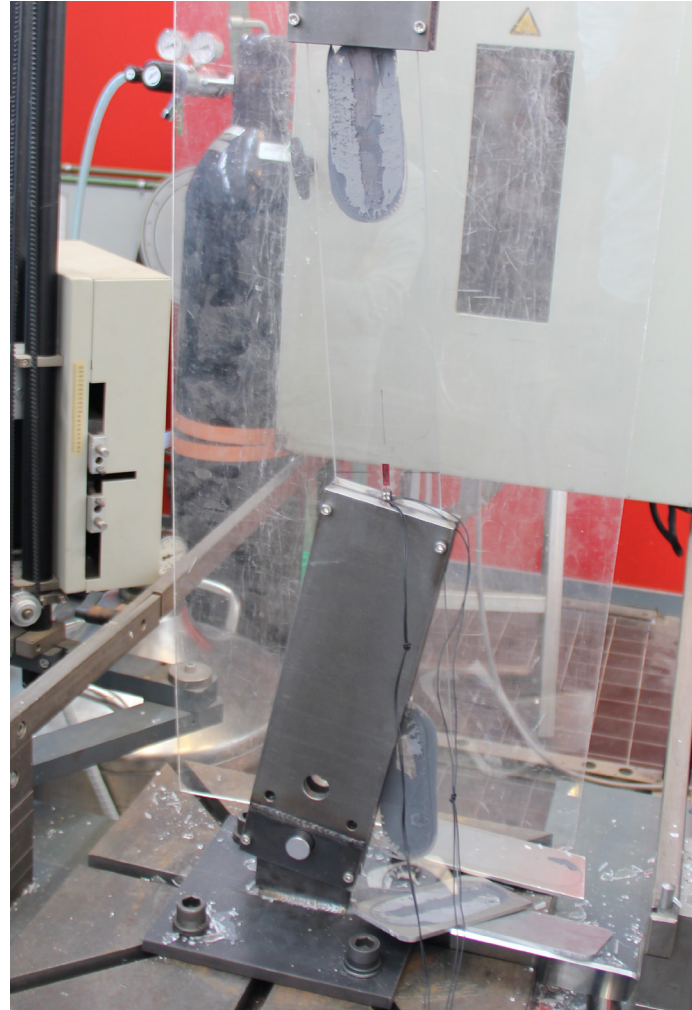
EXPERIMENTAL INVESTIGATION

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TEST RESULT SPECIMEN #3



**Failure at
30 164 N
3.576 mm**

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TEST RESULT SPECIMEN #4



Failure at
32 767 N
4.923 mm

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TENSILE STRENGTH

250 MPa

TENSILE STRENGTH

250 MPa

1/3

of the earlier mentioned bending
tensile strength of 750MPa...

TENSILE STRENGTH

250 MPa

1/3

of the earlier mentioned bending
tensile strength of 750MPa...

Same yield strength as structural A36
steel!

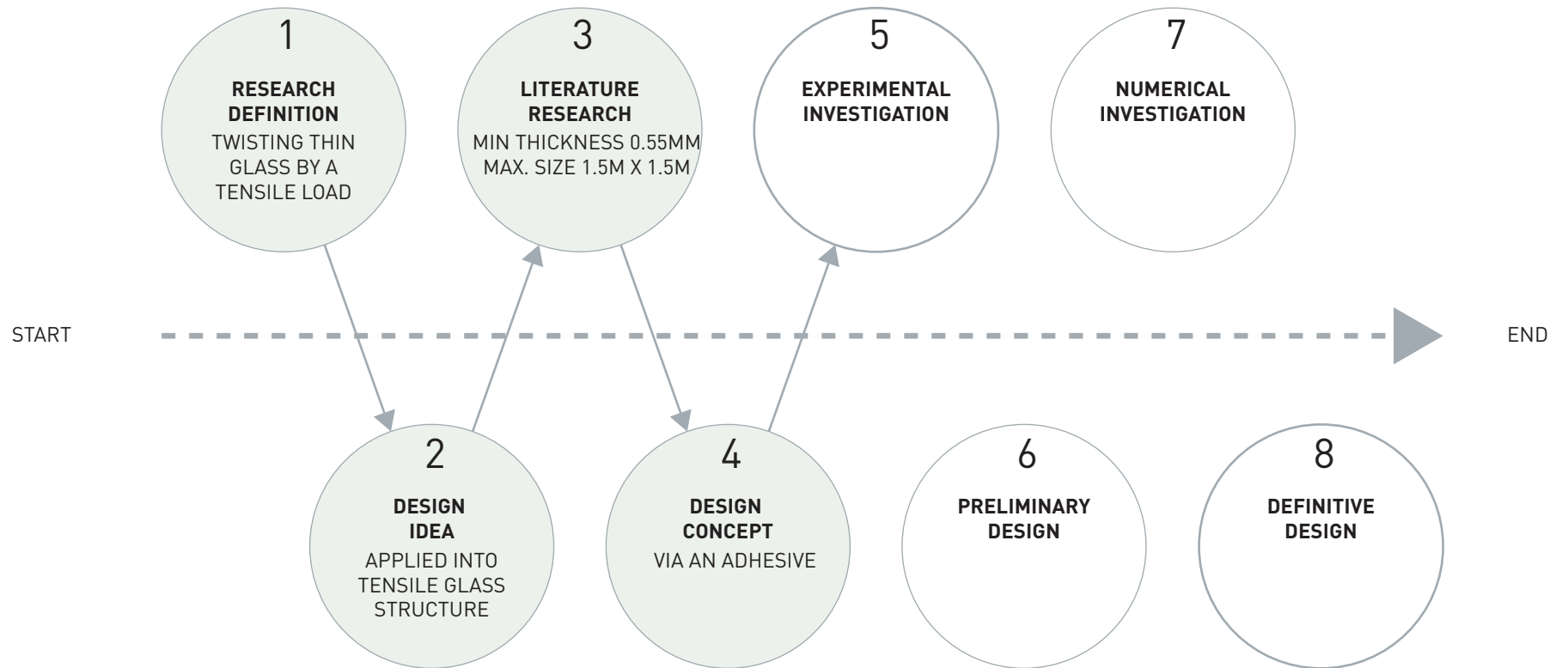
TENSILE STRENGTH

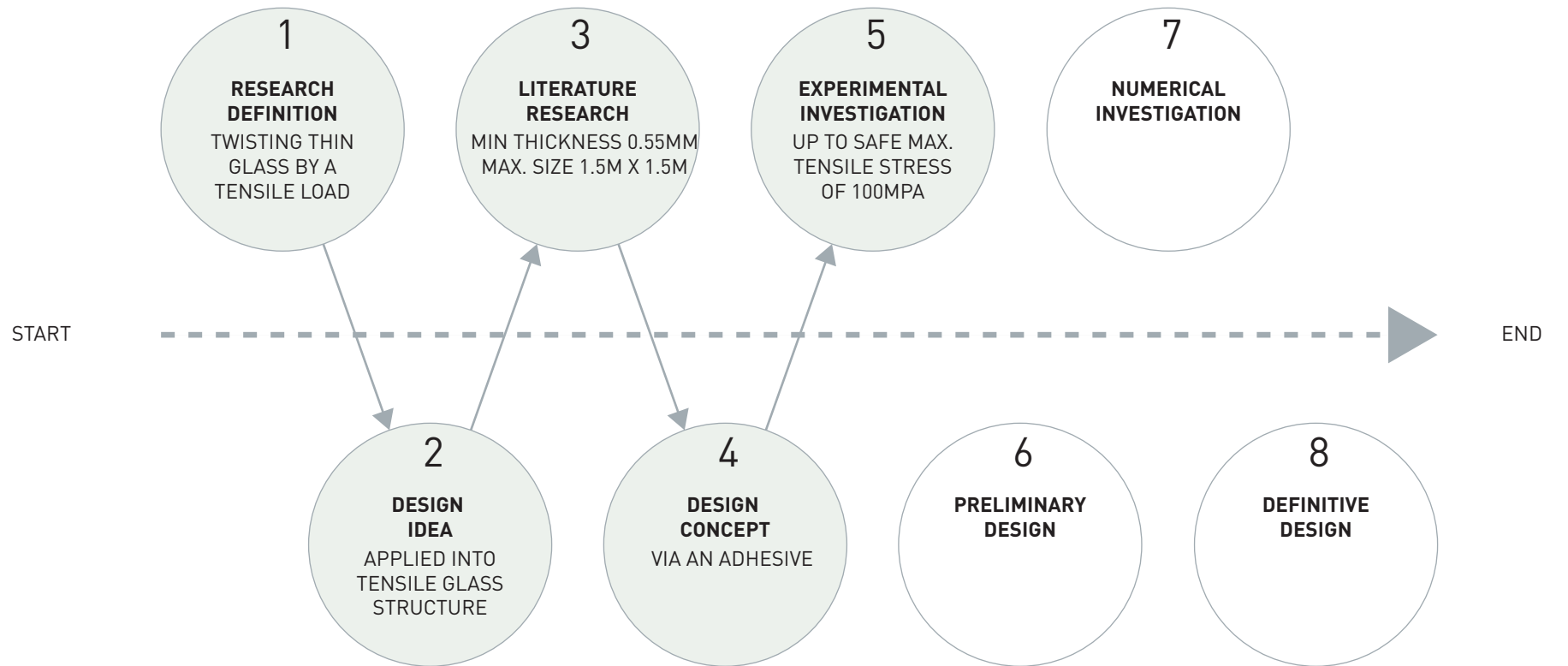
250 MPa

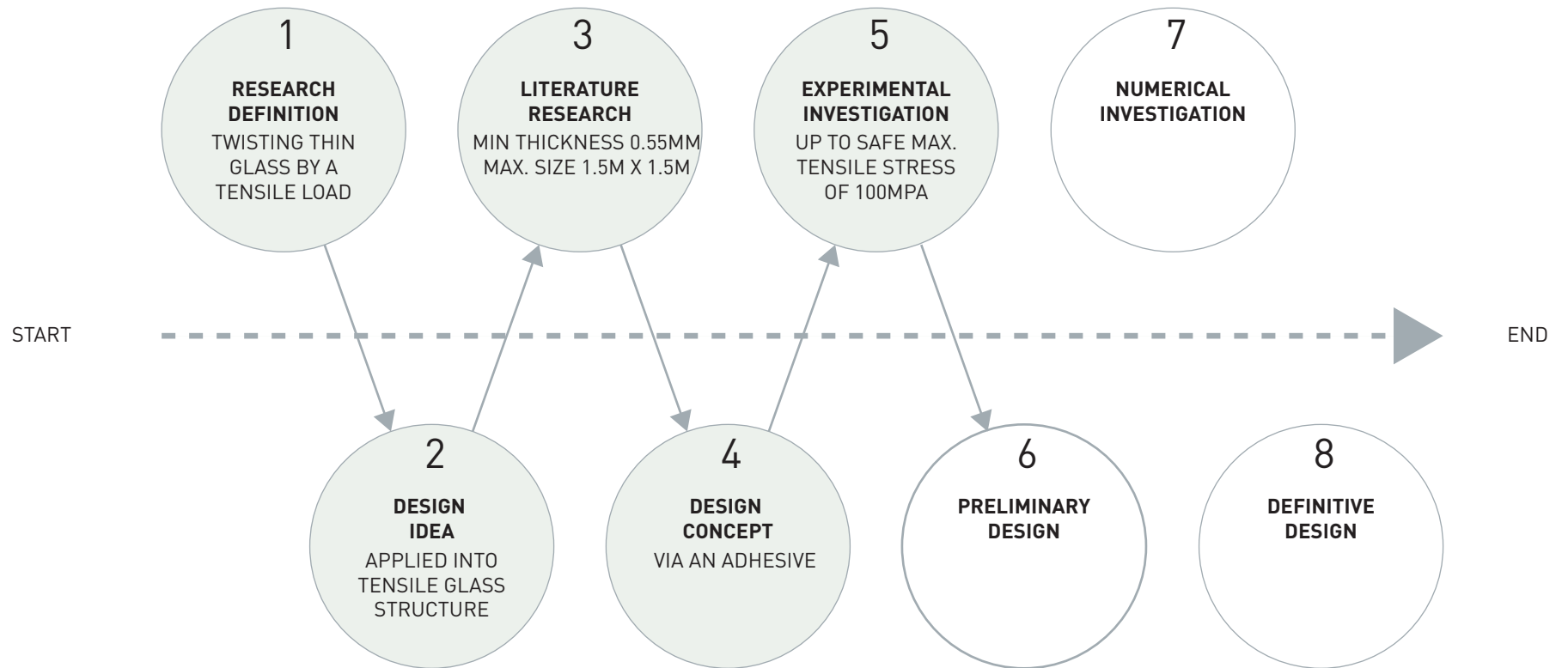
1/3 of the earlier mentioned bending
tensile strength of 750MPa...

Same yield strength as structural A36
steel!

...of course, there has to be a design safety
factor taken into account



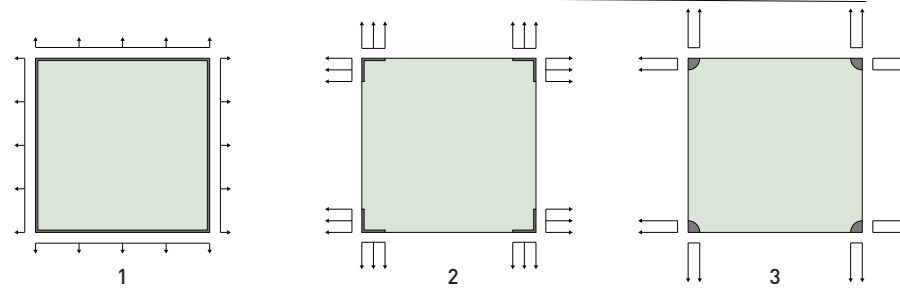




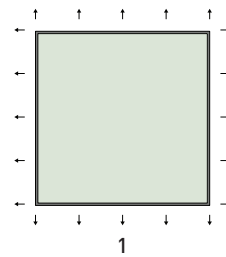
PRELIMINARY DESIGN

WHERE TO APPLY THE SUPPORT?

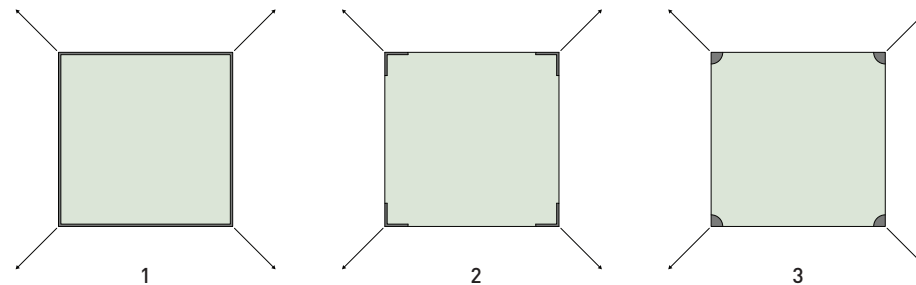
A. Linear distributed support



B. Linear support



C. Punctiform support



HOW DOES THE SUPPORT GOING TO LOOK LIKE?



Reviewed aspects:

- Easiness of fabrication & assembling
- Structural behaviour
- Lightweightness

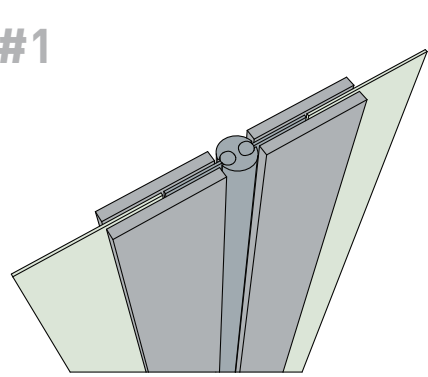
PRELIMINARY DESIGN

DESIGN OF THE CONNECTION

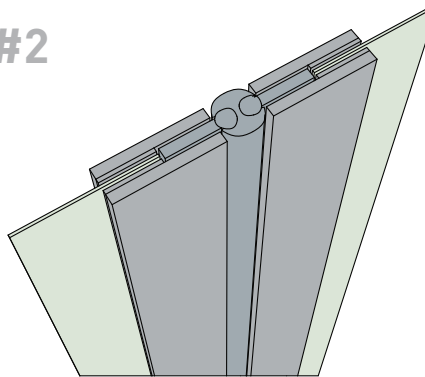
SWOT ANALYSES

DYNAMIC EDGE STIFFNESS

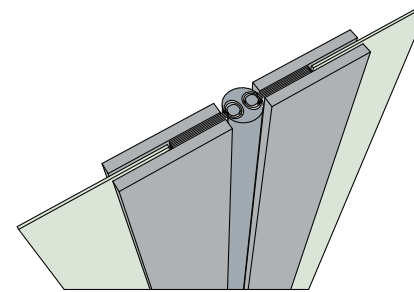
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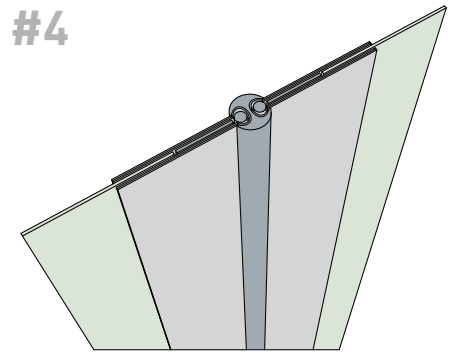
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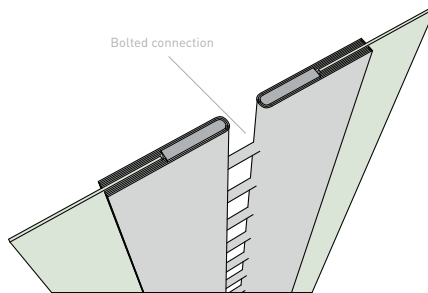
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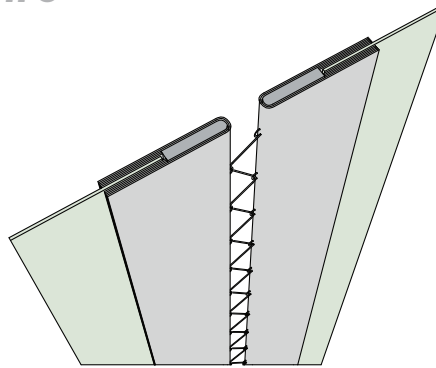
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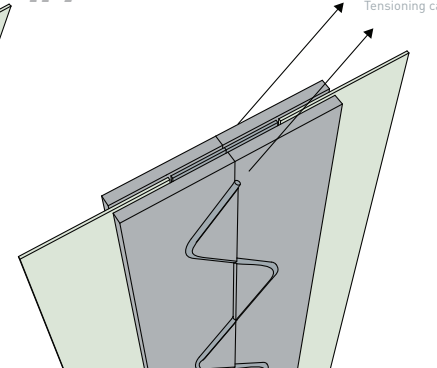
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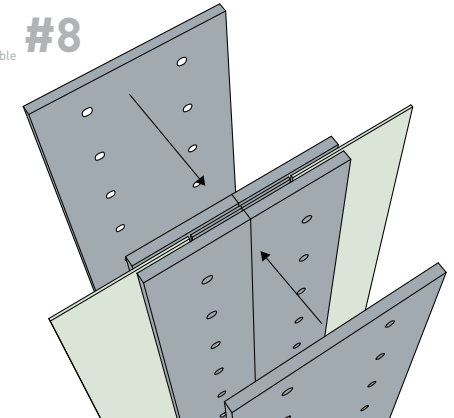
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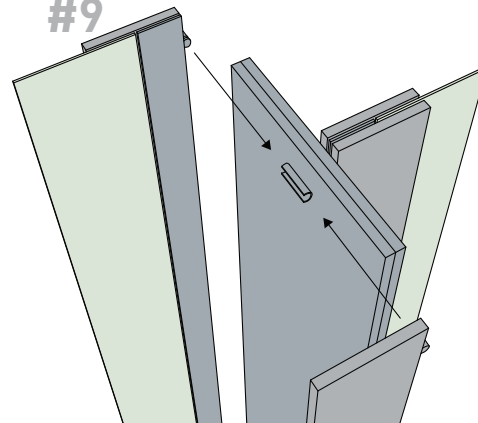
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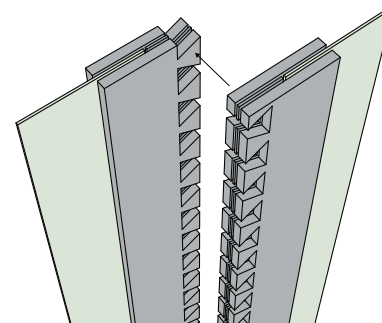
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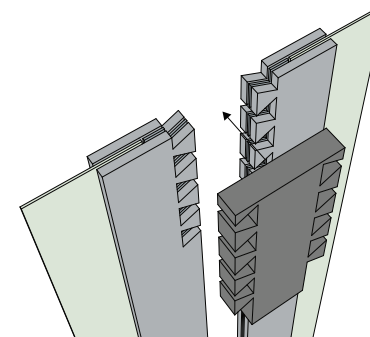
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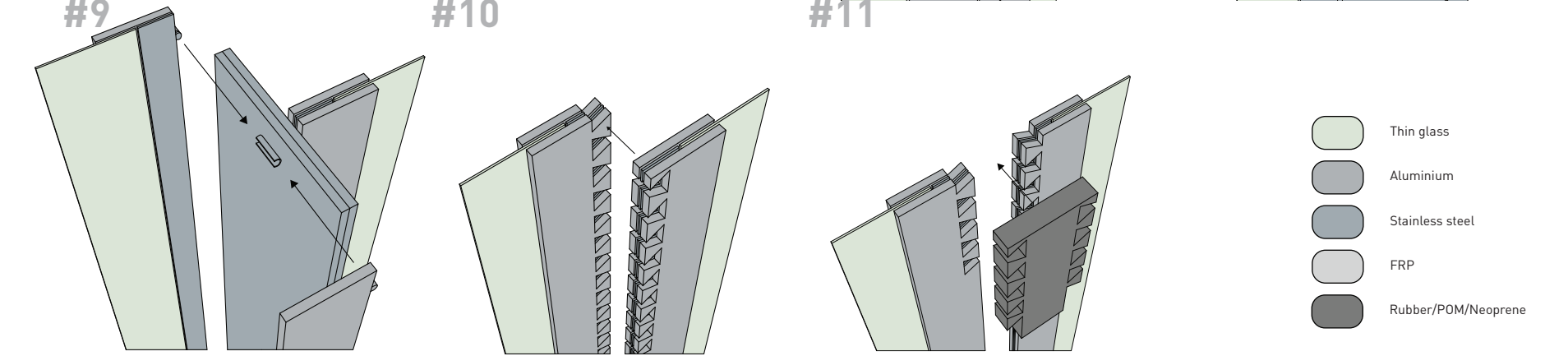
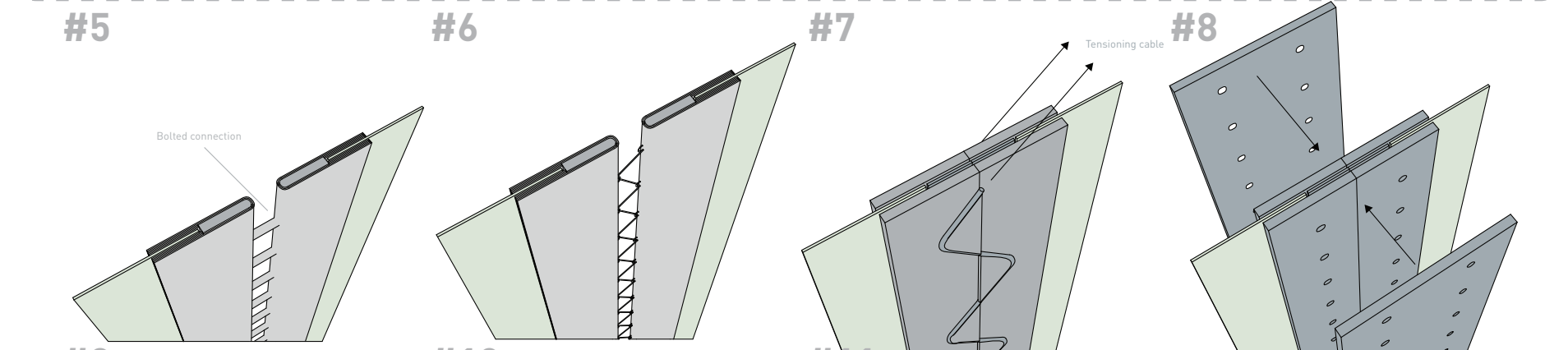
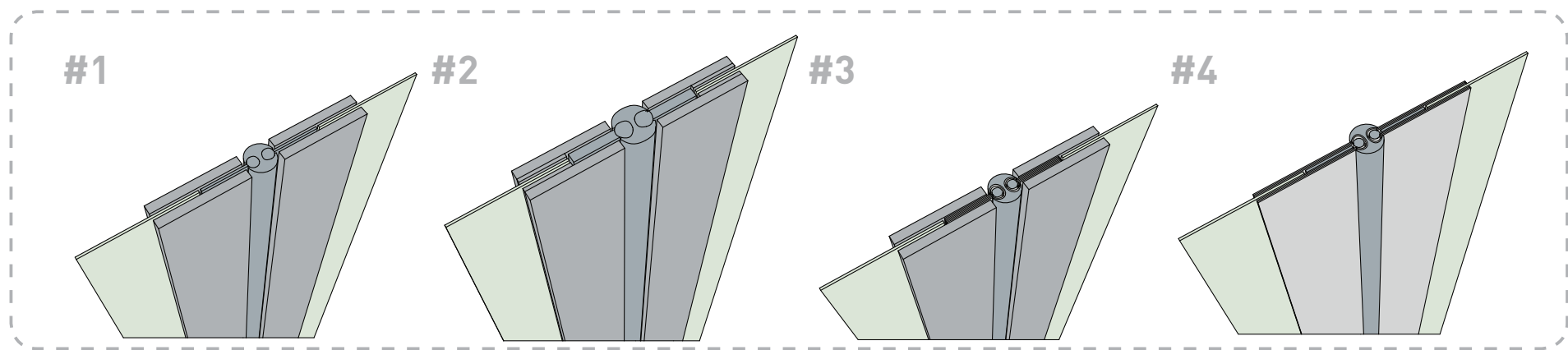
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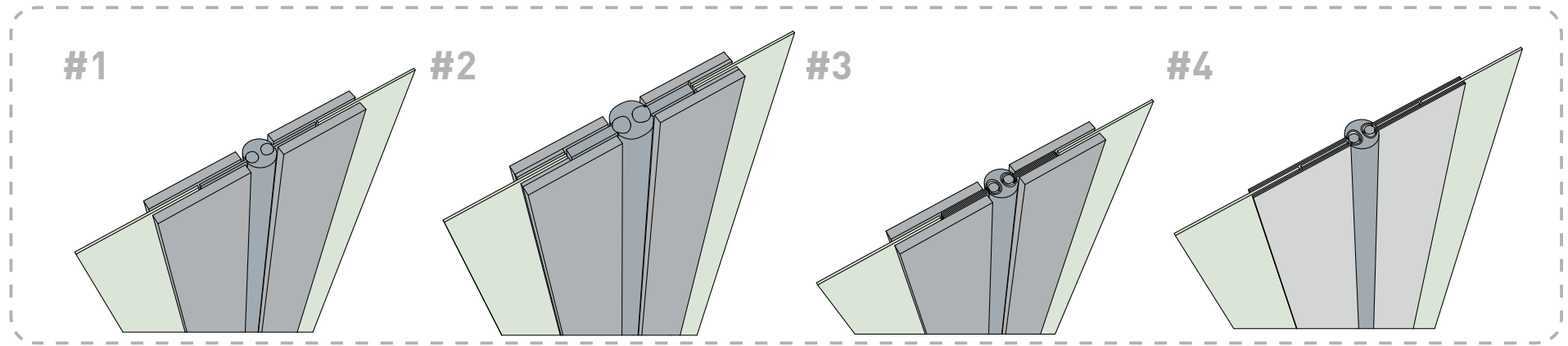
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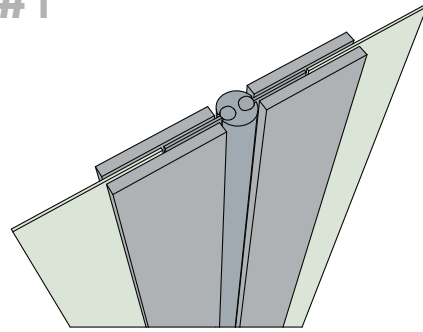
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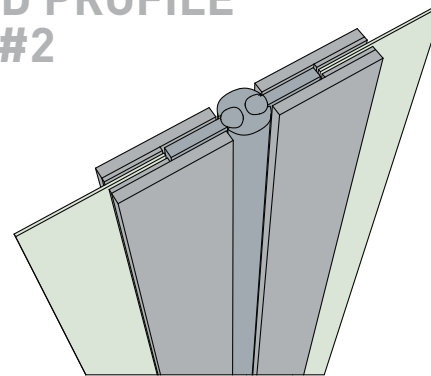
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CATEGORY EXTRUDED PROFILE

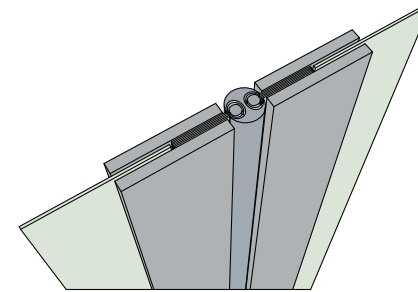
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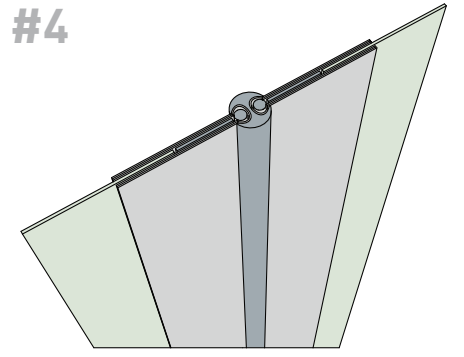
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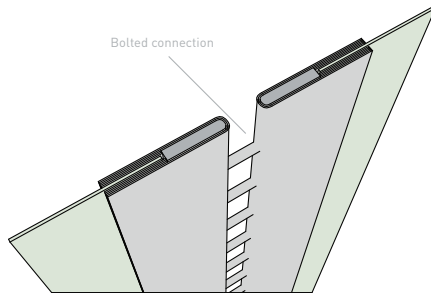
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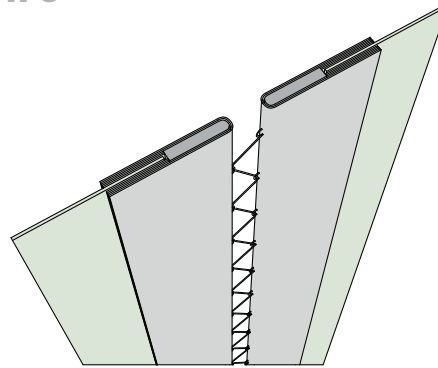
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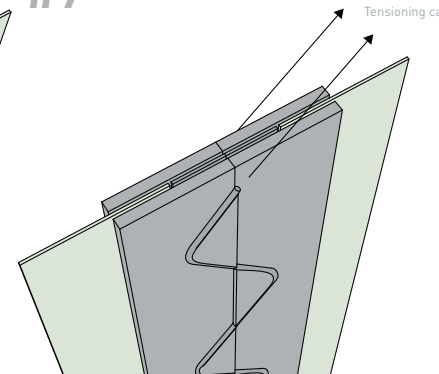
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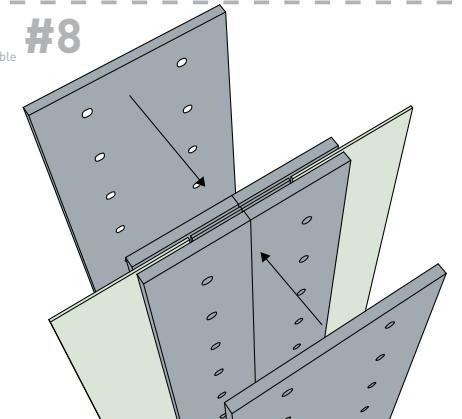
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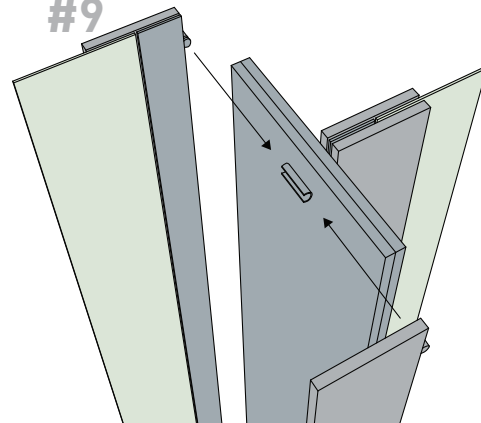
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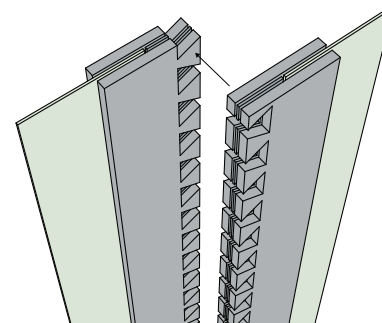
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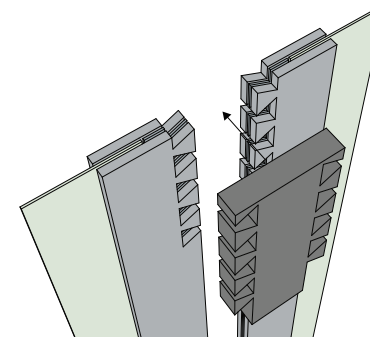
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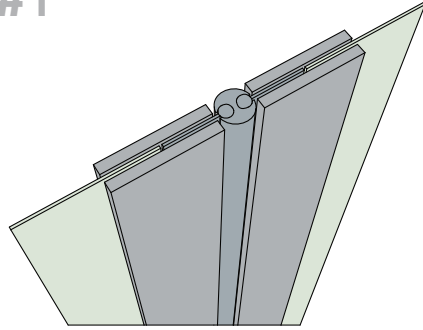
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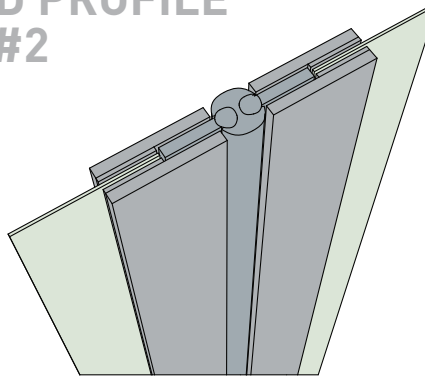
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CATEGORY EXTRUDED PROFILE

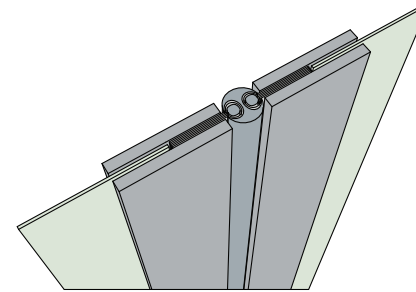
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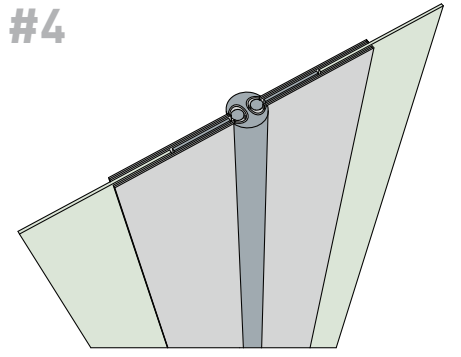
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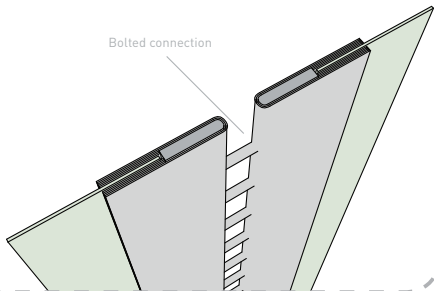
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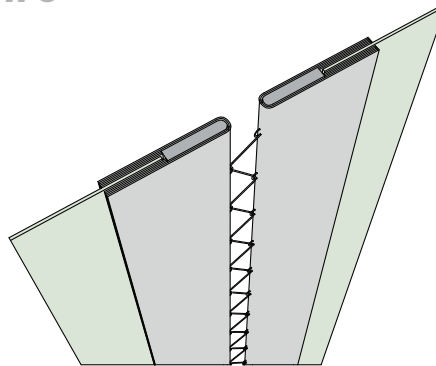
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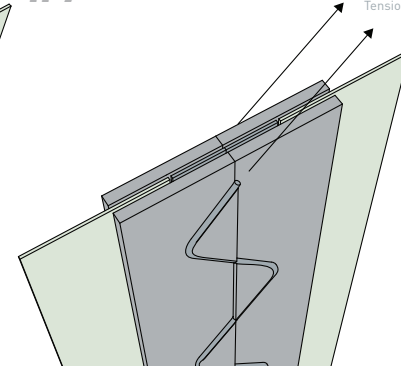
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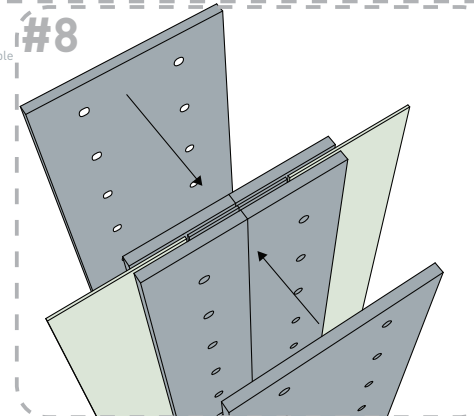
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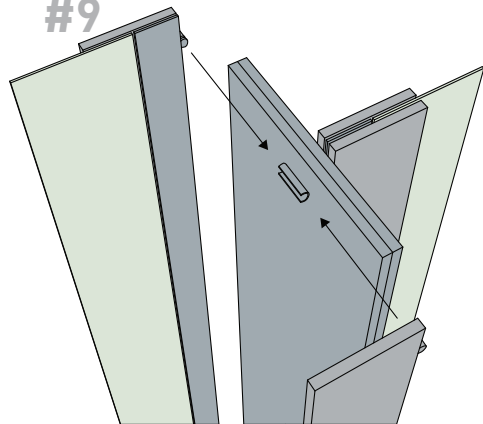
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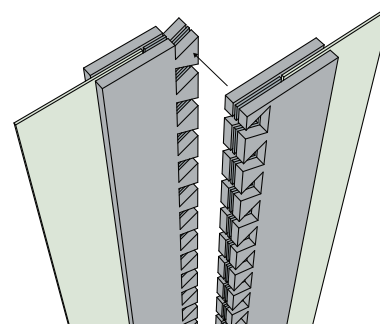
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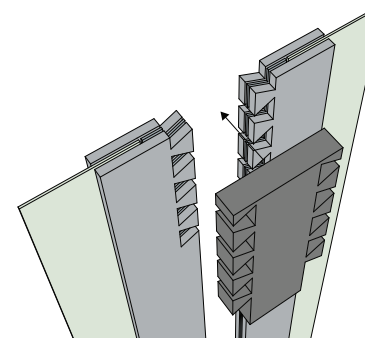
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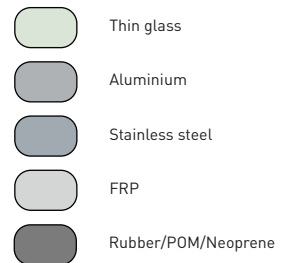
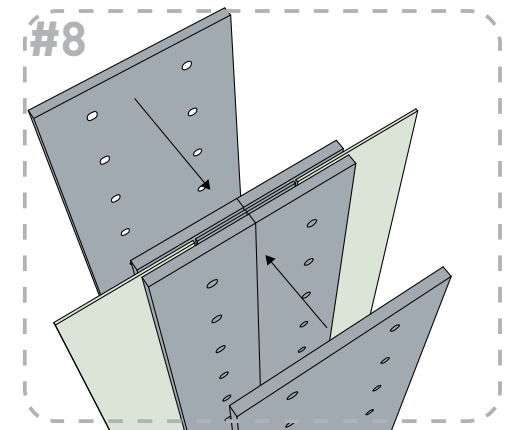
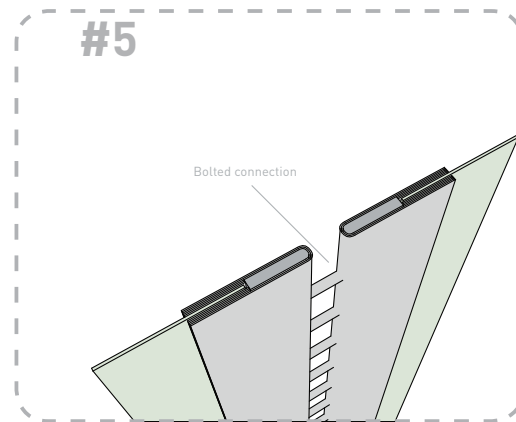
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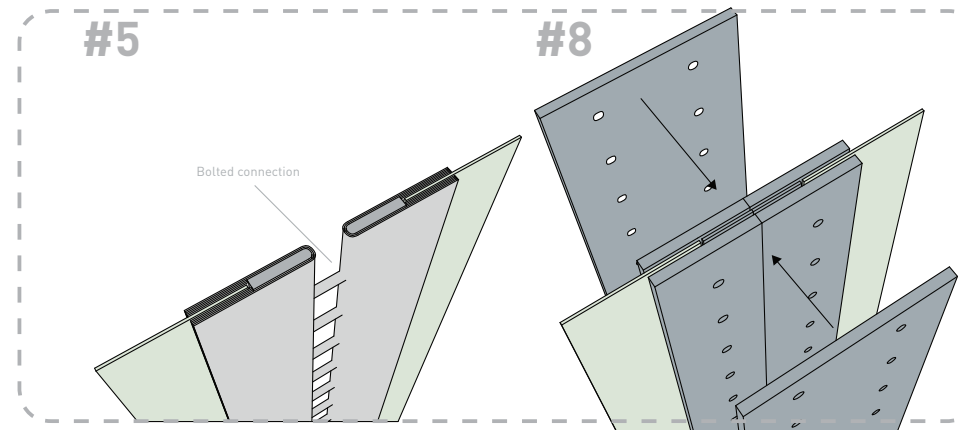
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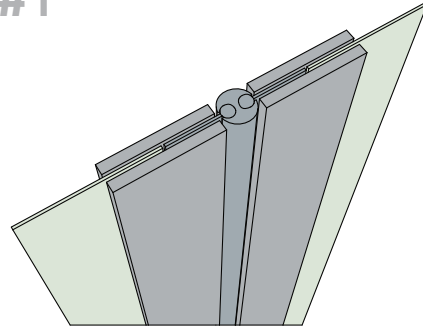
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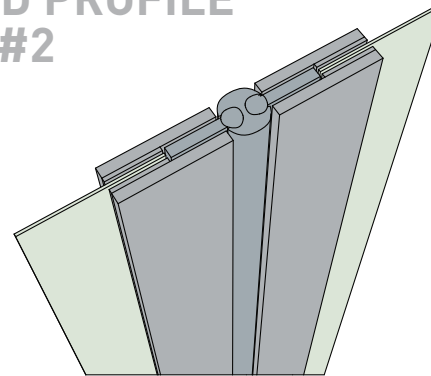
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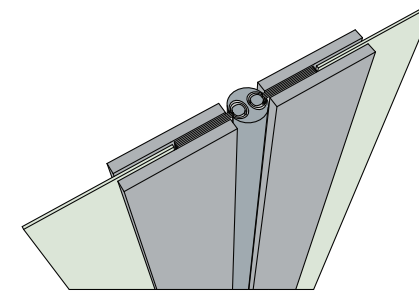
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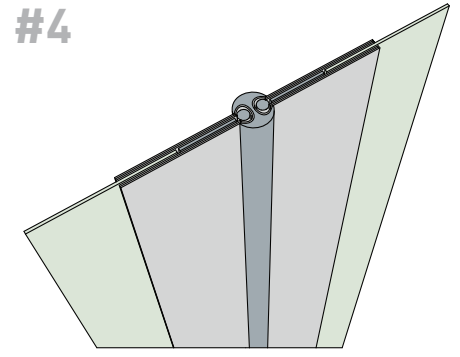
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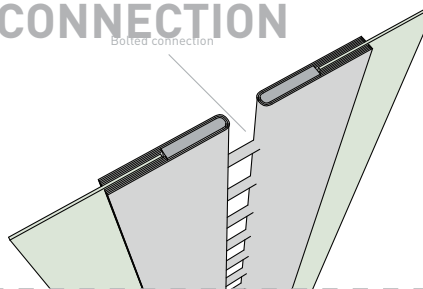


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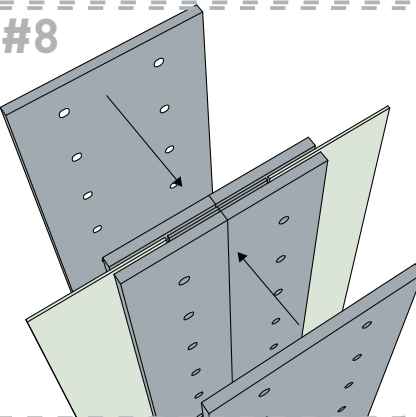


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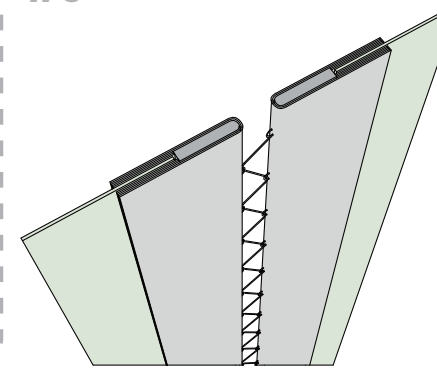
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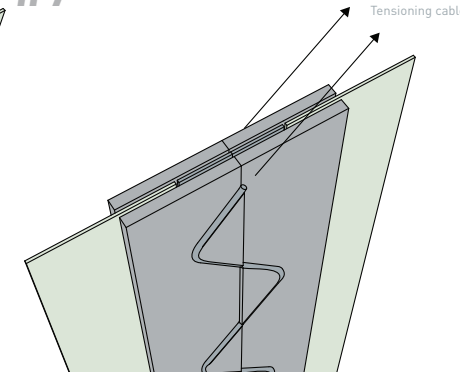
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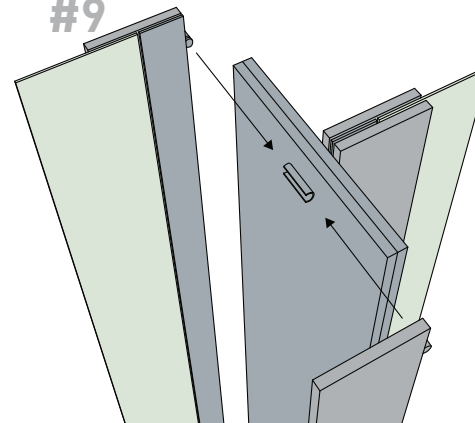
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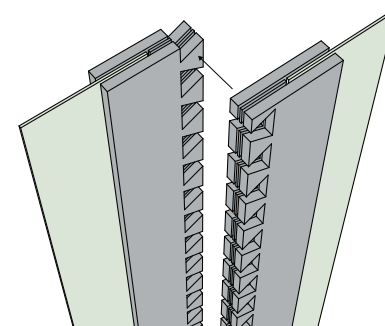
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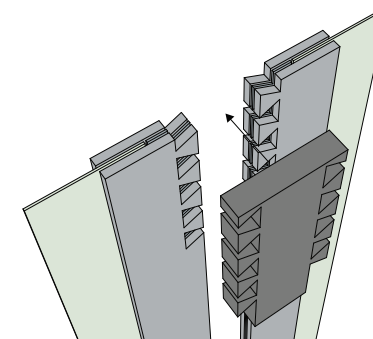
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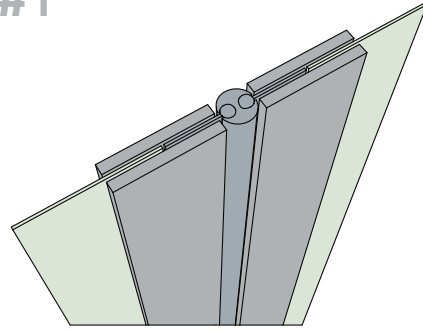
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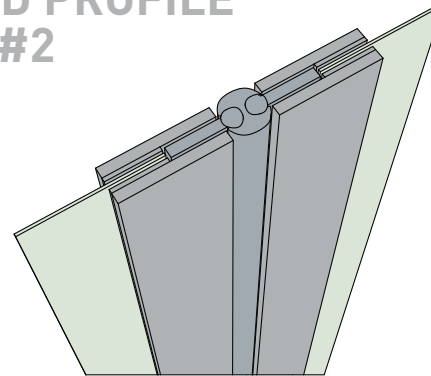
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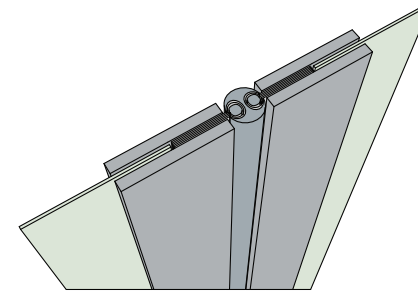
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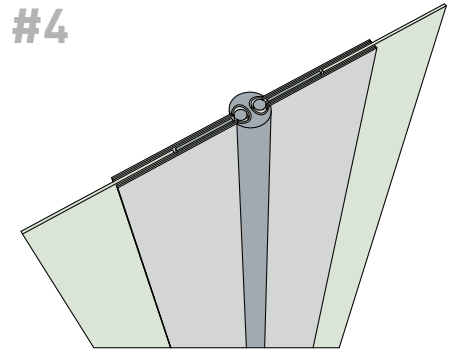
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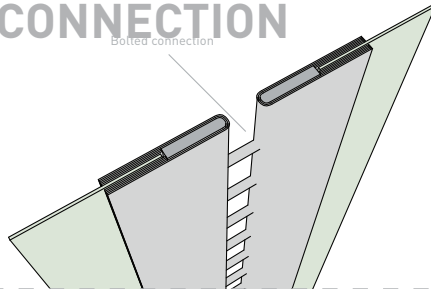


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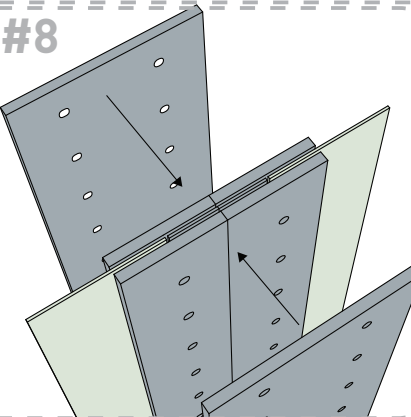


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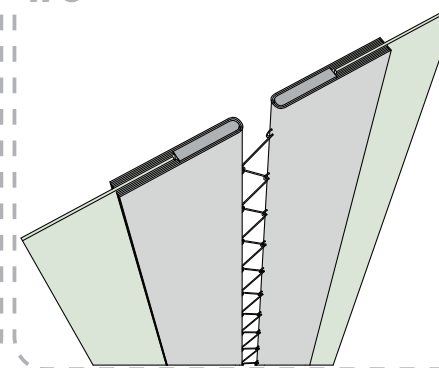
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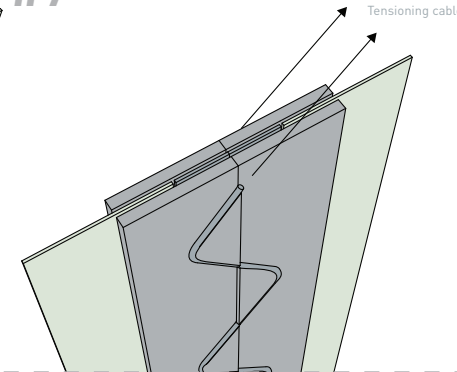
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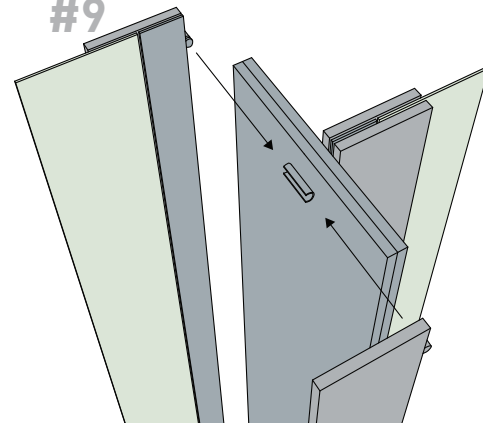
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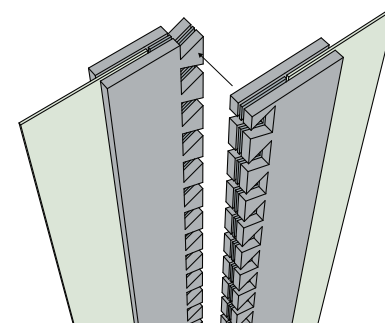
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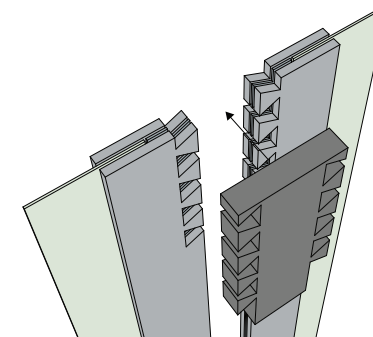
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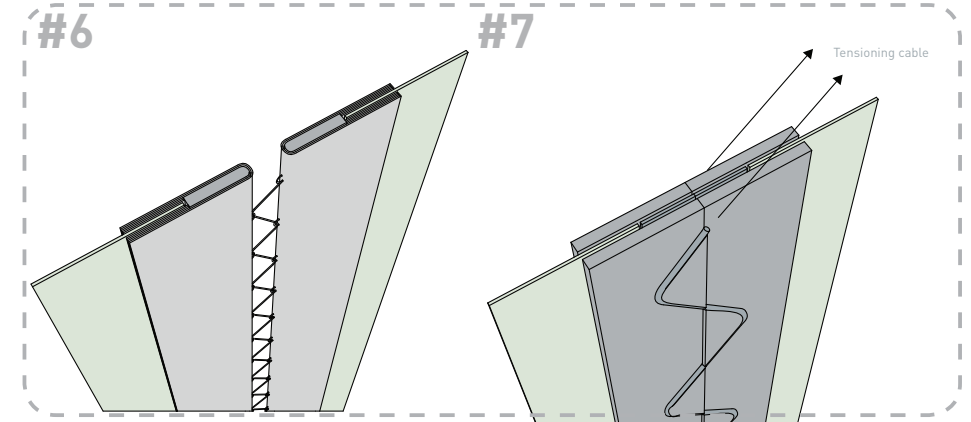
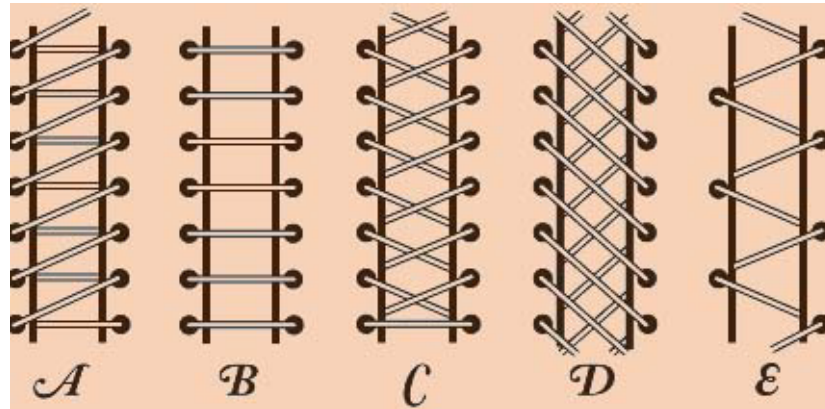
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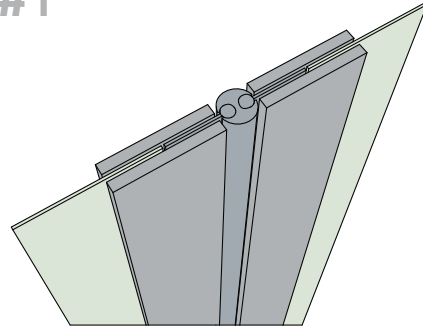
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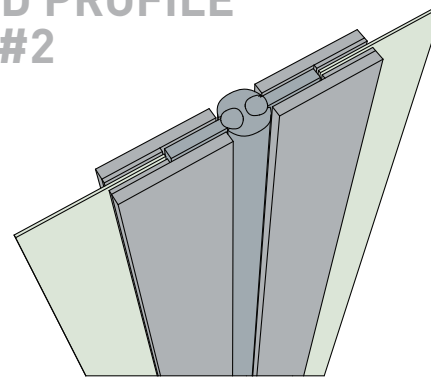
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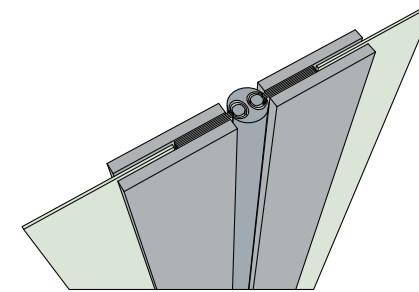
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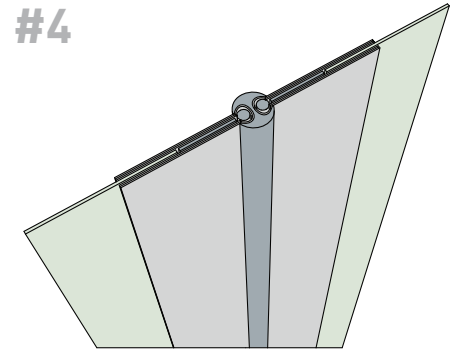
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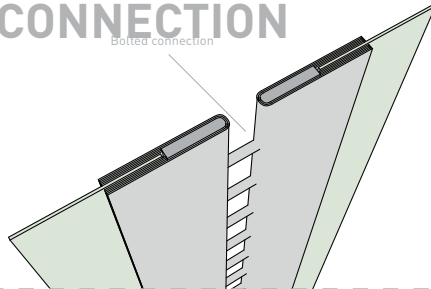


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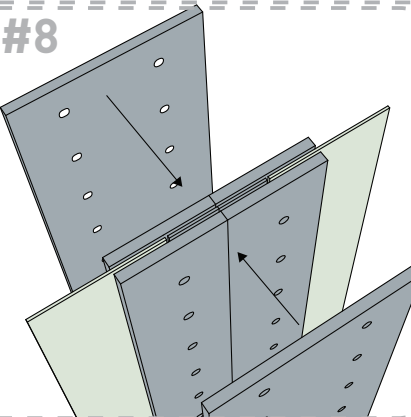


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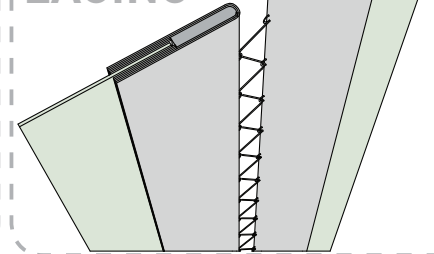


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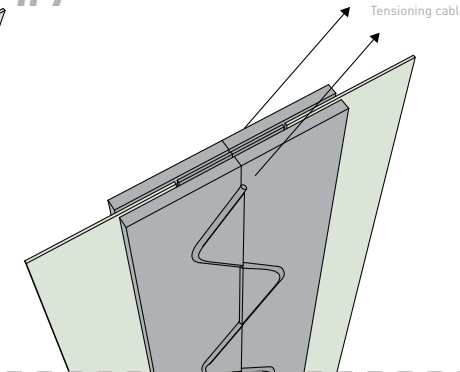


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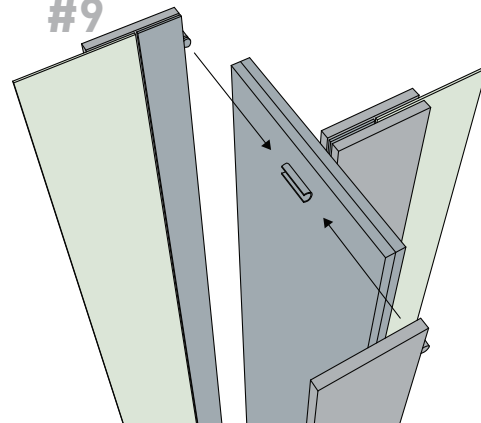
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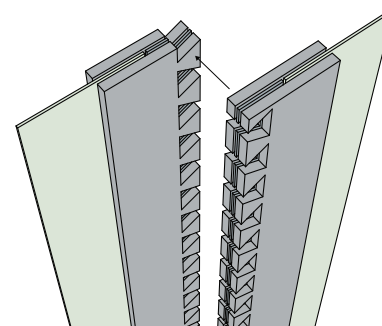
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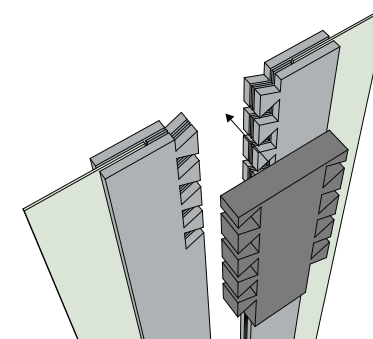
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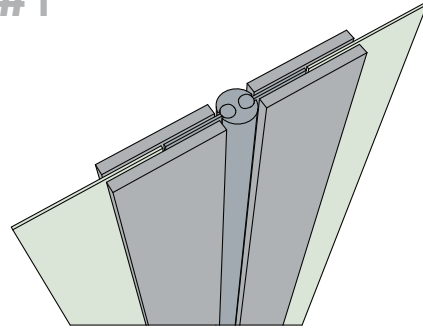
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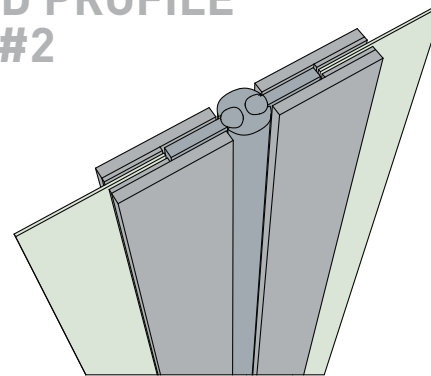
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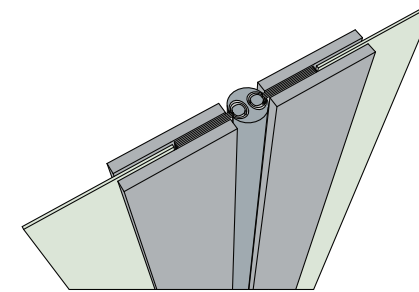
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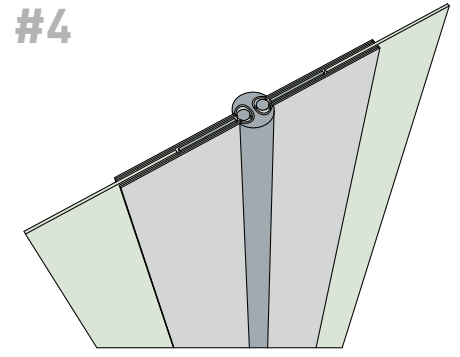
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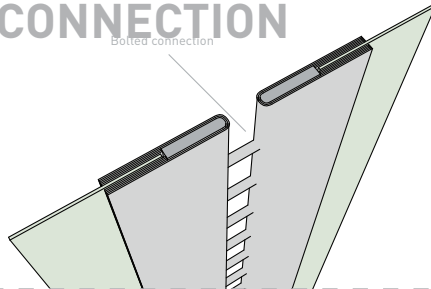


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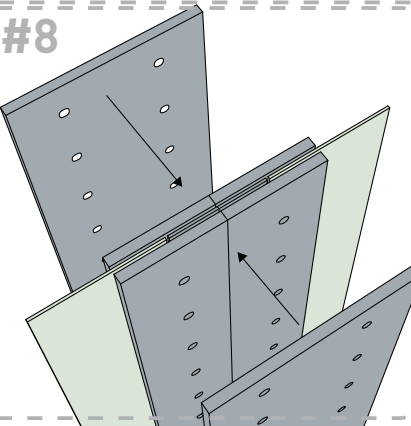


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CATEGORY BOLTED CONNECTION

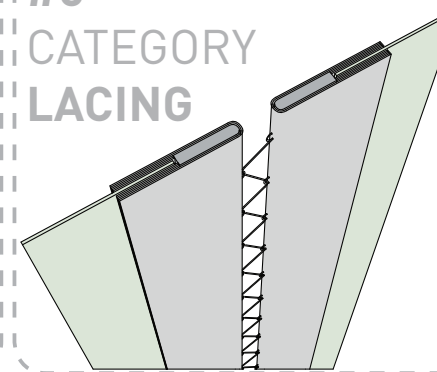


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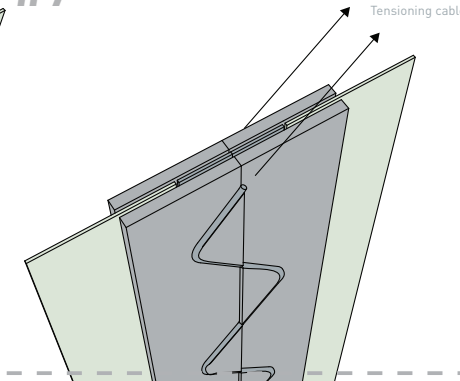


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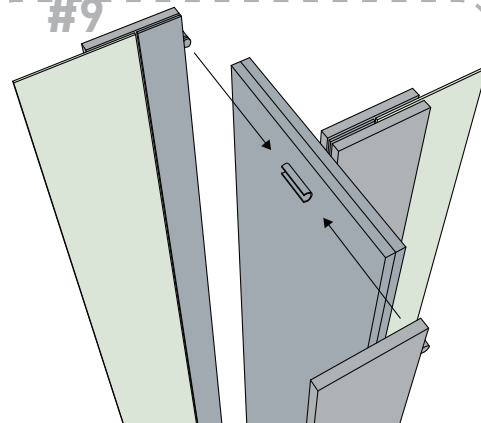
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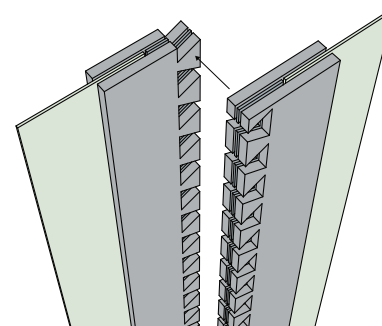
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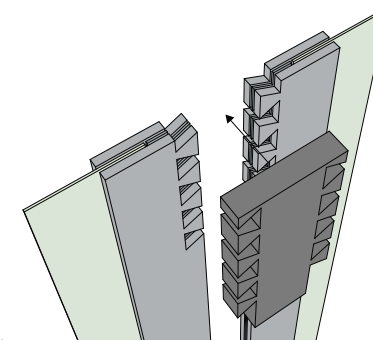
#9








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#11



-  Thin glass
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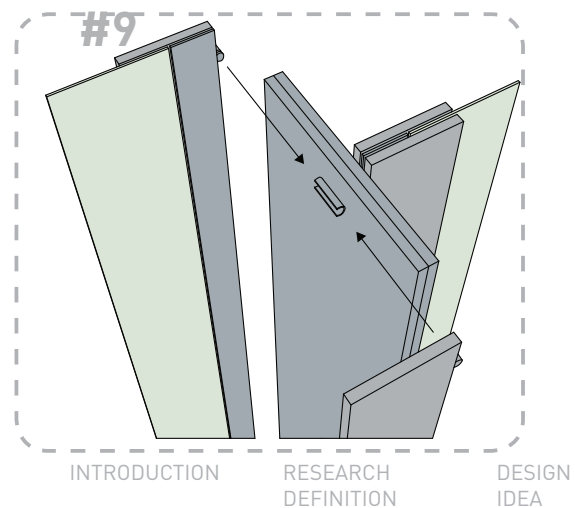
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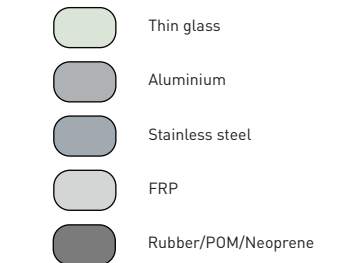
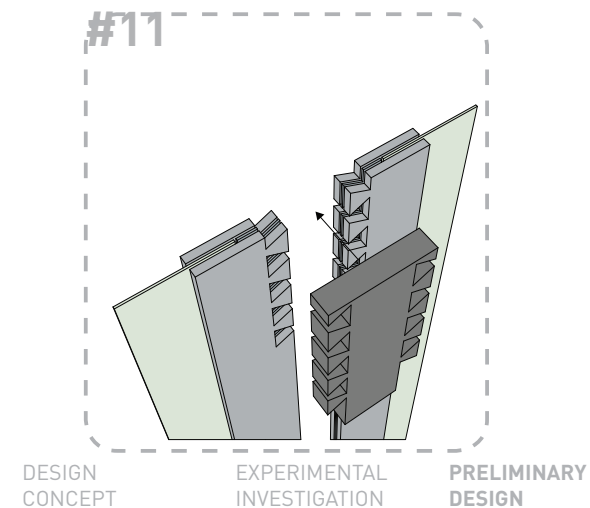
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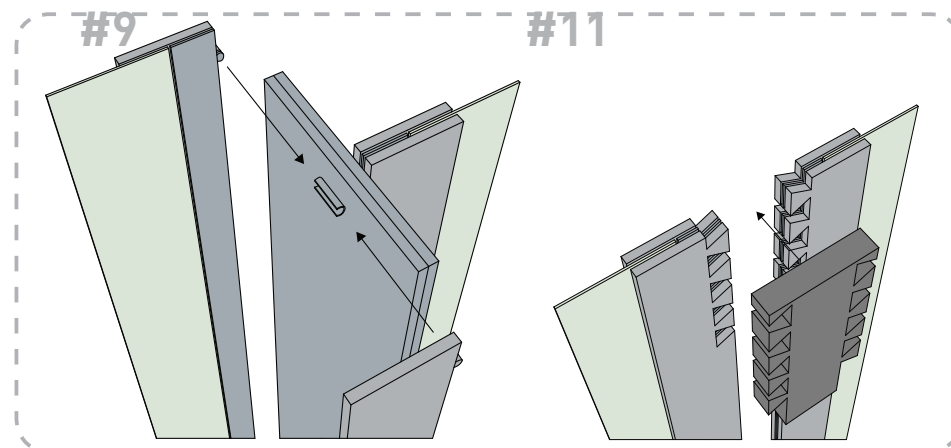
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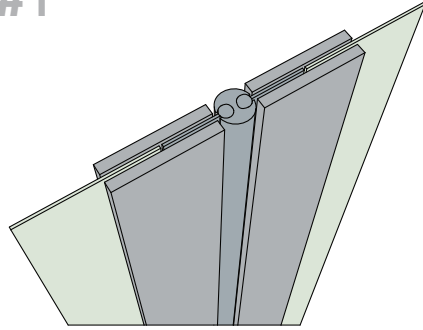
DESIGN OF THE CONNECTION

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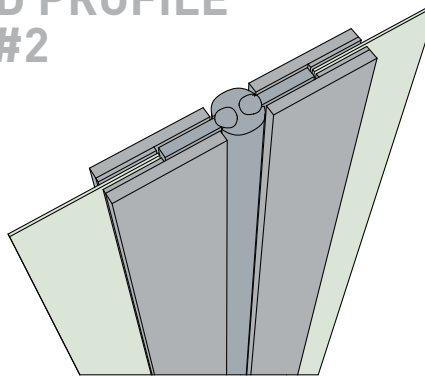
DYNAMIC EDGE STIFFNESS

CATEGORY EXTRUDED PROFILE

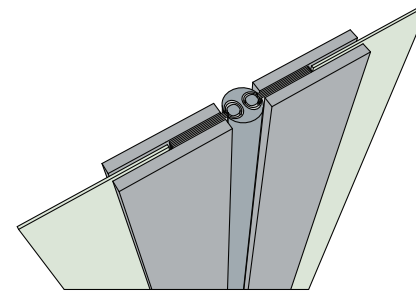
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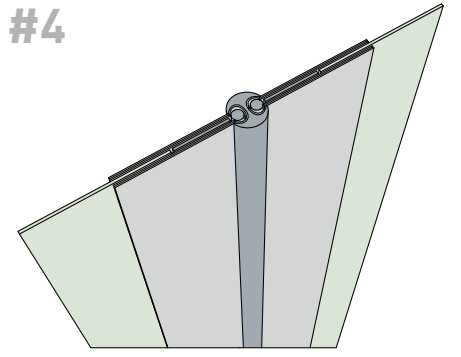
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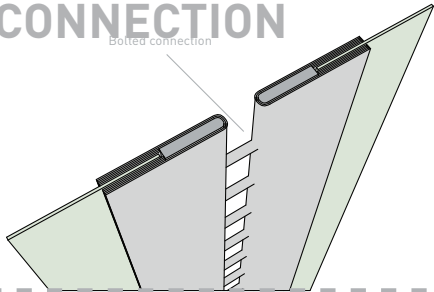


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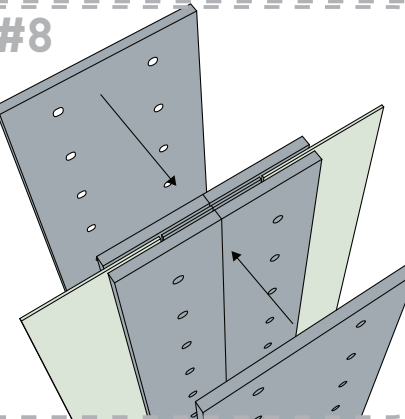


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CATEGORY BOLTED CONNECTION

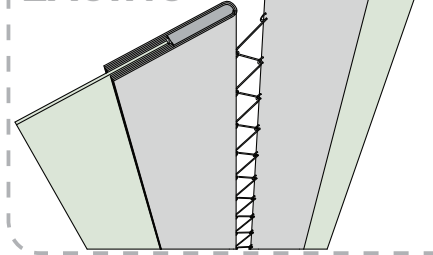


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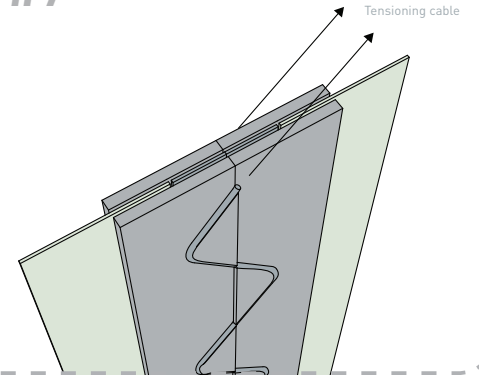


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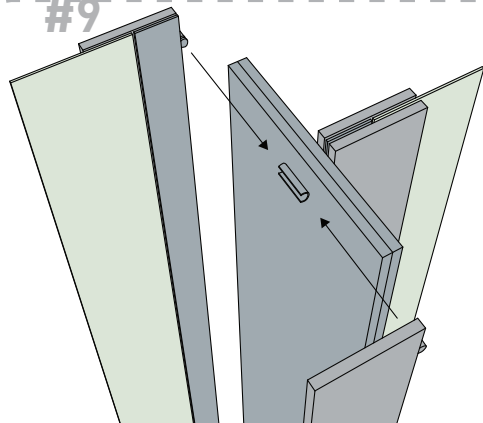
CATEGORY LACING



#7

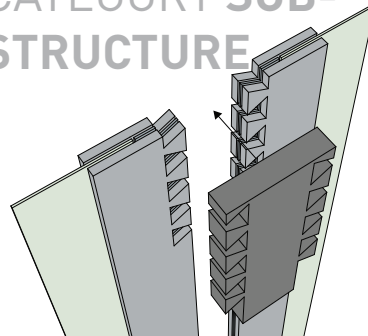


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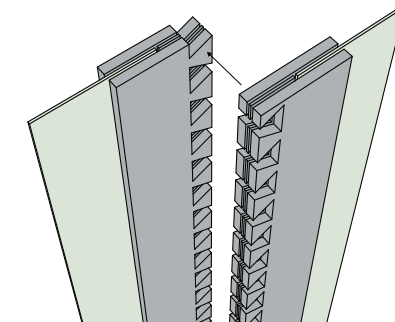


#11

CATEGORY SUB-STRUCTURE



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- Thin glass
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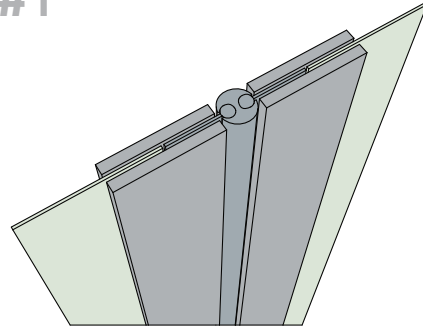
DESIGN OF THE CONNECTION

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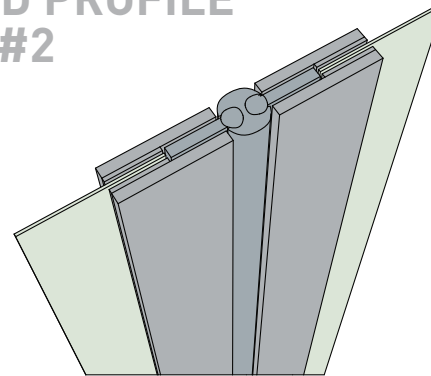
DYNAMIC EDGE STIFFNESS

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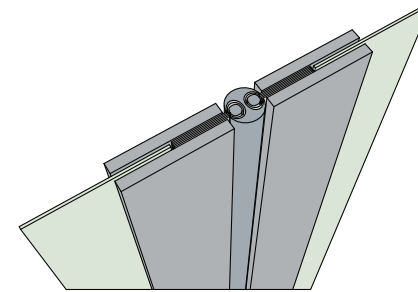
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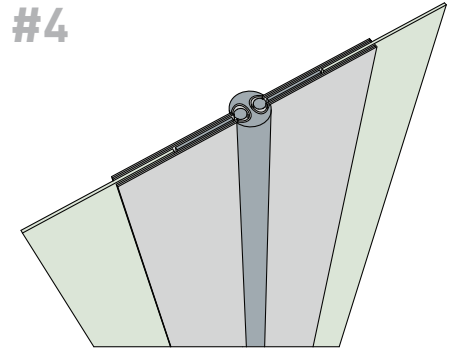
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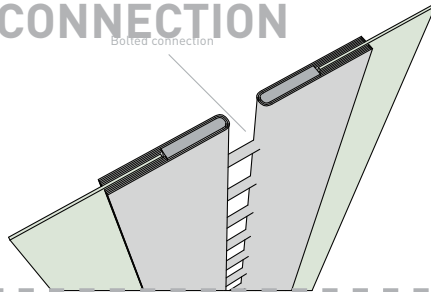


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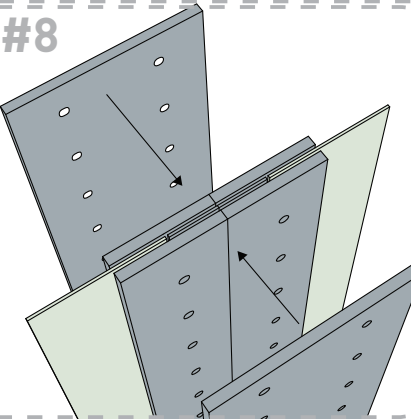


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CATEGORY BOLTED CONNECTION

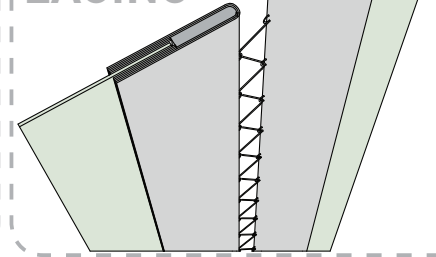


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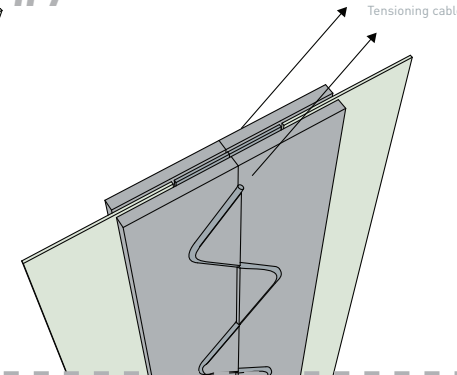


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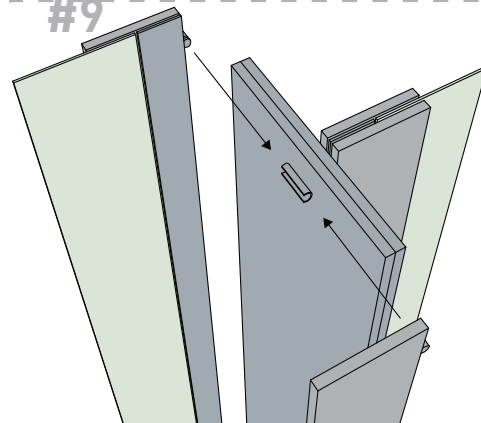
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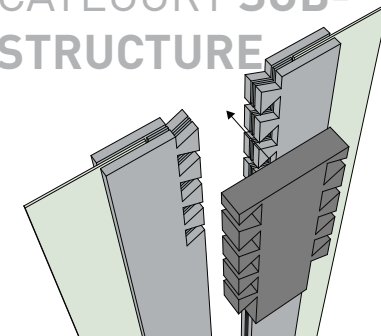


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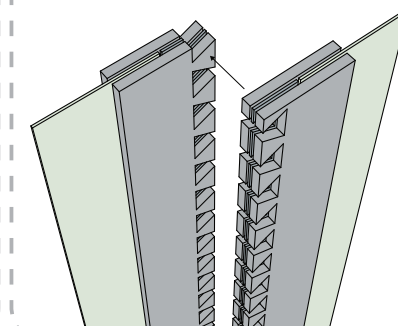


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- Thin glass
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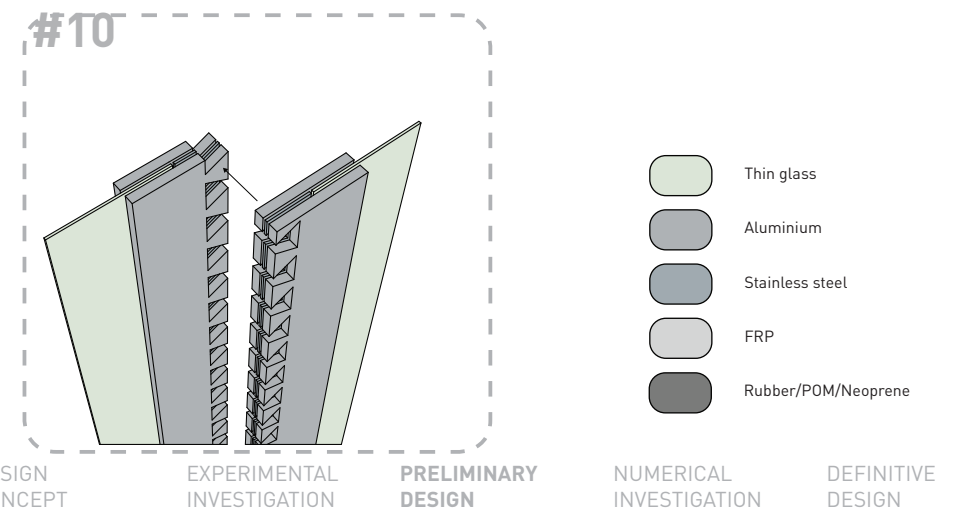
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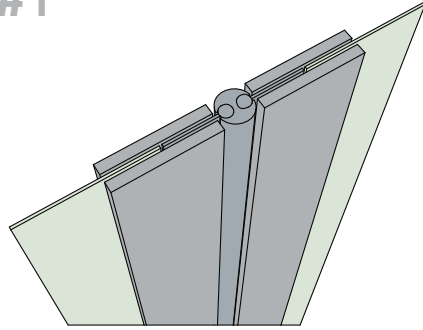
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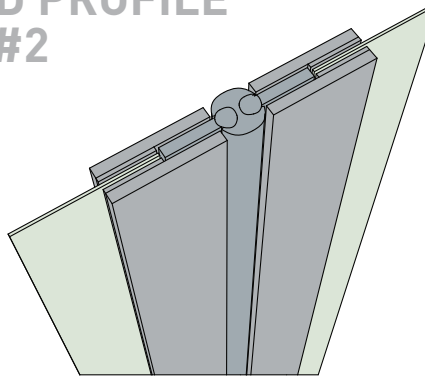
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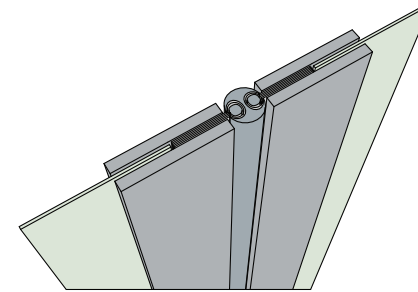
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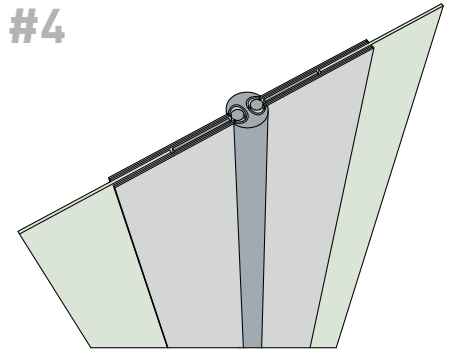
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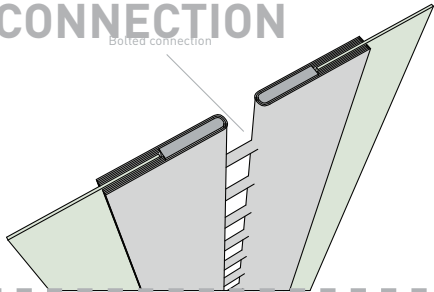


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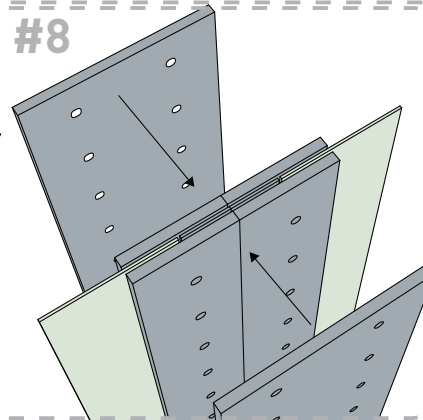


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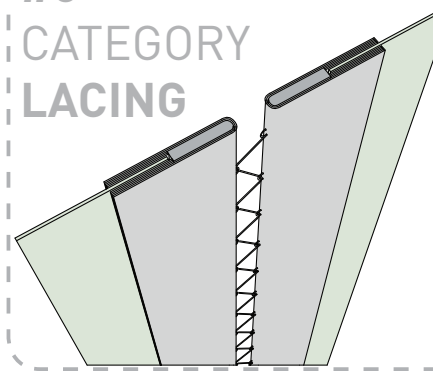


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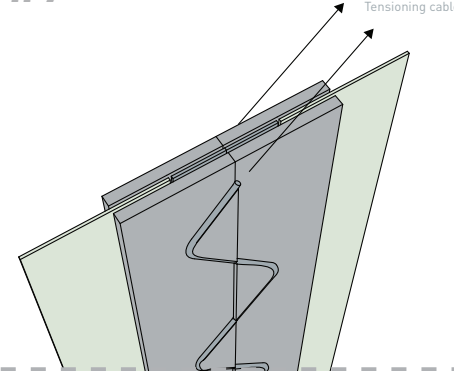


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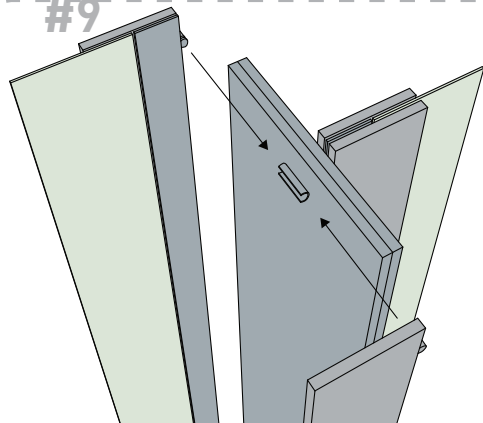
CATEGORY LACING



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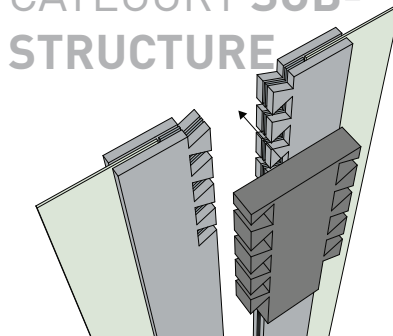


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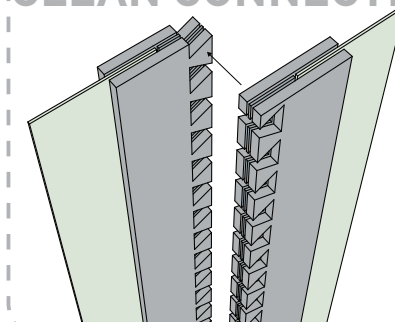
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




CATEGORY SUB-STRUCTURE



#10

CATEGORY CLEAN CONNECTION



-  Thin glass
-  Aluminium
-  Stainless steel
-  FRP
-  Rubber/POM/Neoprene

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CATEGORY **BOLTED CONNECTION**



CATEGORY **LACING**








CATEGORY **SUB-STRUCTURE**



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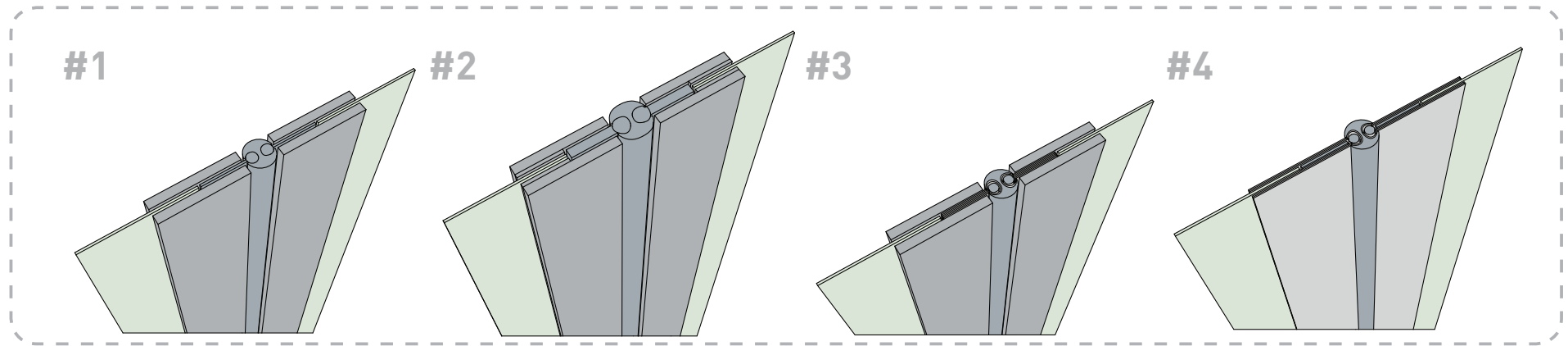
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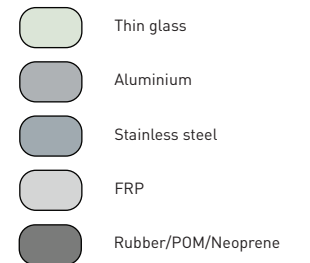
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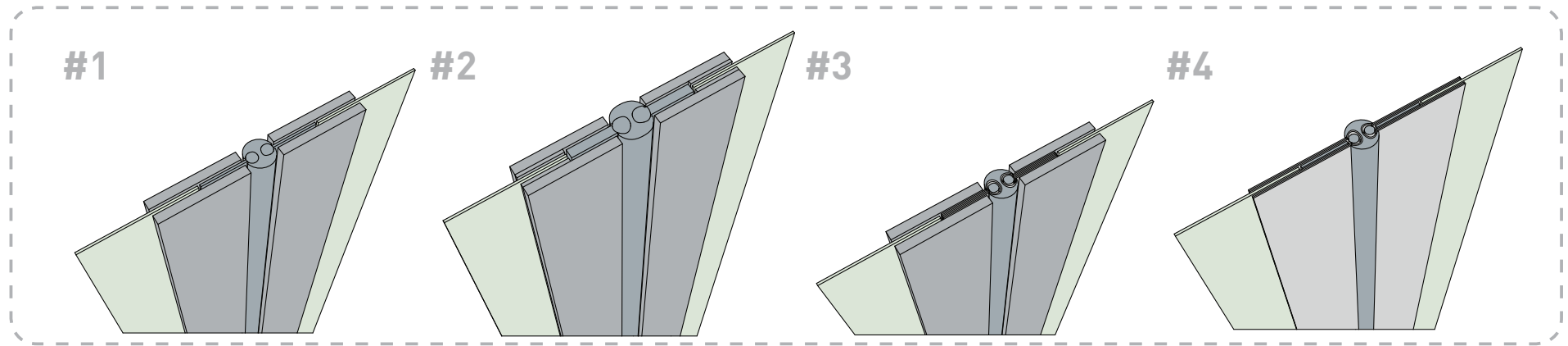
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- TOO HEAVY

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- Thin glass
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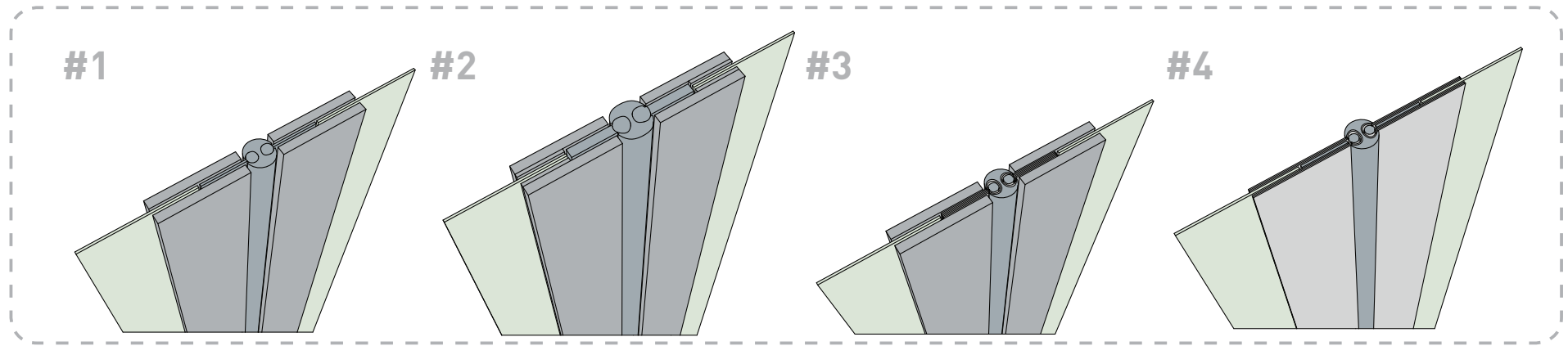
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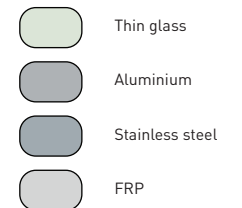
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- HIGH INTERNAL STRESSES
IN EXTRUDED PROFILE

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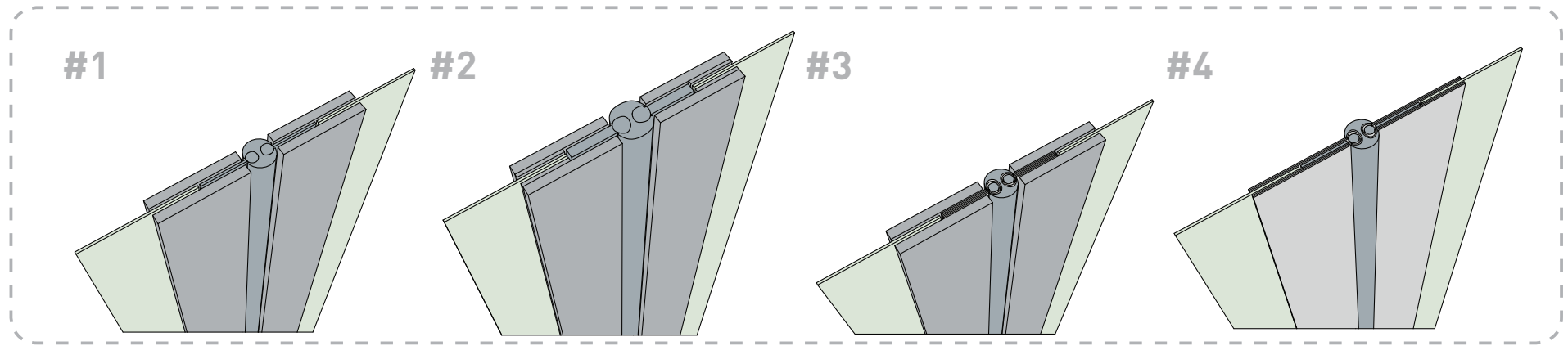


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- DIFFICULT TO FABRICATE

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- Thin glass
- Aluminium
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- FRP

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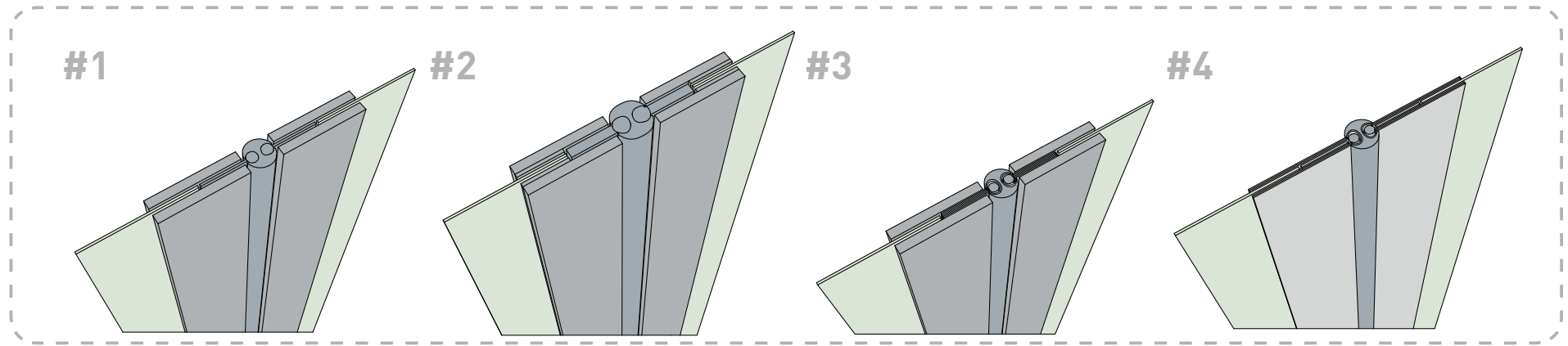
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- DIFFICULT TO ASSEMBLY

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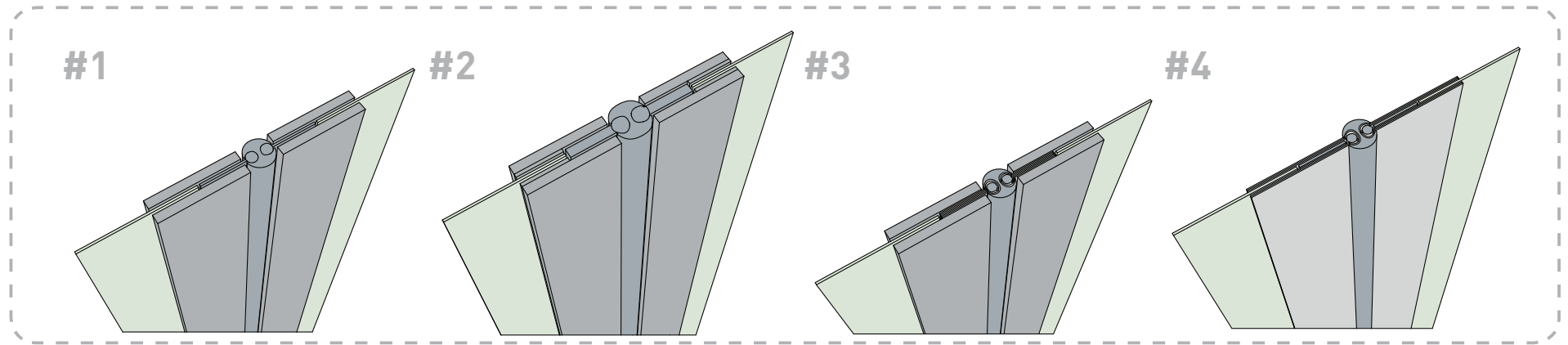
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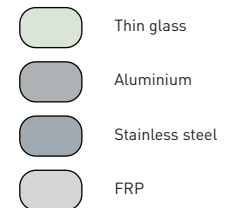
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+ TENSILE STRESSES CAN BE CONTROLLED BY COMPOSITE MATERIAL

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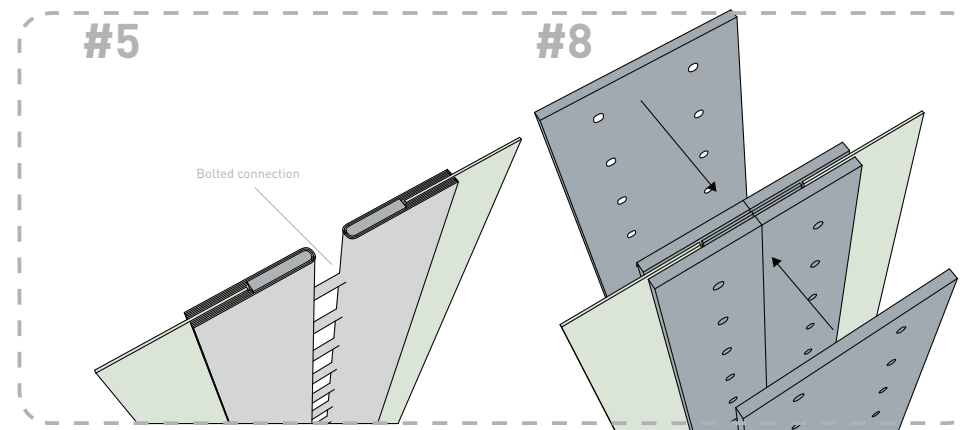
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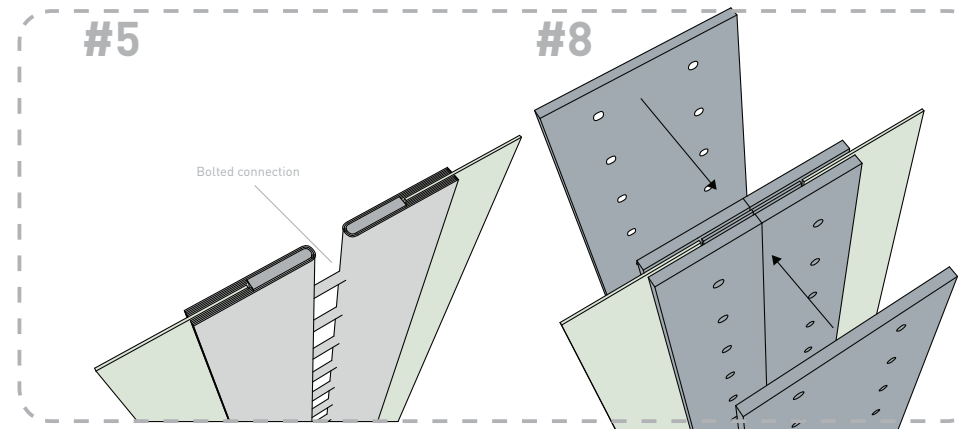
CATEGORY II BOLTED CONNECTION



- DISTANCE BETWEEN PANELS

- Thin glass
- Aluminium
- Stainless steel
- FRP

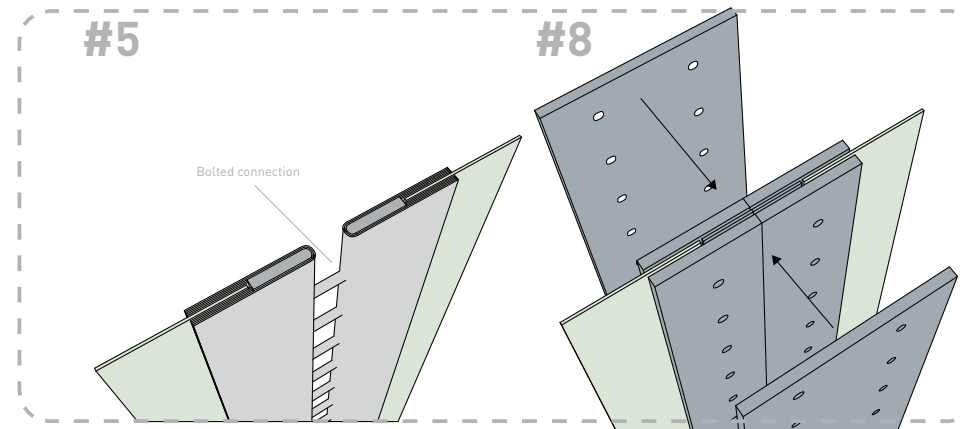
CATEGORY II BOLTED CONNECTION



+ REDUCED DISTANCE BETWEEN PANELS

- Thin glass
- Aluminium
- Stainless steel
- FRP

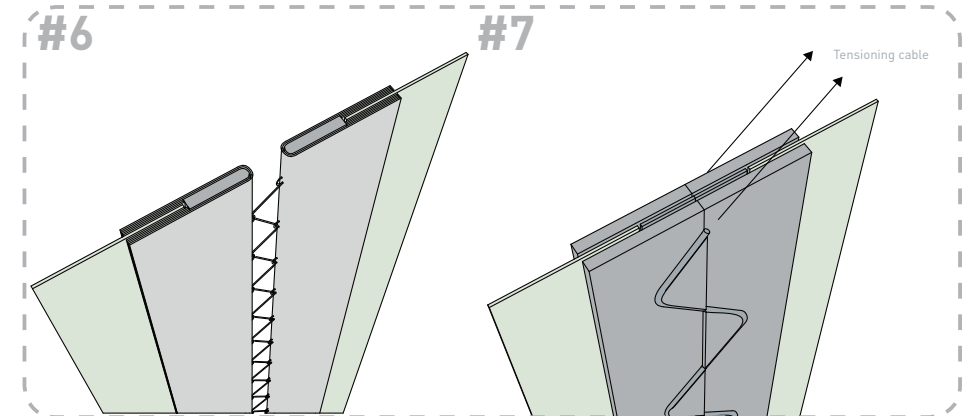
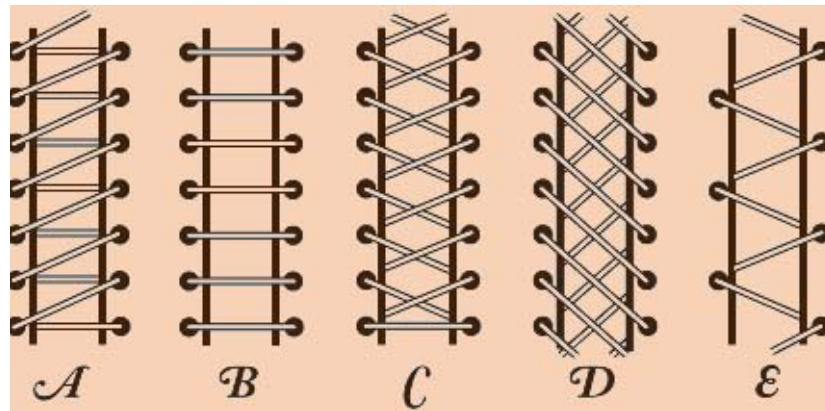
CATEGORY II BOLTED CONNECTION



- LOTS OF BOLTS

- Thin glass
- Aluminium
- Stainless steel
- FRP

CATEGORY III LACING



- DIFFICULT TO MOUNT

- Thin glass
- Aluminium
- Stainless steel
- FRP

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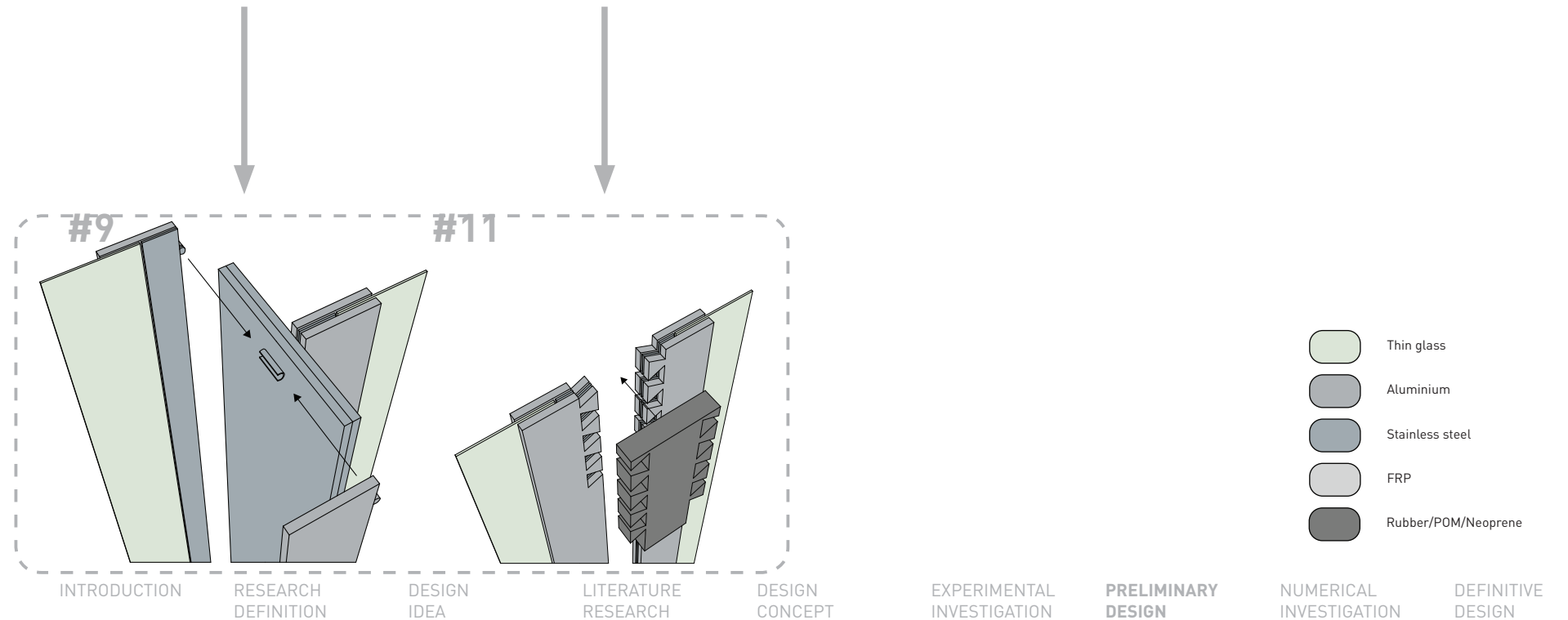
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CATEGORY IV SUBSTRUCTURE

- LOTS OF SUBSTRUCTURE → LOOSING TRANSPARENCY



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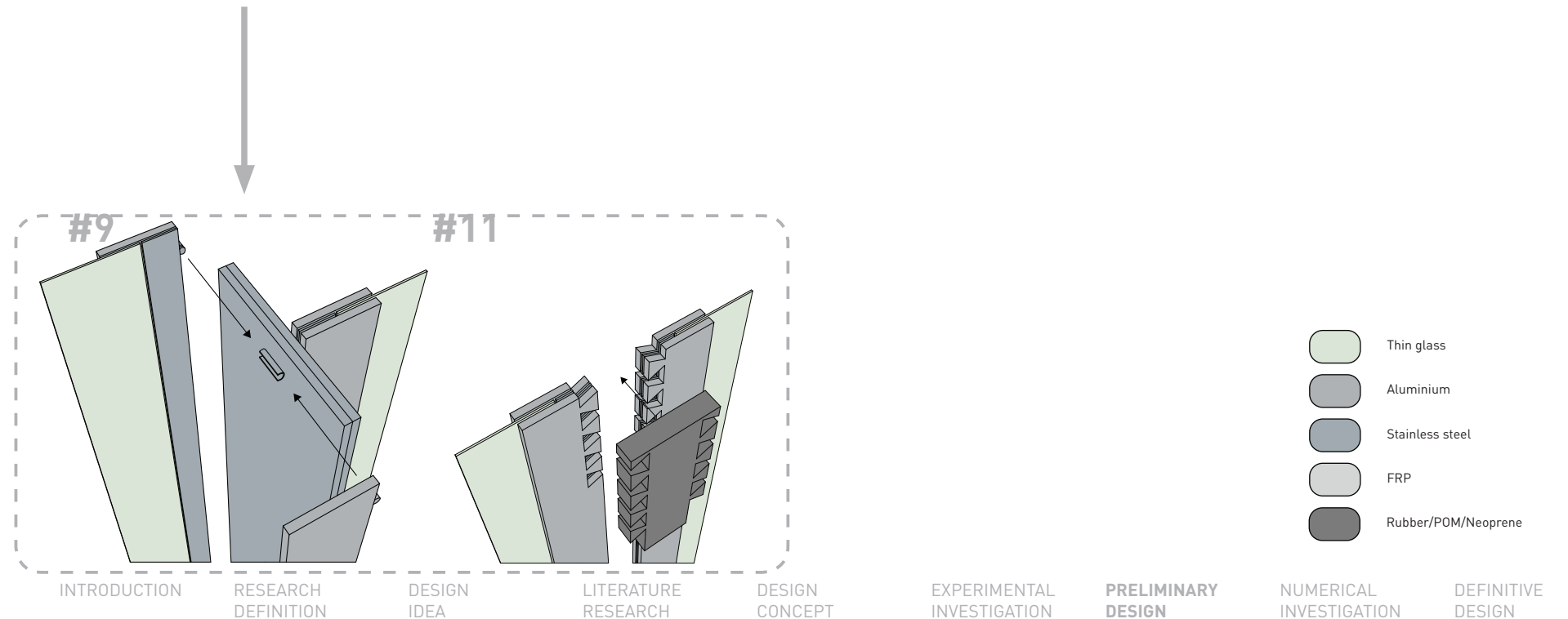
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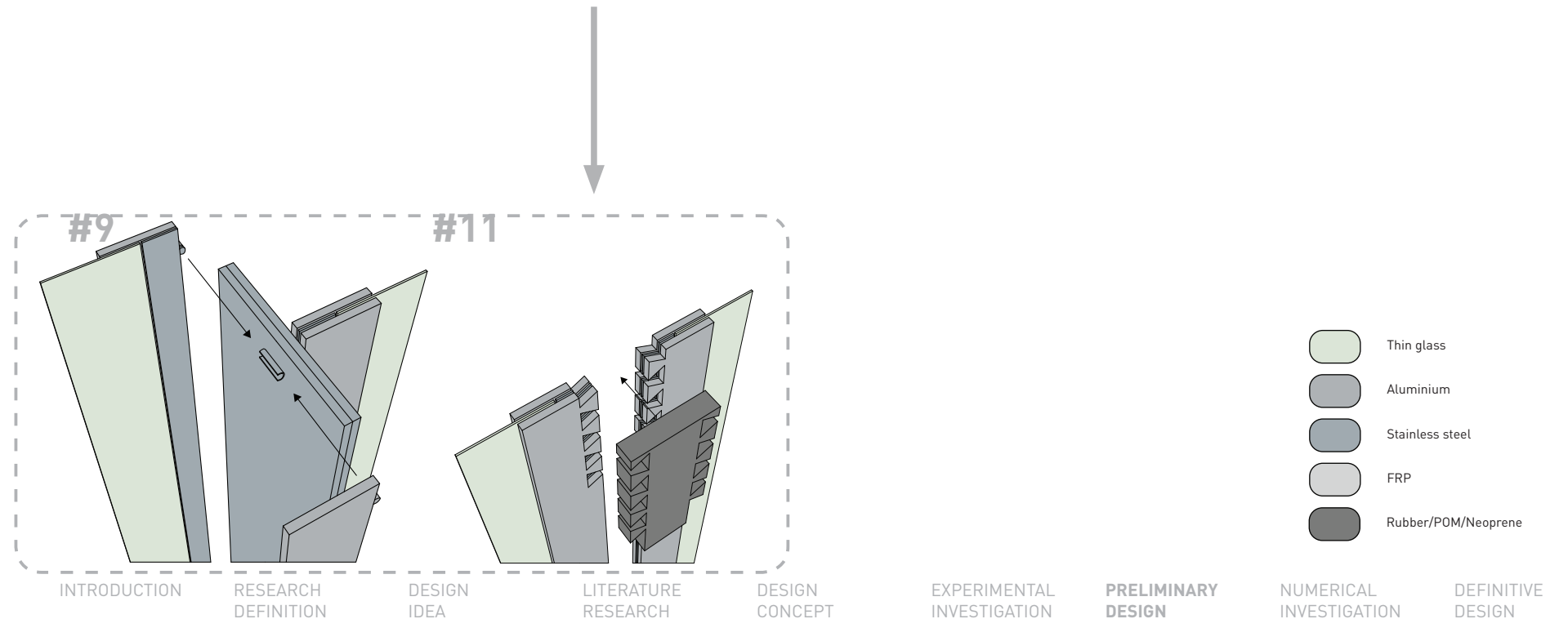
CATEGORY IV SUBSTRUCTURE

- NO CONTROL OF APPLIED TENSION



CATEGORY IV SUBSTRUCTURE

+/- ADDED SUBSTRUCTURE OF RUBBER CAN BE STRAINED
BUT HAS NO CAPABILITY OF TRANSFERRING TENSION



PRELIMINARY DESIGN

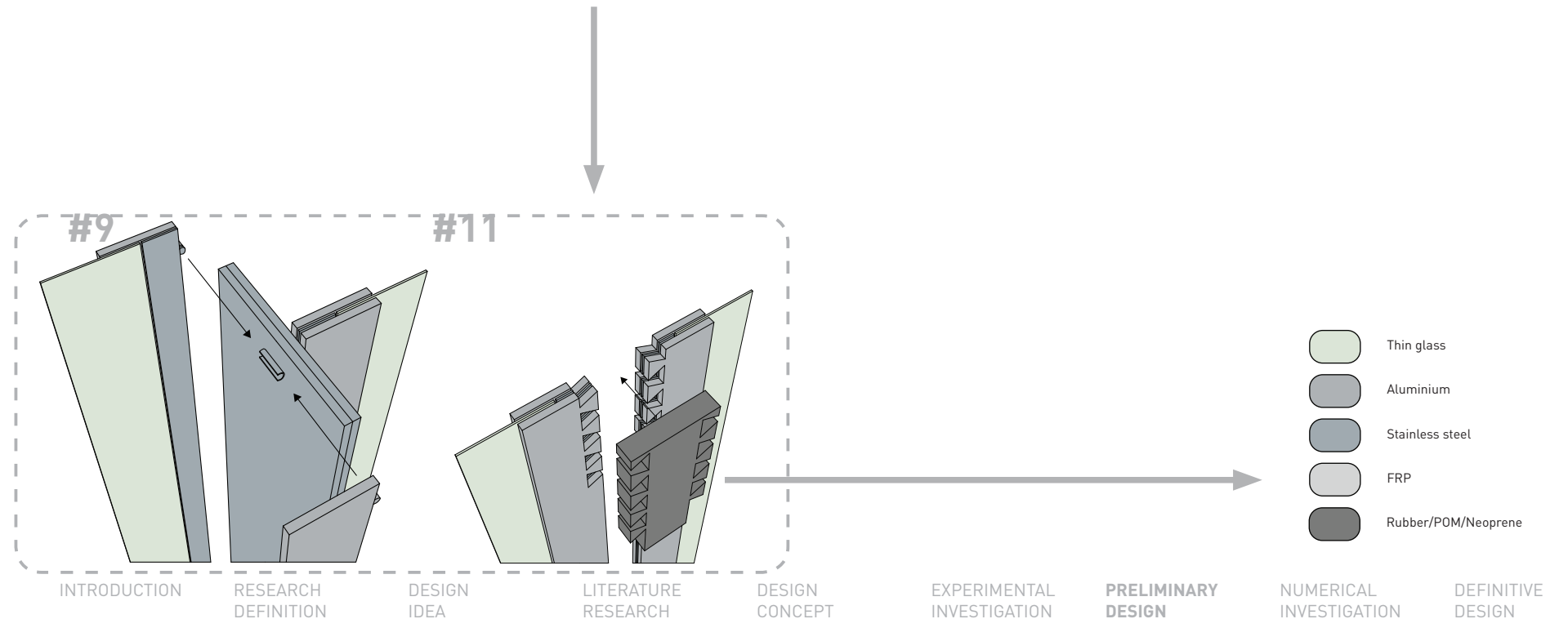
DESIGN OF THE CONNECTION

SWOT ANALYSES

DYNAMIC EDGE STIFFNESS

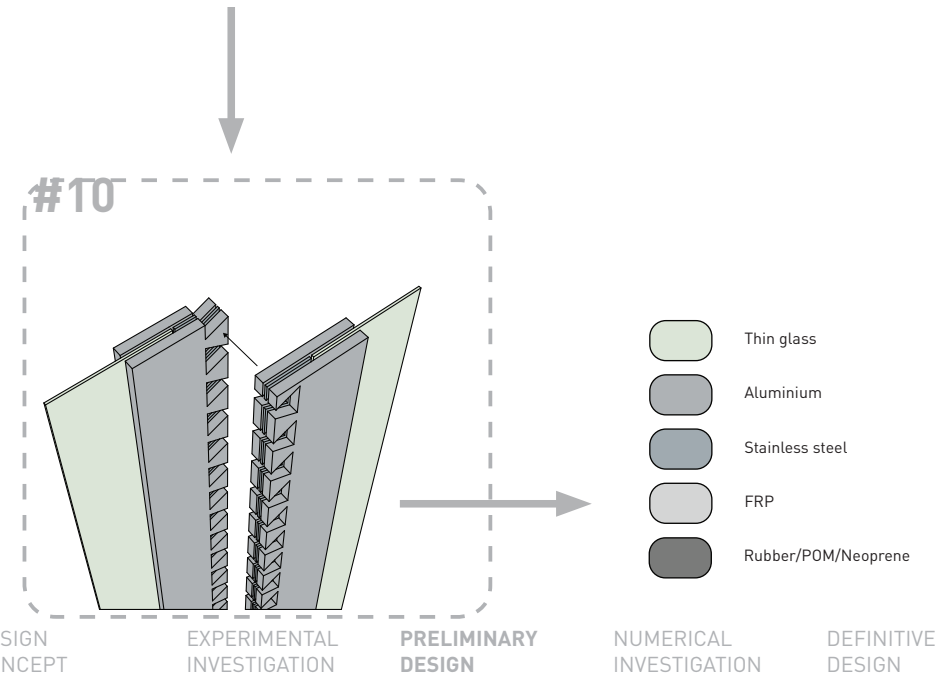
CATEGORY IV SUBSTRUCTURE

+ ADDING FIBRES WOULD GIVE THE POSSIBILITY OF TRANSFERRING TENSILE STRESSES



CATEGORY V CLEAN CONNECTION

+ BETTER TO MAKE IT FROM 1
MATERIAL WITHOUT THE USE
OF EXTRA CONSTRUCTION
MATERIAL



PRELIMINARY DESIGN

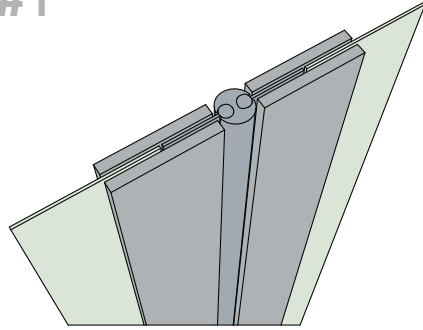
DESIGN OF THE CONNECTION

SWOT ANALYSES

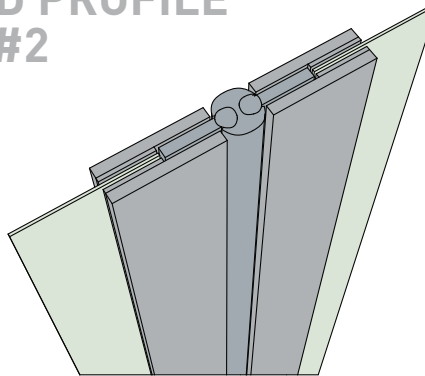
DYNAMIC EDGE STIFFNESS

CATEGORY EXTRUDED PROFILE

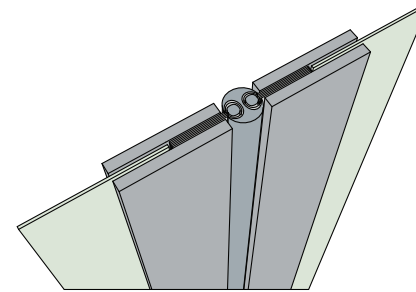
#1



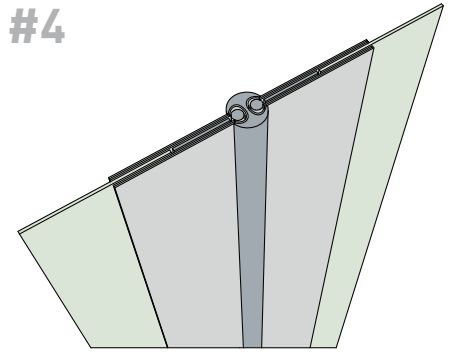
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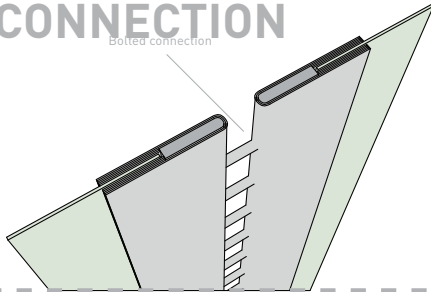


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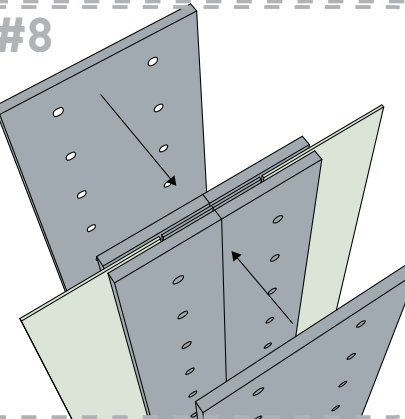


#5

CATEGORY BOLTED CONNECTION

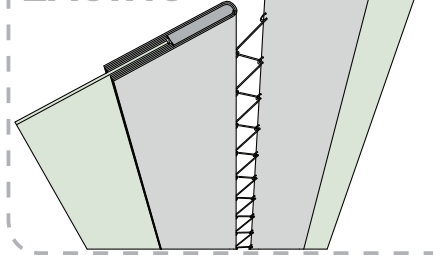


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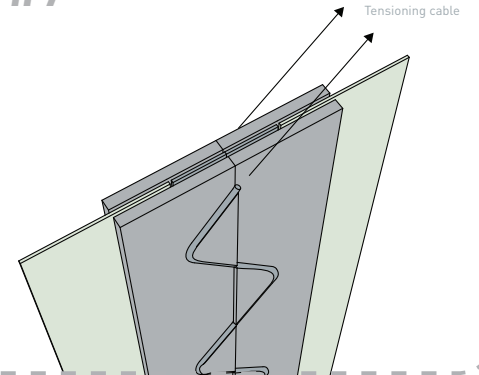


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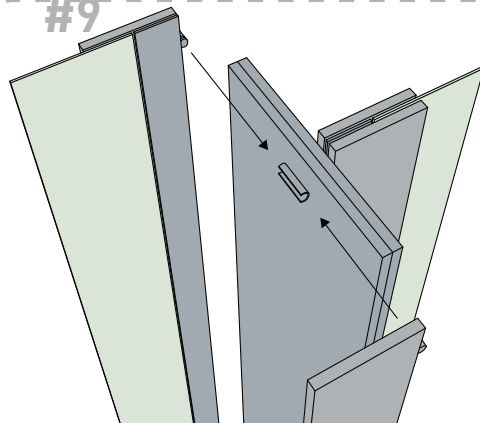
CATEGORY LACING



#7

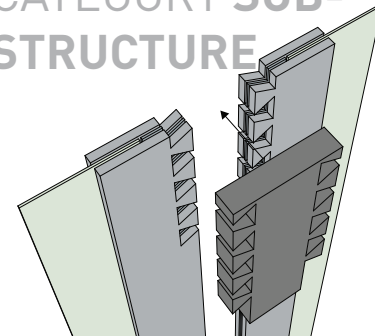


#9



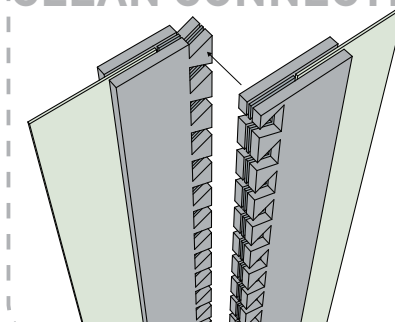
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




CATEGORY SUB-STRUCTURE



#10

CATEGORY CLEAN CONNECTION



-  Thin glass
-  Aluminium
-  Stainless steel
-  FRP
-  Rubber/POM/Neoprene

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PRELIMINARY DESIGN

DESIGN OF THE CONNECTION

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DYNAMIC EDGE STIFFNESS

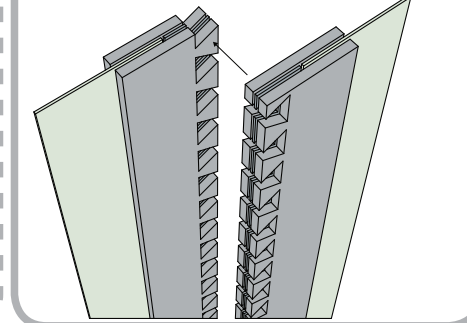
CATEGORY **EXTRUDED PROFILE**

CATEGORY **BOLTED CONNECTION**

CATEGORY **LACING**

CATEGORY **SUB-STRUCTURE**

CATEGORY **CLEAN CONNECTION**



- Thin glass
- Aluminium
- Stainless steel
- FRP
- Rubber/POM/Neoprene

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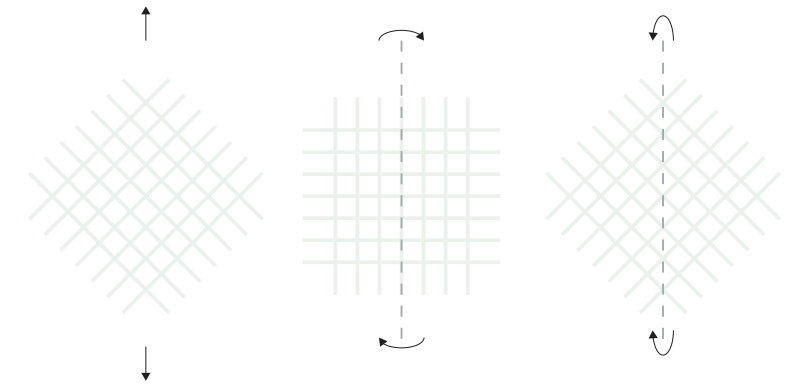
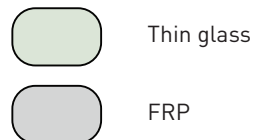
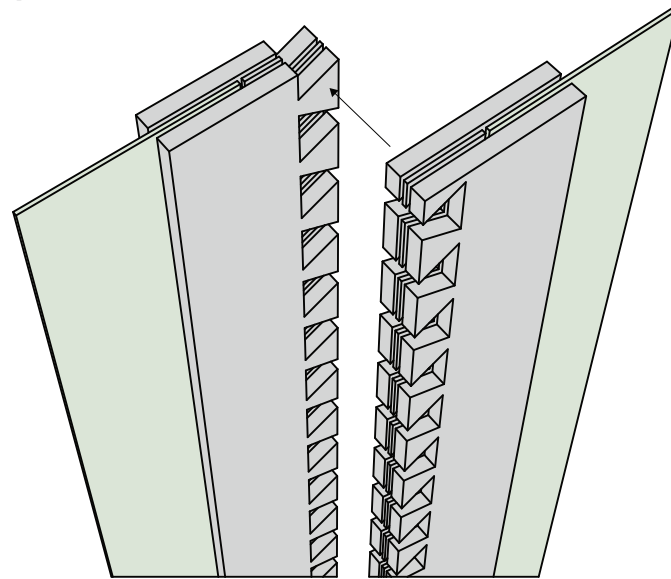
SWOT ANALYSES

DYNAMIC EDGE STIFFNESS

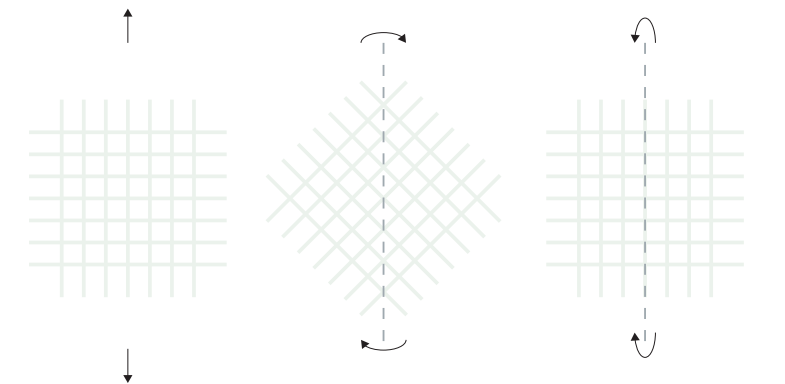
WITH A **COMPOSITE MATERIAL** NEEDED **STRAIN/TENSION** CAN BE CONTROLLED

→ MORE LAYERS OF GFRP

→ DIFFERENT DIRECTION OF FIBRES



More strain in *low stiffness* direction



Lower strain in *higher stiffness* direction

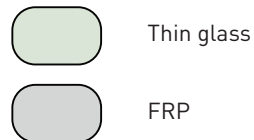
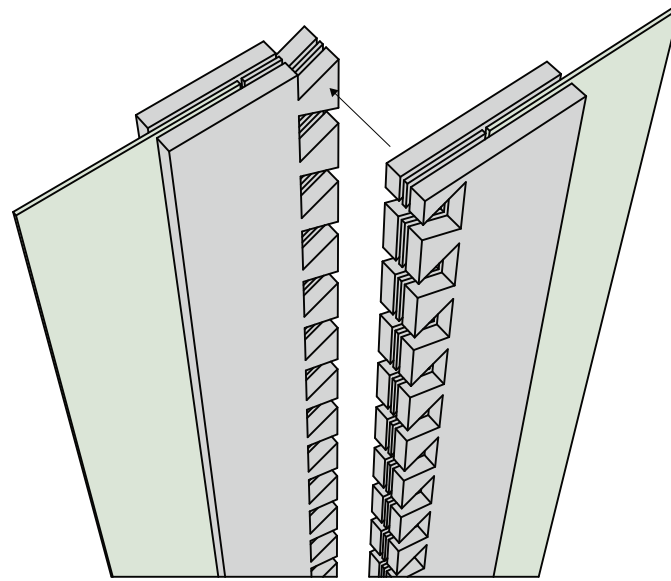
PRELIMINARY DESIGN

DESIGN OF THE CONNECTION

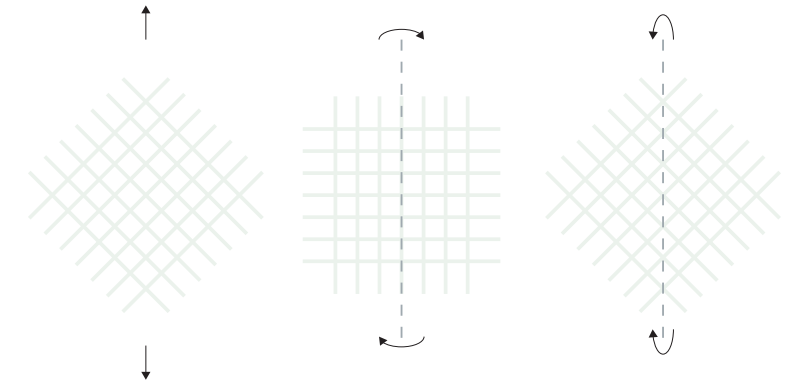
SWOT ANALYSES

DYNAMIC EDGE STIFFNESS

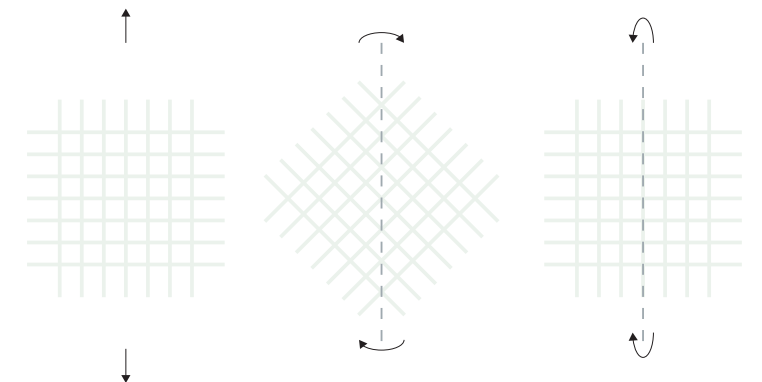
WITH A **COMPOSITE MATERIAL** NEEDED **STRAIN/TENSION** CAN BE CONTROLLED



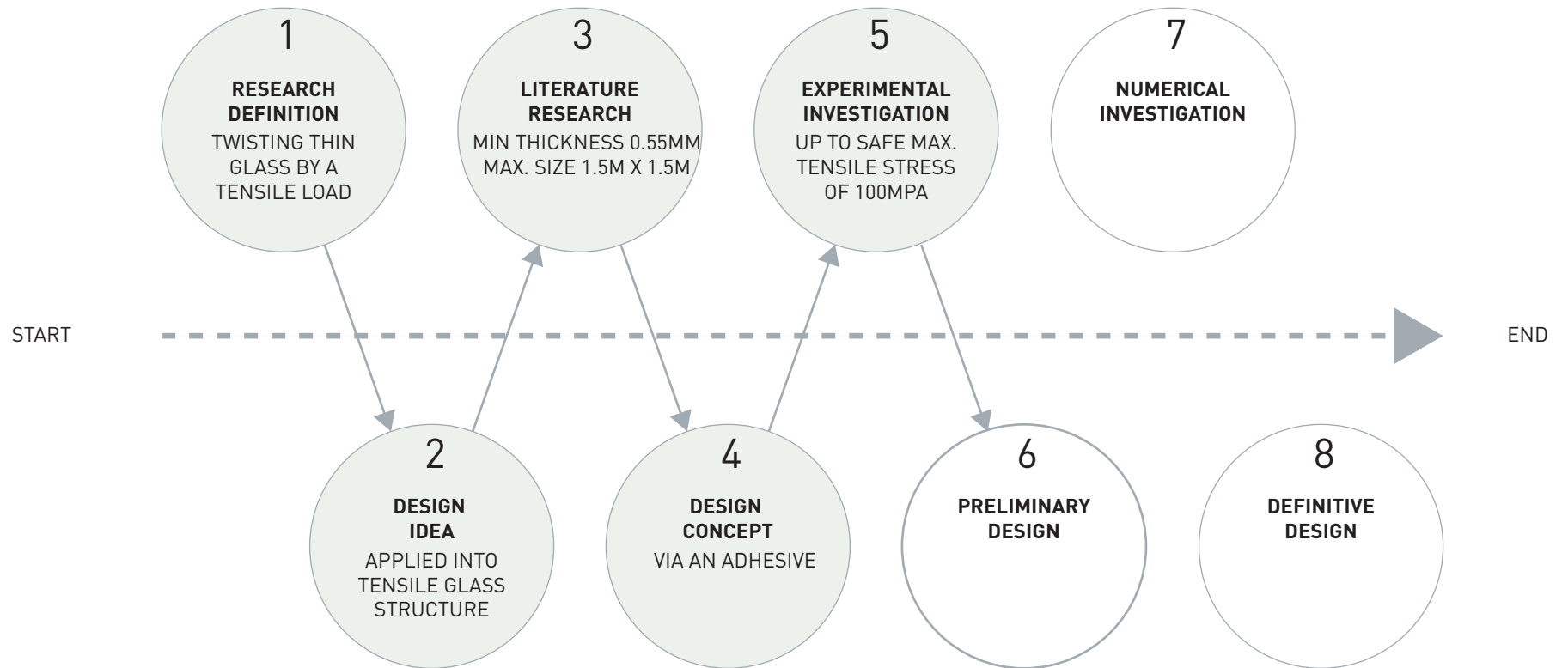
→ **NUMERICAL SIMULATION**
WILL DETERMINE THE STIFFNESS

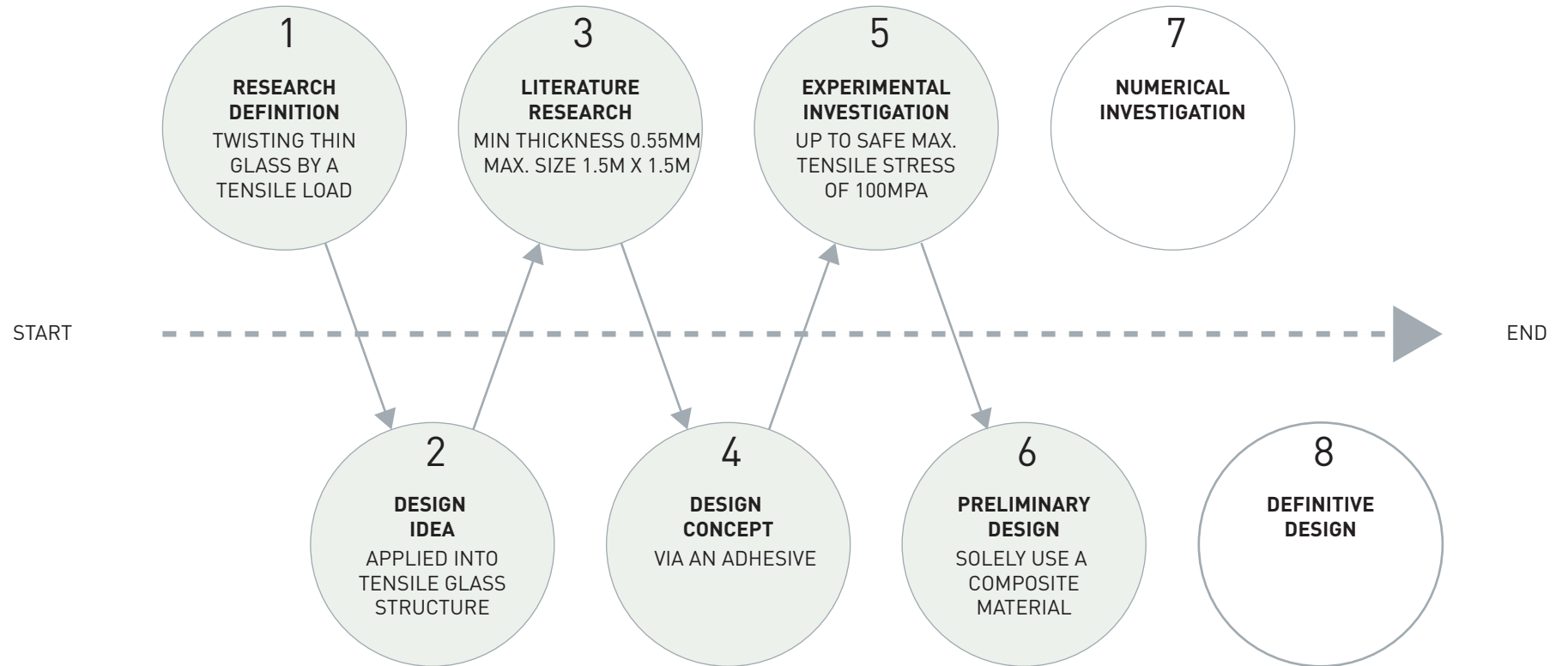


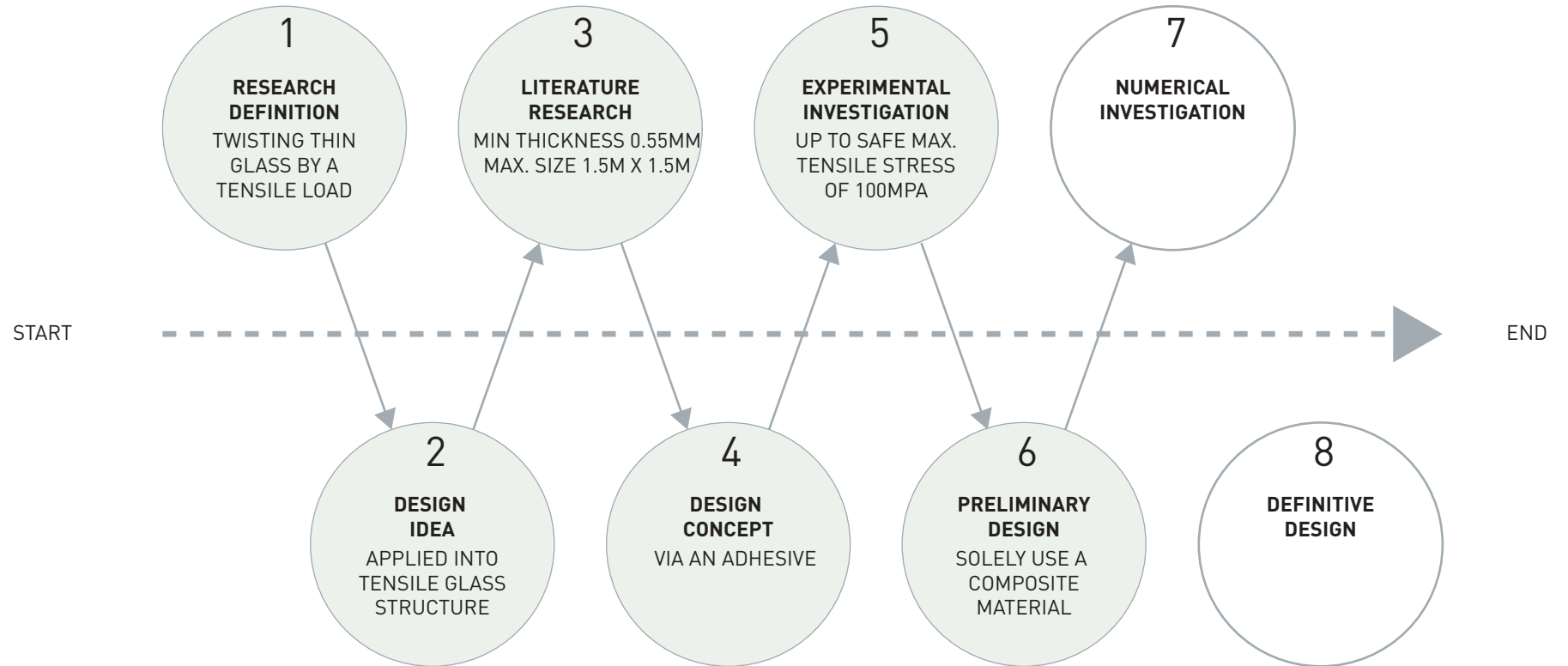
More strain in *low stiffness* direction



Lower strain in *higher stiffness* direction

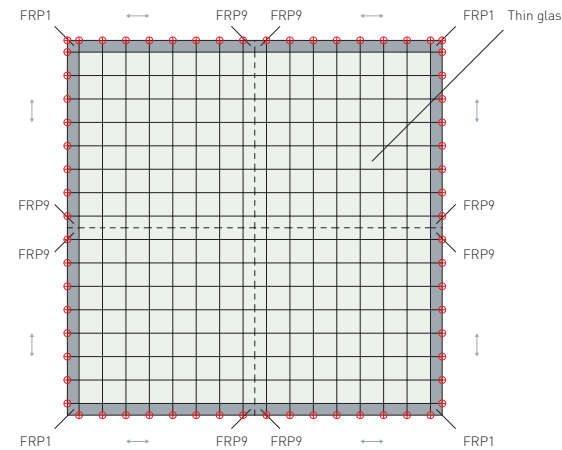




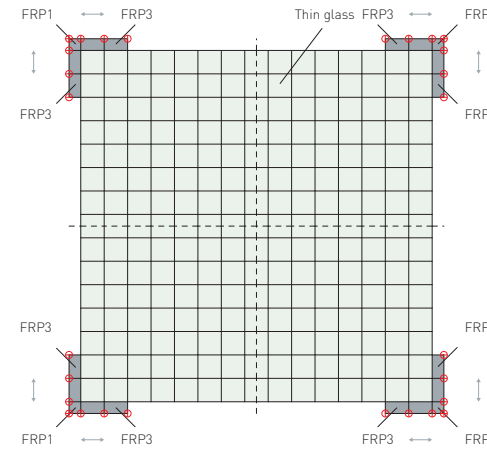


NUMERICAL INVESTIGATION

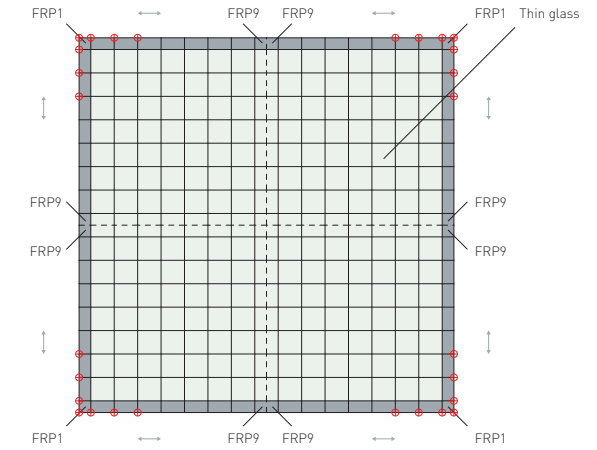
DYNAMIC EDGE STIFFNESS: **THREE MODELS**



I. Twisting from the middle

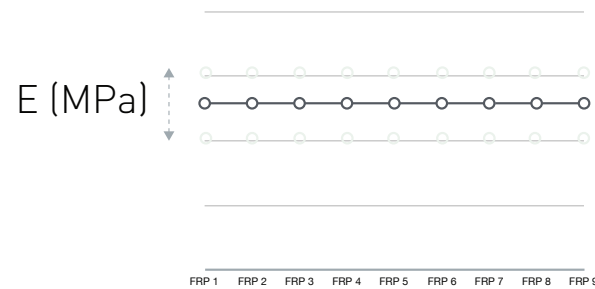


II. Twisting from the corners

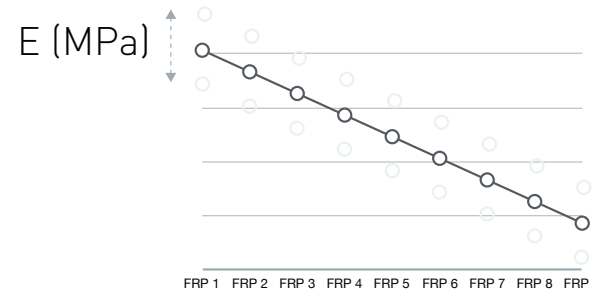


III. Twisting from the corners

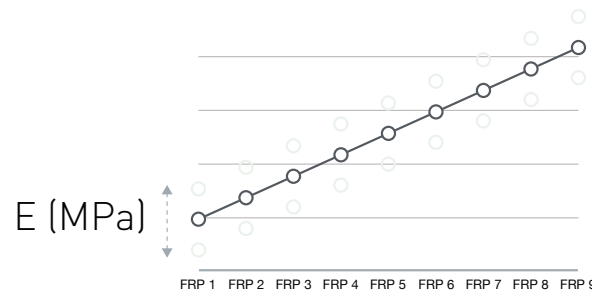
DYNAMIC EDGE STIFFNESS: FIVE DIFFERENT GRADIENTS



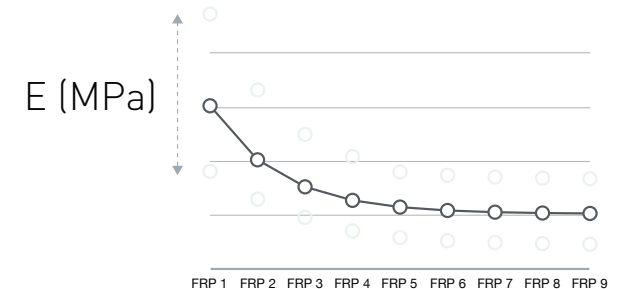
A. Constant stiffness



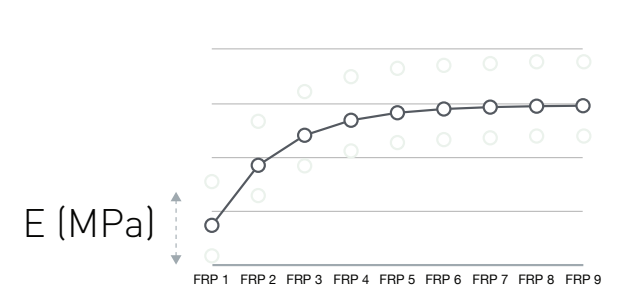
B. Linear decreased stiffness



C. Linear increased stiffness

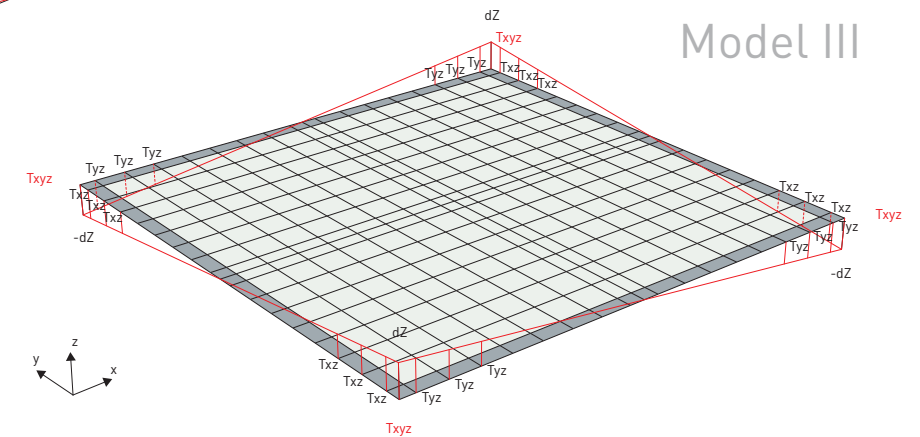
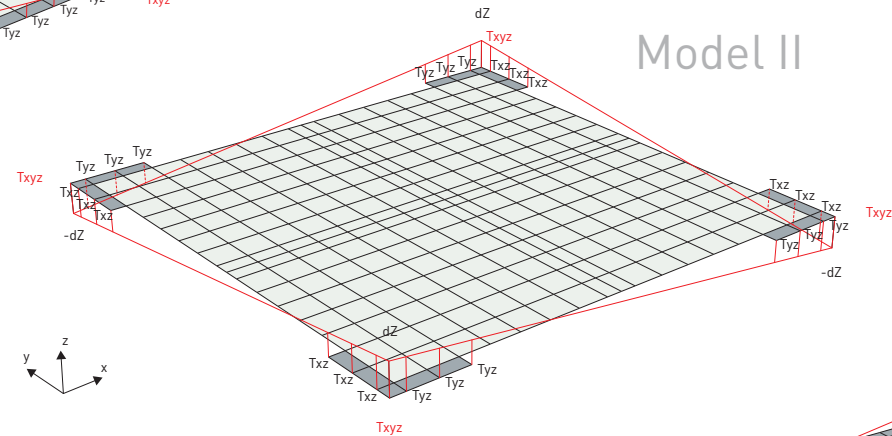
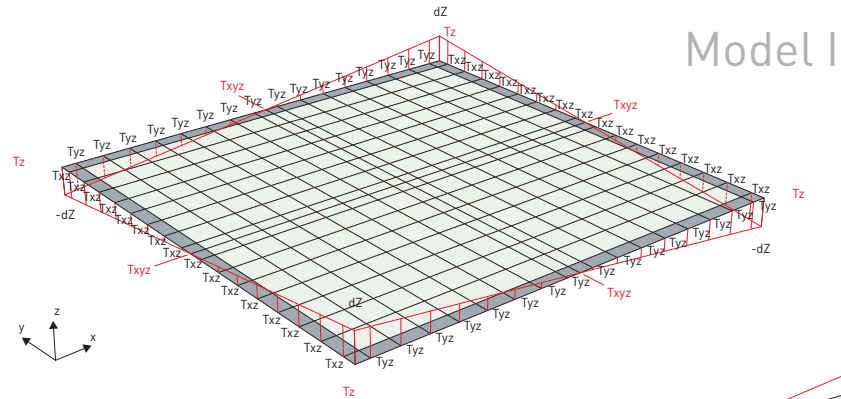


D. Digressive decreased stiffness



E. Digressive increased stiffness

APPLYING THE 5 DIFFERENT STIFFNESS GRADIENTS TO THE MODELS



How far the thin glass plate can be twist within allowable generated stresses?

NUMERICAL INVESTIGATION

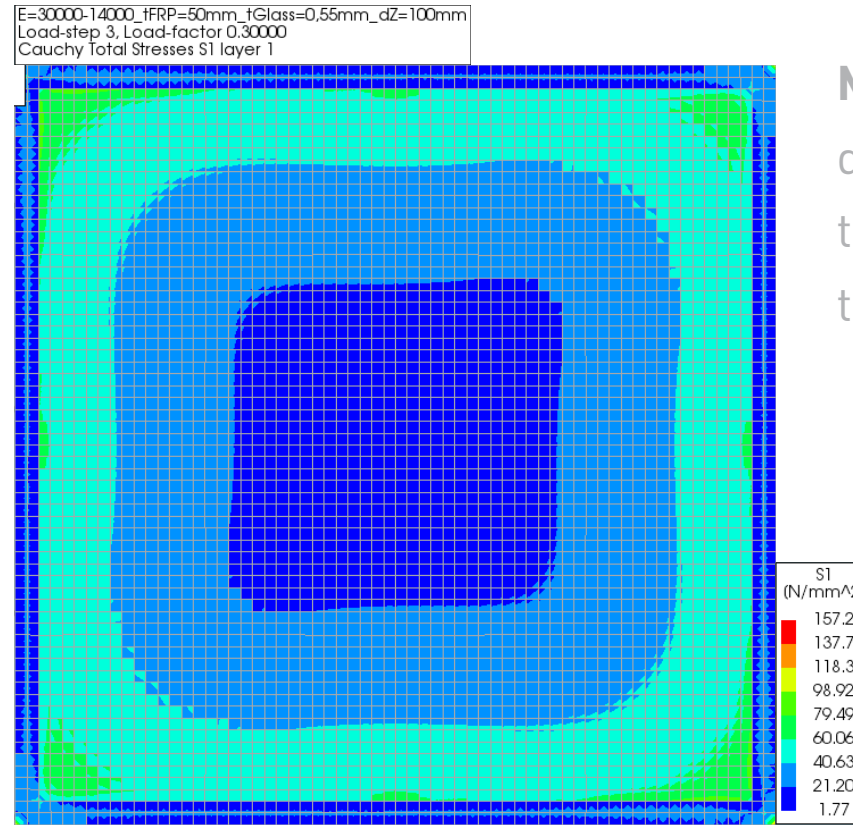
THREE NUMERICAL MODELS

FIVE DIFFERENT STIFFNESS GRADIENTS

RESULTS & DISCUSSION

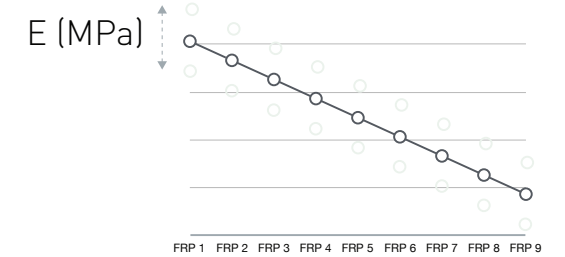
CONCLUSION

MODEL III TWISTING FROM & AT THE CORNERS

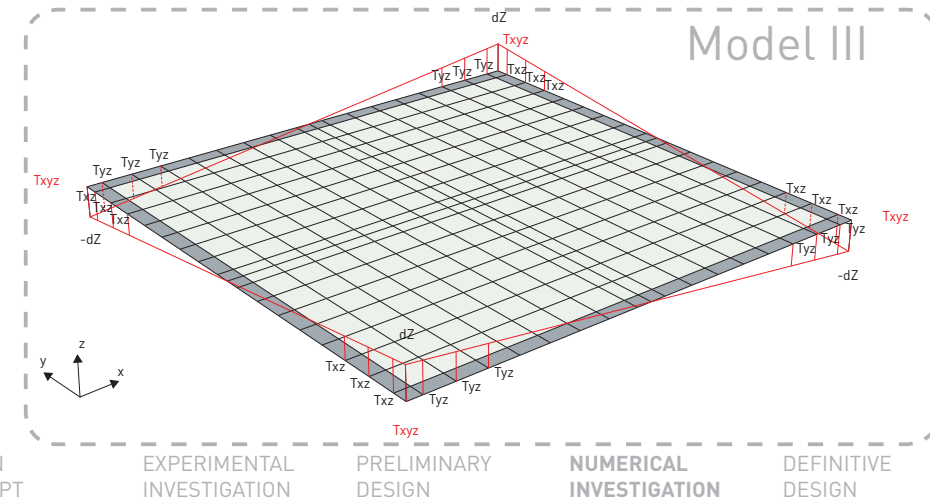


→ Highest tension in the *FRP*

Maximum twist
 $dZ = 30\text{mm}$
 $t_{FRP} = 50\text{mm}$
 $t_{Glass} = 0.55\text{mm}$



B. Linear decreased stiffness



NUMERICAL INVESTIGATION

THREE NUMERICAL MODELS

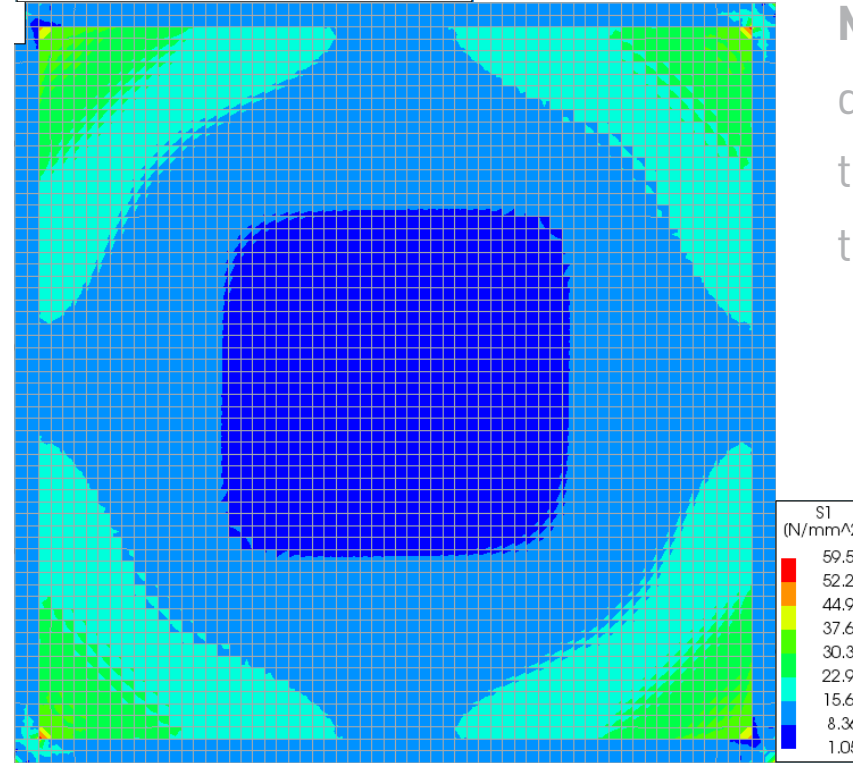
FIVE DIFFERENT STIFFNESS GRADIENTS

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MODEL III STIFFNESS IN THE CORNERS NEED TO BE HIGHER THAN MIDDLE

E=14000-30000_tFRP=50mm_tGlass=0,55mm_dZ=100mm
 Load-step 2, Load-factor 0,20000
 Cauchy Total Stresses S1 layer 1



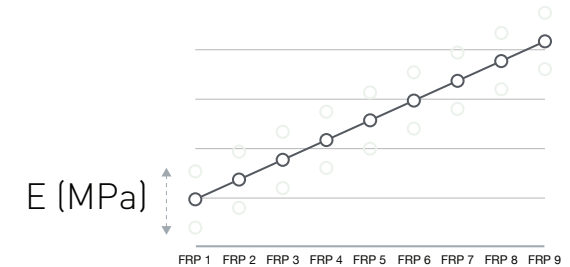
→ Highest tension in the *glass*

Maximum twist

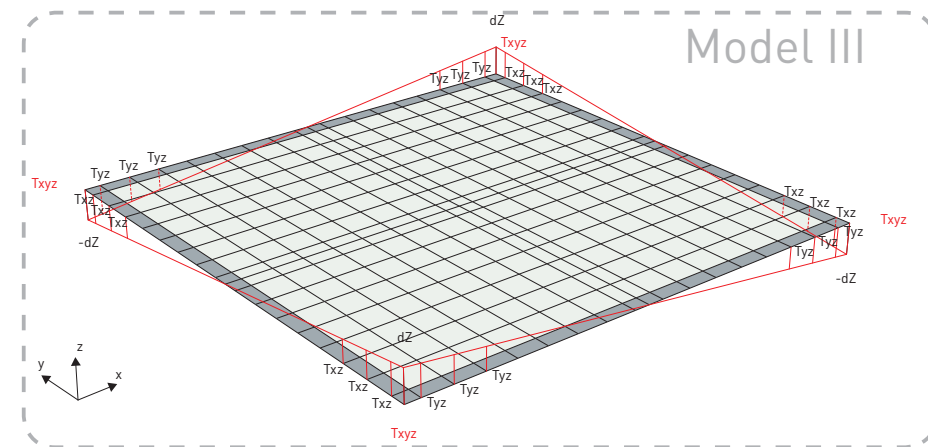
dZ = 20mm

tFRP = 50mm

tGlass = 0.55mm



C. Linear increased stiffness



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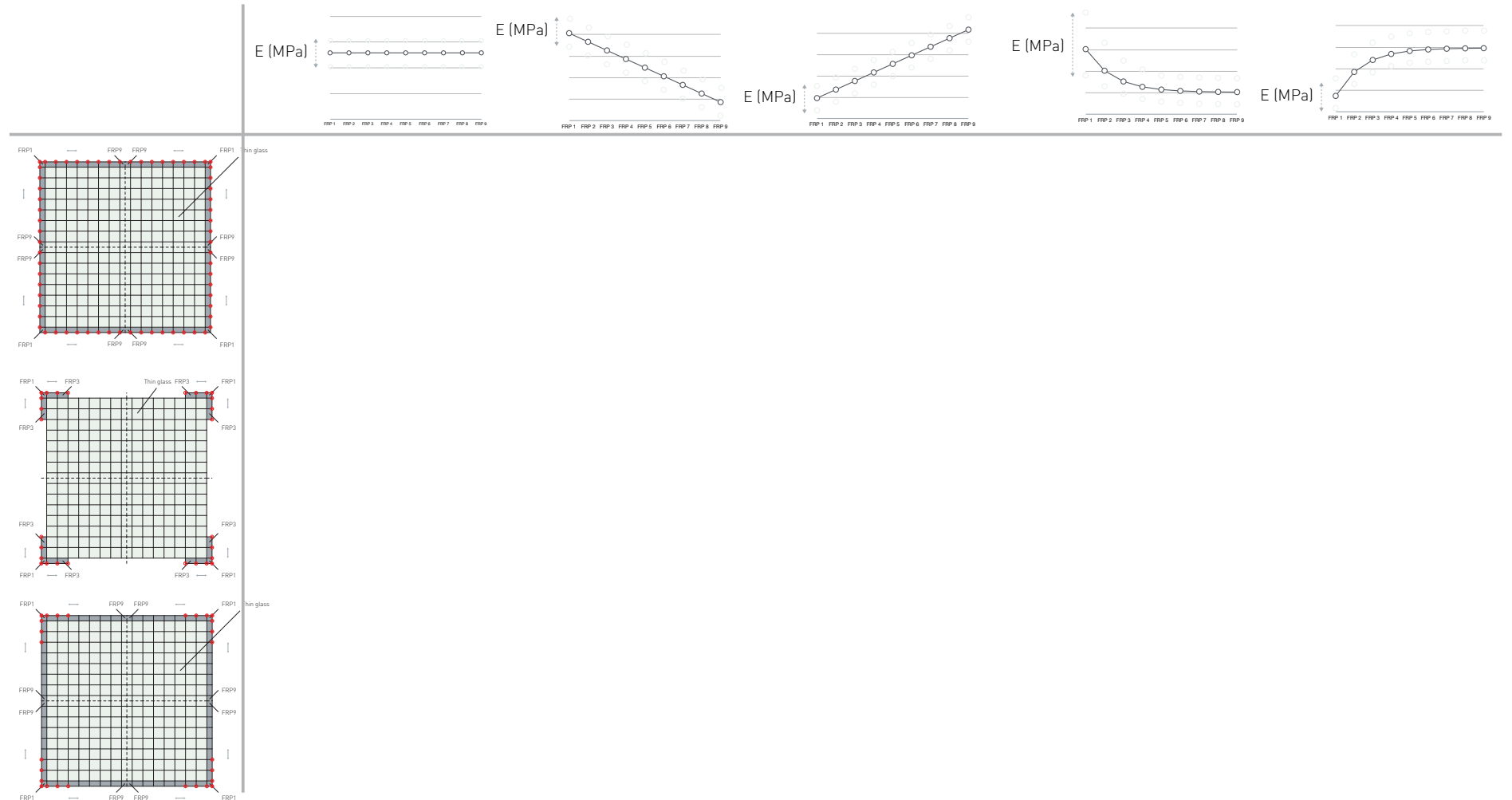
THREE NUMERICAL MODELS

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NUMERICAL INVESTIGATION

THREE NUMERICAL MODELS

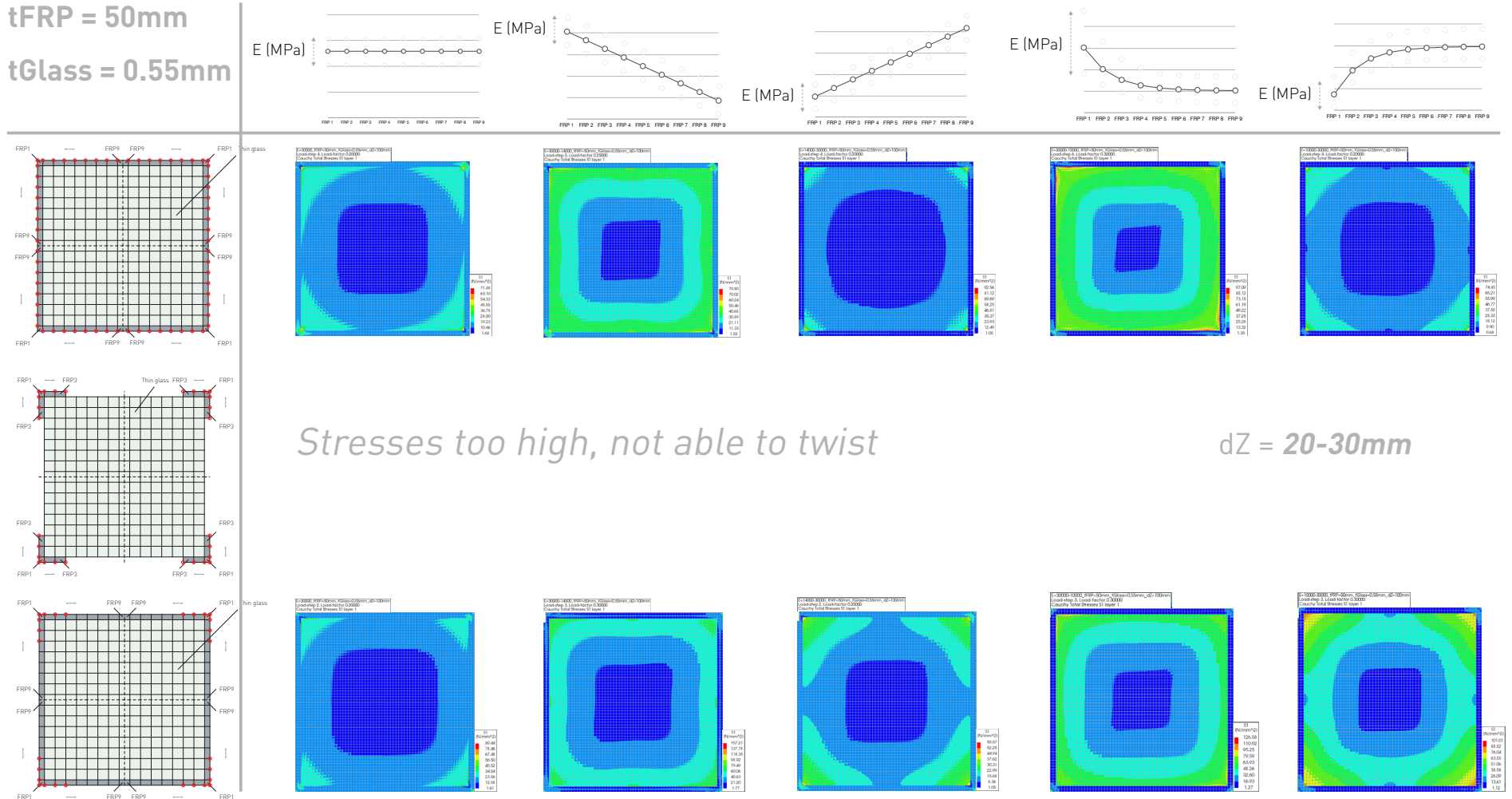
FIVE DIFFERENT STIFFNESS GRADIENTS

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tFRP = 50mm
tGlass = 0.55mm



NUMERICAL INVESTIGATION

THREE NUMERICAL MODELS

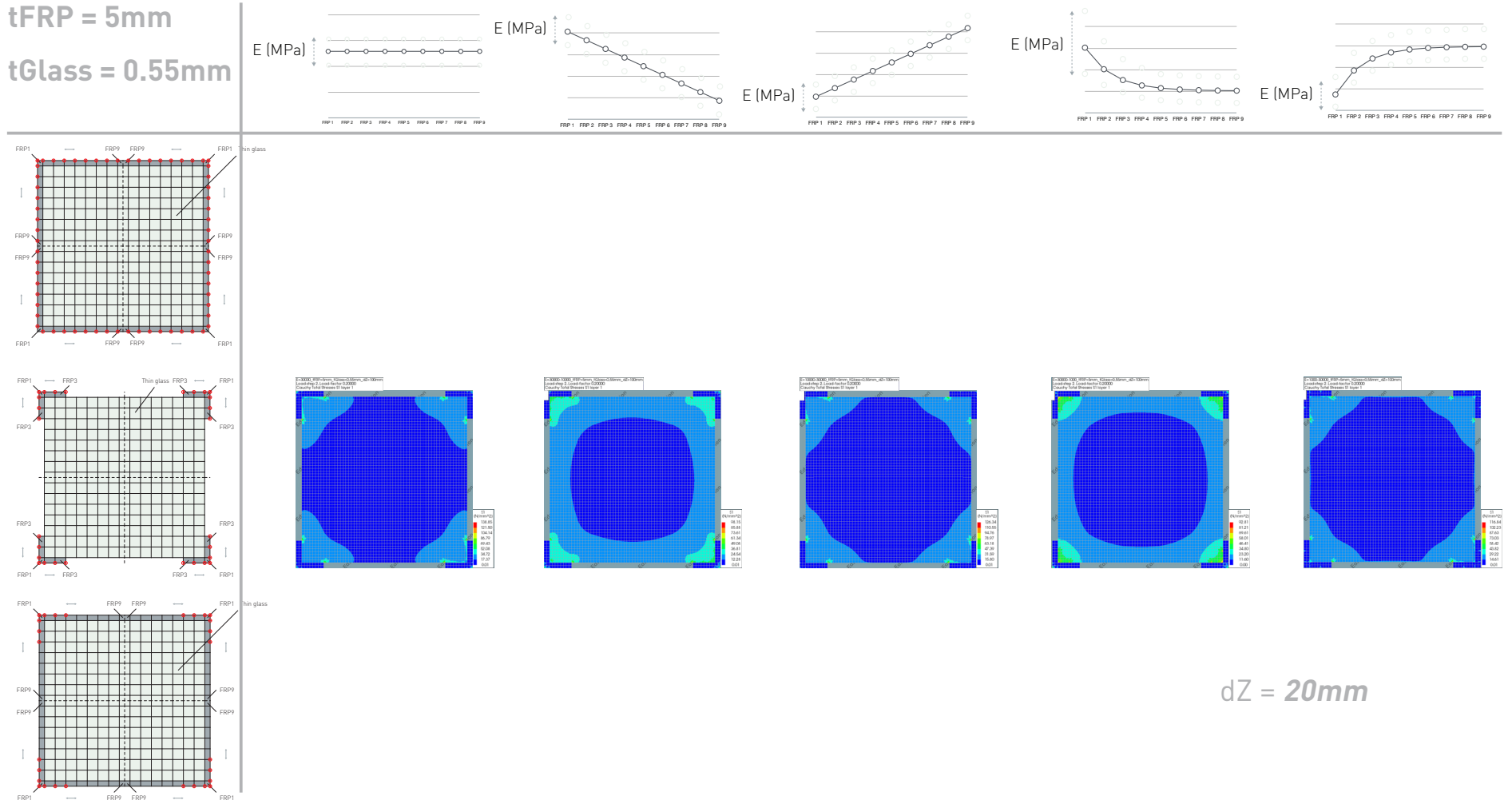
FIVE DIFFERENT STIFFNESS GRADIENTS

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$t_{FRP} = 5mm$
 $t_{Glass} = 0.55mm$



$dZ = 20mm$

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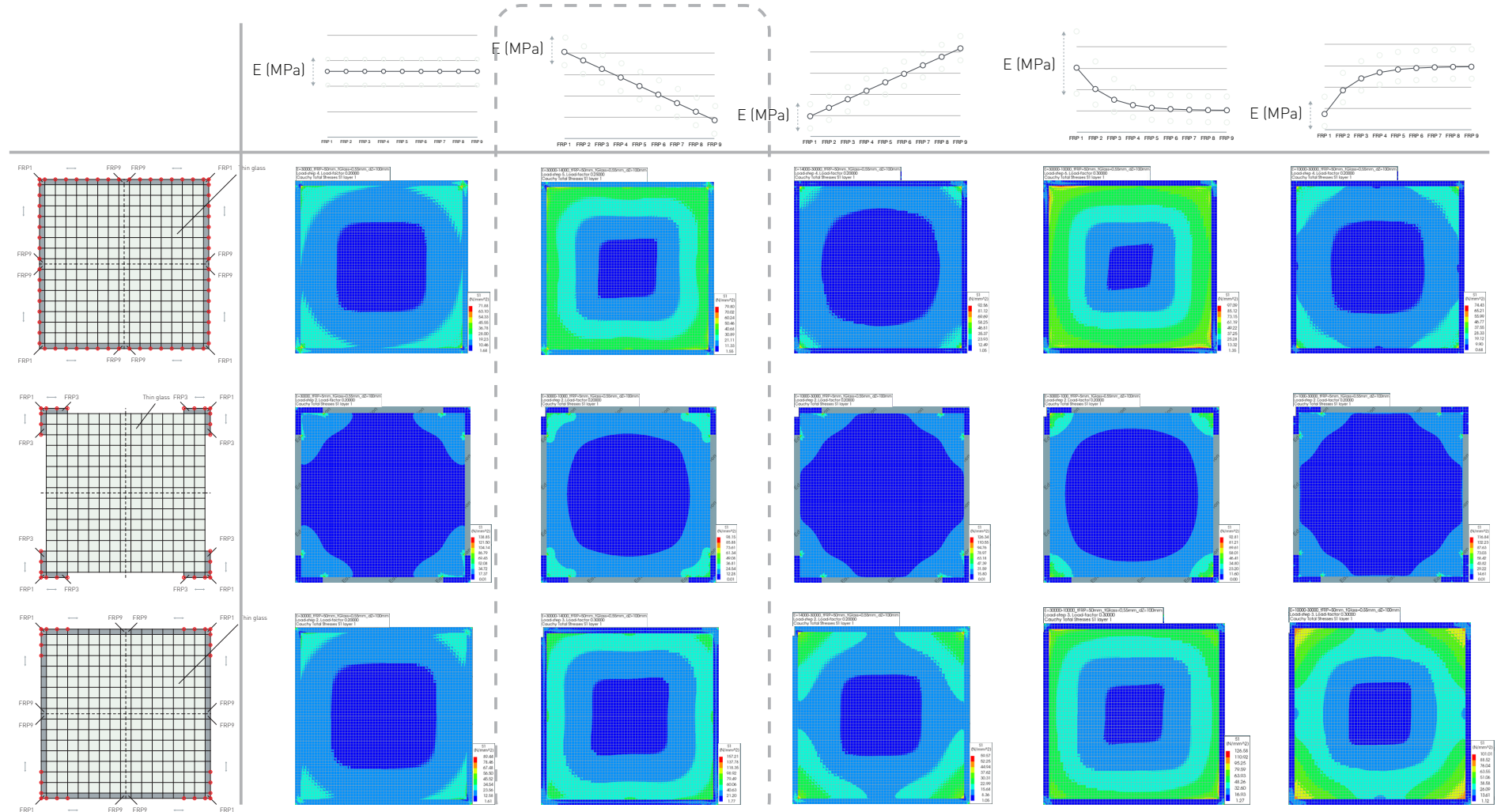
THREE NUMERICAL MODELS

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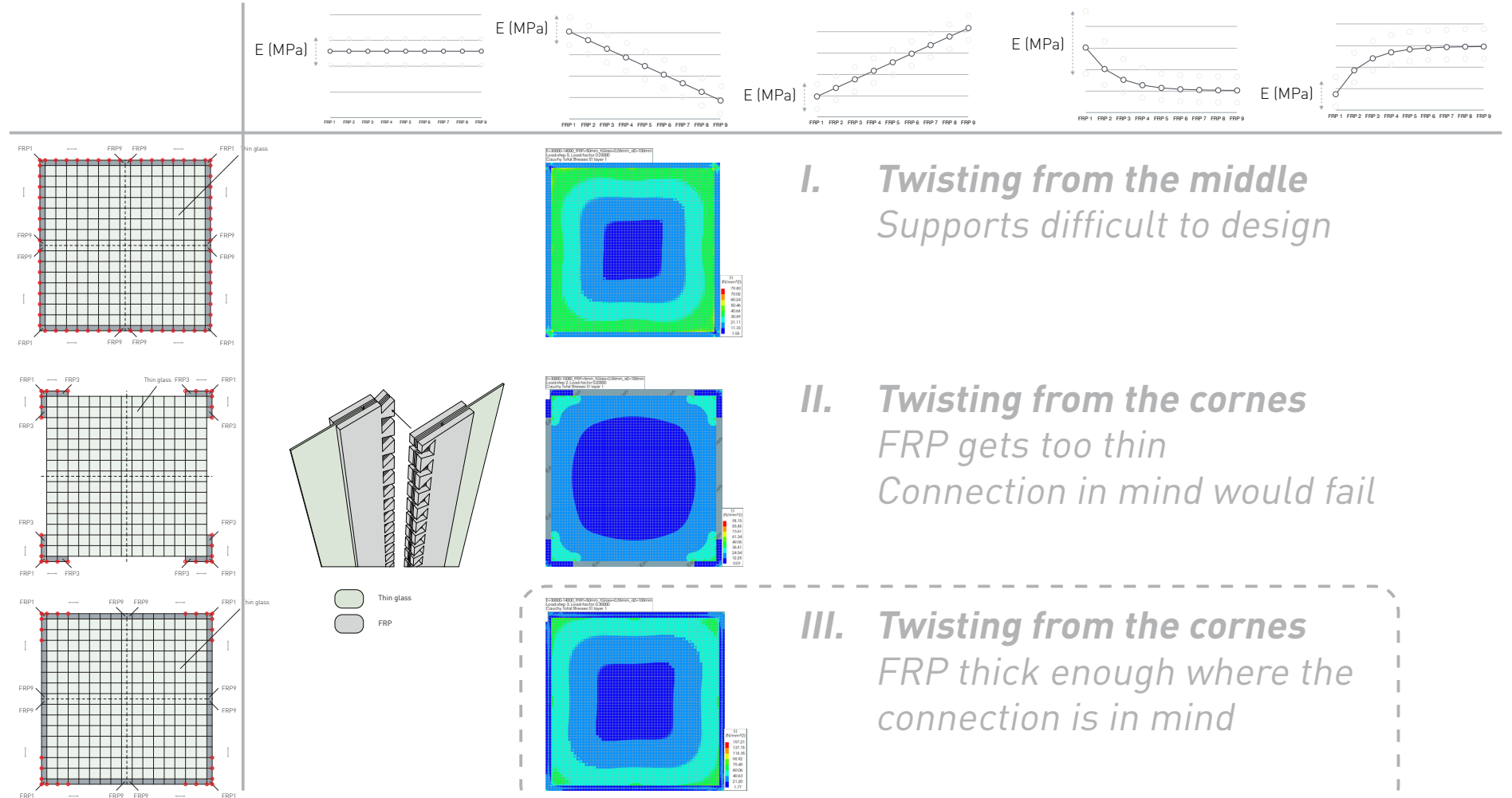
THREE NUMERICAL MODELS

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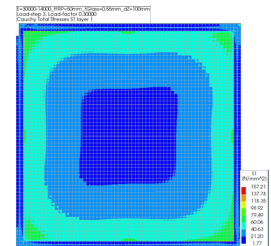
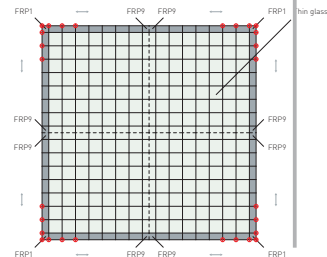
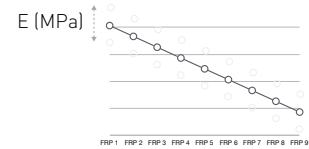


I. Twisting from the middle
Supports difficult to design

II. Twisting from the corners
FRP gets too thin
Connection in mind would fail

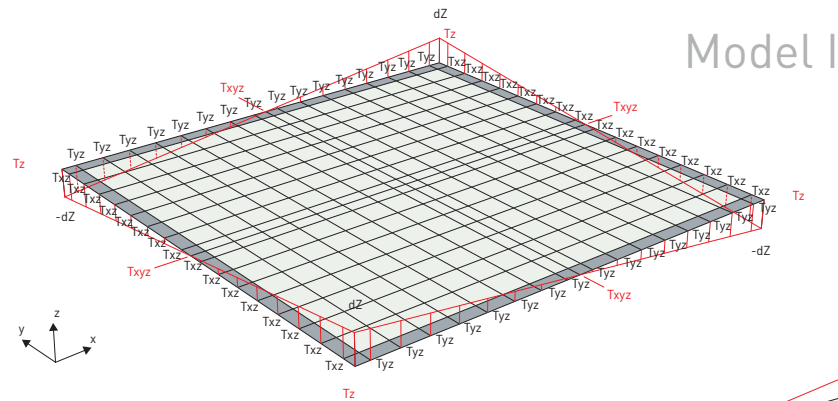
III. Twisting from the corners
FRP thick enough where the connection is in mind

APPLYING THE 5 DIFFERENT STIFFNESS GRADIENTS TO THE MODELS

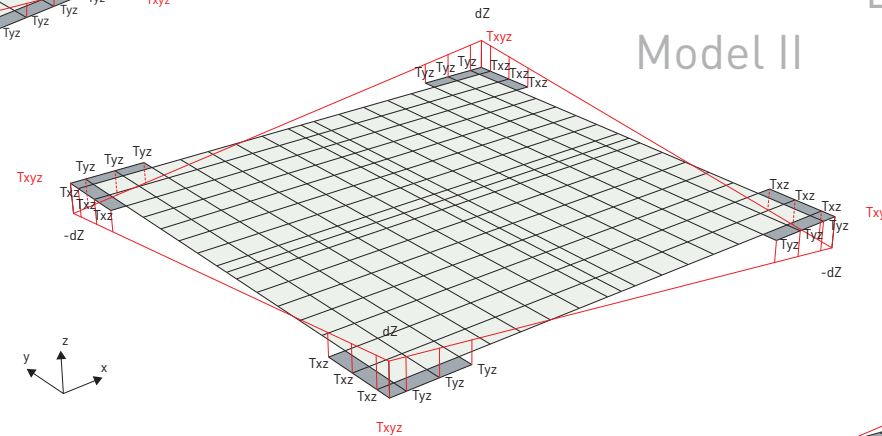


III. *Twisting from the corners*
Most appropriate one for a definitive design

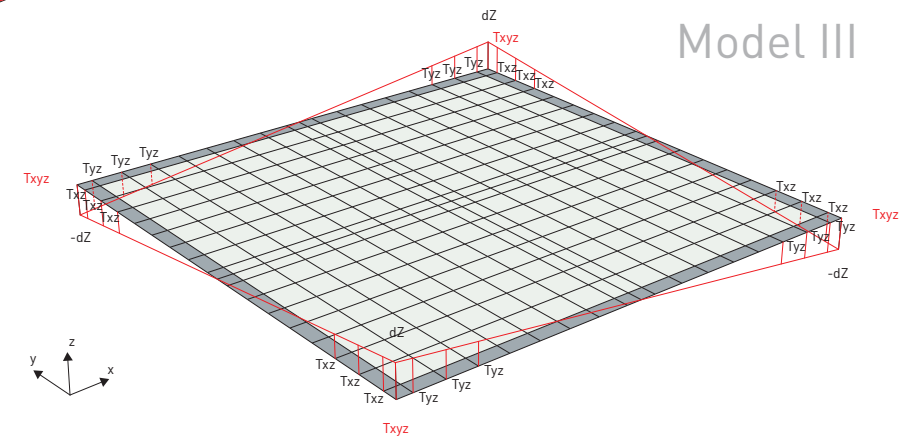
LINEAR DECREASED EDGE STIFFNESS FOR ALL MODELS



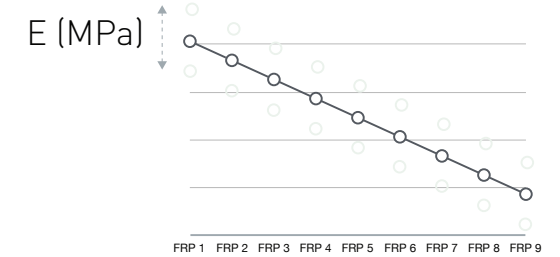
Model I



Model II



Model III



B. Linear decreased stiffness

NUMERICAL INVESTIGATION

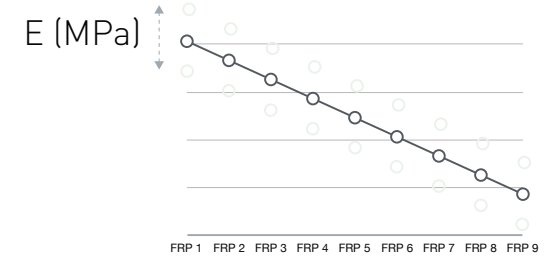
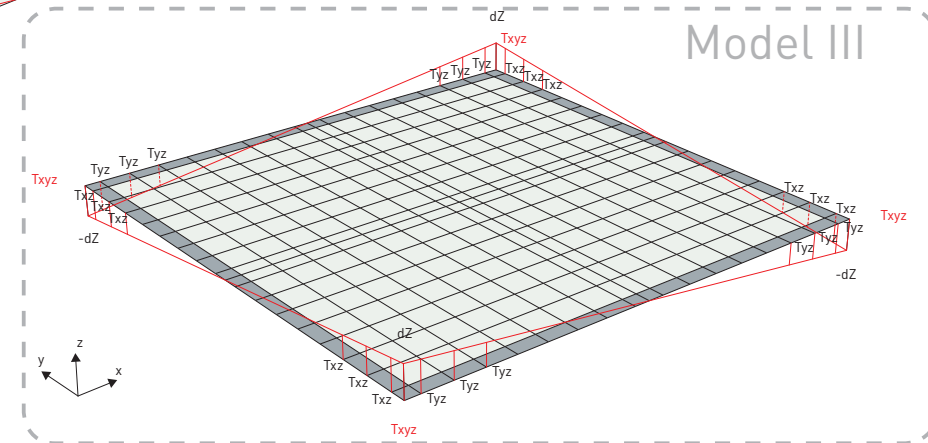
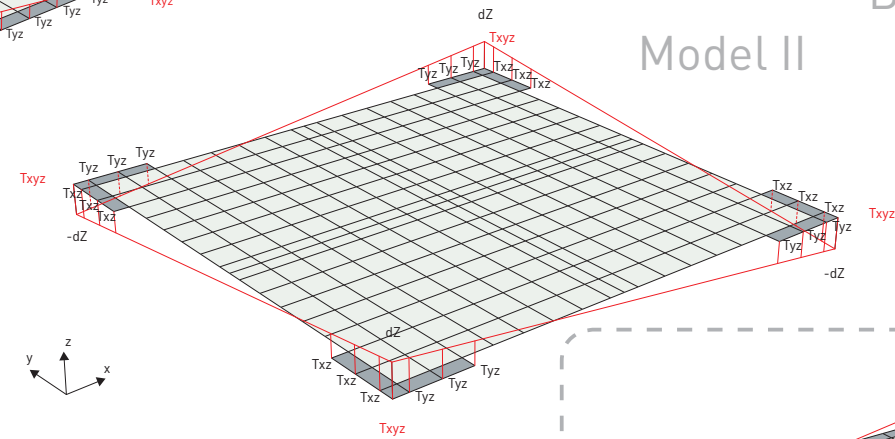
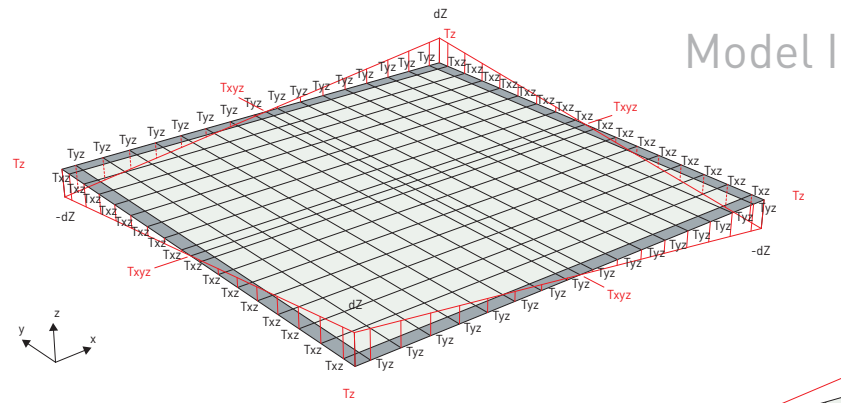
THREE NUMERICAL MODELS

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LINEAR DECREASED EDGE STIFFNESS FOR ALL MODELS



B. Linear decreased stiffness

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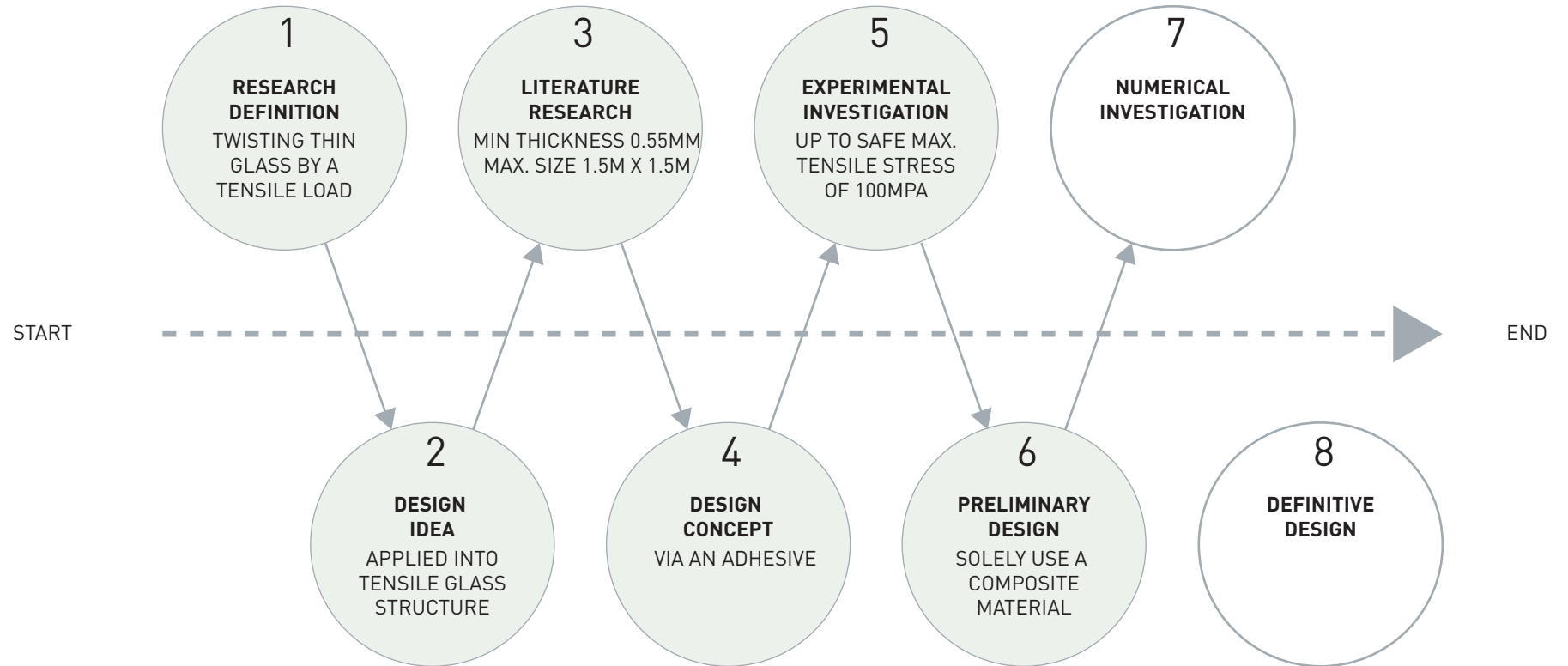
DESIGN CONCEPT

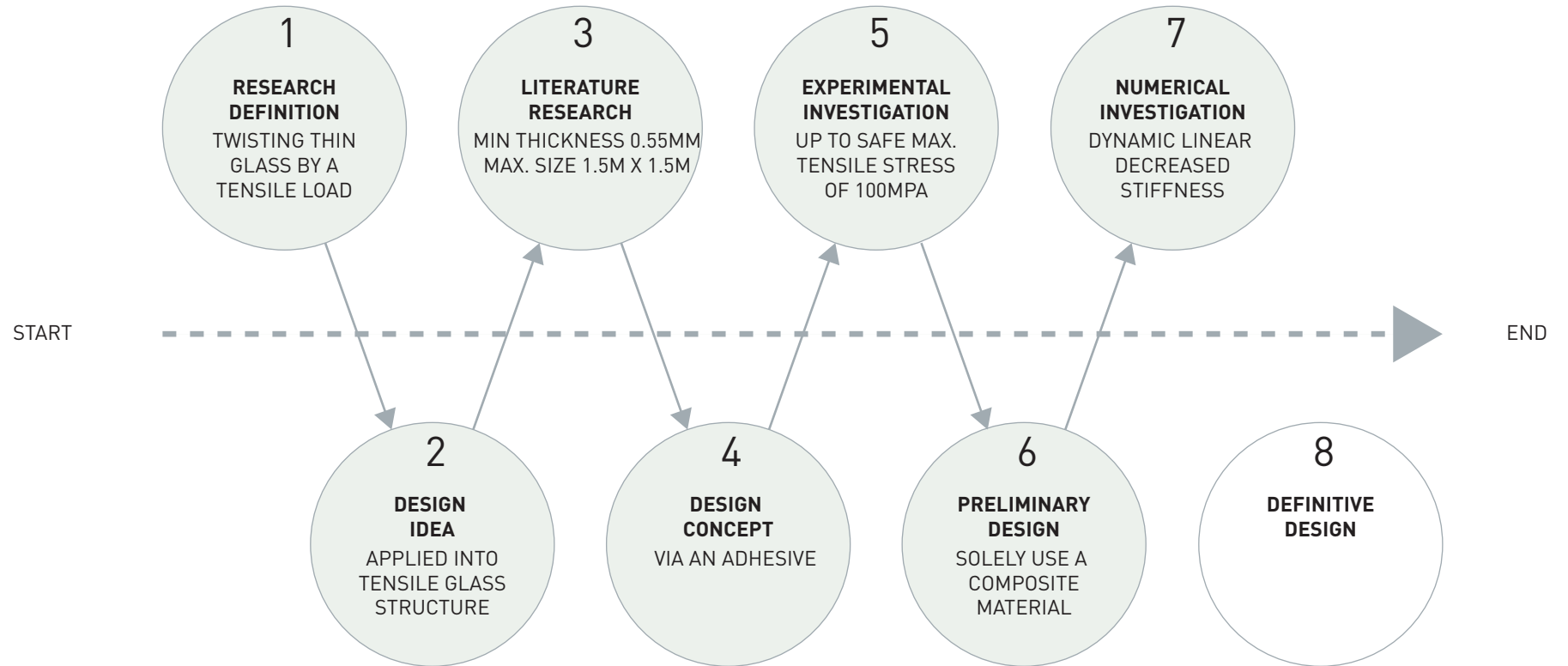
EXPERIMENTAL INVESTIGATION

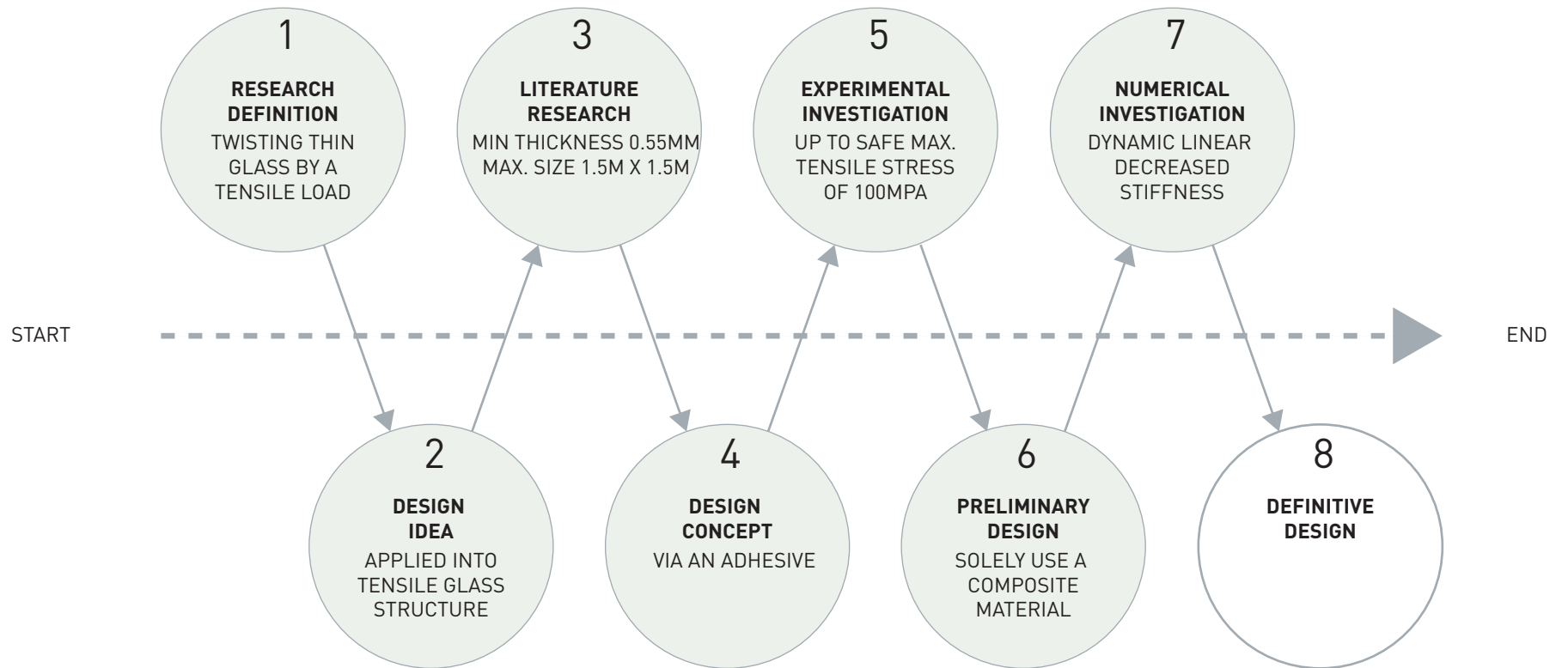
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DEFINITIVE DESIGN

DEFINITIVE
DESIGN

BUILD UP GFRP
LAYERS

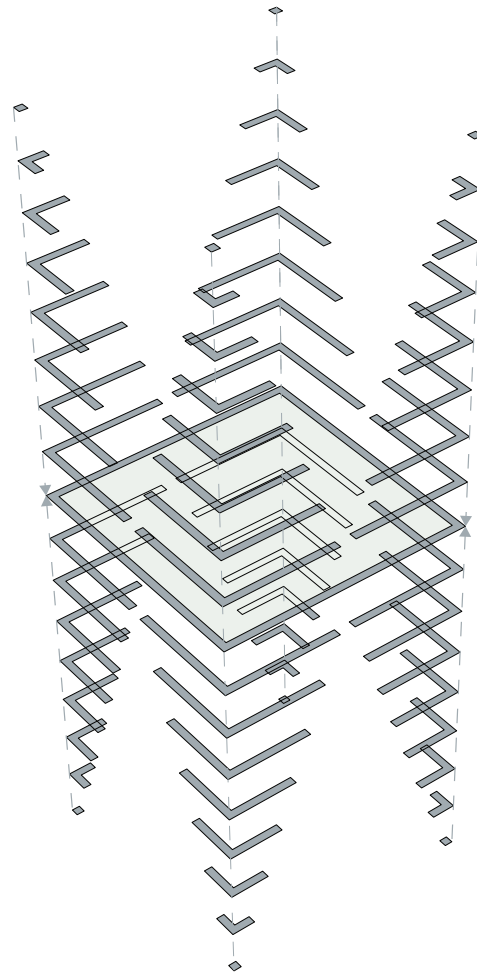
INTEGRATED
DOVETAIL JOINT

SCALABILITY

TECHNIQUE OF
TWISTING

EXTREME TWISTING

LINEAR DECREASED EDGE STIFFNESS *THROUGH* THE AMOUNT OF LAYERS



DEFINITIVE
DESIGN

BUILD UP GFRP
LAYERS

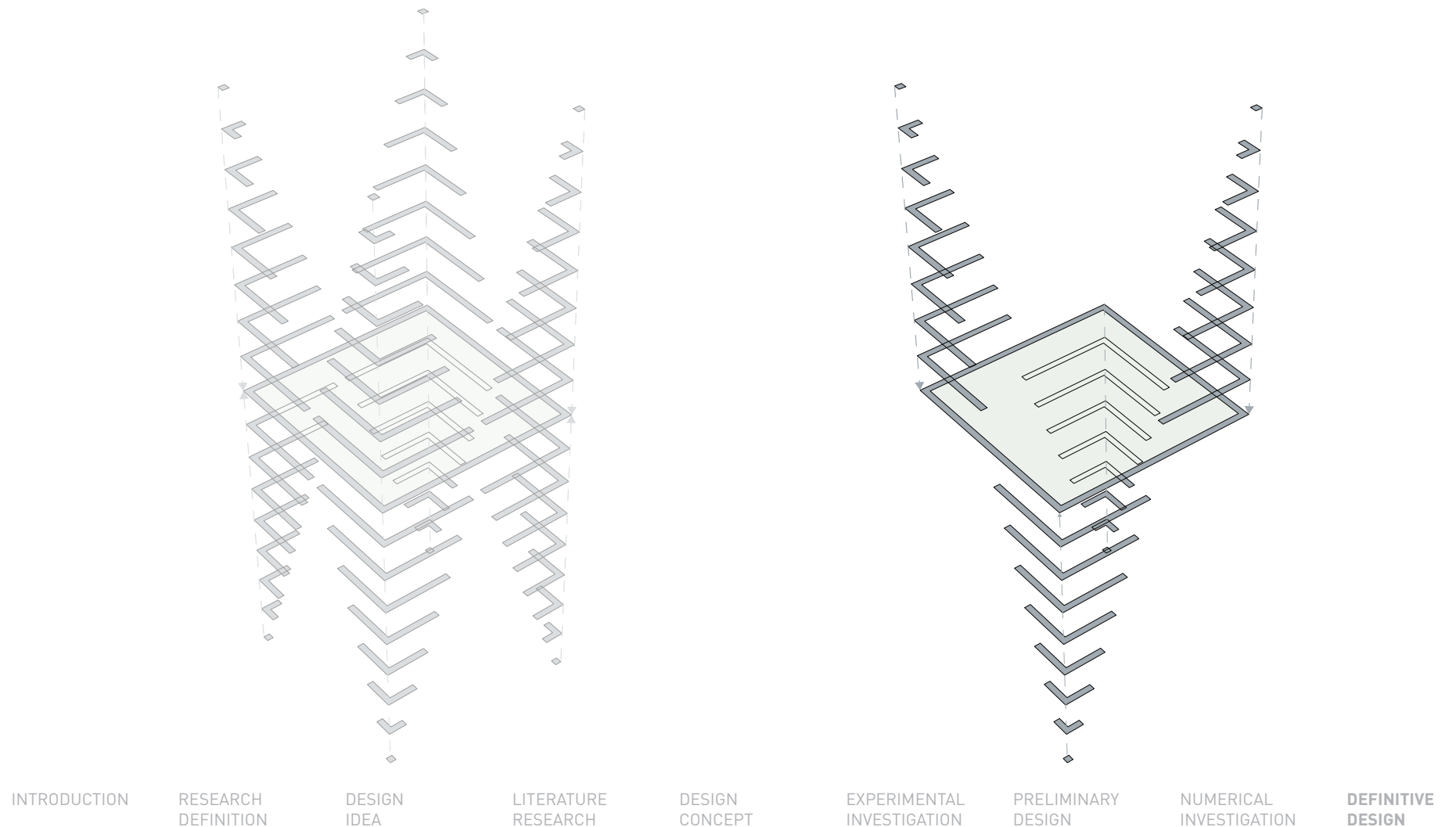
INTEGRATED
DOVETAIL JOINT

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LINEAR DECREASED EDGE STIFFNESS THROUGH THE AMOUNT OF LAYERS



DEFINITIVE
DESIGN

BUILD UP GFRP
LAYERS

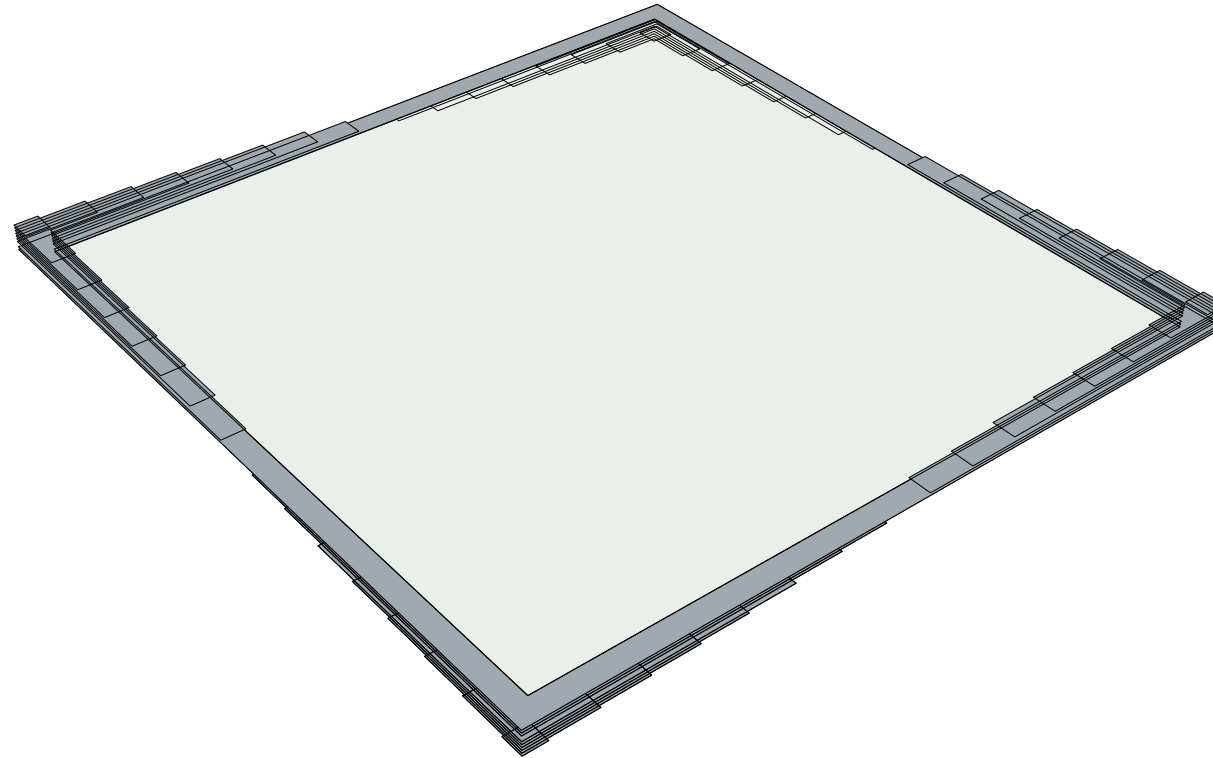
INTEGRATED
DOVETAIL JOINT

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INTEGRATING THE DOVETAIL JOINT WITHIN THE GFRP EDGES



DEFINITIVE DESIGN

BUILD UP GFRP LAYERS

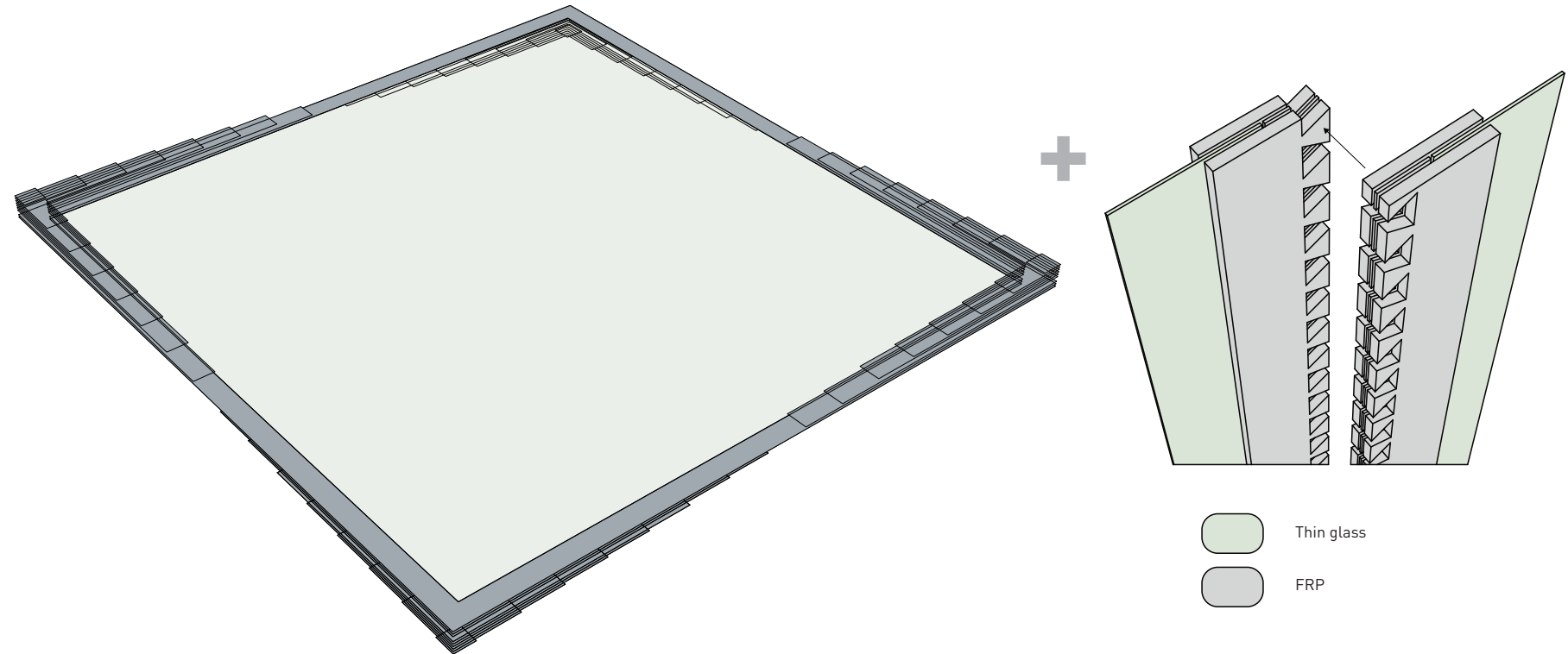
INTEGRATED DOVETAIL JOINT

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DEFINITIVE
DESIGN

BUILD UP GFRP
LAYERS

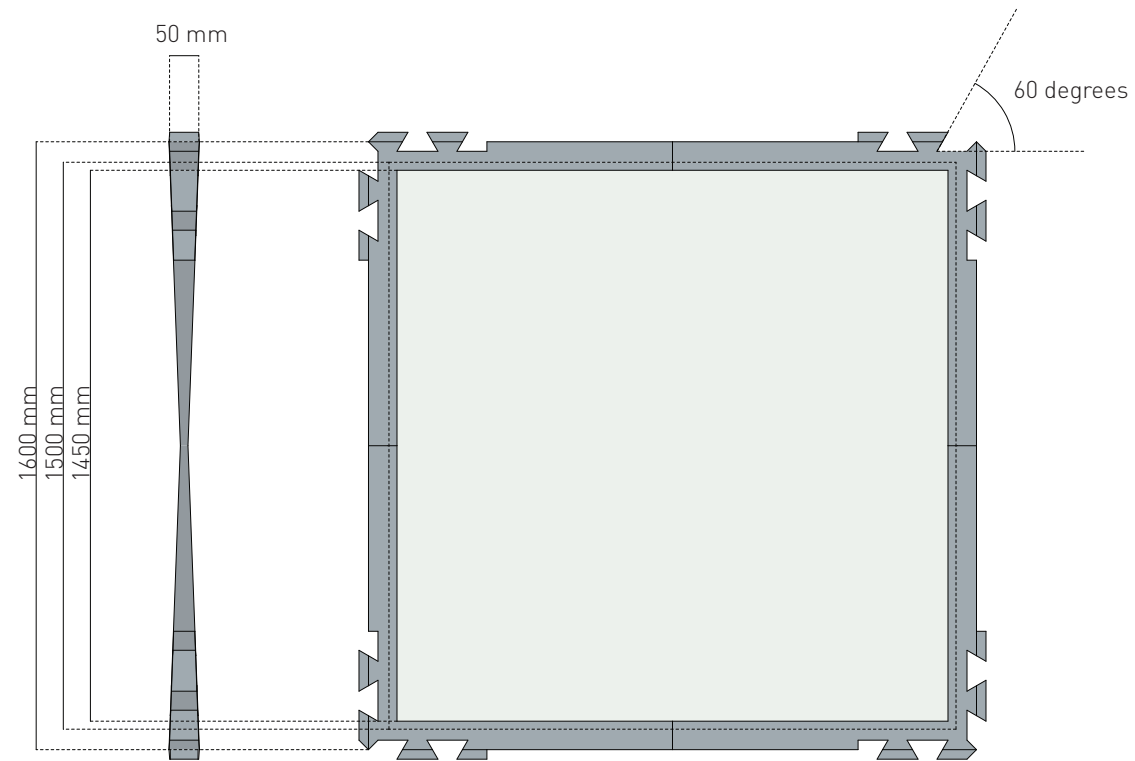
INTEGRATED
DOVETAIL JOINT

SCALABILITY

TECHNIQUE OF
TWISTING

EXTREME TWISTING

SUPPORT GFRP EDGE AT THE CORNERS



DEFINITIVE
DESIGN

BUILD UP GFRP
LAYERS

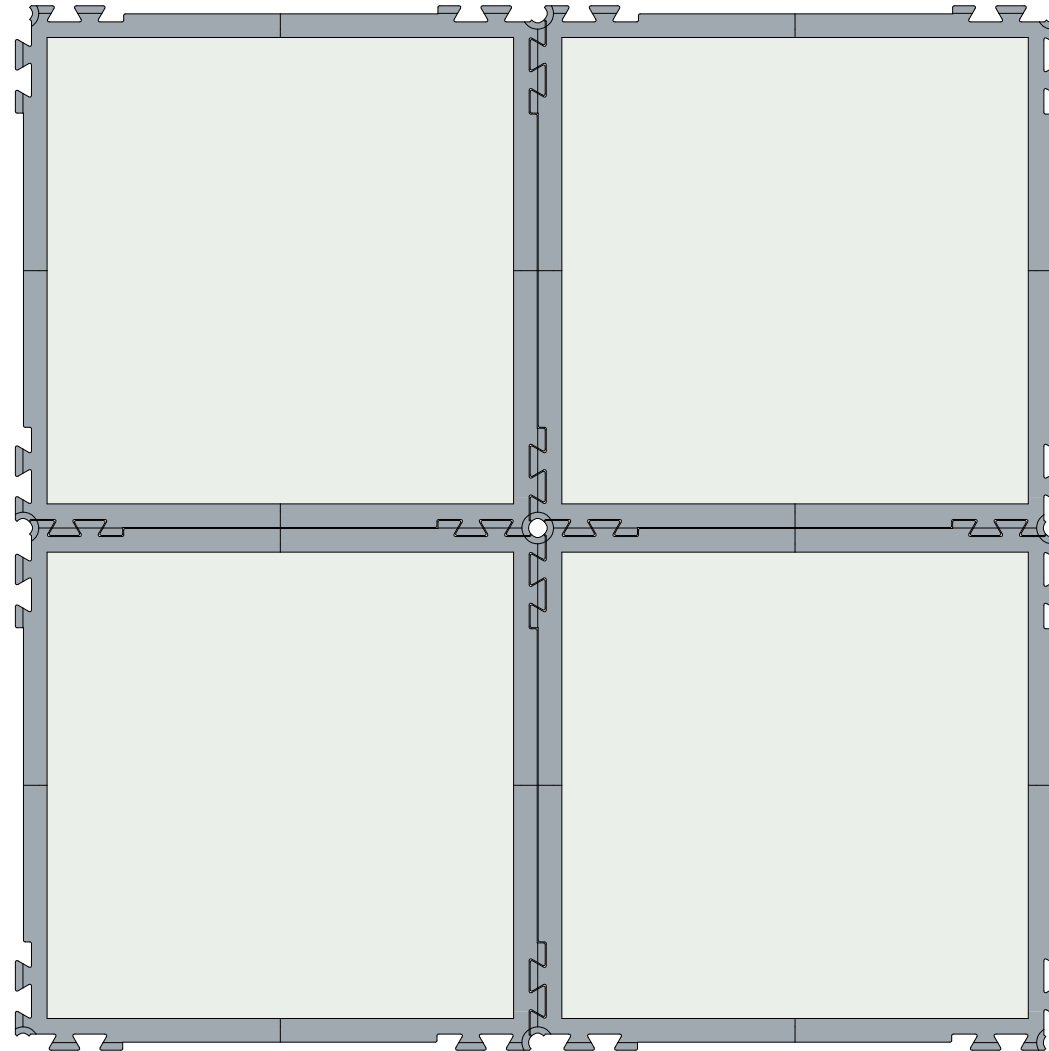
INTEGRATED
DOVETAIL JOINT

SCALABILITY

TECHNIQUE OF
TWISTING

EXTREME TWISTING

REPETITIVE HYPAR SURFACE



INTRODUCTION

RESEARCH
DEFINITION

DESIGN
IDEA

LITERATURE
RESEARCH

DESIGN
CONCEPT

EXPERIMENTAL
INVESTIGATION

PRELIMINARY
DESIGN

NUMERICAL
INVESTIGATION

**DEFINITIVE
DESIGN**

DEFINITIVE
DESIGN

BUILD UP GFRP
LAYERS

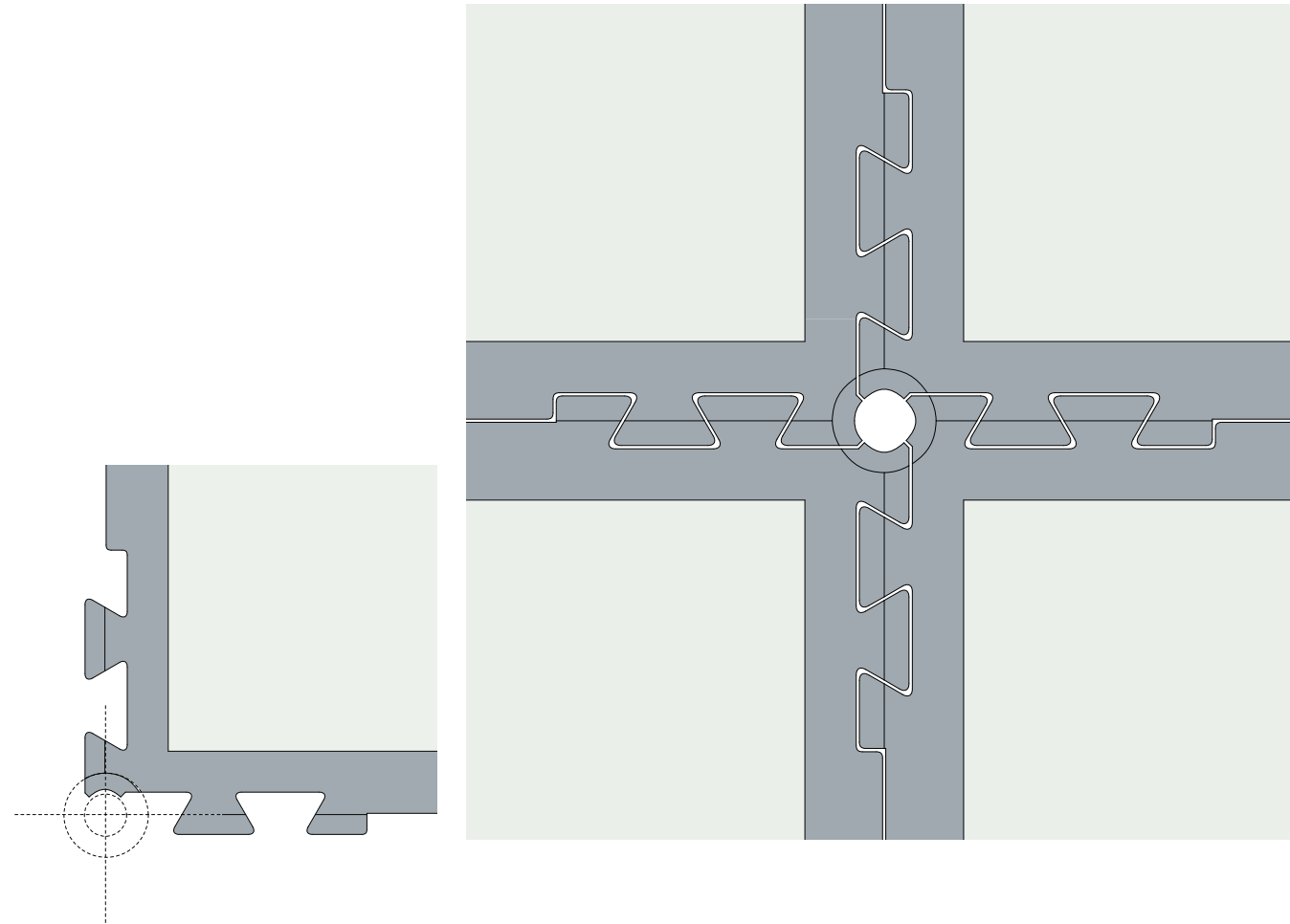
INTEGRATED
DOVETAIL JOINT

SCALABILITY

TECHNIQUE OF
TWISTING

EXTREME TWISTING

BY ASSEMBLING EACH PANEL TO EACH OTHER



DEFINITIVE
DESIGN

BUILD UP GFRP
LAYERS

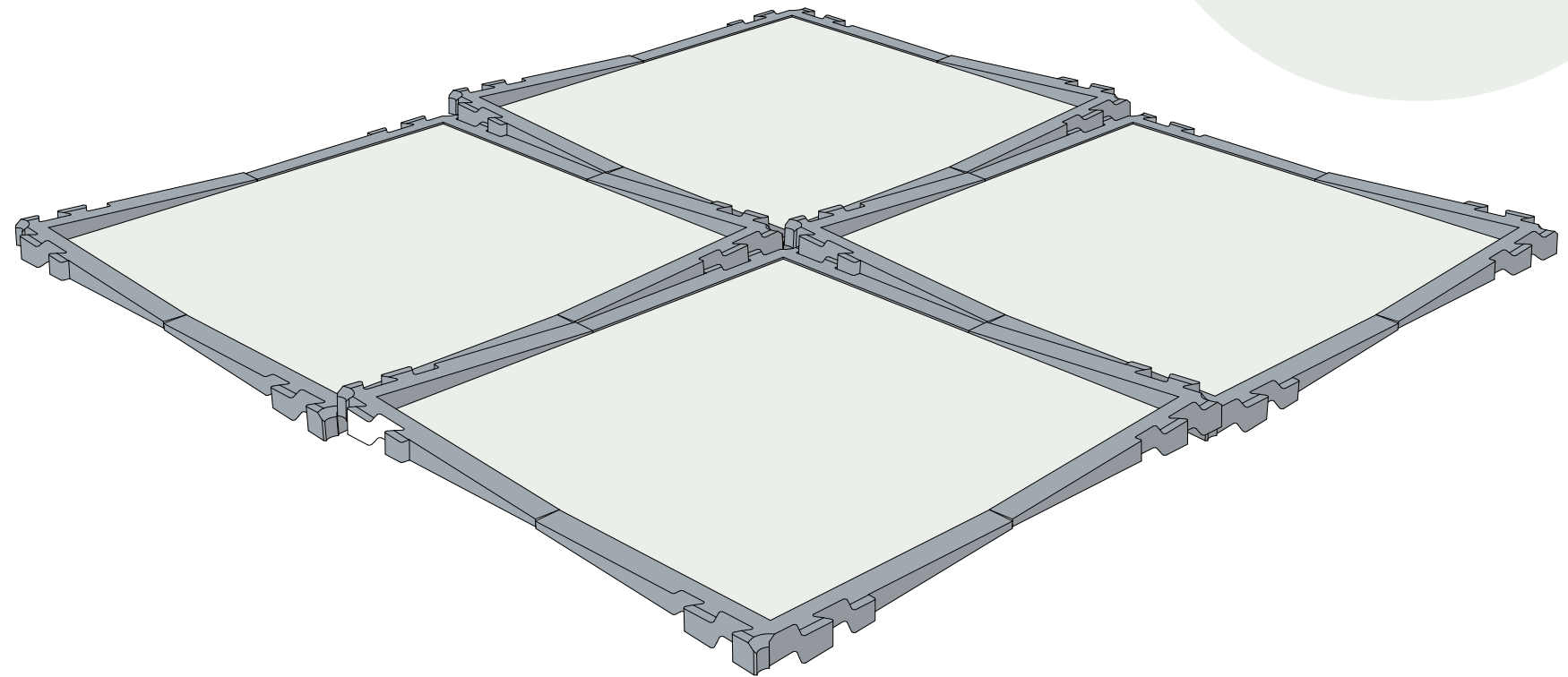
INTEGRATED
DOVETAIL JOINT

SCALABILITY

TECHNIQUE OF
TWISTING

EXTREME TWISTING

BY ASSEMBLING EACH PANEL TO EACH OTHER
FROM FLAT, THIN GLASS



DEFINITIVE
DESIGN

BUILD UP GFRP
LAYERS

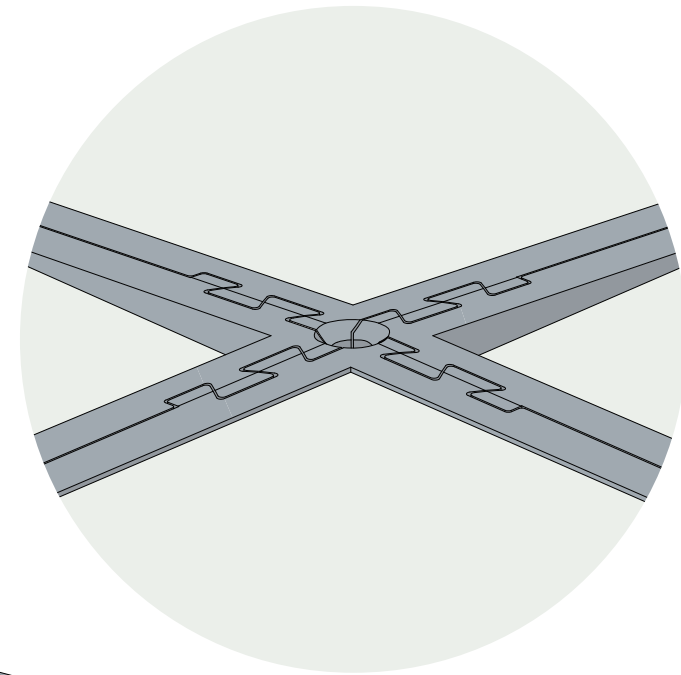
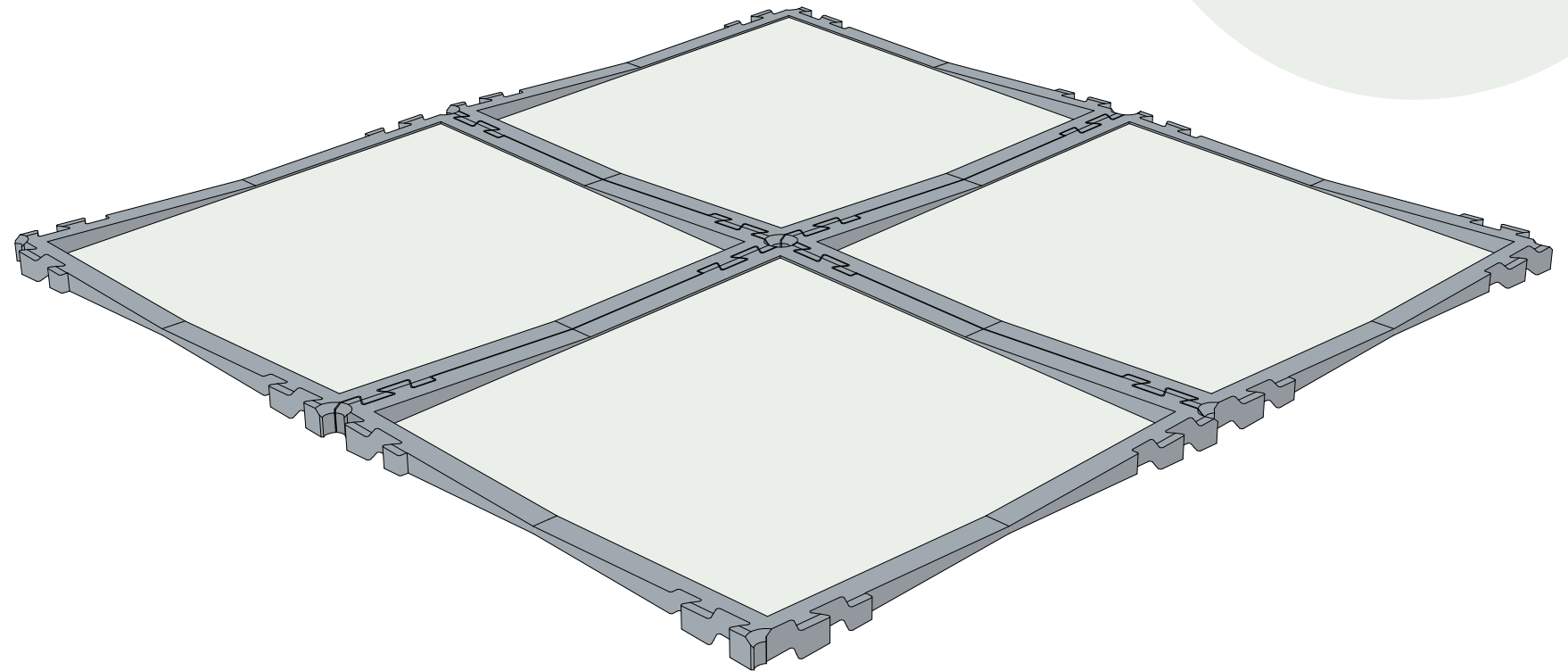
INTEGRATED
DOVETAIL JOINT

SCALABILITY

TECHNIQUE OF
TWISTING

EXTREME TWISTING

BY ASSEMBLING EACH PANEL TO EACH OTHER
TO DOUBLE, ANTICLASTIC, COLD BENT, THIN GLASS



DEFINITIVE
DESIGN

BUILD UP GFRP
LAYERS

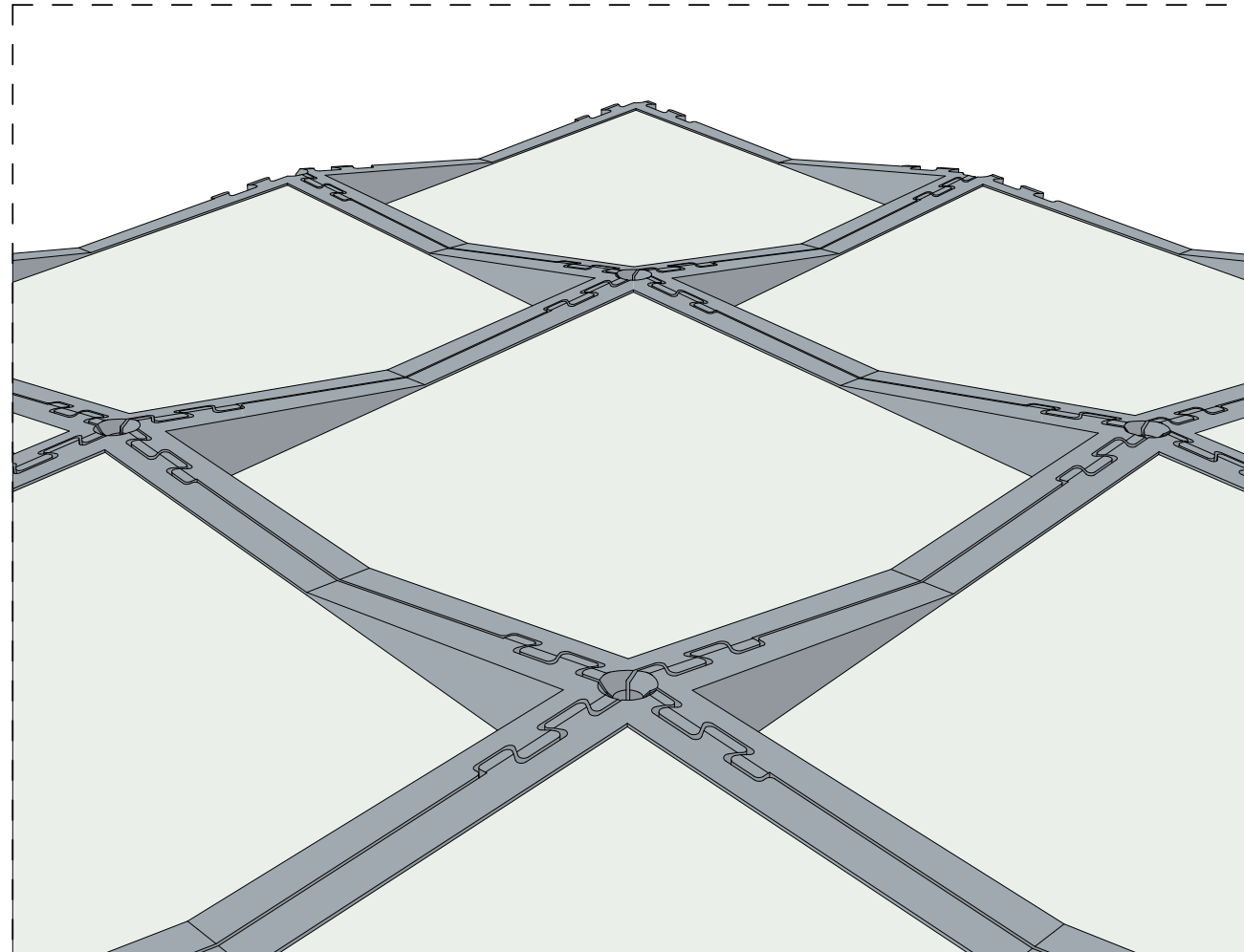
INTEGRATED
DOVETAIL JOINT

SCALABILITY

TECHNIQUE OF
TWISTING

EXTREME TWISTING

MAXIMUM TENSILE STRESS CAPACITY



DEFINITIVE
DESIGN

BUILD UP GFRP
LAYERS

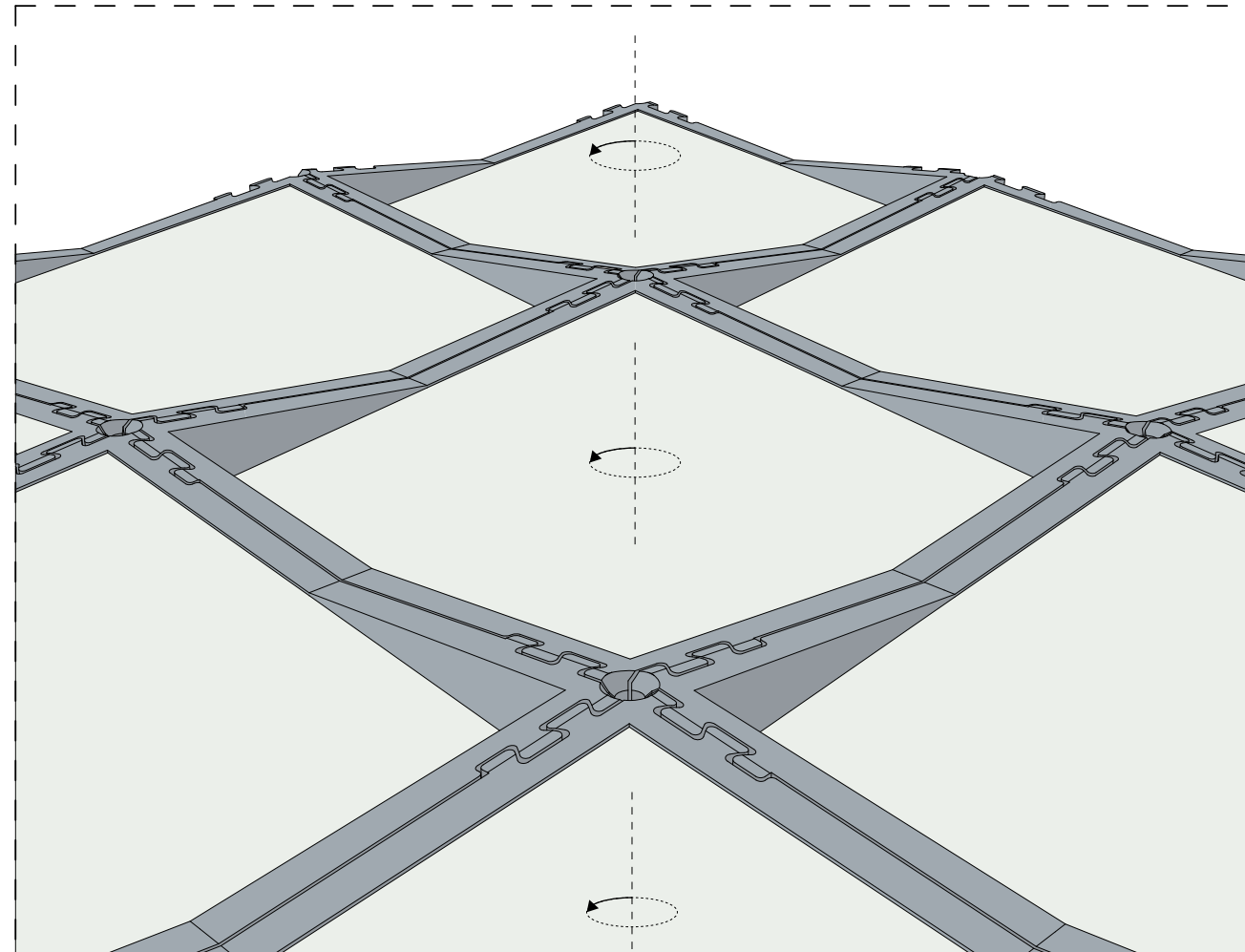
INTEGRATED
DOVETAIL JOINT

SCALABILITY

TECHNIQUE OF
TWISTING

EXTREME TWISTING

MAXIMUM TENSILE STRESS CAPACITY



DEFINITIVE
DESIGN

BUILD UP GFRP
LAYERS

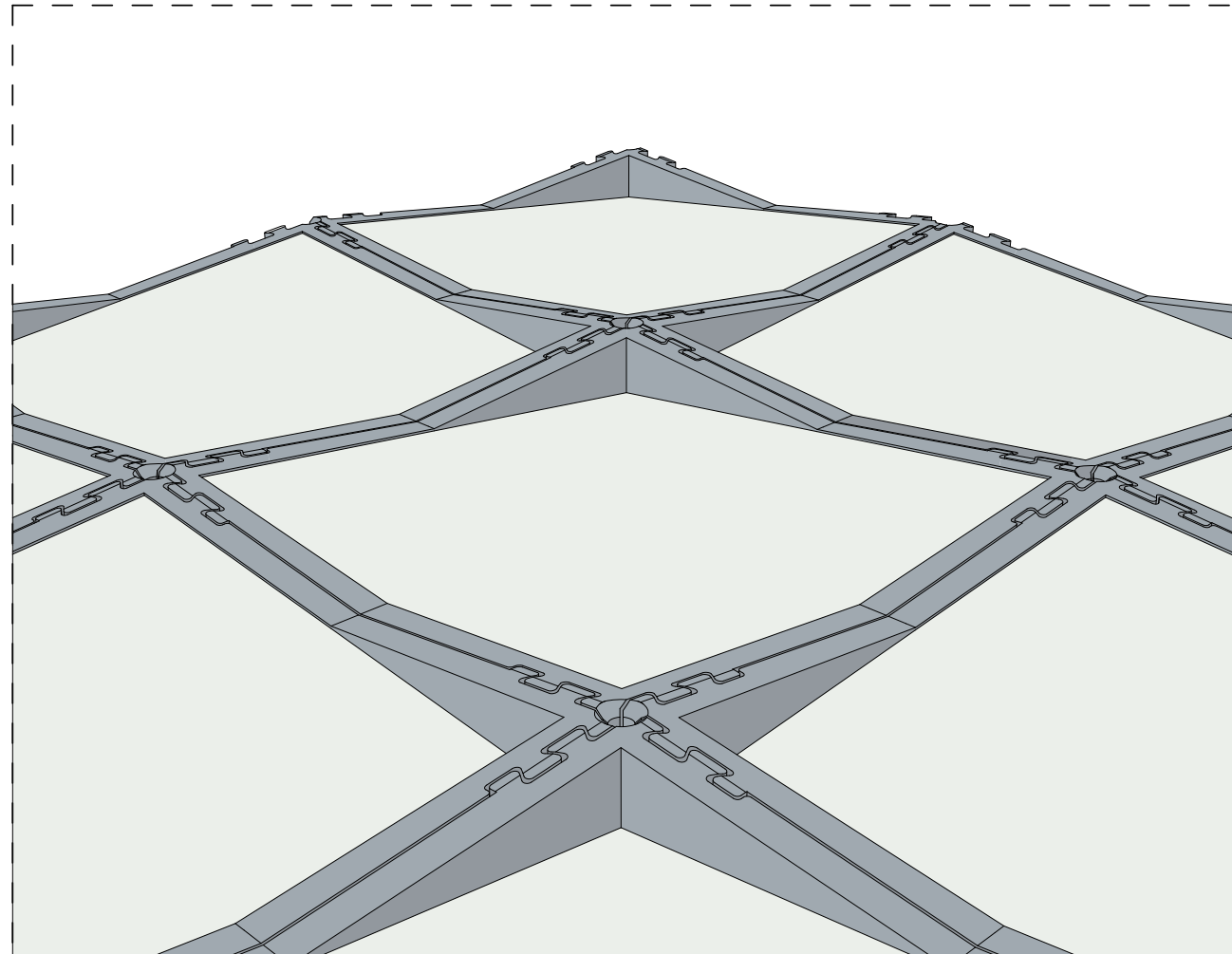
INTEGRATED
DOVETAIL JOINT

SCALABILITY

TECHNIQUE OF
TWISTING

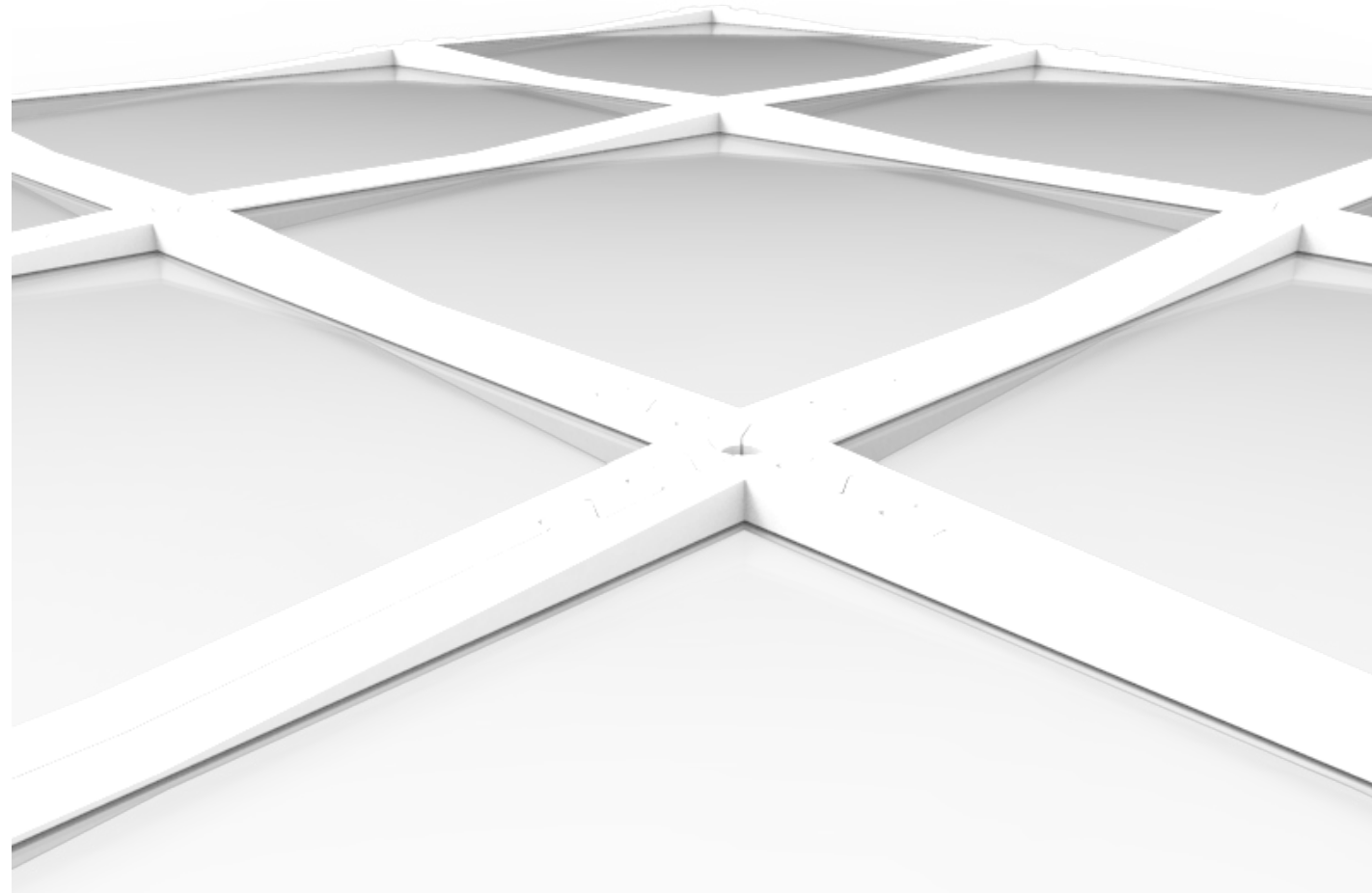
EXTREME TWISTING

MAXIMUM TENSILE STRESS CAPACITY



“TO WHAT EXTENT IS IT POSSIBLE TO CURVE A FLAT SHEET OF THIN GLASS INTO A DOUBLE ANTICLASTIC BENT SURFACE BY ADDING TENSION TO THE CURRENTLY USED COLD TWISTING TECHNIQUE?”

“TO WHAT EXTENT IS IT POSSIBLE TO CURVE A FLAT SHEET OF THIN GLASS INTO A DOUBLE ANTICLASTIC BENT SURFACE BY ADDING TENSION TO THE CURRENTLY USED COLD TWISTING TECHNIQUE?”





HIGH STRENGTH THIN GLASS AS STIFF STRUCTURAL FABRIC ?



EVALUATION



HIGH STRENGTH THIN GLASS AS STIFF STRUCTURAL FABRIC

