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On-line Bayesian Model Updating and Model Selection of a Piece-wise model for the Creep-growth rate prediction of a Nuclear component

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Abstract

This work presents an application of the recently-developed Sequential Ensemble Monte Carlo sampler in performing on-line Bayesian model updating for the Prognostics Health Management of a passive component of an Advanced Reactor. The passive component involves a stainless-steel material subjected to a thermal creep deformation whose growth rate is modelled by a continuous piece-wise model consisting of 3 models, each representing a creep-growth stage.

There are 2 investigations done in this research. For the first investigation, the model identification capability of the Sequential Monte Carlo sampler is evaluated in identifying the most probable model for each creep-growth stage. For the second investigation, the on-line Bayesian model updating procedure via the aforementioned sampler is then undertaken. In addition, a method is proposed where the model updating approach will be done for each model sequentially across the different creep-growth stage. This process involves utilising information of the boundary conditions obtained from the model output interval at the transition times to determine the prior bounds for each model parameter to be updated. This method seeks to minimise the discontinuity in the updated piece-wise model at the transition times. From there, the Remaining Useful Life analysis on the component is performed.

Keywords: Bayesian Model Updating, Model Selection, Uncertainty Quantification, Nuclear, Prognostics, Remaining Useful Life

1. Introduction

In recent years, on-line Bayesian model updating technique has been gaining popularity as a technique to address numerous problems in engineering. This involves the updating of knowledge of the inferred parameter(s) while the distinct data-sets are obtained sequentially across different times. As such, this technique is of importance in the context of Prognostics Health Management where real-time monitoring of the component's state of health is of importance for timely maintenance and Remaining Useful Life (RUL) prediction [1]. There are 2 significant advantages to such approach: 1) it does not require a complete data-set to be present in order to perform Bayesian inference; and 2) it allows for condition-based maintenance to be done rather than time-based maintenance which is more frequent and costly [1].

For the work presented in this paper, on-line Bayesian model updating is implemented to perform probabilistic model updating on a continuous piece-wise model. To the best of the authors' knowledge, such work has not been done previously which will be addressed here. This research comprises of 2 key objectives: 1) to assess and evaluate the capability of the recently-developed Sequential Ensemble Monte Carlo (SEMC) [2] sampler to identify the most probable model for the corresponding sub-domain under uncertainty; and 2) to propose a method to account for boundary conditions when determining the prior bounds for the selected inferred model parameters based on interval arithmetic [3]. The eventual goal of this research is to arrive at an approach to ensure that the updated piece-wise model captures most of the information contained by the observed data whilst ensuring minimal discontinuities between the sub-domains.

1.1. Bayesian Model Updating

A well-known probabilistic model updating technique commonly used in engineering is Bayesian model updating [4]. The framework based on Bayesian inference [5]:

$$P(\theta|\mathbf{D}, M) = \frac{P(\theta|M) \cdot P(\mathbf{D}|\theta, M)}{P(\mathbf{D}|M)} \quad (1)$$

The terms in Eq. (1) follows: θ is the vector of the inferred epistemic parameters; \mathbf{D} is the vector of measurements; M is the mathematical model which predicts the observed \mathbf{D} as a function of θ ; $P(\theta|M)$ is the prior distribution; $P(\mathbf{D}|\theta, M)$ is the likelihood function; $P(\theta|\mathbf{D}, M)$ is the posterior distribution; and $P(\mathbf{D}|M)$ is the evidence. Detailed explanations to the above terms are found in [6].

In the on-line Bayesian model updating framework, data is obtained sequentially at different time t_s where s denotes the time index. Such set-up is used to infer θ which can be either time-invariant or time-varying. In this paper, we shall only consider the case where θ is time-invariant. As such, assuming independence between the data obtained at different t_s , the posterior at a given t_s is defined [7]:

$$P(\theta|\mathbf{D}^{1:s}, M) \propto P(\theta|M) \cdot \prod_{s=1}^{s_{end}} P(\mathbf{D}^s|\theta, M) \quad (2)$$

where s_{end} is the index for the terminal time.

Eq. (2), implies that $P(\theta|\mathbf{D}^{1:s}, M)$ is time-varying. As such, samples have to be obtained sequentially across all t_s . To do this, several sampling techniques can be employed such as Kalman Filter [8], Gaussian Sum Filters [9], [10], and Sequential Monte Carlo samplers [11]. For the research work presented here, a new variant of Sequential Monte Carlo sampler, known as the Sequential Ensemble Monte Carlo (SEMC) sampler [2], will be implemented.

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1.2. Review of the Sequential Ensemble Monte Carlo

The SEMC sampler presents 2 key features: 1) the use of the Affine-invariant Ensemble sampler (AIES) in place of the Metropolis-Hastings (MH) sampler for the Markov Chain Monte Carlo (MCMC) step; and 2) an adaptive-tuning algorithm which tunes automatically the step-size parameter of the AIES [2].

1.2.1. Affine-invariant Ensemble sampler

The AIES is a MCMC algorithm developed by Goodman and Weare in 2010 which involves the use of multiple chains (i.e. an ensemble) to explore the sample space defined by the target distribution. From which, it utilises an affine-invariant stretch-move kernel to generate candidate samples θ^* between chains contrary to the MH algorithm which utilises a proposal distribution (i.e. a Normal distribution) to generate θ^* for one chain at a time which does not exhibit the affine-invariant property [12]. As a result, the AIES is able to sample from highly-skewed, anisotropic distributions compared to its MH counterpart. To highlight this, extensive studies have been done in [12], [13] to which readers can refer for details.

The AIES generates N_e ensemble as follows: Defining the i^{th} ensemble $\vec{\theta}_i = \{\theta_{1,i}, \theta_{2,i}, \dots, \theta_{N_c-1,i}, \theta_{N_c,i}\}$, where N_c is the total number of chains; and $i = 1, \dots, N$ is the iteration number. It needs to be noted that $N_c \geq 2 \times N_d$ where N_d is the total number of inferred parameters [12]. For each iteration i , a given chain k , for $k = 1, \dots, N_c$, is updated through the stretch-move kernel [12]:

$$\theta_k^* = \theta_{[k]}^* + \lambda \cdot (\theta_{k,i}^* - \theta_{[k]}^*) \quad (3)$$

where θ_k^* is the candidate sample of the k^{th} chain; $\theta_{[k]}$ is a randomly chosen sample from the complementary set $\vec{\theta}_{[k]} = \{\theta_{1,i+1}, \dots, \theta_{k-1,i+1}, \theta_{k+1,i}, \dots, \theta_{N_c,i}\}$; and λ is real-valued scalar proposal stretch factor. λ is a random variable following a proposal distribution $g(\lambda)$:

$$g(\lambda) = \begin{cases} \frac{1}{2 \cdot (\sqrt{u} - \frac{1}{\sqrt{u}})} \cdot \frac{1}{\sqrt{\lambda}} & \text{if } \lambda \in [\frac{1}{u}, u] \\ 0 & \text{otherwise} \end{cases} \quad (4)$$

where $u \geq 1$ is the user-defined step-size auxiliary parameter of the AIES sampler. From there, θ_k^* is accepted with probability α_k :

$$\alpha_k = \min \left[1, \lambda^{N_d-1} \cdot \frac{P(\theta_k^* | \mathbf{D}^{1:s}, M)}{P(\theta_{k,i} | \mathbf{D}^{1:s}, M)} \right] \quad (5)$$

This process is repeated for all N_c chains upon which when this is done, the algorithm proceeds to iteration $i = i + 1$ and repeats the above procedure until $i = N_e$.

1.2.2. Adaptive Tuning Algorithm

The adaptive tuning algorithm was proposed in [13] to allow for the automatized tuning of u which, in turn, helps to control the acceptance-rates of the sampler at each iteration j . The algorithm works as such: At $j = 1$, an initial value of u is set. Although the recommended value is 2, as this is the "optimal" value for most problems [12], this initial value can vary depending on the complexity of the problem

and the number of parameters to be inferred. From this initial value, the nominal step-size u_{nom} is computed after the MCMC step:

$$u_{nom} = u^j \cdot \exp[\alpha^j - \alpha_{tr}] \quad (6)$$

where α^j is the overall acceptance rate of the AIES sampler at iteration j of the SEMC sampler, while α_{tr} is the target acceptance rate defined as [14]:

$$\alpha_{tr} = \frac{0.21}{N_d} + 0.23 \quad (7)$$

If $u_{nom} > 1$, set $u^{j+1} = u_{nom}$. Else, set $u^{j+1} = 1.01$.

1.2.3. SEMC Sampling Algorithm

The SEMC algorithm generates N samples from the posterior as such [2]:

1. Initialise sampler (i.e. $j = 0$). Sample N samples of $\theta_i^{j+1} \sim P(\theta | M)$ for $i = 1, \dots, N$;
2. Set $j = 1$ and $u^{j=1} = 2$.
3. Compute the weights $\hat{w}_i^j = \frac{P(\mathbf{D}^j | \theta_i^j, M)}{\sum_{i=1}^N P(\mathbf{D}^j | \theta_i^j, M)}$;
4. Compute $N_{eff} = \frac{1}{\sum_{i=1}^N (\hat{w}_i^j)^2}$;
5. If $N_{eff} < \frac{N}{2}$, resample N $\theta_i^j \sim \hat{w}_i^j$ and set $\hat{w}_i^j = \frac{1}{N}$.
6. Resample N samples of $\theta_i^j \sim \hat{w}_i^j$ and set them as initial ensemble $\vec{\theta}_1$. Generate $\vec{\theta}_2$ via 1 iteration of the AIES algorithm according to $P(\theta^j | \mathbf{D}^{1:j}, M)$;
7. Compute u_{nom} via Eq. (6).
8. If $u_{nom} > 1$, set $u^{t+1} = u_{nom}$. Else, set $u^{t+1} = 1.01$;
9. Set $P(\theta^j | \mathbf{D}^{1:j}, M)$ as the new prior PDF and θ_i^j as the new prior samples;
10. Compute evidence: $P(\mathbf{D}^{1:j} | M) \approx \frac{1}{N} \prod_{m=1}^j \sum_{i=1}^N P(\mathbf{D}^m | \theta_i^m, M)$;
11. Set $j = j + 1$ and repeat Steps 3 to 10 until $j = j_{end}$ (Terminal iteration).

2. Case Study

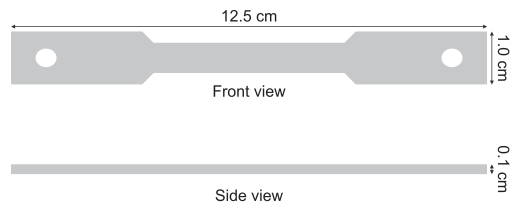


Figure 1. Schematic diagram of the Advanced Reactor passive component with its corresponding dimensions. Image adopted from [15].

The set-up involves an Advanced Reactor passive component whose schematics is illustrated in Figure 1. In [15],

the effect of thermal creep degradation of the component is studied for the purpose of assessing its Prognostics Health Management (PHM) framework. To do so, the literature presented a numerical study using synthetic data of creep-growth rate $\frac{d\epsilon}{dt}$, in units of percent strain, generated from 3 different models representing the corresponding creep-growth stage: 1) \hat{M}_1 (Primary stage); 2) \hat{M}_2 (Secondary stage); and 3) \hat{M}_3 (Tertiary stage). These models are defined respectively following [15]:

$$\hat{M}_1(t) = 1 - \exp(-0.40 \cdot t), \text{ for } 0 \leq t \leq 6 \quad (8)$$

$$\hat{M}_2(t) = 0.07 \cdot t + 0.75, \text{ for } 6 < t \leq 24 \quad (9)$$

$$\hat{M}_3(t) = 3.52e - 0.4 \cdot t^3 - 1e - 0.5 \cdot t^2 - 0.63 \cdot t + 12.93, \text{ for } t > 24 \quad (10)$$

where t is in hrs.

The synthetic data-set $\mathbf{D}(t)$ is obtained at $t = \{0, 2, 3, 4, 7, 11, 15, 19, 23, 26, 27, 28, 30\}$ hrs. For each t , the corresponding $\mathbf{D}(t)$ is obtained following [15]:

$$\mathbf{D}(t) = \hat{M}(t) + \varepsilon, \text{ for } \varepsilon \sim N(0, 0.1^2) \quad (11)$$

where $\hat{M}(t)$ is the creep-growth model (i.e. see Eq. (8) to (10)), and ε is the simulated "measurement error" term. The resulting synthetic data is illustrated in Figure 2.

There are 2 investigations involved in this case-study: 1) to evaluate the capability of the SEMC sampler to identify the appropriate creep-growth model for each creep-growth stage; and 2) to propose a methodology for the on-line model updating of the piece-wise creep-growth rate model.

3. Investigation 1: Model Identification

To identify the most probable model for each creep-growth stage under uncertainty, at a given t_s , the model probability posterior $P(M|\mathbf{D}^{1:s})$ is used as the metric. For a given v^{th} model M_v , its model probability posterior computed as [16]:

$$P(M_v|\mathbf{D}^{1:s}) = \frac{P(M_v) \cdot P(\mathbf{D}^{1:s}|M_v)}{P(\mathbf{D}^{1:s})} \quad (12)$$

where $P(M_v)$ is the prior probability of model M_v , $P(\mathbf{D}^{1:s}|M_v)$ is the evidence computed from the SEMC sampler (i.e. see Section 1.2.3); and $P(\mathbf{D}^{1:s}) = \sum_v P(M_v) \cdot P(\mathbf{D}^{1:s}|M_v)$ is the normalisation constant.

In this investigation, it will be assumed that we have no a priori knowledge that the creep-growth rate model is piece-wise. As such, the approach would involve the use of 5 different possible models, each defined for $t \in [0, 30]$ hrs as follows:

$$M_1(t) = \theta_2 \cdot [1 - \exp(-\theta_1 \cdot t)] \quad (13)$$

$$M_2(t) = \theta_2 \cdot t + \theta_1 \quad (14)$$

$$M_3(t) = \theta_4 \cdot t^3 + \theta_3 \cdot t^2 + \theta_2 \cdot t^1 + \theta_1 \quad (15)$$

$$M_4(t) = \theta_2 \cdot \exp(\theta_1 \cdot t) \quad (16)$$

$$M_5(t) = \exp(\theta_2 \cdot t^2 + \theta_1 \cdot t) \quad (17)$$

where θ_1 to θ_4 are the epistemic model parameters. Models M_4 and M_5 are introduced as potential functions, in

addition to model M_3 , to model the creep-growth rate in Stage III. There are 2 reasons for this: 1) Model M_3 is a cubic function which could be too specific of a choice of function to model Stage III of creep-growth rate; and 2) Model M_3 introduces more (and possibly unnecessary) inferred parameters to infer which makes it relatively complex compared to models M_4 and M_5 which involve less inferred parameters and would less-likely over-fit the data in Stage III (i.e. Occam's razor [17]).

Another assumption in this investigation is that we do not have any a priori information on the prior probability of model M_v , for $v = 1, \dots, 5$. As such, it will be treated that all models M_v are equally probable. Hence, Eq. (12) is simplified as:

$$P(M_v|\mathbf{D}^{1:s}) = \frac{P(\mathbf{D}^{1:s}|M_v)}{\sum_v P(\mathbf{D}^{1:s}|M_v)} \quad (18)$$

3.1. Bayesian Inference Set-up

For each of the given model in Eq. (13) to (17), its corresponding epistemic model parameters are assigned a Uniform prior with the respective bounds presented in Table 1. In addition, the measurement error term σ will also be inferred given the lack of prior knowledge and is assigned a Uniform prior with the interval: $[0.001, 1]$ %.

Table 1. Uniform prior bounds for the respective inferred model parameters.

Model	θ_1	θ_2	θ_3	θ_4
M_1	$[-5, 5]$	$[0, 5]$	–	–
M_2	$[-5, 5]$	$[0, 5]$	–	–
M_3	$[0, 15]$	$[-1, 1]$	$[-0.1, 0.1]$	$[0, 0.01]$
M_4	$[0.01, 1]$	$[0.01, 50]$	–	–
M_5	$[0, 1]$	$[-5, 5]$	–	–

The likelihood function at t_s , given model M_v , is modelled as a Normal distribution [6]:

$$P(\mathbf{D}^s|\theta, M_v) = \frac{1}{\sigma \cdot \sqrt{2\pi}} \exp\left[-\frac{(\mathbf{D}^s - M_v(\theta))^2}{2 \cdot \sigma^2}\right] \quad (19)$$

The SEMC sampler is implemented for each M_v with the number of samples set at $N = 1000$.

3.2. Results and Discussions

The resulting $P(M_v|\mathbf{D}^{1:j})$ is computed using Eq. (18) and the numerical results are presented in Table 2 while corresponding graphical plots are illustrated in Figure 3.

From Figure 3, it is observed that the SEMC sampler is able to identify models M_1 and M_2 being the most probable models for creep-growth Stages I and II respectively. The results are consistent with the true set-up described in Section 2 as well as the results obtained in the work by Ramhalli *et. al* [15]. However, from iteration $j = 9$ onwards, it can be seen that model M_2 is the most probable model to describe Stage III of creep-growth rate with a probability close to 1. In addition, models M_3 , M_4 , and M_5 are observed to have probabilities close to 0 which is mathe-

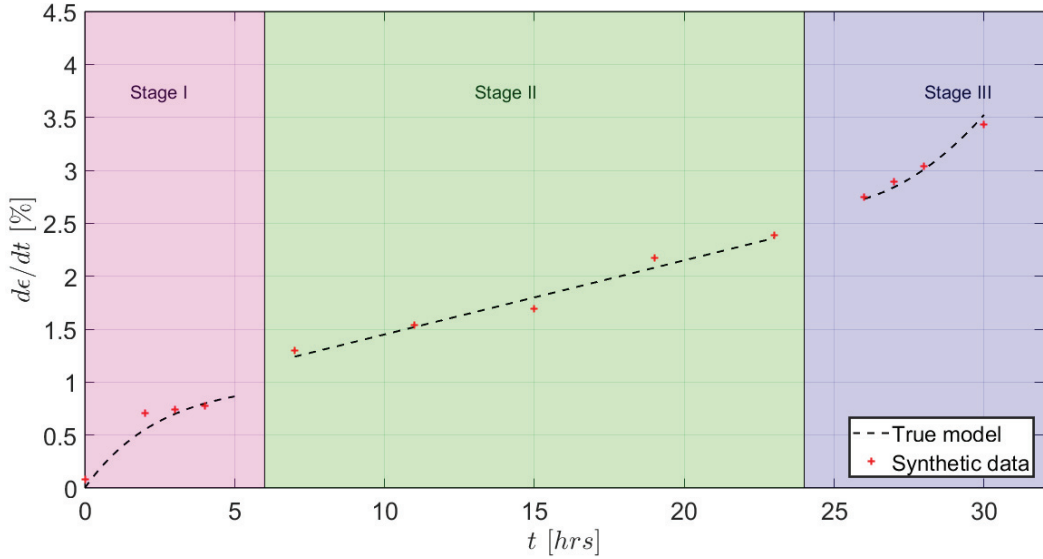


Figure 2. Synthetic data of creep-strain growth rate, $\frac{d\epsilon}{dt}$, against time, t .

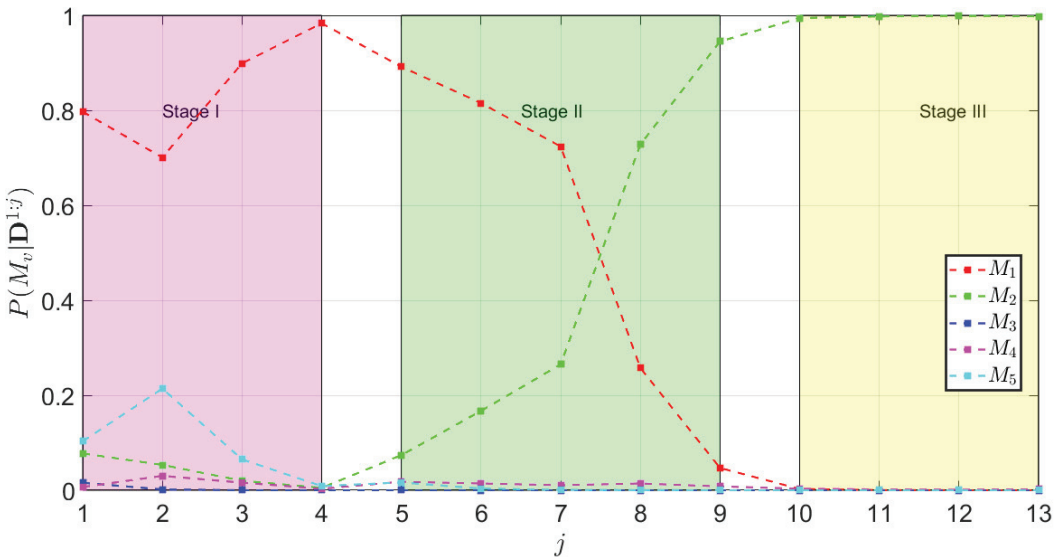


Figure 3. Results of $P(M_v | D^{1:j})$ for all models M_v across iterations j .

matically inconsistent. This is especially so for the case of model M_3 to which the result also disagrees to the set-up described in Section 2.

The above observations imply that the SEMC sampler is able to effectively identify the most probable models up to the 9th data point (i.e. iteration $j = 9$). The reason behind the failure of the SEMC sampler to correctly identify the most appropriate model from the 10th data point onwards is

due to the posterior at iteration $j = 9$ (i.e. $P(\theta | D^{1:9}, M_v)$) being dominated by $P(D^j | \theta, M_v)$ obtained from iterations $j = 1$ to $j = 9$. As a result, any further information contained in $P(D^j | \theta, M_v)$ from $j = 10$ onwards would not significantly update the posterior obtained from the iteration before. This, in turn, leads to the data in Stage III being ineffective in providing information towards the identification of either models M_3 , M_4 , or M_5 .

Table 2. Numerical results of $P(M_v|D^{1:j})$ obtained at each iteration j for the corresponding model M_v .

j	M_1	M_2	M_3	M_4	M_5
1	0.797	0.077	0.000	0.007	0.103
2	0.701	0.053	0.000	0.030	0.214
3	0.899	0.020	0.000	0.016	0.065
4	0.983	0.005	0.000	0.003	0.009
5	0.892	0.074	0.000	0.018	0.017
6	0.815	0.167	0.000	0.014	0.004
7	0.724	0.265	0.000	0.011	0.000
8	0.258	0.728	0.000	0.014	0.000
9	0.047	0.945	0.000	0.008	0.000
10	0.003	0.994	0.000	0.003	0.000
11	0.000	0.998	0.000	0.002	0.000
12	0.000	0.999	0.000	0.001	0.000
13	0.000	0.998	0.000	0.002	0.000

To address this issue, the procedure is repeated involving only the data in Stage III. Considering that the results from the previous analysis have concluded that model M_1 is the most probable model given the data in Stage I, it will be excluded from this round of the analysis. For models M_2 and M_3 , inferred model parameters are assigned a Uniform prior with the respective bounds as per in Table 1. For the case of models M_4 and M_5 , the inferred model parameters are also assigned a Uniform prior with the following bounds presented in Table 3. It needs to be noted that the logarithmic scale is used for the bounds to provide numerical stability.

Table 3. Uniform prior bounds for the respective inferred model parameters of models M_4 and M_5 .

Model	$\log(\theta_1)$	$\log(\theta_2)$
M_4	$[-4, -1.9]$	$[-4, -1]$
M_5	$[-10, -3]$	$[-3, -2]$

The numerical results to $P(M_v|D^{1:j})$ across the iterations j for the respective models M_v are presented in Table 4 while the resulting graphical plots are illustrated in Figure 4. From the figure, it is evident that the model posterior probability is consistently the highest for model M_4 instead of M_3 which substantiates the hypothesis set-forth by Occam’s razor.

Table 4. Numerical results of $P(M_v|D^{1:j})$ obtained at each iteration j for the corresponding model M_v .

j	M_2	M_3	M_4	M_5
1	0.048	0.080	0.832	0.041
2	0.070	0.073	0.850	0.008
3	0.163	0.036	0.799	0.001
4	0.114	0.033	0.852	0.000

Hence, from the results presented in this section, it can be concluded that the following models are the most probable to represent the data for the corresponding creep-

growth Stage: I) Model M_1 ; II) Model M_2 ; and III) Model M_4 . These findings will be used to perform the Bayesian model updating of the piece-wise creep-growth rate model to which the procedure is described in Section 4.

4. Investigation 2: Model Updating

In updating the piece-wise creep-growth rate model, the objective is to minimise discontinuity in the updated model between the different creep-growth stages. To achieve this, the following set of procedures are proposed and implemented: 1) For Stage I, model M_1 is updated with information from the data in Stage I as well as the first data in Stage II (i.e. at $t = 7$ hrs); 2) For Stage II, model M_2 is updated with information from the data in Stage II, the last data in Stage I (i.e. at $t = 4$ hrs), and the first data in Stage III (i.e. at $t = 26$ hrs); and 3) For Stage III, model M_4 is updated with information from the data in Stage III as well as the last data in Stage II (i.e. at $t = 23$ hrs).

In addition to the above procedures, boundary conditions are introduced when determining the prior bounds on the inferred model parameters. This will be done as follows: 1) Upon updating model M_1 , the bounds on the probabilistic model output at $t = 6$ hrs, denoted as $[m_1, \bar{m}_1]$, are obtained; 2) For a given set of Uniform prior bounds on θ_2 for model M_2 , denoted as $[\theta_2, \bar{\theta}_2]_{M_2}$, the Uniform prior bounds on θ_1 is computed following:

$$[\theta_1, \bar{\theta}_1]_{M_2} = [m_1, \bar{m}_1] - [\theta_2, \bar{\theta}_2]_{M_2} \cdot 6 \quad (20)$$

3) Similarly, upon updating model M_2 , the bounds on the probabilistic model output at $t = 24$ hrs, denoted as $[m_2, \bar{m}_2]$, are obtained; 4) For a given set of Uniform prior bounds on θ_1 for model M_4 , denoted as $[\theta_1, \bar{\theta}_1]_{M_4}$, the Uniform prior bounds on θ_2 is computed following:

$$[\theta_2, \bar{\theta}_2]_{M_4} = \frac{[m_2, \bar{m}_2]}{\exp([\theta_1, \bar{\theta}_1]_{M_4} \cdot 24)} \quad (21)$$

4.1. Bayesian Inference Set-up

Based on the methodology described in Section 4, the Uniform prior bounds of the inferred model parameters for the respective models are presented in Table 5. Note that the logarithmic scale is used for the inferred model parameters for model M_4 to provide numerical stability.

Table 5. Uniform prior bounds for the respective inferred model parameters.

Model	Bounds
M_1	$\theta_1 \in [0, 2]; \theta_2 \in [0, 2]$
M_2	$\theta_1 \in [\theta_1, \bar{\theta}_1]_{M_2}; \theta_2 \in [0, 1]$
M_4	$\log(\theta_1) \in [-4, 0]; \log(\theta_2) \in \log([\theta_2, \bar{\theta}_2]_{M_4})$

As per in Section 3.1, the measurement error term σ will also be inferred with its aforementioned Uniform prior bounds and the Normal distribution is assigned as the likelihood function (i.e. see Eq. (19)).

The SEMC sampler is implemented to perform Bayesian

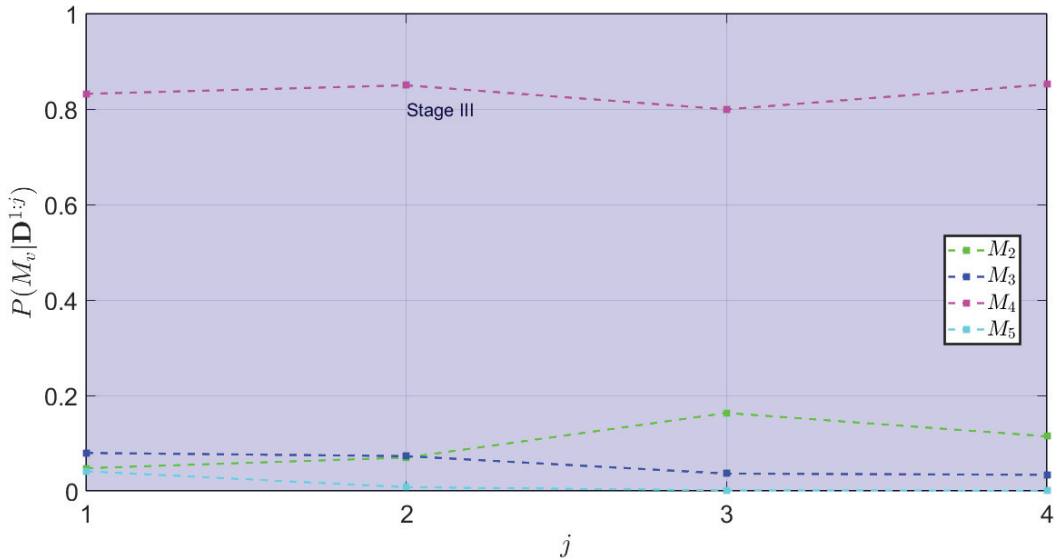


Figure 4. Results of $P(M_v | D^{1:j})$ for models M_2 to M_5 across iterations j .

model updating on each model with a sample size of $N = 1000$.

4.2. Results and Discussions

The resulting graphical plots for the updated piece-wise creep-growth rate model are illustrated in Figure 5. From the figure, it can be observed that the updated piece-wise model generally encompasses the synthetic data points as well as the true models for the respective creep-growth rate stage. In addition, the updated piece-wise model is generally smooth and continuous except at $t = 6$ hrs and $t = 24$ hrs where small degrees of discontinuity can be seen. This indicates that the Bayesian model updating procedure, along with the proposed methodologies presented in Section 4, are effective to a large extent.

Following this, the analysis on the RUL of the Advanced Reactor component is conducted at $t = \{7, 11, 15, 19, 23, 26, 27, 28, 30\}$ hrs with the end-of-life of the component is set at $t = 30$ hrs [15]. The mean RUL at each t is computed by first considering the value of $\frac{d\epsilon}{dt}$ for that particular t . From there, the output distribution of t from the updated piece-wise model given $\frac{d\epsilon}{dt}$ is obtained from which the mean RUL is derived. From the output distribution of t , the 90 % Credible Interval (CI) of the RUL estimates can be generated based on the interval obtained by taking its alpha-cut at $\alpha = 0.05$ level [18]. The numerical results to the mean RUL and its 90 % CI for the respective t are presented in Table 6 while its graphical plots are illustrated in Figure 6.

From Table 6 and Figure 6, it can be seen that in most cases, the 90 % CI of the RUL estimates includes the true RUL which verifies the Bayesian model updating results and validates the proposed methodologies. It can be no-

Table 6. Results of the RUL estimates, along with its corresponding 90 % CI, for the respective t .

Time [hrs]	True RUL [hrs]	Mean RUL [hrs]	90 % CI [hrs]
7	23	21.09	[20.49, 21.73]
11	19	18.21	[17.69, 18.76]
15	15	16.28	[15.68, 16.87]
19	11	10.47	[9.62, 11.20]
23	7	7.66	[4.04, 8.85]
26	4	3.90	[3.58, 4.45]
27	3	2.95	[2.72, 3.25]
28	2	2.08	[1.76, 2.37]
30	0	0.09	[0, 0.42]

ticed, however, the significantly larger 90 % CI of the RUL estimate at $t = 23$ hrs. The reason behind this due to the discontinuity in the updated piece-wise creep-growth rate model at $t = 24$ hrs which results in the bounds being artificially wider.

5. Conclusion

This paper has demonstrated the application of the SEMC sampler for on-line Bayesian model updating of a continuous piece-wise model in the context of the creep-growth rate model for an Advanced Reactor passive component. This is achieved through 2 investigations: 1) the identification of the corresponding model for each creep-growth rate stage; and 2) the introduction of the appropriate boundary conditions at the model transition times (i.e. at $t = 6$ hrs and $t = 24$ hrs) for the Bayesian model updating procedure.

For the first investigation, the SEMC sampler serves to

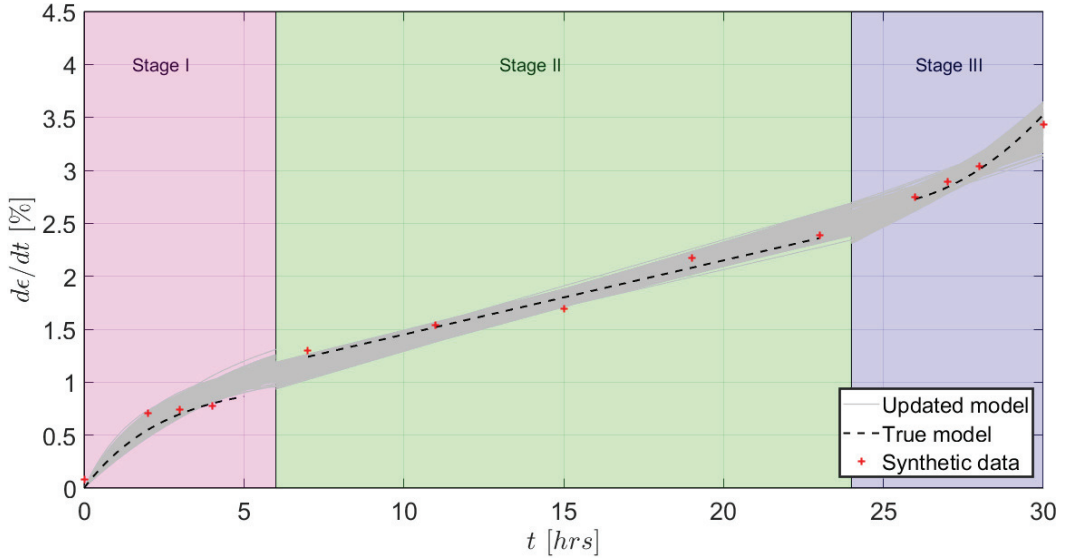


Figure 5. Graphical plots illustrating the updated piece-wise creep-growth model with reference to the synthetic data and the true models.

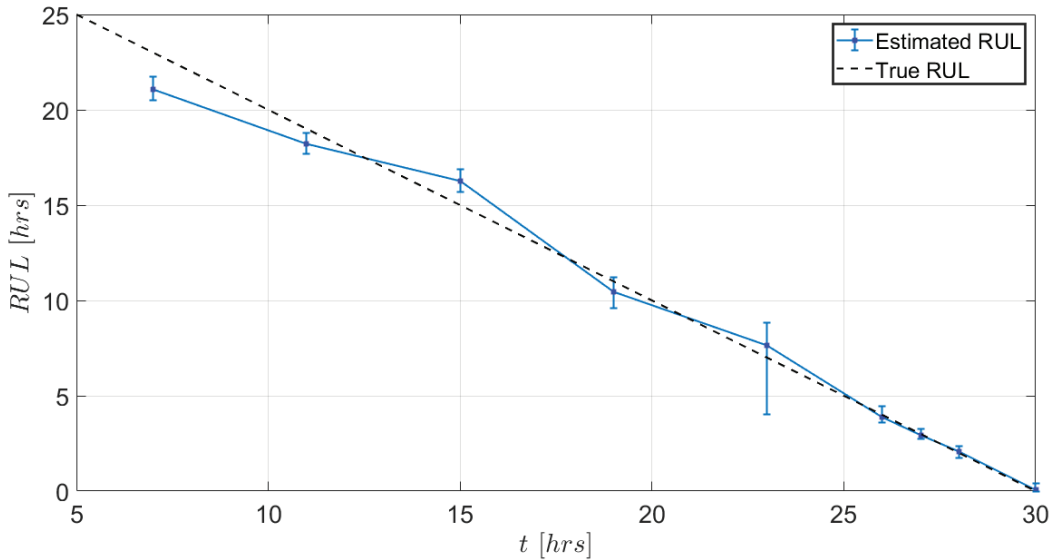


Figure 6. Graphical plots illustrating the estimated RUL at $t = \{7, 11, 15, 19, 23, 26, 27, 28, 30\}$ hrs along with its corresponding 90 % CI.

facilitate the computation of $P(M_v | \mathbf{D}^{1:s})$ to determine the most probable model for the respective creep-growth stage. Simultaneously, the investigation also serves to evaluate the capability of the SEMC sampler to identify the most probable model under such settings. The results shown that the sampler was able to identify the most probable model for

the respective creep-growth stages up to Stage II at $t = 24$ hrs. In addition, for Stage III creep-growth rate, it was found that the exponential model in Eq. (16) was the most probable model despite the true model being described by a cubic equation in Eq. (15) due to a reduced number of inferred parameters which not only simplifies the model

assumptions, but also eliminates the problem of over-fitting the data.

For the second investigation, a method of determining prior bounds for the inferred model parameters is proposed. This involves using information of the model output bounds at the model transition times to introduce constraints on the prior bounds of the selected inferred model parameters which resulted in the reduction in the degree of model discontinuity at those transition times. From there, the Remaining Useful Life analysis was performed where results show that in general, the interval estimates based on the 90 % credible interval mostly encompass the true values of the remaining lifetime of the component as shown in Figure 6. This observation, along with the resulting updated creep-growth rate model encompassing most of the synthetic data points as shown in Figure 5, provide strong verification towards the proposed methodology to perform Bayesian model updating on a piece-wise model.

As an extension to this work, the following investigations need to be done: 1) to devise methods to improve the performance of the SEMC sampler in its model identification performance; 2) to look into methods to help further reduce the discontinuities at the model transition times for piece-wise continuous models; and 3) to consider the case where data is obtained at irregular intervals compared to the study presented here.

The MATLAB codes to the SEMC sampler and the case study presented in this paper are available on GitHub: https://github.com/Adolphus8/Sequential_Ensemble_Monte_Carlo.git

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