# Improving a fiber optic interferometer for the SAFARI instrument

In Cooperation with Technobis

Finn van Rij, Department: PME, Specialisation: MSD

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#### Graduate commission:

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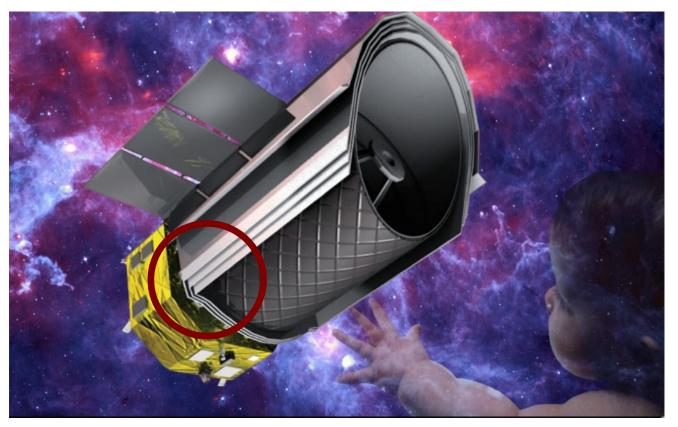
Dr. J.J. van den Dobbelsteen



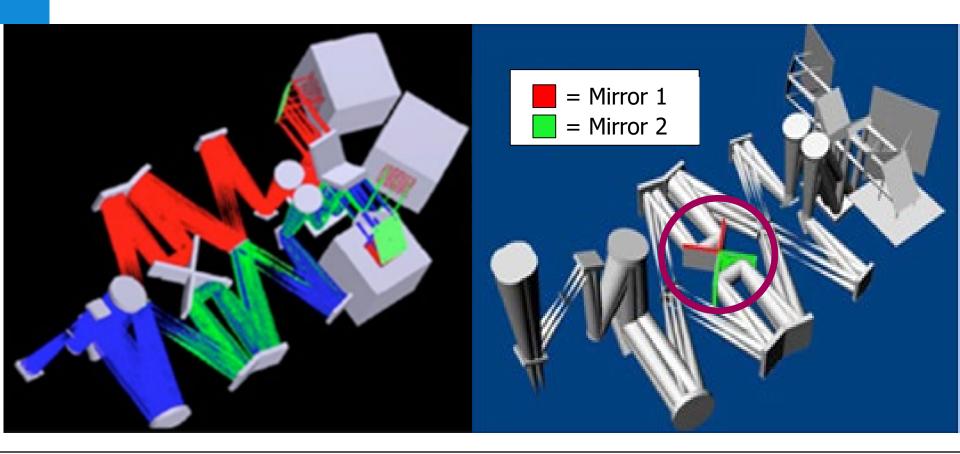


# Please turn of your mobile phones or switch them to silent mode!

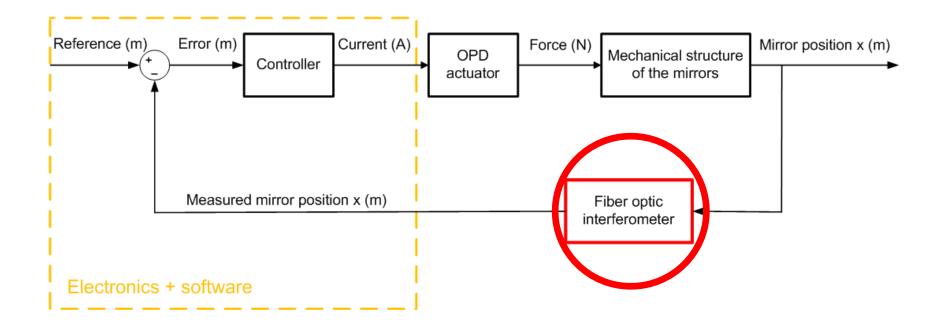
Space telescope: "SPICA"



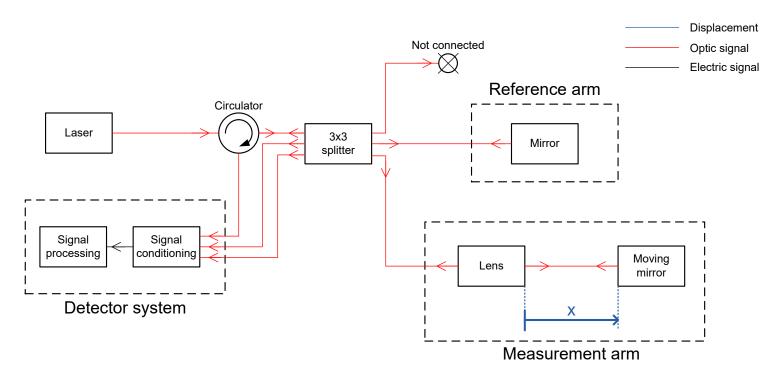
Instrument: "SAFARI"



Optical Delay Line: "ODL"



#### Fiber optic interferometer: "LUNASYS"



Resolution = 1 (nm)

### Main goal:

Operate at 4.5 (K) =  $-269^{\circ}$  C

Improve the fiber optic interferometer from

Technobis such that it fulfills the requirements for

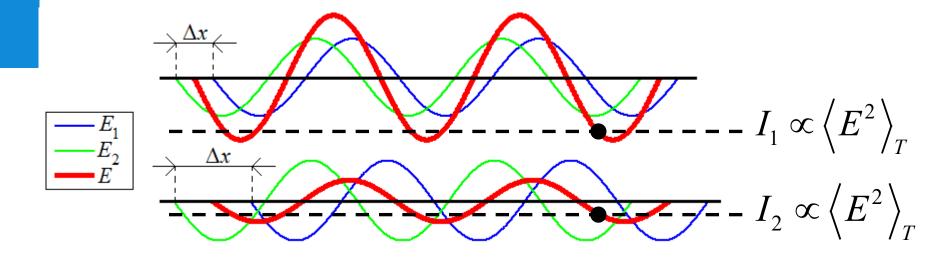
within the SAFARI instrument.

Accuracy = 10 (nm)

Heat load  $< 100 (\mu W)$ 

Stray light power < 890 (nW)

Measurement range = 35 (mm)



$$E_{1}(x,t) = E_{01} \sin(\omega t - k(x + \Delta x))$$

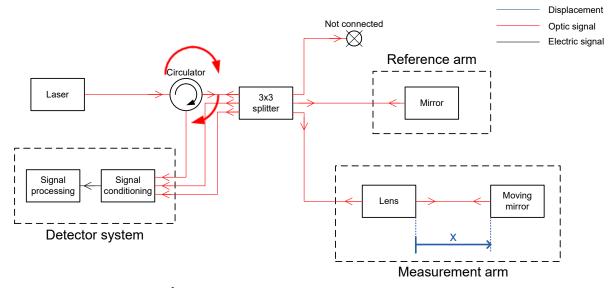
$$E_{2}(x,t) = E_{01} \sin(\omega t - kx)$$

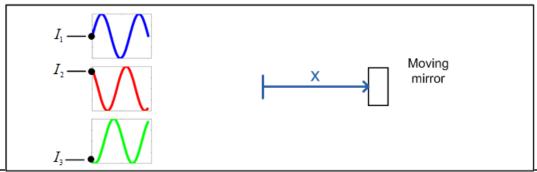
$$E = 2E_{01} \cos\left(\frac{k\Delta x}{2}\right) \sin\left[\omega t - k\left(x + \frac{\Delta x}{2}\right)\right]$$

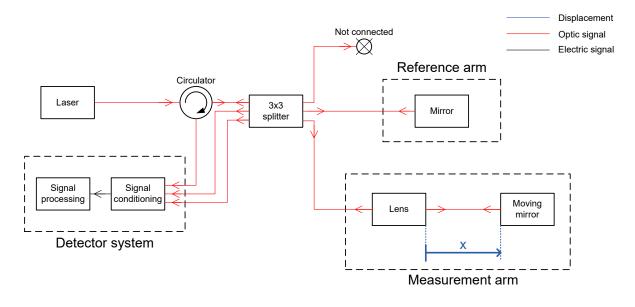
#### Irradiance:

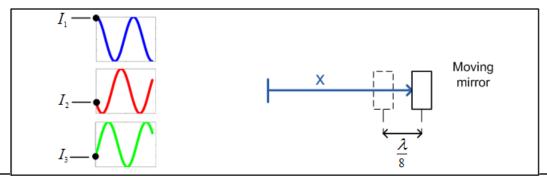
$$\Delta x = OPD$$

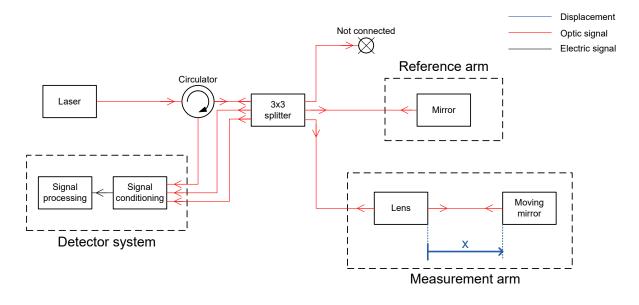
$$I = c\varepsilon_0 E_{01}^{2} \left[ 1 + \cos \left( \frac{2\pi}{\lambda} OPD \right) \right]$$

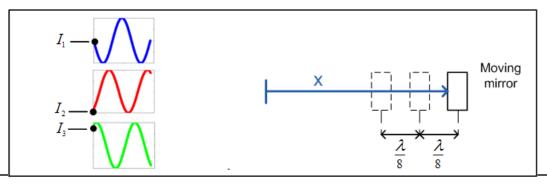












### Contents

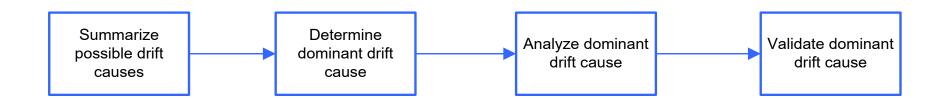
- Research questions
- Requirements and specifications
- Problem analysis
- New concept
- Conclusions
- Recommendations

- 1) Is the current setup of LUNASYS operational for the SAFARI instrument?
  - a) What are the requirements for LUNASYS for the SAFARI application?
  - b) What are the specifications of the current setup of LUNASYS?
- 2) What needs to be improved on the current setup of LUNASYS to make the system operational for the SAFARI application?
  - c) Is temperature the dominant factor causing the drift of LUNASYS?
  - d) What needs to be improved on the current setup of LUNASYS in order to reach the targeted requirements?

# Requirements and specifications

Type of specification	Required value	Specified value
Acquiroció	10 (pm) over 200(c)	1100 (nm) over 1 (hr)
Accuracy	10 (nm) over 200(s)	, , , , ,
Resolution	1 (nm)	0.19 (nm)
Stroke	34.5 (mm)	34.5 (mm)
Sample frequency	439 (Hz)	781 (Hz)
Heat load	100 (μW)	20.9 (μW)
Stray light power	0.89 (μW)	2.4E-12 (µW)
Space qualified	Yes	No
Maximal required electrical power	1.0 (W)	6.67 (W)
Functionality at cryogenic temperature of 4.5 (K)	Yes	No
Relative displacement measurement	Yes	Yes
Laser + electronics placed in room of 253 (K)	Yes	Yes
Sensor head placed near the ODL	Yes	Yes

#### Method:



#### Summarize possible drift causes

- Laser wavelength stability
- Mechanical vibrations
- Refractive index changes of air
- Phase and gain changes of the 3x3 splitter
- Temperature disturbances acting on the measurement and the reference arm

1(nm)

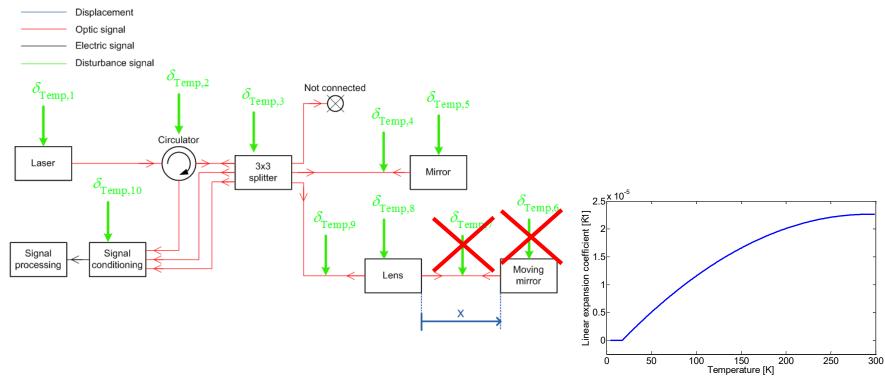
12 (nm)

94 (nm)

???

750 (nm)

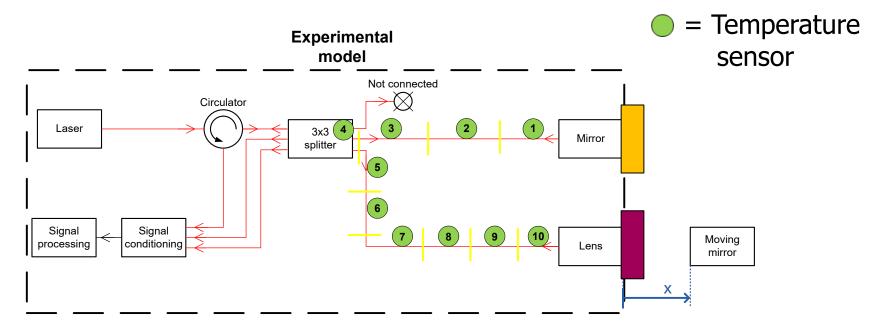
#### Determine dominant drift cause



In vacuum: n = constant

**a** 4.5 (K):  $\alpha_{A1} = 0$ 

#### Analyze dominant drift cause



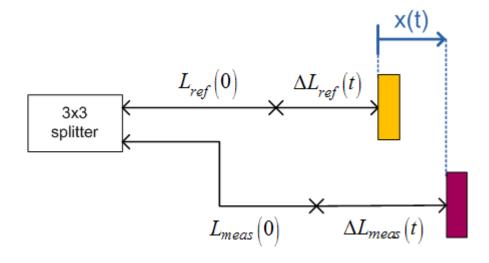
Calculate position drift with the measured temperature changes in the fibers!



$$\Delta l = l_0 \alpha \Delta T$$

# Problem analysis

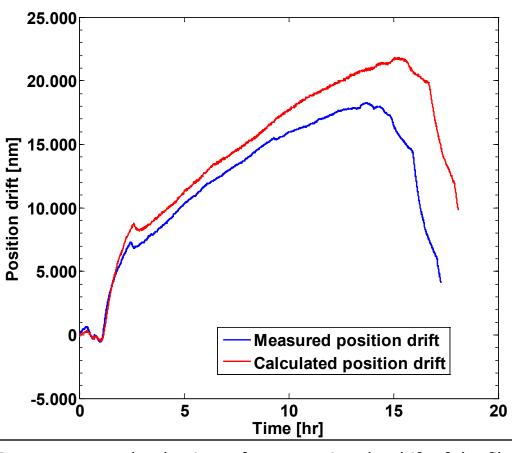
### Analyze dominant drift cause



$$x_{drift}(t) = (L_{meas}(0) + \Delta L_{meas}(t)) - (L_{ref}(0) + \Delta L_{ref}(t))$$

$$x_{drift}(t) = \sum_{m=1}^{3} L_{0m} \left( 1 + \alpha_{eff} \left( T_{m}(t) - T_{m}(0) \right) \right) - \sum_{m=5}^{10} L_{0m} \left( 1 + \alpha_{eff} \left( T_{m}(t) - T_{m}(0) \right) \right)$$

#### Validate dominant drift cause



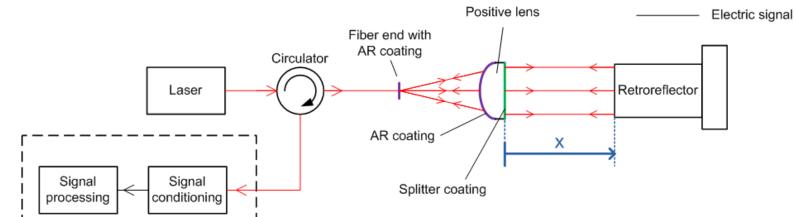
Temperature disturbances acting on the measurement and the reference arm are the dominant factor causing the drift!

c) Is temperature the dominant factor causing the drift of the fiber optic interferometer?

Displacement Optic signal

# New concept

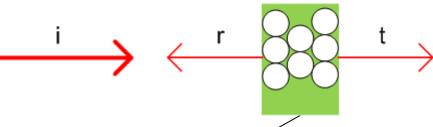
#### Tekst afmaken!!



Detector system

$$I = c\varepsilon_0 E_{01}^2 \left[ 1 + \cos\left(\frac{2\pi}{\lambda}OPD\right) \right]$$

i = r + t  $w \sim 1 (\mu m)$ 



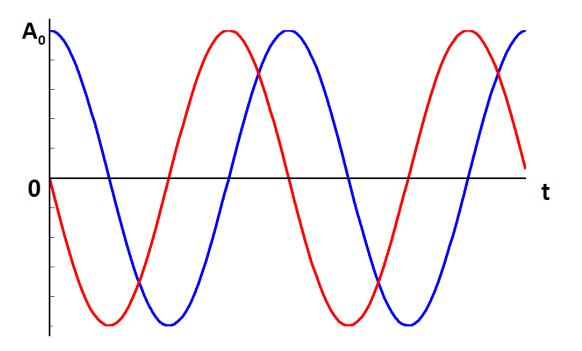
Splitter coating

# New concept

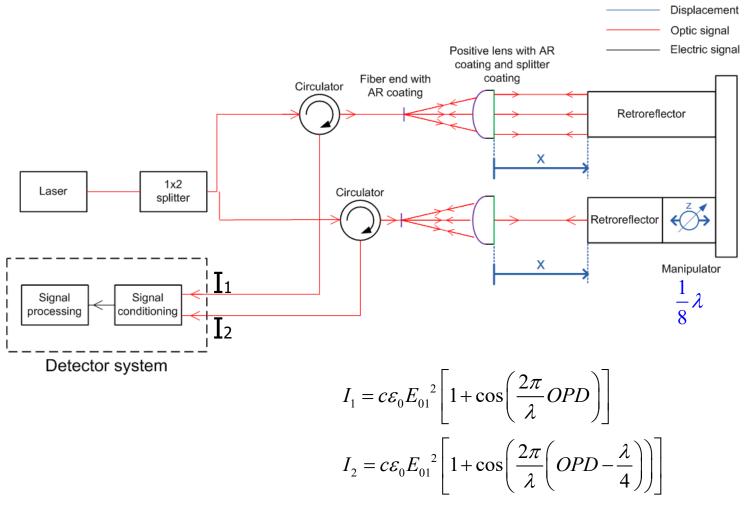
#### Quadrature phase relation:

$$S_1 = A_0 \cos(ft)$$

$$S_2 = A_0 \cos\left(ft + \frac{\pi}{2}\right)$$



# New concept



- The current setup of LUNASYS is not yet operational for the SAFARI application
- Temperature disturbances acting on the reference and the measurement arm are the dominant factor causing the drift in the current setup of LUNASYS
- The new fiber optic interferometer concept is much less sensitive to temperature disturbances (a factor of 1,000,000) and less strict demands regarding cryogenic functionality
- Stray light has been reduced to a acceptable level
- The calculated heat load meets the requirements

Verbeteren!!

### Recommendations

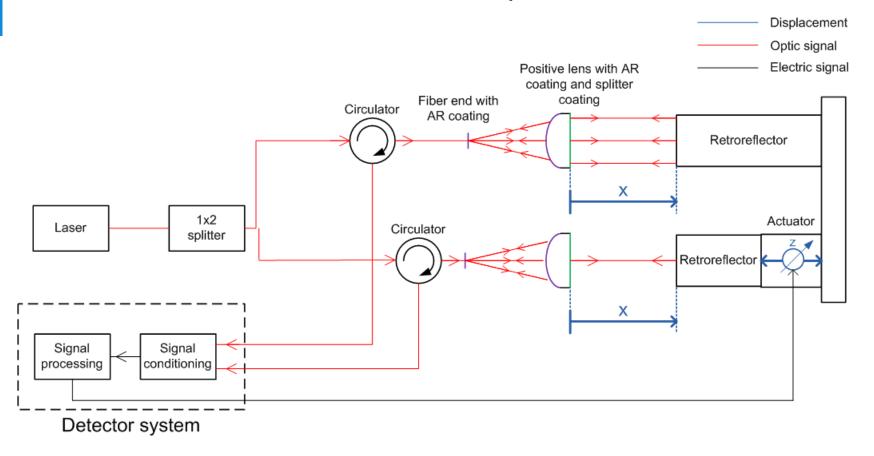
- Work out the promising new fiber optic interferometer concept
- Custom design the lens for 4.5 (K) in order to obtain functionality at cryogenic temperature
- Reduce the required electrical power for the laser, by choosing another laser or improve the current laser
- Space qualification in corporation with SRON.

Positiever maken!!

# Questions

Questions or compliments?

#### Extra interferometer concept 2



### Extra interferometer concept 3

