Incorporating AM-specific Manufacturing Constraints into Topology Optimization

Final presentation

Reuben Serphos June 13, 2014

Coaches

Professor

: Dr.ir. M. Langelaar (TU Delft)
: Dr. J. Fatemi, MSc (Dutch Space)
: Prof.dr.ir. F. van Keulen (TU Delft)





Contents

- Introduction
- Problem
- Goal
- Approach
- Results
- Conclusion
- Future work





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Additive Manufacturing

- Commonly known as 3D-printing
- Focus on Selective Laser Melting (SLM)







Additive Manufacturing

- Benefitting from AM
 - Complex geometry
- Topology optimization
 - Structural optimization method







Topology Optimization

an EADS Astrium compo



Manufacturing constraints

- Minimum feature size
- Minimum slot/hole size
- Overhang≥ 45 degrees
- Orientation





Manufacturing constraints

- Minimum feature size
- Minimum slot/hole size
- Overhang \geq **45** degrees
- Orientation





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Problem

- The design obtained from TO does not comply with manufacturing constraints
- Modification is necessary
- Maybe a reduction in optimality







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Goal

• Extend capabilities of existing program to include AM-specific manufacturing constraint: 45 degree overhang





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Approach Method and test models

- Use publicly available MATLAB code to test approach
 - Solves 2D problem
- Cantilever beams
- Tension beam





Approach Detecting overhang

- Using discrete finite element nature of optimization problem
- Element must be supported by candidate support elements
- Find maximum density of candidate support elements
- Approximate maximum using P-norm





$$\rho_{max} = \lim_{p_n \to \infty} \sqrt[p_n]{\sum_{a=1}^k \rho_a^{p_n}}$$





Approach Three methods

- 1. Multiple objective
- 2. Global constraint
- 3. Filter





Approach 1. Multiple objective

- New optimization problem
 - Minimize overhang along with compliance

$$\min_{\boldsymbol{\rho}} \qquad \mathbf{U}^{\mathbf{T}}\mathbf{K}\mathbf{U} + \Omega_{fac}\Omega_{tot} = \sum_{e=1}^{N} (x_e)^{p} \boldsymbol{u}_{e}^{T} \boldsymbol{k}_{e} \boldsymbol{u}_{e} + \Omega_{fac}\Omega_{tot}$$
subject to
$$\mathbf{K}\mathbf{U} = \mathbf{F}$$

$$\frac{V(\boldsymbol{\rho})}{V_0} = f$$

$$\mathbf{0} < \boldsymbol{\rho}_{min} \le \boldsymbol{\rho} \le \mathbf{1}$$

Where:

 $\Omega_{tot} = A$ function that defines a value for the level of overhang $\Omega_{fac} = A$ weight factor for the additional overhang term

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My approach 2. Global constraint

- New optimization problem
 - Original problem but with added constraint

$$\begin{split} \min_{\boldsymbol{\rho}} & c(\boldsymbol{\rho}) = \mathbf{U}^{\mathbf{T}} \mathbf{K} \mathbf{U} = \sum_{e=1}^{N} (\rho_e)^p \boldsymbol{u}_e^T \boldsymbol{k}_e \boldsymbol{u}_e \\ \text{subject to} & \mathbf{K} \mathbf{U} = \mathbf{F} \\ & \frac{V(\boldsymbol{\rho})}{V_0} = f \\ & \Omega_{fac} \Omega_{tot} = 0 \\ & \mathbf{0} < \boldsymbol{\rho}_{min} \leq \boldsymbol{\rho} \leq \mathbf{1} \end{split}$$





My approach Global measure for overhang

- Based on difference between element under inspection and maximum density of candidate support element
- No overhang when: $\rho_{\Delta} \leq 0$

$$\boldsymbol{\rho}_{\Delta} = \boldsymbol{\rho}_i - \boldsymbol{\rho}_{max} \qquad \qquad \boldsymbol{\Omega} = \begin{cases} 1 & \text{if } \boldsymbol{\rho}_{\Delta} > 0 \\ 0 & \text{if } \boldsymbol{\rho}_{\Delta} \le 0 \end{cases}$$







My approach Global measure for overhang

- Overhang of element
 - Approximate step using logistic function
 - Normalized by number of elements in design space

$$\Omega = \begin{cases} 1 & \text{if } \rho_{\Delta} > 0 \\ 0 & \text{if } \rho_{\Delta} \le 0 \end{cases}$$

$$\Omega_i = \frac{1}{1 + e^{-M(\rho_\Delta - \delta)}}$$

$$\Omega_i^* = \frac{1}{1 + e^{-M(\rho_\Delta - \delta)}} \frac{1}{N}$$

Dutch Space

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My approach Global measure for overhang

- Overhang coefficient
 - Sum of normalized overhang of each element

$$\Omega_i^* = \frac{1}{1 + e^{-M(\rho_\Delta - \delta)}} \frac{1}{N}$$
$$\Omega_{tot} = \sum_{i=1}^N \Omega_i^*$$
$$\Omega_{tot} = 0.011$$





x 10⁻⁴

3 25 2

My approach 3. Filter

- Original problem
 - Densities are modified through filtering scheme to comply with restriction

$$\tilde{\rho}_i = \begin{cases} \rho_i & \text{if } \rho_i \le \rho_{max} \\ \rho_{max} & \text{if } \rho_i > \rho_{max} \end{cases}$$

$$\tilde{\rho}_i = 1 - \sqrt[p_n]{(1 - \rho_i)^{p_n}} + (1 - \rho_{max})^{p_n}$$







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Results 1. Multiple objective

- Drastic design change
- Stalactite formation
- Low volume fraction
- High compliance
- Significant decrease in overhang coefficient





Results 1. Multiple objective

- Some struts re-oriented
- Stalactite formation
- Low volume fraction
- High compliance
- Overhang coefficient decreases then increases





Results 1. Multiple objective

Test case 3

- Stalactite formation
- Low volume fraction

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- High compliance
- Only slightly lower overhang coefficient



Results 2. Global constraint

- Some struts re-oriented
- Stalactite formation
- Low volume fraction
- High compliance
- Lower overhang coefficient







Results 2. Global constraint

- Some struts re-oriented
- Stalactite formation
- Low volume fraction
- High compliance
- Only slighlty lower overhang coefficient







Results 2. Global constraint

- Low volume fraction
- High compliance
- Stalactite formation







Results 3. Filter

- High cost
- Negative densities
- Low volume fraction
- High compliance
- OVERHANG NEGLIGIBLE!





















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Conclusions

- Proof of concept achieved
- At this point the filter has shown the most promising results
- Further development still necessary

	Multi. Ob.	Glob. Cons.	Filter
Design altered	Yes	Yes	Yes
Overhang	Yes	Yes	No!
Compliance	Higher	Higher	Higher
Computational cost	Acceptable	Acceptable	High





Conclusions

- Proof of concept achieved
- At this point the filter has shown the most promising results
- Further development still necessary

	Multi. Ob.	Glob. Cons.	Filter
Design altered	Yes	Yes	Yes
Overhang	Yes	Yes	No!
Compliance	Higher	Higher	Higher
Computational cost	Acceptable	Acceptable	High





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Future work

- Further investigation of parameters for multiple objective/global constraint
- Further refine the filtering scheme
- Speed-up the process for filter method
- Extend to 3D
- Include part orientation in the optimization process





Extra slides Stalactite formation

- Provides work-around
- Numerically efficient way to decrease overhang
- Not a practical solution





Extra slides Why overhang ≥ 45 degrees?

- Sagging, not enough support from powder
- Residual stress leads to curl









Extra slides Identifying a maximum

- The P-norm
- Approximates maximum

$$\rho_{max} = \lim_{p_n \to \infty} \sqrt[p_n]{\sum_{a=1}^k \rho_a^{p_n}}$$

Where:

 ρ_{max} = the maximum value of the included density values

 p_n = a parameter that influences how well the true maximum value is approximated

a = the element number for a = 1...k

k = the number of elements being evaluated

 $\rho_a = \text{the density value of element a}$





Extra slides Identifying a maximum

• The P-norm







Extra slides P-norm and density difference

$$\rho_{\Delta} = \rho_i - \sqrt[p_n]{\rho_A^{p_n} + \rho_B^{p_n} + \rho_C^{p_n}}$$





Extra slides Why a step function?

- Negative overhang for negative values of ρ_{Δ}
- Linear function means: overhang is more acceptable for lower density values







Extra slides Why a step function?





Overhang with M = 10 and $\delta = 0, 5$



Challenge the future 42

Extra slides What is the logistic function?



Where:

M = A parameter that controls the steepness of the curve (i.e. higher values result in a steeper curve)

x = The independent variable in the function



Extra slides Potential of multiple objective



Cantilever beam corner-load with parameters $\delta = 0.2$, M = 8, $p_n = 8$ and $\Omega_{fac} = 10^{\bar{3}}$



Extra slides Potential of filtering





(a) Result from filtering approach for mid loaded cantilever beam with compliance value: 474.55; Volume fraction: 0.24; Number of iterations: 98

(b) Threshold applied for elements above 0.3



(c) Filtered black-white structure with compliance: 53.88; Volume fraction: 0.5

Extracting a black-white topology from the filter result





My approach Continuous vs. discrete

Continuous

- Use gradient
- Needs interpetation step
- Competes with penalization



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Discrete

- Must indentify maximum locally
- Straightforward



Extra slides Why should the functions be continuous?

- Optimization method is gradient based
- Makes use of sensitivities to choose new values
- Discrete optimization methods not suitable for many variables





Extra slides Why is the volume fraction low?

- Overhang is zero when density of element is zero
 - Turns out this is always an option locally
- Gradients in approximations still high
 - Makes it difficult for the optimizer to find other solutions
- In some cases overhang increases before it decreases due to errors

