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# 1 An assessment of transport timescales and return coefficient in adjacent tropical estuaries

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14

## 15 Abstract –

16 Transport timescales (TTS), namely residence time and exposure time, were computed for adjacent  
17 shallow meso-tidal tropical estuarines system using the Lagrangian model D-Waq Part coupled with  
18 the hydrodynamic model Delft3D-Flow, and the Constituent-oriented Age and Residence time  
19 Theory, CART. The main results are threefold: (a) The TTS differs more between releases at high  
20 or low tide than between those at spring and neap tides. The exposure time was also calculated and  
21 found to be larger than the residence time by a few days. (b) The exposure and residence times were  
22 used to evaluate the return coefficient ( $r$ ) for different scenarios. As with residence and exposure  
23 times, the return coefficient was found to differ more between releases at high or low tide than  
24 between those at spring and neap tides. (c) For the Caravelas Estuary, where the river inflow was  
25 low ( $\sim 4 \text{ m}^3 \text{ s}^{-1}$ ), the residence time was found to be much larger than for the Peruípe Estuary, where  
26 the river discharge was greater and nearly constant during the sampling period ( $\sim 20 \text{ m}^3 \text{ s}^{-1}$ ). These  
27 results shows the importance of advection in decreasing TTS in the Peruípe Estuary compared to  
28 the Caravelas Estuary. The influence of the advection and dispersion agrees with previous simple  
29 estimates obtained using the newly modified Land Ocean Interaction Coastal Zone (LOICZ) model  
30 by Andutta et al. (2014).

31

32 Keywords: tropical estuary; residence time; exposure time; return coefficient; numerical model;  
33 hydrodynamics.

34

## 35 **1. Introduction**

36 Since the dynamics of most estuarine systems is relatively complex, studies of transport  
37 timescales (TTS) provide valuable insight into estuarine behaviour. Transport timescales represent a  
38 more holistic way of interpreting the flow in complex systems (e.g. Monsen et al. 2002), and allow  
39 us to understand how advective and dispersive mechanisms transport water.

40 Transport timescales are driven by the water currents, which in turn are influenced by sea  
41 level oscillation, bathymetry and the temperature and salinity fields. It is therefore necessary to have  
42 an accurate representation of these quantities in order to satisfactorily estimate transport timescales.

43 This article has the following tasks:

44 (1) to demonstrate, using a 3D hydrodynamic model combined with particle simulations,  
45 how release times (e.g. slack waters of high and low tides, neap and spring tides) affect the  
46 exposure time and residence time in a shallow meso-tidal tropical estuary.

47 (2) to compare TTS results from numerical modelling with estimates using the simple  
48 newly modified Land Ocean Interaction Coastal Zone (LOICZ) model by Andutta et al. (2014).

49 (3) to calculate and evaluate the return coefficient ( $r$ ) numerically and analytically using  
50 CART. This is a measure of the propensity of a water parcel to return into the domain of interest  
51 after leaving it.

52

### 53 *a. Overview of Transport Timescales*

54 Since the pioneering work by Ketchum (1951) and Bolin and Rodhe (1973), the theory of  
55 TTS has evolved (e.g. CART, [www.climate.be/cart](http://www.climate.be/cart)), and other TTS definitions have been  
56 introduced in order to fill scientific gaps. Therefore, there are many different transport timescale  
57 definitions, e.g. flushing time (Ketchum, 1951; Fischer et al., 1979; Monsen et al., 2002), residence

58 time (Bolin and Rodhe, 1973; Monsen et al., 2002; Delhez et al. 2004; Deleersnijder et al., 2006),  
 59 exposure time (Monsen et al., 2002), transit time (Holzer and Hall 2000), influence time (Delhez et  
 60 al., 2014), age (Bolin and Rodhe, 1973; Monsen et al., 2002), e-folding flushing time (Monsen et  
 61 al., 2002), turnover time (Sheldon and Alber, 2006) and renewal time (Andutta et al., 2014) – all of  
 62 which have their own interpretation.

63 Two timescales, residence time and exposure time, are used to provide an indication of  
 64 increase or decrease of non-reactive and reactive substances in estuaries, bays, lagoons, and atolls  
 65 (Andutta et al., 2014). The residence time ( $\Theta$ ) is the time needed for a particle constituent to reach  
 66 for the first time an open boundary of the domain of interest (e.g. Delhez et al., 2004). The exposure  
 67 time ( $\varphi$ ) is the time the particle will stay in the domain (e.g. Monsen et al., 2002) (Figure 2).  
 68 Therefore, at a given time and location, the exposure time is always larger than or equal to the  
 69 residence time. The larger the difference between the two timescales, the more often the particles  
 70 tend to re-enter the domain of interest after leaving it for the first time. To evaluate the exposure  
 71 time, the computational domain must be larger than the domain of interest (de Brauwere et al.,  
 72 2011, de Brye et al., 2012). Estimates of these timescales may be obtained in an Eulerian or a  
 73 Lagrangian framework. The latter often requires sufficiently large number of numerical particles in  
 74 order to provide a result that statistically approaches the real condition.

75 A dimensionless return coefficient,  $r$ , represents the propensity of particles to return into the  
 76 estuary after reaching an open boundary for the first time, as illustrated in Figure 1A (de Brauwere  
 77 et al., 2011). It is defined as the relative difference between  $\varphi$  and  $\Theta$ , i.e.

$$78 \quad r = \frac{(\Theta - \varphi)}{\Theta} . \quad (1)$$

79 Clearly, this coefficient lies in the interval [0,1].

80 The larger the  $r$  the more likely it is that particles will re-enter the estuary after crossing one  
 81 of its open boundaries for the first time. Accordingly, particles that never return into the estuary  
 82 have  $r = 0$ , while particles returning often or for long periods of time have  $r$  close to unity.

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### Preferred position for figure 1

#### 87 *b. Chosen estuary and coastal area*

88           The domain of interest is the estuarine System of the Caravelas and Peruípe Rivers (ESCP),  
89 in southern Bahia state, Brazil (see Figure 2); more details may be found in Appendix 1. It is  
90 located at the approximate latitude of 17°50'S, nearly 60 km from the National Maritime Park of  
91 Abrolhos, which is one of the largest reef structures of the Atlantic ocean, providing habitat for  
92 innumerable marine species. The ESCP has two main mouths: the Caravelas Estuary in the north  
93 (17°45'S), with two small channels named Barra Velha (~1 km wide) and Tomba's Mouth (~600 m  
94 wide), and the Peruípe Estuary in the south (17°54'S) with a funnel shape ranging in width from  
95 ~3500 m to ~700 m in the first few hundred meters. These two mouths are separated by a distance  
96 of ~25 km alongshore, and are internally connected by shallow and narrow channels around  
97 Cassurubá or Cassumba Island. Our simulations consider the domain shown in Figure 1C, for which  
98 results were computed according to the number of particles in the control domain with boundaries  
99  $\omega_1$  and  $\omega_2$ .

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### Preferred position for figure 2

## 104 **2. Methods**

105

#### 106 *a. Numerical model*

107           The ESCP comprises a number of channels varying significantly in width, from 60 m  
108 upstream to 1000 m near the mouth, and thus a high resolution mesh is necessary to resolve the  
109 many small channels in the domain. The numerical model used is the curvilinear-mesh, three-  
110 dimensional Delft3D-Flow from Deltares ([www.deltares.nl](http://www.deltares.nl)). This model is hydrostatic, and its

111 equations are solved by the method of finite differences (Delft Hydraulics, 2008). A curvilinear  
112 mesh is appropriate for the domain, although there are some disadvantages in the horizontal  
113 resolution distribution compared to unstructured meshes. Delft3D's curvilinear mesh is efficient in  
114 minimizing noise due to the steps in the horizontal plane, and allows the mesh cells to follow the  
115 channels more easily compared to non-curvilinear quadrangular meshes. The degree of non-  
116 orthogonality between mesh elements is always smaller than 0.02 thus satisfying the criteria ( $\cos \theta$   
117  $< 0.02$ ), which helps to preserve numerical stability of the simulations (Delft Hydraulics, 2008).  
118 The diagonal horizontal resolution ranges from ~20 m to ~300 m. The number of quadrangular  
119 mesh cells on the horizontal plane is 22,928. A lower resolution is applied in the coastal region  
120 ~[130-300] m, but this is increased toward the coast and the estuary ~[20-100] m (Figure 1B). The  
121 refined mesh within the estuary combined with high water speeds requires the time-step to be  
122 relatively small (around 1 second), to satisfy the Courant–Friedrichs–Lewy condition. The mesh  
123 used in the simulations of the ESCP (Figure 1B) is relatively complex, covering a small part of the  
124 Peruípe River, near the city of Nova Viçosa. This river is the main channel connecting the northern  
125 and southern mouths. The main tributaries of the Caravelas River, namely the Cupído and Jaburuna  
126 Rivers, are covered by the mesh. With 10 equally spaced sigma vertical layers, this mesh also  
127 covers a few kilometers of the adjacent coastal region.

128         The bathymetry in the estuarine channels was obtained using an Echo sounder and Global  
129 Position System. Two tide gauges were installed in Caravelas and Nova Viçosa (see locations A and  
130 C in Figure 2), meant to remove the tides from the Echo sounder data. For the Peruípe River  
131 estuary, the bathymetry was measured only in the first 6 km, near anchor station D. Thus an  
132 extrapolation was applied, considering the depth to be 4 meters for the next 14 km along the Peruípe  
133 River. The bathymetry was combined from these sources, and the triangular interpolation  
134 application in Delft3D-Flow was used. The bottom topography has depths ranging from ~0.2 m to a  
135 maximum of ~18 m (Tombo's Mouth), whilst in the coastal region do not exceed ~10 m.

136 A more detailed description of the field work carried out to obtain measurements of  
 137 thermohaline properties and other parameters is provided in Appendix 2.

138  
 139 *b. Model Boundary conditions, initial conditions and physical parameters*

140 Rainfall and river discharge measurements in the Peruípe River are shown in Figure 3B. The  
 141 river discharge data, obtained from the National Agency of Waters ANA (<http://www.ana.gov.br/>),  
 142 was measured at a gauge station upstream of the river, at station Helvécia n° 55510000 (code  
 143 1739006). This station covers a large part of the drainage basin of the river. During rainy conditions  
 144 the total drainage basin of the river may be used to estimate the total river flow to be applied at the  
 145 upstream inflow boundary of the river. The factor to account for the missing drainage basin area is  
 146  $\alpha = \frac{A_1 + A_2}{A_1} = 1.6$ , in which station Helvécia  $A_1 \sim 2,840 \text{ km}^2$ , and the downstream area not covered  
 147 by this gauge station is  $A_2 \approx 1,760 \text{ km}^2$ . The area values were obtained from the ANA  
 148 (<http://hidroweb.ana.gov.br/>).

149 Data from the gauge station were also used to estimate the river discharge range for the  
 150 Cupído and Jaburuna rivers. This was done by comparing their watershed areas with the watershed  
 151 of the Peruípe river, and assuming homogeneous rainfall and evapotranspiration distributions over  
 152 these areas (Andutta, 2011; Pereira et al., 2010). The total river flow into Caravelas Estuary was  
 153 then roughly estimated using  $Q = Q_P \beta$ , where  $\beta = 600/4600$  is the ratio between the catchment  
 154 areas of the Caravelas ( $600 \text{ km}^2$ ) and the Peruípe ( $A_1 + A_2 = 4600 \text{ km}^2$ ) rivers, and  $Q_P$  is the  
 155 average discharge for the Peruípe). This estimation was adjusted by comparing observed flow  
 156 velocities at locations A and B with model predictions.

157 The monthly estimate of fresh water inflow for the Peruípe River reveals small inflow for  
 158 the dry season, often between June and September (see Figure 3C). The combined freshwater input  
 159 from the Jaburuna and Cupído rivers estimated using the factor  $\beta$  is less than 10% of the river  
 160 discharge into the Peruípe River. Because the field work was conducted during a relatively dry wet

161 season, when rainfall was negligible prior to and during measurements obtained in January 2008  
162 (Figure 3A), it is logical not to consider the application of the factor  $\alpha$  at the Helvécia gauge  
163 station. Although this approach of river flow estimation is not required, the technique described  
164 above would be required under homogeneous rainfall conditions over the drainage basin of the  
165 Peruípe, Jaburuna and Cupído rivers.

166 The best fit between observations and model results was obtained using the mean river  
167 discharge shown in Table 1 for the Cupído and Jaburuna rivers, and the daily measurements shown  
168 in Figure 3B for the Peruípe River. In other words, the value measured at Helvécia gauge station  
169 was used in the simulation with additional tuning to extrapolate results for the other two smaller  
170 rivers.

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172 **Preferred position for figure 3**  
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176 **Preferred position for Table 1**  
177

178 The measurements from this tide gauge were compared with the simulation results during  
179 neap and spring tides using the “Skill” method described below. In addition, a qualitative  
180 comparison was carried out between the axial salinity distribution found in the simulations, and the  
181 observed distribution presented in Schettini and Miranda (2010).

182 We used the initial condition of a homogeneous thermohaline distribution for the salinity (30  
183 practical salinity unit - psu) and temperature (27 °C). The spin up simulation was made for about  
184 two months to obtain a dynamic equilibrium condition. Since the temperature has previously been  
185 found to be nearly homogeneous in this estuary (Andutta, 2011), its mean value was used for all  
186 simulations. The first flow field and salinity distribution, obtained from the equilibrium condition,



187 was used to provide a varied initial field for simulations starting at slack waters in both spring and  
 188 neap tidal conditions.

189 Computational modellers often assume that vertical eddy diffusion and viscosity coefficients  
 190 vary in time, by using turbulent closure models, e.g. algebraic, *k-L*, *k-Epsilon* schemes. On the other  
 191 hand, the horizontal eddy diffusivity,  $K_h$ , and horizontal viscosity coefficients,  $K_v$ , are often  
 192 estimated according to the mesh element size (Okubo, 1971). Therefore, modellers need to choose a  
 193 parameterisation scheme that provides the right amount of mixing in the estuary. We have  
 194 considered the parameterisation of horizontal eddy viscosity by Uittenbogaard et al. (1992), which  
 195 is available in Delft3D-Flow and reproduces well the turbulent fluxes of momentum.

196 The best fit between results and simulations was obtained assuming the horizontal eddy  
 197 diffusivity,  $K_h$ , to be in the range of  $\sim[2-30] \text{ m}^2 \text{ s}^{-1}$  with small and large values applied respectively  
 198 to small and large mesh cells. The sensitivity analysis for  $K_h$ , was conducted following Okubo  
 199 (1971). Because Okubo's formula applies for open-water, it was observed that it was not properly  
 200 simulating the true dispersion in the estuary, thus a factor  $f$  was used to increase and decrease  
 201 mixing at the sub-grid scale (See Equation 2). Varying  $f$  allowed us to achieve the best fit between  
 202 measurements and model results.

$$203 \quad K_h = f [ 2.05 \times 10^{-4} \times d^{1.15} ] \quad (2)$$

204  
 205 where  $d$  is the mesh cell size (from  $\sim 20$  to  $\sim 300$  metres), and  $f$  is the factor set to different values  
 206 but only shown for 2, 100, 150, 200, 250, 400 and 2000 in the sensitivity analyses (see Table 3).

207 The *k-Epsilon* turbulent closure scheme was used to compute values for the vertical viscosity  
 208 and diffusivity. We assumed the typical Manning roughness coefficient of  $(0.02 \text{ m}^{-1/3} \text{ s})$ , which  
 209 characterises the higher percentage of local sediment (Souza et al., 2013). This resulted in a Chézy  
 210 coefficient of  $\sim 40 \text{ m}^{-1/2}/\text{s}$ . Wind speed and directions, assumed to be **constant** over this small region,  
 211 were obtained at the Caravelas station from the Instituto Nacional de Meteorologia INMET (code  
 212 INMET 86764), at (source: <http://www.inmet.gov.br/portal/>), see Figure 4.

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215 The wind was assumed to only affect mesh cells in coastal areas. In other words, the wind  
216 stress did not affect mesh cells inside the estuarine channels. Moreover, Andutta et al. (2013)  
217 applied Hansen and Rattray's analytical equation of the velocity and salinity components, and  
218 demonstrated that the wind effect in January 2008 was negligible at station C (near Nova Viçosa  
219 estuarine mouth), which is the closest to the coast. Hansen and Rattray's analytical solution required  
220 an adjustment of no more than 0.02 Pascal for the wind stress, which correspond to wind speeds of  
221  $\sim 3 \text{ m s}^{-1}$  (Andutta et al., 2013). South-southwestward alongshore currents occur between October  
222 and January, while north-northeastward alongshore currents are observed during the fall and winter  
223 months Lessa and Cirano (2006).

224 Sea level data from TOPEX were used to force tides at the open boundary nodes. A time  
225 series of water surface elevation from May to July 2007 was recorded at Terminal Aracruz (TA in  
226 Figure 2), which is a few kilometers away from the coastal open boundary. At TA a total of  
227 16,264 tidal measurements were recorded at five minute intervals, and were processed using the  
228 tidal component extraction program PACMARÉ (Franco, 2000). These tidal measurements were  
229 used to obtain the amplitude and phase of the main tidal components, shown in Table 2.  
230 Additionally, sea-level data were recorded at stations A and C from 14<sup>th</sup> to 19<sup>th</sup> of January 2008,  
231 and these data were used to validate modelled sea-level oscillation (comparison shown in Results  
232 and Discussion section). Sea surface elevation observations from sites A and C showed the same  
233 phase, strongly suggesting that tides propagate across the shelf, because tides propagating along the  
234 coast would results in a phase shift between sea level observations at sites A and C (see Figure 2).  
235 The measurements of tidal heights of  $\sim 1 \text{ m}$  and  $\sim 3 \text{ m}$  during neap and spring tides, respectively.  
236 This ranks as meso-tidal, according to the criteria of Davies (1964) for tidal classification. From  
237 the tidal heights shown in Table 3, the tidal form-number is  $[N_f = (K_1 + O_1) / (M_2 + S_2) =$   
238  $0.19]$ , indicating a semidiurnal tidal estuary (Defant, 1960). The tidal components from Table 2  
239 represent over 97% of sea level variations for the estuarine system (Andutta, 2011).

**Preferred position for Table 2**

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241

242 *d. Model validation criteria*

243 In order to quantify the agreement between the simulated velocity and salinity profiles the  
 244 method suggested by Wilmott (1981), based on the Skill parameter was used. Accordingly, the skill  
 245 is measured as follows

$$246 \quad Skill = 1 - \frac{\sum |X_{\text{mod}} - X_{\text{obs}}|^2}{\sum \left( |X_{\text{mod}} - \bar{X}_{\text{obs}}| + |X_{\text{obs}} - \bar{X}_{\text{obs}}| \right)^2}, \quad (3)$$

247 where  $X_{\text{obs}}$  and  $X_{\text{model}}$  denote the observational and simulated properties, respectively,  $\bar{X}_{\text{obs}}$  being  
 248 the mean observational values. The Skill parameter varies from 1 to zero, with 1 indicating the best  
 249 fit, and zero indicating a complete disagreement between observation and model results.

250

251 *e. Modelling approach to calculate the Transport Timescales*

252 To quantify the residence time and exposure time 35 thousand numerical particles were  
 253 released in the estuary by coupling D-Waq PART with results from the Delft3D-FLOW (i.e. within  
 254 the subdomain denoted  $\omega$ ). Numerical particles were deployed near the bottom and top layers. The  
 255 particle concentration using conservative tracer module was normalized to value 1 within the  
 256 volume of  $\omega$ . Therefore, the number of particles decreases when particles exit  $\omega$ , and increases  
 257 when particles re-enter  $\omega$ . The minimal initial number of particles, i.e. 25 thousand, was computed  
 258 considering a minimum thickness of 2 m and a grid cell of ~20 by 10 meters.

259 A total of four simulation scenarios were made: ( $S_1$ ) particle released at high water in neap  
 260 tide, ( $S_2$ ) particle released at low water in neap tide, ( $S_3$ ) particle released at high water in spring  
 261 tide, and ( $S_4$ ) particle released at low water in spring tide.

262 In order to be consistent with CART timescales, for the computation of the residence time,  
 263 particles are discarded once they have reached an open boundary, e.g. estuarine head or an open

264 boundary in coastal waters (de Brauwere et al., 2011; de Brye et al., 2012). The arithmetic mean of  
 265 the individual residence times,  $\varphi$ , was computed as the time necessary for particles to exit the  
 266 domain ( $\omega$ ) for the first time. As for the exposure time, the particles are assumed to immediately  
 267 bounce back into the domain only at estuarine heads. This simplifying hypothesis is unlikely to  
 268 entail any major error, since a particle crossing the upstream estuarine boundary in the upstream  
 269 direction (because of diffusive processes) will most likely return into the estuary after a relatively  
 270 small time under the influence of the river flow, e.g., the St. Johans River in Florida, which  
 271 experiences backflows over significant durations (Hendrickson et al., 2003).

272 Results from residence and exposure times were used to estimate the return coefficient  
 273 distribution. The residence and exposure times may vary according to the time of release, such as  
 274 during neap/spring tides or high/low tides, and this would also affect the return coefficient. This  
 275 notwithstanding, results of exposure and residence times must be calculated for the same conditions  
 276 when computing the return coefficient, i.e.  $r = (\Theta - \varphi) / \Theta$ .

277

#### 278 *f. The modified LOICZ analytical model*

279 The modified LOICZ model of Andutta et al. (2014) applies the salinity balance proposed  
 280 by Fischer et al. (1979) into the original formulation of the LOICZ. This water renewal timescale  
 281 model has been shown to be sensitive to changes to some of its free parameters (e.g. river flow and  
 282 salinity gradient). We expect that the estimates of the timescales from our numerical results would  
 283 fit within the ranges derived from the LOICZ model. Details of its derivation are provided in  
 284 Andutta et al. (2014); however we provide the simplified relation for water renewal timescale.

285

$$286 \quad \frac{1}{T_p} = \frac{1}{T_1} + \frac{1}{T_2}, \quad (4)$$

287

288 where  $T_1 = L/U$  and  $T_2 = L^2 / K$  are the advective and dispersive timescales, respectively.  $L$ ,  $U$ ,  $K$   
 289 and  $T_p$  are respectively the selected estuarine segment length, the flow speed, the characteristic  
 290 value of the longitudinal diffusivity and the water renewal timescale. This expression may be re-

291 written in terms of the dimensionless Péclet number  $Pe = ULK^{-1}$ , the ratio  $P_e = T_2/T_1$  of the  
 292 dispersive to the advective timescale. Similarly, this number provides a comparison of contributions  
 293 from advective and dispersive processes to transport timescales, yielding

294

$$295 \quad T_P = \frac{VP_e}{Q_R(1+P_e)}. \quad (5)$$

296 Where  $V$  and  $Q_R$  denote the estuarine volume and river discharge, respectively. The contribution of  
 297 advection to the total water renewal timescale  $T_P$ ,  $\theta$  ( $0 \leq \theta \leq 1$ ), is given by

$$298 \quad \theta = T_P/T_1 = Q_R/(Q_R + Q_D), \quad (6)$$

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### g. The CART analytical model

As previously mentioned, in the framework of CART, the TTS that may be used to calculate water renewal rates can be obtained at any time and position as the solution of partial differential equations (Deleersnijder et al., 2006; de Brye et al., 2012; Andutta et al., 2014). For instance, residence time and exposure time were estimated using calibrated/validated numerical simulations for the Scheldt Estuary (de Brauwere et al. 2011, de Brye et al. 2012). As an easy acceptable method, analytical solutions may provide results that are representative of real situations (e.g. CART and LOICZ). The idealised CART timescales were used to obtain the exact analytical solution of the so called return coefficient for the ESCP. Different values of the Péclet number were considered, in order to assess the axial variation of return coefficient values. The advective timescale,  $T_1 = V/Q_R$ , and a dispersive timescale,  $T_2 = P_EV/Q_R$ , are defined taking into consideration the estuarine volume  $V$ . Andutta et al. (2014) provides a detailed description depicting an idealized channel for the time scales.

318 Consider an estuarine channel ( $-\infty < x < \infty$ ) with a constant cross-sectional area  $A$ , and a  
 319 flow under steady-state. The volumetric flow rate is denoted as  $Q_R$ . The downstream and upstream  
 320 boundaries of our idealised estuary are located at  $x = L_0$  and  $x = L_1$ , respectively. The estuarine  
 321 length is  $L = L_0 - L_1$ , and thus the volume is  $V = AL$ . The water velocity is then  
 322  $U = Q_R / A = LQ_R / V$ . For the abovementioned conditions, the residence time satisfies the adjoint  
 323 of the classical passive tracer transport equation (Delhez et al. 2004, Andutta et al. 2014), i.e.

324

$$325 \quad \frac{d}{dx} \left( AK \frac{d\varphi}{dx} + Q_R \varphi \right) = -A \quad (7)$$

326

327 where,  $x$ , denotes the particle position. The solution for the equation needs to satisfy the upstream  
 328 and downstream boundary conditions,

329

$$330 \quad \varphi(L_1) = 0 = \varphi(L_0). \quad (8)$$

331

332 It represents the average time required by particles initially located in the interval  $[x, x + \delta x]$   
 333 (with  $\delta x \rightarrow 0$ ) to reach one of the open boundaries. The solution is then easily derived:

334

$$335 \quad \varphi(x) = \frac{V}{Q_R} \left( 1 - \frac{\xi}{L} \right) + \frac{V}{Q_R} \left( \frac{e^{-Pe} - e^{-Pe \xi/L}}{1 - e^{-Pe}} \right) \quad (9)$$

336 where  $\xi = x - L_1$ .

337 The exposure time was also derived (Andutta et al., 2014), and is defined in the domain of interest  
 338 and its surrounding environment.

$$339 \quad -\infty \leq x \leq L_1 \quad : \quad \Theta(x) = \frac{V}{Q_R} \quad (10a)$$

$$340 \quad L_1 \leq x \leq L_0 \quad : \quad \Theta(x) = \frac{V}{Q_R} \left( 1 - \frac{\xi}{L} \right) + \frac{V}{Q_R} \left( \frac{1 - e^{-Pe \xi/L}}{Pe} \right) \quad (10b)$$

$$341 \quad L_0 \leq x < \infty \quad : \quad \Theta(x) = \frac{V}{Q_R} \left( \frac{e^{-Pe} - 1}{Pe} e^{-Pe \xi/L} \right) \quad (10c)$$

342

343 From Equations (9) and (10), which are valid within the upstream and downstream open  
 344 boundaries, the return coefficient is:

345

$$346 \quad r = \frac{\Theta(x) - \varphi(x)}{\Theta(x)} = \frac{\left( \frac{1 - e^{-Pe \zeta/L}}{Pe} \right) - \left( \frac{e^{-Pe} - e^{-Pe \zeta/L}}{1 - e^{-Pe}} \right)}{\left( 1 - \frac{\zeta}{L} \right) + \left( \frac{1 - e^{-Pe \zeta/L}}{Pe} \right)} \quad (11)$$

347 Note that  $r$  is bounded by  $[0,1]$ , as mentioned before.

348 In principle, the residence time and the exposure time can be obtained by solving classical  
 349 passive transport equations. However, to do so, time- and position-dependent concentrations must  
 350 first be **obtained and**, then, time and space integral must be performed to derive the relevant  
 351 timescales. This is not straightforward, even for highly idealised flows. This is why it is preferable  
 352 to have recourse to the adjoint method established by Delhez et al. (2004), which requires the  
 353 solution of simpler differential problems to be determined: in the present case, only ordinary  
 354 differential equations are to be dealt with rather than partial differential ones. The disadvantage of  
 355 this approach is that the theoretical underpinning of an adjoint model sometimes appears elusive,  
 356 which is probably the reason why Errico (1997) wrote a general, enlightening paper on this matter,  
 357 explaining the nature and purpose of adjoint models.

358

### 359 **3. Results and Discussion**

360

#### 361 *a. Model calibration of salinity, velocity and tides*

362 We carried out a sensitivity analysis considering different values for the horizontal diffusion  
 363 coefficient  $k_h$  using Equation 2. These adjustments of factor  $f$  for the horizontal diffusivity based on  
 364 the grid size allowed us to obtain a proper representation of the salinity field and its time variability.

365

**Preferred position for Table 3**

366 The mean Skill parameters for the simulation are shown in Table 3 for different values of  
367 factor  $f$ , which was described with Equation 2. The comparison of sea-level oscillation over a tidal  
368 modulation period, from the 14<sup>th</sup> to the 29<sup>th</sup> of January 2008, showed good skill values for locations  
369 A (Figure 5) and C (not shown), and the Skill parameter for tides was calculated to be over 0.97 for  
370 both locations, i.e. A and C. The comparison of tides, velocity, and salinity showed good skill  
371 values during spring tides (not shown), and reasonable values during neap tides (Figure 6).

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**Preferred position for figure 5**  
**Preferred position for figure 6**

376 The Skill parameter for the water column height variation in time was calculated to be over  
377 0.98 for all the sites under neap and spring tides (Table 4), and the tidal ranges were ~1.0 m and  
378 ~2.5 m for neap and spring tides, respectively. Observations have shown that the tidal phase  
379 between sites A (Caravelas mouth) and C (Peruípe mouth) is almost the same. The similarity of  
380 their phases indicates that tides propagate mainly perpendicular to the coast line in this region, a  
381 result which is in close agreement with observations previously reported by Lessa and  
382 Cyrano (2006).

383 For the modeled velocity validation, good results (Skill from 0.77 to 0.93) were obtained in  
384 spring tides in the estuaries of Caravelas (sites A and B) and Nova Viçosa (sites C and D). For neap  
385 tides due to small differences on tidal asymmetry, the Skill was lower, at ~ 0.6.

386 The model agreed well with observations of maximum ebb and flood currents at site A. The  
387 model also properly simulated the velocity profiles for sites B, C, and D. Therefore, the description  
388 of maximum ebb and flood currents from in-situ data also apply to the model simulations. At site B  
389 there were maximum speeds of ~0.5 m s<sup>-1</sup> and 1.0 m s<sup>-1</sup> (ebb events), and ~-0.3 m s<sup>-1</sup> and ~-0.6 m s<sup>-1</sup>  
390 (flood events), during neap and spring tides, respectively. For site A the vertical shear of the  
391 velocity was negligible in flood and ebb conditions, while for site B there was a small vertical shear  
392 of the horizontal velocity during ebb events. During flood events, the water velocity was  
393 homogenous over the water column. In addition, a residual velocity of ~0.05 m s<sup>-1</sup> was calculated at



394 site B, indicating a residual circulation from Nova Viçosa towards the Caravelas River. Site A had a  
395 residual current of  $\sim 0.06 \text{ m s}^{-1}$ , indicating a small discharge from the Cupído and Jaburuna Rivers.  
396 At sites C and D, located in the Peruípe River, the downstream velocities showed more intensity  
397 than observed in the Caravelas Channel. For site C the downstream velocities varied from  $\sim -0.9 \text{ m}$   
398  $\text{s}^{-1}$  to  $\sim -1.5 \text{ m s}^{-1}$ , for neap and spring tides, respectively. During flood events, the velocities were  $\sim$   
399  $0.3 \text{ m s}^{-1}$  and  $\sim -0.7 \text{ m s}^{-1}$ , for neap and spring tides, respectively. At site D the maximum  
400 downstream velocities were only  $\sim 0.7 \text{ m s}^{-1}$  and  $\sim 1.0 \text{ m s}^{-1}$  at neap and spring tides, and upstream  
401 velocities were  $\sim -0.3 \text{ m s}^{-1}$  and  $\sim -0.4 \text{ m s}^{-1}$ . The residual velocities at sites C and D, which have  
402 values of  $\sim 0.10 \text{ m s}^{-1}$  to  $\sim 0.15 \text{ m s}^{-1}$ , indicate a higher advective contribution from the Peruípe River  
403 compared with the Caravelas estuary.

404 In addition to the tides and the velocity field, the model simulated the temporal variation of  
405 the salinity well for all sites (A, B, C, and D). During spring tides the calculated Skill values were  
406 over 0.83, while for neap tides they were over 0.73 (Table 4). At the Caravelas estuarine channel,  
407  $\sim 3 \text{ km}$  near the mouth (site A), during low tide, salinity was observed in intervals of  $\sim 34.5 \text{ psu}$  to  
408  $\sim 35.0 \text{ psu}$  and  $\sim 34.0 \text{ psu}$  to  $\sim 34.5 \text{ psu}$  for the observational and theoretical results,  
409 respectively. About  $6 \text{ km}$  away from the mouth we obtained a good agreement for the salinity, with  
410  $\sim 32.0 \text{ psu}$  and  $\sim 32.5 \text{ psu}$  for observation and simulation, respectively. In the vicinity of the  
411 interconnection with Cupído and Jaburuna Rivers (site B), which is about  $12 \text{ km}$  upstream from the  
412 mouth, the salinity decreased to  $\sim 30.0 \text{ psu}$  and  $\sim 28.5 \text{ psu}$  for the observational and calculated  
413 results, respectively. At high tide, near the mouth (site A) and at a distance of  $6 \text{ km}$  from the mouth,  
414 the salinity was  $\sim 36.5 \text{ psu}$  and  $\sim 36.0 \text{ psu}$ , respectively, for both simulation and field measurements.  
415 In the upper reaches of the estuary, near the junction of the rivers, Cupído and Jaburuna ( $\sim 12 \text{ km}$   
416 from the mouth), a close agreement between simulated and observed salinity values ( $\sim 33.0 \text{ psu}$ ) was  
417 obtained at high tide. Along the Peruípe River estuary at neap tides, the surface salinities vary in the  
418 range of  $20.0 \text{ psu}$  to  $34.0 \text{ psu}$  at the surface, and  $32.5 \text{ psu}$  to  $36.0 \text{ psu}$  near the bottom. The region of  
419 Nova Viçosa has more vertical stratification of the salinity than at sites A and B in the Caravelas

420 River. This is due to Peruípe River's larger freshwater discharge. The observed value of ~36.0 psu  
421 near the bottom is characteristic of the Tropical Water Mass, which was already reported to enter  
422 this estuarine system (Schettini et al., 2010). During spring tides the vertical mixing causes the  
423 erosion of the halocline, and thus decreases vertical stratification. This results in a smaller vertical  
424 variation of 31.0 psu to 36.0 psu from the surface to the bottom.

425 **Preferred position for Table 4**

426 A comparison of the axial distribution of salinity was made for the Caravelas River (Figure  
427 7A,B). For the first 12 km along the estuarine channel, results from simulations were compared to  
428 observations made by Schettini and Miranda (2010). The measurements were obtained on the 10<sup>th</sup>  
429 of April, 2001 during spring tides. Although the field data are likely to be from different conditions  
430 of river flow, the simulation showed a good correlation of the axial distribution of the salinity in the  
431 Caravelas River (See Figures 7C and 7D), with values of  $R^2 \sim 0.97$  and  $R^2 \sim 0.99$  for low and high  
432 tides respectively. This indicates that the model has well represented the mixing processes in the  
433 Caravelas Estuary. During low tide (Figure 7A,C), a good agreement is found near the mouth, with  
434 salinity values of ~35.2 psu and ~ 34.5 psu, for the model results and observations, respectively. At  
435 nearly 6 km upstream, there is still a good agreement ( $R^2 \sim 0.99$ ) with the salinity values of ~33  
436 psu (model), and ~32 psu (observation). Further upstream and near the inter-connection between the  
437 Cupído and Jaburuna rivers (i.e. ~ 12 km upstream), the agreement is slightly poorer with the  
438 salinity values of ~30 psu (model) and ~29 psu (observation). At high tide (Figure 7B, D), the  
439 model predicted the longitudinal salinity variations well along the Caravelas Channel. The salinity  
440 values near the mouth were ~36.4 psu (model and observation), and reduced to ~36 psu 6 km  
441 further upstream. Moreover, during high tides the agreement was also good near the channel  
442 between the Cupído and Jaburuna rivers with salinity of ~33 psu.

443 **Preferred position for figure 7**

444  
445 *b. Results of the residence time, the exposure time and the return coefficient*

446

447 The transport timescales, namely residence time ( $\varphi$ ), exposure time ( $\Theta$ ), and the return  
448 coefficient ( $r$ ), were estimated for the Caravelas and Peruípe estuarine channels with simulation  
449 under different scenarios, i.e. S<sub>1</sub> to S<sub>4</sub> (Figures 8, and 9).

450 For scenarios S<sub>1</sub> and S<sub>3</sub> (Figure 8), the residence time along the Caravelas Channel, from the  
451 mouth to 12 km upstream, was found to vary from 0 to ~15.0 days. The inflow boundaries of the  
452 Cupído and Jaburuna rivers were found to have residence times of ~27 and ~22 days, respectively.  
453 For the Peruípe Channel the residence times ranged from 0 to ~7.4 days, from the mouth to 5 km  
454 upstream, with a maximum value of ~18 days at the inflow boundary of the Peruípe Estuary.

455 The residence time estimated at ~6 km further upstream in the Caravelas Estuary ( $\varphi = 11.7$   
456 days) is almost three times larger than the residence time calculated for the same distance along the  
457 Peruípe Estuary ( $\varphi < 4.4$  days). The difference between results in the Caravelas and the Peruípe  
458 estuaries is due to the larger velocity contribution in the Peruípe Estuary.

459 Comparing scenarios S<sub>1</sub> and S<sub>3</sub>, the residence time was found to be slightly lower for S<sub>3</sub> (c.a.  
460 a few hours) and this difference is due to increased diffusive contribution during stronger spring  
461 tidal conditions. In contrast to scenarios S<sub>1</sub> and S<sub>3</sub>, the simulations considering scenarios S<sub>2</sub> and S<sub>4</sub>  
462 yielded an increased residence time. This increase was maximum near the estuarine mouths (~5  
463 days), and observed to reduce in the upstream direction (few hours). The increase in residence time  
464 for particles released in slack water of low tide is caused by tidal excursion from reversing currents  
465 (i.e. flood currents). These results reflect and add value to recent simulations by de Brye et al.  
466 (2012) for the Scheldt Estuary (in Belgium and the Netherlands), whose results showed larger  
467 residence time values for particles released at slack water of low tides than for high tides (difference  
468 of a few days).

469 The virtual Lagrangian particles showed that a negligible number of particles crossed the  
470 connecting channel between the Caravelas ( $\omega_1$ ) and Peruípe Estuaries ( $\omega_2$ ), which indicates that this  
471 relatively narrow and shallow interconnection channel allows little exchange of water properties  
472 between these estuaries. Moreover, the residence time is observed to be larger within the

473 enlargement of the interconnecting channel between these two estuaries. Schettini and Miranda  
 474 (2010) and Schettini et al. (2013) have addressed the importance of the interconnection channel  
 475 between Caravelas and Peruípe, and found that sediment deposited near the Caravelas mouth was  
 476 both inner shelf **local resuspension** and upstream transport, or sourced from the Peruípe River via  
 477 the interconnection channel.

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### Preferred position for figure 8

481 Exposure time results showed that particles re-entered the system for up to two days (Figure  
 482 9). Note that the difference between the exposure time and the residence time ( $\Theta - \varphi$ ) showed little  
 483 spatial variation for scenarios  $S_1$  and  $S_3$ .

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### Preferred position for figure 9

486 The spatially averaged difference between exposure and residence times ( $\Theta - \varphi$ ) are  
 487 calculated in days, and its respective RMSE to be  $\sim 1.98 \pm 0.06$  for  $S_1$ ,  $\sim 1.87 \pm 0.12$  for  $S_2$ ,  $\sim 1.92$   
 488  $\pm 0.07$  for  $S_3$ ,  $\sim 2.19 \pm 0.08$  for  $S_4$ . These results strongly suggest that ( $\Theta - \varphi \sim \text{const.}$ ) for the  
 489 ESCP under the four different scenarios considered. The results also suggest that  $t_3 - t_2$  varies little  
 490 away from the open boundaries, so particles deployed at different times and locations in the estuary  
 491 re-enter for similar lengths of time, assuming the circulation in coastal waters does not considerably  
 492 change over time due to additional forcings, e.g. sudden alongshore wind driven currents.

493 Equation (5) was used to estimate the range of water renewal timescales for the Caravelas  
 494 and Peruípe estuaries using the parameters given in the appendices of Andutta et al. (2014), see  
 495 Figure 10. The straight line labelled  $\theta$  (lowercase) indicate the relative advective contribution to  
 496 water renewal, where  $0 \leq \theta \leq 1$ . The line at  $\theta = 0.5$  separates the areas where transport is  
 497 dominated by advection (diagram upper zone,  $\theta > 0.5$ ) and dispersion (diagram lower zone,  $\theta <$   
 498  $0.5$ ).

499 The Caravelas and Peruípe estuaries have mean depths of  $\sim 6.5$  and  $\sim 7.5$  meters,  
 500 respectively, and the maximum and minimum tidal ranges in these estuaries are  $\sim 2.5$  and  $\sim 0.5$

501 meters. According to Andutta et al. (2013), these tidal ranges combined with the relatively the small  
502 depths result in a high rate of change of the potential energy ( $\sim 6.1 \text{ J m}^{-3} \text{ s}^{-1}$ ), which contributes  
503 towards large dispersion. It is valid to compare these results to the Sheldt Estuary, where tidal  
504 oscillation is typically 4-5 meters along the first  $\sim 100$  km, and where the mean water depth is  $\sim 10$   
505 meters. Tidal range in the Sheldt can reach  $\sim 7$  m, which is about 45% of the mean water depth  
506 value for the first  $\sim 25$  km near the estuarine mouth (Soertaert and Herman, 1995; de Brye et al.  
507 2012), and this system is classified as well-mixed due to dispersion prevailing over advection. The  
508 numerical results for the ESCP fit within the timescale ranges estimated using the simple LOICZ  
509 method.

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### Preferred position for figure 10

513 The return coefficient cannot be calculated using the modified LOICZ model. However, it  
514 was computed numerically and compared to the non-dimensional solution obtained using CART.  
515 The return coefficient converges to one at the estuarine mouths and near estuarine heads (Figure 11,  
516 for all scenarios  $S_1$  to  $S_4$  and Figure 12B). However, this is only a direct consequence of the  
517 definition of the residence time, which converges to zero at the entrance, and thus the return  
518 coefficient will always increase towards unity.  $r$  was observed to be smaller upstream, because the  
519 ratio  $(\Theta - \varphi)/\Theta$  is likely to decrease. It can be noticed that the axial variation of the return  
520 coefficient is similar for both CART solution and numerical approach (Figures 11 and 12C). The  
521 return coefficient calculated from CART and from numerical simulations is observed to increase  
522 towards the upstream boundary. This increase towards the estuarine head is due to the boundary  
523 condition assumed in the analytical and numerical solutions, where particles do not re-enter the  
524 domain after crossing the estuarine head, although in a real estuary water particles would re-enter  
525 through the estuarine head due to river flow conditions.

526 Figure 12A shows results of the residence and exposure time and return coefficient for a  
527 range of values of the Péclet number. High values of the Péclet number yield a boundary layer in  
528 the vicinity of the upstream location.

529 The greater the relative importance of advection, the less likely it is that dispersion will  
530 cause a water particle to hit the upstream boundary of the domain ( $x = L_0$ ). In accordance with their  
531 definitions, the exposure time is larger than the residence time for any location in the domain ( $L_1 \leq$   
532  $\xi/L \leq L_0$ ). These idealised results of the return coefficient were used to access results obtained  
533 from our numerical simulations.

534

535  
536 **Preferred position for figure 11**  
537

538 **Preferred position for figure 12**  
539

540 In the illustration shown in Figure 11A, the ratio is simply the difference between times  $t_3$   
541 and  $t_2$ . Evidently this is a simple case where the particle is assumed to have re-entered the domain  
542 only once.

543 Particles are expected to first cross the estuarine mouth during ebb currents, which would be  
544 alternating with flood currents and dispersive processes. Therefore, we could presume that  
545 Lagrangian particles would have a time window of  $\sim 6.5$  hours to cross the entrance (for semi-  
546 diurnal tidal estuaries), and this time window would then close for  $\sim 6.5$  hours (the period of flood  
547 currents).

548 Our simulations were for relatively calm weather conditions, which were predominant over  
549 the region, c.a. wind speeds in the range  $1-4 \text{ m s}^{-1}$  (wind from NE). Andutta et al. (2013) showed  
550 that wind conditions did not affect the water circulation in this estuarine system in January 2008.  
551 However, for stronger wind conditions the results would not be the same. Evidently alongshore  
552 wind-driven currents would reduce the difference between the exposure time and the residence  
553 time, and the return coefficient would thus decrease towards zero. This is because alongshore  
554 currents inhibit the propensity of particles to re-enter the estuarine system. The alongshore shelf  
555 currents are observed to be driven by the N-S migration of the South Atlantic High between  
556 summer and winter. South-southwestward alongshore currents occur between October and January,  
557 while stronger north-northeastward alongshore currents are observed during the fall and winter  
558 months (Lessa and Cirano, 2006).

559

560 **4. Conclusions**

561

562 *Overall goal*

563 This study provides the first estimates of the residence time, exposure time and the return  
564 coefficient for the Caravelas and Peruípe estuaries and might be a reference for future studies  
565 related to **the control of pollutants and sediment transport**. These transport timescales were  
566 estimated using a Lagrangian model only as a tool, and this model has been properly calibrated and  
567 validated using field data.

568 *Specific conclusions*

569 • *Achievements regarding goals (1 and 2)*

570 The residence time for particles released far upstream in the Caravelas Estuary was found to  
571 be nearly 3 weeks for particles, regardless of whether they are released at high or low tide, and is  
572 driven by tidal dispersion combined with the discharge from the Cupído and Jaburuna Rivers  
573 (typical range of 4 to 9 m<sup>3</sup> s<sup>-1</sup>). These results are consistent with previous estimates derived from  
574 simple analytical solutions (Andutta et al., 2014), see Figure 10. For the Peruípe Estuary, our  
575 estimates of the residence time were for less than one week, due to the tidal dispersion combined  
576 with the larger river input from the Peruípe River (typical range of 20 to 70 m<sup>3</sup> s<sup>-1</sup>).

577 The transport timescales (exposure and residence times) were found to be quite similar for  
578 particles released in high tide under spring and neap tidal conditions, thus confirming previous  
579 estimations made for the Scheldt Estuary (de Brye et al., 2012). In contrast, the transport timescales  
580 were shown to be more sensitive to tidal-phase release time (i.e. high or low tides) in this estuarine  
581 system. Similar observations were made for the Scheldt Estuary (de Brauwere et al., 2011), in  
582 which there was a difference of days for results of residence time using particles released at high  
583 and low tides. This suggests that tidal-phase release time for a meso-tidal shallow estuary forced by  
584 low-moderate river discharge conditions is important for quantification of TTS, especially for water  
585 particles near mouths where larger tidal excursions are expected compared to locations further  
586 upstream, and since their initial movement would be upstream/downstream if released during  
587 low/high tide, respectively.



588 The Lagrangian simulation also showed that the narrow and shallow inter-connecting  
589 channel between the Peruípe and Caravelas estuaries allows **little** water exchange between the two  
590 estuaries, and only a few particles were capable of crossing the inter-connection passage with  
591 prevailing direction from the Peruípe to the Caravelas, in agreement with Schettini et al. (2013).  
592 Therefore, both exposure time and residence time were large at that location, and the exchange of  
593 water properties is likely to happen through alongshore currents at inner coastal areas.

594 • *Achievements regarding goal (3)*

595 Similarly to the exposure and residence times, the return coefficient was shown to be more  
596 sensitive to tidal phase (high and low tide), than to neap and spring tidal conditions. It may be  
597 summarized as follows: (1) the return coefficient is larger for particles released at high tide than at  
598 low tide; (2) the return coefficient is larger for particles released during spring tides than during  
599 neap tides.

600 For these two estuaries the exposure time was higher than the residence time in all  
601 simulations, thus showing that water may return to the system after having first crossed the mouth.  
602 The propensity of this water to return to the estuary was quantified using the return coefficient,  
603 which depends on the difference between the exposure and residence times, and thus also on the  
604 residual circulation due to river discharge, as well as the circulation in coastal waters. For instance,  
605 swift longshore currents decrease the difference between the exposure and residence times, and  
606 therefore reduce the return coefficient. The wind conditions over our measurement period were  
607 characteristic of calm weather, c.a. a few  $\text{m s}^{-1}$  (see Figure 4), and different scenarios may produce  
608 different results for the transport timescales, for **instance** under stronger north-northeastward  
609 alongshore currents which are often observed during the fall and winter months Lessa and Cirano  
610 (2006). Due to its definition, the return coefficient is predicted to be larger at the estuarine mouths,  
611 because the residence time tends to zero (see Equation 1). Our results have additionally shown that  
612 for our scenarios the difference between exposure and residence times ( $\Theta - \varphi$ ) is nearly constant  
613 within our domain. This can also be observed from our analytical solution (Figure 12C).

614

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616

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625

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1 **An assessment of transport timescales and return coefficient in adjacent tropical estuaries**

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14

15 **Abstract –**

16 Transport timescales (TTS), namely residence time and exposure time, were computed for adjacent  
17 shallow meso-tidal tropical estuarines system using the Lagrangian model D-Waq Part coupled with  
18 the hydrodynamic model Delft3D-Flow, and the Constituent-oriented Age and Residence time  
19 Theory, CART. The main results are threefold: **(a)** The TTS differs more between releases at high  
20 or low tide than between those at spring and neap tides. The exposure time was also calculated and  
21 found to be larger than the residence time by a few days. **(b)** The exposure and residence times were  
22 used to evaluate the return coefficient ( $r$ ) for different scenarios. As with residence and exposure  
23 times, the return coefficient was found to differ more between releases at high or low tide than  
24 between those at spring and neap tides. **(c)** For the Caravelas Estuary, where the river inflow was  
25 low ( $\sim 4 \text{ m}^3 \text{ s}^{-1}$ ), the residence time was found to be much larger than for the Peruípe Estuary, where  
26 the river discharge was greater and nearly constant during the sampling period ( $\sim 20 \text{ m}^3 \text{ s}^{-1}$ ). These  
27 results shows the importance of advection in decreasing TTS in the Peruípe Estuary compared to  
28 the Caravelas Estuary. The influence of the advection and dispersion agrees with previous simple  
29 estimates obtained using the newly modified Land Ocean Interaction Coastal Zone (LOICZ) model  
30 by Andutta et al. (2014).

31

32 Keywords: tropical estuary; residence time; exposure time; return coefficient; numerical model;  
33 hydrodynamics.

34

## 35 **1. Introduction**

36 Since the dynamics of most estuarine systems is relatively complex, studies of transport  
37 timescales (TTS) provide valuable insight into estuarine behaviour. Transport timescales represent a  
38 more holistic way of interpreting the flow in complex systems (e.g. Monsen et al. 2002), and allow  
39 us to understand how advective and dispersive mechanisms transport water.

40 Transport timescales are driven by the water currents, which in turn are influenced by sea  
41 level oscillation, bathymetry and the temperature and salinity fields. It is therefore necessary to have  
42 an accurate representation of these quantities in order to satisfactorily estimate transport timescales.

43 This article has the following tasks:

44 (1) to demonstrate, using a 3D hydrodynamic model combined with particle simulations,  
45 how release times (e.g. slack waters of high and low tides, neap and spring tides) affect the  
46 exposure time and residence time in a shallow meso-tidal tropical estuary.

47 (2) to compare TTS results from numerical modelling with estimates using the simple  
48 newly modified Land Ocean Interaction Coastal Zone (LOICZ) model by Andutta et al. (2014).

49 (3) to calculate and evaluate the return coefficient ( $r$ ) numerically and analytically using  
50 CART. This is a measure of the propensity of a water parcel to return into the domain of interest  
51 after leaving it.

52

### 53 *a. Overview of Transport Timescales*

54 Since the pioneering work by Ketchum (1951) and Bolin and Rodhe (1973), the theory of  
55 TTS has evolved (e.g. CART, [www.climate.be/cart](http://www.climate.be/cart)), and other TTS definitions have been  
56 introduced in order to fill scientific gaps. Therefore, there are many different transport timescale  
57 definitions, e.g. flushing time (Ketchum, 1951; Fischer et al., 1979; Monsen et al., 2002), residence

58 time (Bolin and Rodhe, 1973; Monsen et al., 2002; Delhez et al. 2004; Deleersnijder et al., 2006),  
 59 exposure time (Monsen et al., 2002), transit time (Holzer and Hall 2000), influence time (Delhez et  
 60 al., 2014), age (Bolin and Rodhe, 1973; Monsen et al., 2002), e-folding flushing time (Monsen et  
 61 al., 2002), turnover time (Sheldon and Alber, 2006) and renewal time (Andutta et al., 2014) – all of  
 62 which have their own interpretation.

63 Two timescales, residence time and exposure time, are used to provide an indication of  
 64 increase or decrease of non-reactive and reactive substances in estuaries, bays, lagoons, and atolls  
 65 (Andutta et al., 2014). The residence time ( $\Theta$ ) is the time needed for a particle constituent to reach  
 66 for the first time an open boundary of the domain of interest (e.g. Delhez et al., 2004). The exposure  
 67 time ( $\varphi$ ) is the time the particle will stay in the domain (e.g. Monsen et al., 2002) (Figure 2).  
 68 Therefore, at a given time and location, the exposure time is always larger than or equal to the  
 69 residence time. The larger the difference between the two timescales, the more often the particles  
 70 tend to re-enter the domain of interest after leaving it for the first time. To evaluate the exposure  
 71 time, the computational domain must be larger than the domain of interest (de Brauwere et al.,  
 72 2011, de Brye et al., 2012). Estimates of these timescales may be obtained in an Eulerian or a  
 73 Lagrangian framework. The latter often requires sufficiently large number of numerical particles in  
 74 order to provide a result that statistically approaches the real condition.

75 A dimensionless return coefficient,  $r$ , represents the propensity of particles to return into the  
 76 estuary after reaching an open boundary for the first time, as illustrated in Figure 1A (de Brauwere  
 77 et al., 2011). It is defined as the relative difference between  $\varphi$  and  $\Theta$ , i.e.

$$78 \quad r = \frac{(\Theta - \varphi)}{\Theta} . \quad (1)$$

79 Clearly, this coefficient lies in the interval [0,1].

80 The larger the  $r$  the more likely it is that particles will re-enter the estuary after crossing one  
 81 of its open boundaries for the first time. Accordingly, particles that never return into the estuary  
 82 have  $r = 0$ , while particles returning often or for long periods of time have  $r$  close to unity.

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### Preferred position for figure 1

#### 87 *b. Chosen estuary and coastal area*

88           The domain of interest is the estuarine System of the Caravelas and Peruípe Rivers (ESCP),  
89 in southern Bahia state, Brazil (see Figure 2); more details may be found in Appendix 1. It is  
90 located at the approximate latitude of 17°50'S, nearly 60 km from the National Maritime Park of  
91 Abrolhos, which is one of the largest reef structures of the Atlantic ocean, providing habitat for  
92 innumerable marine species. The ESCP has two main mouths: the Caravelas Estuary in the north  
93 (17°45'S), with two small channels named Barra Velha (~1 km wide) and Tomba's Mouth (~600 m  
94 wide), and the Peruípe Estuary in the south (17°54'S) with a funnel shape ranging in width from  
95 ~3500 m to ~700 m in the first few hundred meters. These two mouths are separated by a distance  
96 of ~25 km alongshore, and are internally connected by shallow and narrow channels around  
97 Cassurubá or Cassumba Island. Our simulations consider the domain shown in Figure 1C, for which  
98 results were computed according to the number of particles in the control domain with boundaries  
99  $\omega_1$  and  $\omega_2$ .

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### Preferred position for figure 2

## 104 **2. Methods**

105

#### 106 *a. Numerical model*

107           The ESCP comprises a number of channels varying significantly in width, from 60 m  
108 upstream to 1000 m near the mouth, and thus a high resolution mesh is necessary to resolve the  
109 many small channels in the domain. The numerical model used is the curvilinear-mesh, three-  
110 dimensional Delft3D-Flow from Deltares ([www.deltares.nl](http://www.deltares.nl)). This model is hydrostatic, and its



111 equations are solved by the method of finite differences (Delft Hydraulics, 2008). A curvilinear  
112 mesh is appropriate for the domain, although there are some disadvantages in the horizontal  
113 resolution distribution compared to unstructured meshes. Delft3D's curvilinear mesh is efficient in  
114 minimizing noise due to the steps in the horizontal plane, and allows the mesh cells to follow the  
115 channels more easily compared to non-curvilinear quadrangular meshes. The degree of non-  
116 orthogonality between mesh elements is always smaller than 0.02 thus satisfying the criteria ( $\cos \theta$   
117  $< 0.02$ ), which helps to preserve numerical stability of the simulations (Delft Hydraulics, 2008).  
118 The diagonal horizontal resolution ranges from ~20 m to ~300 m. The number of quadrangular  
119 mesh cells on the horizontal plane is 22,928. A lower resolution is applied in the coastal region  
120 ~[130-300] m, but this is increased toward the coast and the estuary ~[20-100] m (Figure 1B). The  
121 refined mesh within the estuary combined with high water speeds requires the time-step to be  
122 relatively small (around 1 second), to satisfy the Courant–Friedrichs–Lewy condition. The mesh  
123 used in the simulations of the ESCP (Figure 1B) is relatively complex, covering a small part of the  
124 Peruípe River, near the city of Nova Viçosa. This river is the main channel connecting the northern  
125 and southern mouths. The main tributaries of the Caravelas River, namely the Cupído and Jaburuna  
126 Rivers, are covered by the mesh. With 10 equally spaced sigma vertical layers, this mesh also  
127 covers a few kilometers of the adjacent coastal region.

128         The bathymetry in the estuarine channels was obtained using an Echo sounder and Global  
129 Position System. Two tide gauges were installed in Caravelas and Nova Viçosa (see locations A and  
130 C in Figure 2), meant to remove the tides from the Echo sounder data. For the Peruípe River  
131 estuary, the bathymetry was measured only in the first 6 km, near anchor station D. Thus an  
132 extrapolation was applied, considering the depth to be 4 meters for the next 14 km along the Peruípe  
133 River. The bathymetry was combined from these sources, and the triangular interpolation  
134 application in Delft3D-Flow was used. The bottom topography has depths ranging from ~0.2 m to a  
135 maximum of ~18 m (Tombo's Mouth), whilst in the coastal region do not exceed ~10 m.

136 A more detailed description of the field work carried out to obtain measurements of  
 137 thermohaline properties and other parameters is provided in Appendix 2.

138  
 139 *b. Model Boundary conditions, initial conditions and physical parameters*

140 Rainfall and river discharge measurements in the Peruípe River are shown in Figure 3B. The  
 141 river discharge data, obtained from the National Agency of Waters ANA (<http://www.ana.gov.br/>),  
 142 was measured at a gauge station upstream of the river, at station Helvécia n° 55510000 (code  
 143 1739006). This station covers a large part of the drainage basin of the river. During rainy conditions  
 144 the total drainage basin of the river may be used to estimate the total river flow to be applied at the  
 145 upstream inflow boundary of the river. The factor to account for the missing drainage basin area is  
 146  $\alpha = \frac{A_1 + A_2}{A_1} = 1.6$ , in which station Helvécia  $A_1 \sim 2,840 \text{ km}^2$ , and the downstream area not covered  
 147 by this gauge station is  $A_2 \approx 1,760 \text{ km}^2$ . The area values were obtained from the ANA  
 148 (<http://hidroweb.ana.gov.br/>).

149 Data from the gauge station were also used to estimate the river discharge range for the  
 150 Cupído and Jaburuna rivers. This was done by comparing their watershed areas with the watershed  
 151 of the Peruípe river, and assuming homogeneous rainfall and evapotranspiration distributions over  
 152 these areas (Andutta, 2011; Pereira et al., 2010). The total river flow into Caravelas Estuary was  
 153 then roughly estimated using  $Q = Q_P \beta$ , where  $\beta = 600/4600$  is the ratio between the catchment  
 154 areas of the Caravelas ( $600 \text{ km}^2$ ) and the Peruípe ( $A_1 + A_2 = 4600 \text{ km}^2$ ) rivers, and  $Q_P$  is the  
 155 average discharge for the Peruípe). This estimation was adjusted by comparing observed flow  
 156 velocities at locations A and B with model predictions.

157 The monthly estimate of fresh water inflow for the Peruípe River reveals small inflow for  
 158 the dry season, often between June and September (see Figure 3C). The combined freshwater input  
 159 from the Jaburuna and Cupído rivers estimated using the factor  $\beta$  is less than 10% of the river  
 160 discharge into the Peruípe River. Because the field work was conducted during a relatively dry wet

161 season, when rainfall was negligible prior to and during measurements obtained in January 2008  
162 (Figure 3A), it is logical not to consider the application of the factor  $\alpha$  at the Helvécia gauge  
163 station. Although this approach of river flow estimation is not required, the technique described  
164 above would be required under homogeneous rainfall conditions over the drainage basin of the  
165 Peruípe, Jaburuna and Cupído rivers.

166 The best fit between observations and model results was obtained using the mean river  
167 discharge shown in Table 1 for the Cupído and Jaburuna rivers, and the daily measurements shown  
168 in Figure 3B for the Peruípe River. In other words, the value measured at Helvécia gauge station  
169 was used in the simulation with additional tuning to extrapolate results for the other two smaller  
170 rivers.

171 .  
172 **Preferred position for figure 3**  
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176 **Preferred position for Table 1**  
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178 The measurements from this tide gauge were compared with the simulation results during  
179 neap and spring tides using the “Skill” method described below. In addition, a qualitative  
180 comparison was carried out between the axial salinity distribution found in the simulations, and the  
181 observed distribution presented in Schettini and Miranda (2010).

182 We used the initial condition of a homogeneous thermohaline distribution for the salinity (30  
183 practical salinity unit - psu) and temperature (27 °C). The spin up simulation was made for about  
184 two months to obtain a dynamic equilibrium condition. Since the temperature has previously been  
185 found to be nearly homogeneous in this estuary (Andutta, 2011), its mean value was used for all  
186 simulations. The first flow field and salinity distribution, obtained from the equilibrium condition,

187 was used to provide a varied initial field for simulations starting at slack waters in both spring and  
 188 neap tidal conditions.

189 Computational modellers often assume that vertical eddy diffusion and viscosity coefficients  
 190 vary in time, by using turbulent closure models, e.g. algebraic, *k-L*, *k-Epsilon* schemes. On the other  
 191 hand, the horizontal eddy diffusivity,  $K_h$ , and horizontal viscosity coefficients,  $K_v$ , are often  
 192 estimated according to the mesh element size (Okubo, 1971). Therefore, modellers need to choose a  
 193 parameterisation scheme that provides the right amount of mixing in the estuary. We have  
 194 considered the parameterisation of horizontal eddy viscosity by Uittenbogaard et al. (1992), which  
 195 is available in Delft3D-Flow and reproduces well the turbulent fluxes of momentum.

196 The best fit between results and simulations was obtained assuming the horizontal eddy  
 197 diffusivity,  $K_h$ , to be in the range of  $\sim[2-30] \text{ m}^2 \text{ s}^{-1}$  with small and large values applied respectively  
 198 to small and large mesh cells. The sensitivity analysis for  $K_h$ , was conducted following Okubo  
 199 (1971). Because Okubo's formula applies for open-water, it was observed that it was not properly  
 200 simulating the true dispersion in the estuary, thus a factor  $f$  was used to increase and decrease  
 201 mixing at the sub-grid scale (See Equation 2). Varying  $f$  allowed us to achieve the best fit between  
 202 measurements and model results.

$$203 \quad K_h = f [ 2.05 \times 10^{-4} \times d^{1.15} ] \quad (2)$$

204  
 205 where  $d$  is the mesh cell size (from  $\sim 20$  to  $\sim 300$  metres), and  $f$  is the factor set to different values  
 206 but only shown for 2, 100, 150, 200, 250, 400 and 2000 in the sensitivity analyses (see Table 3).

207 The *k-Epsilon* turbulent closure scheme was used to compute values for the vertical viscosity  
 208 and diffusivity. We assumed the typical Manning roughness coefficient of  $(0.02 \text{ m}^{-1/3} \text{ s})$ , which  
 209 characterises the higher percentage of local sediment (Souza et al., 2013). This resulted in a Chézy  
 210 coefficient of  $\sim 40 \text{ m}^{-1/2}/\text{s}$ . Wind speed and directions, assumed to be constant over this small region,  
 211 were obtained at the Caravelas station from the Instituto Nacional de Meteorologia INMET (code  
 212 INMET 86764), at (source: <http://www.inmet.gov.br/portal/>), see Figure 4.

**Preferred position for figure 4**213  
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215 The wind was assumed to only affect mesh cells in coastal areas. In other words, the wind  
216 stress did not affect mesh cells inside the estuarine channels. Moreover, Andutta et al. (2013)  
217 applied Hansen and Rattray's analytical equation of the velocity and salinity components, and  
218 demonstrated that the wind effect in January 2008 was negligible at station C (near Nova Viçosa  
219 estuarine mouth), which is the closest to the coast. Hansen and Rattray's analytical solution required  
220 an adjustment of no more than 0.02 Pascal for the wind stress, which correspond to wind speeds of  
221  $\sim 3 \text{ m s}^{-1}$  (Andutta et al., 2013). South-southwestward alongshore currents occur between October  
222 and January, while north-northeastward alongshore currents are observed during the fall and winter  
223 months Lessa and Cirano (2006).

224 Sea level data from TOPEX were used to force tides at the open boundary nodes. A time  
225 series of water surface elevation from May to July 2007 was recorded at Terminal Aracruz (TA in  
226 Figure 2), which is a few kilometers away from the coastal open boundary. At TA a total of  
227 16,264 tidal measurements were recorded at five minute intervals, and were processed using the  
228 tidal component extraction program PACMARÉ (Franco, 2000). These tidal measurements were  
229 used to obtain the amplitude and phase of the main tidal components, shown in Table 2.  
230 Additionally, sea-level data were recorded at stations A and C from 14<sup>th</sup> to 19<sup>th</sup> of January 2008,  
231 and these data were used to validate modelled sea-level oscillation (comparison shown in Results  
232 and Discussion section). Sea surface elevation observations from sites A and C showed the same  
233 phase, strongly suggesting that tides propagate across the shelf, because tides propagating along the  
234 coast would results in a phase shift between sea level observations at sites A and C (see Figure 2).  
235 The measurements of tidal heights of  $\sim 1 \text{ m}$  and  $\sim 3 \text{ m}$  during neap and spring tides, respectively.  
236 This ranks as meso-tidal, according to the criteria of Davies (1964) for tidal classification. From  
237 the tidal heights shown in Table 3, the tidal form-number is  $[N_f = (K_1 + O_1) / (M_2 + S_2) =$   
238  $0.19]$ , indicating a semidiurnal tidal estuary (Defant, 1960). The tidal components from Table 2  
239 represent over 97% of sea level variations for the estuarine system (Andutta, 2011).

**Preferred position for Table 2**

240

241

242 *d. Model validation criteria*

243 In order to quantify the agreement between the simulated velocity and salinity profiles the  
 244 method suggested by Wilmott (1981), based on the Skill parameter was used. Accordingly, the skill  
 245 is measured as follows

$$246 \quad Skill = 1 - \frac{\sum |X_{\text{mod}} - X_{\text{obs}}|^2}{\sum \left( |X_{\text{mod}} - \bar{X}_{\text{obs}}| + |X_{\text{obs}} - \bar{X}_{\text{obs}}| \right)^2}, \quad (3)$$

247 where  $X_{\text{obs}}$  and  $X_{\text{model}}$  denote the observational and simulated properties, respectively,  $\bar{X}_{\text{obs}}$  being  
 248 the mean observational values. The Skill parameter varies from 1 to zero, with 1 indicating the best  
 249 fit, and zero indicating a complete disagreement between observation and model results.

250

251 *e. Modelling approach to calculate the Transport Timescales*

252 To quantify the residence time and exposure time 35 thousand numerical particles were  
 253 released in the estuary by coupling D-Waq PART with results from the Delft3D-FLOW (i.e. within  
 254 the subdomain denoted  $\omega$ ). Numerical particles were deployed near the bottom and top layers. The  
 255 particle concentration using conservative tracer module was normalized to value 1 within the  
 256 volume of  $\omega$ . Therefore, the number of particles decreases when particles exit  $\omega$ , and increases  
 257 when particles re-enter  $\omega$ . The minimal initial number of particles, i.e. 25 thousand, was computed  
 258 considering a minimum thickness of 2 m and a grid cell of ~20 by 10 meters.

259 A total of four simulation scenarios were made: ( $S_1$ ) particle released at high water in neap  
 260 tide, ( $S_2$ ) particle released at low water in neap tide, ( $S_3$ ) particle released at high water in spring  
 261 tide, and ( $S_4$ ) particle released at low water in spring tide.

262 In order to be consistent with CART timescales, for the computation of the residence time,  
 263 particles are discarded once they have reached an open boundary, e.g. estuarine head or an open

264 boundary in coastal waters (de Brauwere et al., 2011; de Brye et al., 2012). The arithmetic mean of  
 265 the individual residence times,  $\varphi$ , was computed as the time necessary for particles to exit the  
 266 domain ( $\omega$ ) for the first time. As for the exposure time, the particles are assumed to immediately  
 267 bounce back into the domain only at estuarine heads. This simplifying hypothesis is unlikely to  
 268 entail any major error, since a particle crossing the upstream estuarine boundary in the upstream  
 269 direction (because of diffusive processes) will most likely return into the estuary after a relatively  
 270 small time under the influence of the river flow, e.g., the St. Johans River in Florida, which  
 271 experiences backflows over significant durations (Hendrickson et al., 2003).

272 Results from residence and exposure times were used to estimate the return coefficient  
 273 distribution. The residence and exposure times may vary according to the time of release, such as  
 274 during neap/spring tides or high/low tides, and this would also affect the return coefficient. This  
 275 notwithstanding, results of exposure and residence times must be calculated for the same conditions  
 276 when computing the return coefficient, i.e.  $r = (\Theta - \varphi) / \Theta$ .

277

#### 278 *f. The modified LOICZ analytical model*

279 The modified LOICZ model of Andutta et al. (2014) applies the salinity balance proposed  
 280 by Fischer et al. (1979) into the original formulation of the LOICZ. This water renewal timescale  
 281 model has been shown to be sensitive to changes to some of its free parameters (e.g. river flow and  
 282 salinity gradient). We expect that the estimates of the timescales from our numerical results would  
 283 fit within the ranges derived from the LOICZ model. Details of its derivation are provided in  
 284 Andutta et al. (2014); however we provide the simplified relation for water renewal timescale.

285

$$286 \quad \frac{1}{T_p} = \frac{1}{T_1} + \frac{1}{T_2}, \quad (4)$$

287

288 where  $T_1 = L/U$  and  $T_2 = L^2 / K$  are the advective and dispersive timescales, respectively.  $L$ ,  $U$ ,  $K$   
 289 and  $T_p$  are respectively the selected estuarine segment length, the flow speed, the characteristic  
 290 value of the longitudinal diffusivity and the water renewal timescale. This expression may be re-

291 written in terms of the dimensionless Péclet number  $Pe = ULK^{-1}$ , the ratio  $P_e = T_2/T_1$  of the  
 292 dispersive to the advective timescale. Similarly, this number provides a comparison of contributions  
 293 from advective and dispersive processes to transport timescales, yielding

294

$$295 \quad T_P = \frac{VP_e}{Q_R(1 + P_e)}. \quad (5)$$

296 Where  $V$  and  $Q_R$  denote the estuarine volume and river discharge, respectively. The contribution of  
 297 advection to the total water renewal timescale  $T_P$ ,  $\theta$  ( $0 \leq \theta \leq 1$ ), is given by

$$298 \quad \theta = T_P/T_1 = Q_R/(Q_R + Q_D), \quad (6)$$

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### g. The CART analytical model

As previously mentioned, in the framework of CART, the TTS that may be used to calculate water renewal rates can be obtained at any time and position as the solution of partial differential equations (Deleersnijder et al., 2006; de Brye et al., 2012; Andutta et al., 2014). For instance, residence time and exposure time were estimated using calibrated/validated numerical simulations for the Scheldt Estuary (de Brauwere et al. 2011, de Brye et al. 2012). As an easy acceptable method, analytical solutions may provide results that are representative of real situations (e.g. CART and LOICZ). The idealised CART timescales were used to obtain the exact analytical solution of the so called return coefficient for the ESCP. Different values of the Péclet number were considered, in order to assess the axial variation of return coefficient values. The advective timescale,  $T_1 = V/Q_R$ , and a dispersive timescale,  $T_2 = P_EV/Q_R$ , are defined taking into consideration the estuarine volume  $V$ . Andutta et al. (2014) provides a detailed description depicting an idealized channel for the time scales.



318 Consider an estuarine channel ( $-\infty < x < \infty$ ) with a constant cross-sectional area  $A$ , and a  
 319 flow under steady-state. The volumetric flow rate is denoted as  $Q_R$ . The downstream and upstream  
 320 boundaries of our idealised estuary are located at  $x = L_0$  and  $x = L_1$ , respectively. The estuarine  
 321 length is  $L = L_0 - L_1$ , and thus the volume is  $V = AL$ . The water velocity is then  
 322  $U = Q_R / A = LQ_R / V$ . For the abovementioned conditions, the residence time satisfies the adjoint  
 323 of the classical passive tracer transport equation (Delhez et al. 2004, Andutta et al. 2014), i.e.

324

$$325 \quad \frac{d}{dx} \left( AK \frac{d\varphi}{dx} + Q_R \varphi \right) = -A \quad (7)$$

326

327 where,  $x$ , denotes the particle position. The solution for the equation needs to satisfy the upstream  
 328 and downstream boundary conditions,

329

$$330 \quad \varphi(L_1) = 0 = \varphi(L_0). \quad (8)$$

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332 It represents the average time required by particles initially located in the interval  $[x, x + \delta x]$   
 333 (with  $\delta x \rightarrow 0$ ) to reach one of the open boundaries. The solution is then easily derived:

334

$$335 \quad \varphi(x) = \frac{V}{Q_R} \left( 1 - \frac{\xi}{L} \right) + \frac{V}{Q_R} \left( \frac{e^{-Pe} - e^{-Pe \xi/L}}{1 - e^{-Pe}} \right) \quad (9)$$

336 where  $\xi = x - L_1$ .

337 The exposure time was also derived (Andutta et al., 2014), and is defined in the domain of interest  
 338 and its surrounding environment.

$$339 \quad -\infty \leq x \leq L_1 \quad : \quad \Theta(x) = \frac{V}{Q_R} \quad (10a)$$

$$340 \quad L_1 \leq x \leq L_0 \quad : \quad \Theta(x) = \frac{V}{Q_R} \left( 1 - \frac{\xi}{L} \right) + \frac{V}{Q_R} \left( \frac{1 - e^{-Pe \xi/L}}{Pe} \right) \quad (10b)$$

$$341 \quad L_0 \leq x < \infty \quad : \quad \Theta(x) = \frac{V}{Q_R} \left( \frac{e^{-Pe} - 1}{Pe} e^{-Pe \xi/L} \right) \quad (10c)$$

342

343 From Equations (9) and (10), which are valid within the upstream and downstream open  
 344 boundaries, the return coefficient is:

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$$346 \quad r = \frac{\Theta(x) - \varphi(x)}{\Theta(x)} = \frac{\left( \frac{1 - e^{-Pe \zeta/L}}{Pe} \right) - \left( \frac{e^{-Pe} - e^{-Pe \zeta/L}}{1 - e^{-Pe}} \right)}{\left( 1 - \frac{\zeta}{L} \right) + \left( \frac{1 - e^{-Pe \zeta/L}}{Pe} \right)} \quad (11)$$

347 Note that  $r$  is bounded by  $[0,1]$ , as mentioned before.

348 In principle, the residence time and the exposure time can be obtained by solving classical  
 349 passive transport equations. However, to do so, time- and position-dependent concentrations must  
 350 first be obtained and, then, time and space integral must be performed to derive the relevant  
 351 timescales. This is not straightforward, even for highly idealised flows. This is why it is preferable  
 352 to have recourse to the adjoint method established by Delhez et al. (2004), which requires the  
 353 solution of simpler differential problems to be determined: in the present case, only ordinary  
 354 differential equations are to be dealt with rather than partial differential ones. The disadvantage of  
 355 this approach is that the theoretical underpinning of an adjoint model sometimes appears elusive,  
 356 which is probably the reason why Errico (1997) wrote a general, enlightening paper on this matter,  
 357 explaining the nature and purpose of adjoint models.

358

### 359 **3. Results and Discussion**

360

#### 361 *a. Model calibration of salinity, velocity and tides*

362 We carried out a sensitivity analysis considering different values for the horizontal diffusion  
 363 coefficient  $k_h$  using Equation 2. These adjustments of factor  $f$  for the horizontal diffusivity based on  
 364 the grid size allowed us to obtain a proper representation of the salinity field and its time variability.

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**Preferred position for Table 3**

366 The mean Skill parameters for the simulation are shown in Table 3 for different values of  
367 factor  $f$ , which was described with Equation 2. The comparison of sea-level oscillation over a tidal  
368 modulation period, from the 14<sup>th</sup> to the 29<sup>th</sup> of January 2008, showed good skill values for locations  
369 A (Figure 5) and C (not shown), and the Skill parameter for tides was calculated to be over 0.97 for  
370 both locations, i.e. A and C. The comparison of tides, velocity, and salinity showed good skill  
371 values during spring tides (not shown), and reasonable values during neap tides (Figure 6).

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**Preferred position for figure 5**  
**Preferred position for figure 6**

376 The Skill parameter for the water column height variation in time was calculated to be over  
377 0.98 for all the sites under neap and spring tides (Table 4), and the tidal ranges were ~1.0 m and  
378 ~2.5 m for neap and spring tides, respectively. Observations have shown that the tidal phase  
379 between sites A (Caravelas mouth) and C (Peruípe mouth) is almost the same. The similarity of  
380 their phases indicates that tides propagate mainly perpendicular to the coast line in this region, a  
381 result which is in close agreement with observations previously reported by Lessa and  
382 Cyrano (2006).

383 For the modeled velocity validation, good results (Skill from 0.77 to 0.93) were obtained in  
384 spring tides in the estuaries of Caravelas (sites A and B) and Nova Viçosa (sites C and D). For neap  
385 tides due to small differences on tidal asymmetry, the Skill was lower, at ~ 0.6.

386 The model agreed well with observations of maximum ebb and flood currents at site A. The  
387 model also properly simulated the velocity profiles for sites B, C, and D. Therefore, the description  
388 of maximum ebb and flood currents from in-situ data also apply to the model simulations. At site B  
389 there were maximum speeds of ~0.5 m s<sup>-1</sup> and 1.0 m s<sup>-1</sup> (ebb events), and ~-0.3 m s<sup>-1</sup> and ~-0.6 m s<sup>-1</sup>  
390 (flood events), during neap and spring tides, respectively. For site A the vertical shear of the  
391 velocity was negligible in flood and ebb conditions, while for site B there was a small vertical shear  
392 of the horizontal velocity during ebb events. During flood events, the water velocity was  
393 homogenous over the water column. In addition, a residual velocity of ~0.05 m s<sup>-1</sup> was calculated at

394 site B, indicating a residual circulation from Nova Viçosa towards the Caravelas River. Site A had a  
395 residual current of  $\sim 0.06 \text{ m s}^{-1}$ , indicating a small discharge from the Cupído and Jaburuna Rivers.  
396 At sites C and D, located in the Peruípe River, the downstream velocities showed more intensity  
397 than observed in the Caravelas Channel. For site C the downstream velocities varied from  $\sim -0.9 \text{ m}$   
398  $\text{s}^{-1}$  to  $\sim -1.5 \text{ m s}^{-1}$ , for neap and spring tides, respectively. During flood events, the velocities were  $\sim$   
399  $0.3 \text{ m s}^{-1}$  and  $\sim -0.7 \text{ m s}^{-1}$ , for neap and spring tides, respectively. At site D the maximum  
400 downstream velocities were only  $\sim 0.7 \text{ m s}^{-1}$  and  $\sim 1.0 \text{ m s}^{-1}$  at neap and spring tides, and upstream  
401 velocities were  $\sim -0.3 \text{ m s}^{-1}$  and  $\sim -0.4 \text{ m s}^{-1}$ . The residual velocities at sites C and D, which have  
402 values of  $\sim 0.10 \text{ m s}^{-1}$  to  $\sim 0.15 \text{ m s}^{-1}$ , indicate a higher advective contribution from the Peruípe River  
403 compared with the Caravelas estuary.

404 In addition to the tides and the velocity field, the model simulated the temporal variation of  
405 the salinity well for all sites (A, B, C, and D). During spring tides the calculated Skill values were  
406 over 0.83, while for neap tides they were over 0.73 (Table 4). At the Caravelas estuarine channel,  
407  $\sim 3 \text{ km}$  near the mouth (site A), during low tide, salinity was observed in intervals of  $\sim 34.5 \text{ psu}$  to  
408  $\sim 35.0 \text{ psu}$  and  $\sim 34.0 \text{ psu}$  to  $\sim 34.5 \text{ psu}$  for the observational and theoretical results,  
409 respectively. About  $6 \text{ km}$  away from the mouth we obtained a good agreement for the salinity, with  
410  $\sim 32.0 \text{ psu}$  and  $\sim 32.5 \text{ psu}$  for observation and simulation, respectively. In the vicinity of the  
411 interconnection with Cupído and Jaburuna Rivers (site B), which is about  $12 \text{ km}$  upstream from the  
412 mouth, the salinity decreased to  $\sim 30.0 \text{ psu}$  and  $\sim 28.5 \text{ psu}$  for the observational and calculated  
413 results, respectively. At high tide, near the mouth (site A) and at a distance of  $6 \text{ km}$  from the mouth,  
414 the salinity was  $\sim 36.5 \text{ psu}$  and  $\sim 36.0 \text{ psu}$ , respectively, for both simulation and field measurements.  
415 In the upper reaches of the estuary, near the junction of the rivers, Cupído and Jaburuna ( $\sim 12 \text{ km}$   
416 from the mouth), a close agreement between simulated and observed salinity values ( $\sim 33.0 \text{ psu}$ ) was  
417 obtained at high tide. Along the Peruípe River estuary at neap tides, the surface salinities vary in the  
418 range of  $20.0 \text{ psu}$  to  $34.0 \text{ psu}$  at the surface, and  $32.5 \text{ psu}$  to  $36.0 \text{ psu}$  near the bottom. The region of  
419 Nova Viçosa has more vertical stratification of the salinity than at sites A and B in the Caravelas

420 River. This is due to Peruípe River's larger freshwater discharge. The observed value of ~36.0 psu  
421 near the bottom is characteristic of the Tropical Water Mass, which was already reported to enter  
422 this estuarine system (Schettini et al., 2010). During spring tides the vertical mixing causes the  
423 erosion of the halocline, and thus decreases vertical stratification. This results in a smaller vertical  
424 variation of 31.0 psu to 36.0 psu from the surface to the bottom.

425 **Preferred position for Table 4**

426 A comparison of the axial distribution of salinity was made for the Caravelas River (Figure  
427 7A,B). For the first 12 km along the estuarine channel, results from simulations were compared to  
428 observations made by Schettini and Miranda (2010). The measurements were obtained on the 10<sup>th</sup>  
429 of April, 2001 during spring tides. Although the field data are likely to be from different conditions  
430 of river flow, the simulation showed a good correlation of the axial distribution of the salinity in the  
431 Caravelas River (See Figures 7C and 7D), with values of  $R^2 \sim 0.97$  and  $R^2 \sim 0.99$  for low and high  
432 tides respectively. This indicates that the model has well represented the mixing processes in the  
433 Caravelas Estuary. During low tide (Figure 7A,C), a good agreement is found near the mouth, with  
434 salinity values of ~35.2 psu and ~ 34.5 psu, for the model results and observations, respectively. At  
435 nearly 6 km upstream, there is still a good agreement ( $R^2 \sim 0.99$ ) with the salinity values of ~33  
436 psu (model), and ~32 psu (observation). Further upstream and near the inter-connection between the  
437 Cupído and Jaburuna rivers (i.e. ~ 12 km upstream), the agreement is slightly poorer with the  
438 salinity values of ~30 psu (model) and ~29 psu (observation). At high tide (Figure 7B, D), the  
439 model predicted the longitudinal salinity variations well along the Caravelas Channel. The salinity  
440 values near the mouth were ~36.4 psu (model and observation), and reduced to ~36 psu 6 km  
441 further upstream. Moreover, during high tides the agreement was also good near the channel  
442 between the Cupído and Jaburuna rivers with salinity of ~33 psu.

443 **Preferred position for figure 7**

444  
445 *b. Results of the residence time, the exposure time and the return coefficient*

446

447 The transport timescales, namely residence time ( $\varphi$ ), exposure time ( $\Theta$ ), and the return  
448 coefficient ( $r$ ), were estimated for the Caravelas and Peruípe estuarine channels with simulation  
449 under different scenarios, i.e. S<sub>1</sub> to S<sub>4</sub> (Figures 8, and 9).

450 For scenarios S<sub>1</sub> and S<sub>3</sub> (Figure 8), the residence time along the Caravelas Channel, from the  
451 mouth to 12 km upstream, was found to vary from 0 to ~15.0 days. The inflow boundaries of the  
452 Cupído and Jaburuna rivers were found to have residence times of ~27 and ~22 days, respectively.  
453 For the Peruípe Channel the residence times ranged from 0 to ~7.4 days, from the mouth to 5 km  
454 upstream, with a maximum value of ~18 days at the inflow boundary of the Peruípe Estuary.

455 The residence time estimated at ~6 km further upstream in the Caravelas Estuary ( $\varphi = 11.7$   
456 days) is almost three times larger than the residence time calculated for the same distance along the  
457 Peruípe Estuary ( $\varphi < 4.4$  days). The difference between results in the Caravelas and the Peruípe  
458 estuaries is due to the larger velocity contribution in the Peruípe Estuary.

459 Comparing scenarios S<sub>1</sub> and S<sub>3</sub>, the residence time was found to be slightly lower for S<sub>3</sub> (c.a.  
460 a few hours) and this difference is due to increased diffusive contribution during stronger spring  
461 tidal conditions. In contrast to scenarios S<sub>1</sub> and S<sub>3</sub>, the simulations considering scenarios S<sub>2</sub> and S<sub>4</sub>  
462 yielded an increased residence time. This increase was maximum near the estuarine mouths (~5  
463 days), and observed to reduce in the upstream direction (few hours). The increase in residence time  
464 for particles released in slack water of low tide is caused by tidal excursion from reversing currents  
465 (i.e. flood currents). These results reflect and add value to recent simulations by de Brye et al.  
466 (2012) for the Scheldt Estuary (in Belgium and the Netherlands), whose results showed larger  
467 residence time values for particles released at slack water of low tides than for high tides (difference  
468 of a few days).

469 The virtual Lagrangian particles showed that a negligible number of particles crossed the  
470 connecting channel between the Caravelas ( $\omega_1$ ) and Peruípe Estuaries ( $\omega_2$ ), which indicates that this  
471 relatively narrow and shallow interconnection channel allows little exchange of water properties  
472 between these estuaries. Moreover, the residence time is observed to be larger within the

473 enlargement of the interconnecting channel between these two estuaries. Schettini and Miranda  
 474 (2010) and Schettini et al. (2013) have addressed the importance of the interconnection channel  
 475 between Caravelas and Peruípe, and found that sediment deposited near the Caravelas mouth was  
 476 both inner shelf local resuspension and upstream transport, or sourced from the Peruípe River via  
 477 the interconnection channel.

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### Preferred position for figure 8

481 Exposure time results showed that particles re-entered the system for up to two days (Figure  
 482 9). Note that the difference between the exposure time and the residence time ( $\Theta - \varphi$ ) showed little  
 483 spatial variation for scenarios  $S_1$  and  $S_3$ .

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### Preferred position for figure 9

486 The spatially averaged difference between exposure and residence times ( $\Theta - \varphi$ ) are  
 487 calculated in days, and its respective RMSE to be  $\sim 1.98 \pm 0.06$  for  $S_1$ ,  $\sim 1.87 \pm 0.12$  for  $S_2$ ,  $\sim 1.92$   
 488  $\pm 0.07$  for  $S_3$ ,  $\sim 2.19 \pm 0.08$  for  $S_4$ . These results strongly suggest that ( $\Theta - \varphi \sim \text{const.}$ ) for the  
 489 ESCP under the four different scenarios considered. The results also suggest that  $t_3 - t_2$  varies little  
 490 away from the open boundaries, so particles deployed at different times and locations in the estuary  
 491 re-enter for similar lengths of time, assuming the circulation in coastal waters does not considerably  
 492 change over time due to additional forcings, e.g. sudden alongshore wind driven currents.

493 Equation (5) was used to estimate the range of water renewal timescales for the Caravelas  
 494 and Peruípe estuaries using the parameters given in the appendices of Andutta et al. (2014), see  
 495 Figure 10. The straight line labelled  $\theta$  (lowercase) indicate the relative advective contribution to  
 496 water renewal, where  $0 \leq \theta \leq 1$ . The line at  $\theta = 0.5$  separates the areas where transport is  
 497 dominated by advection (diagram upper zone,  $\theta > 0.5$ ) and dispersion (diagram lower zone,  $\theta <$   
 498  $0.5$ ).

499 The Caravelas and Peruípe estuaries have mean depths of  $\sim 6.5$  and  $\sim 7.5$  meters,  
 500 respectively, and the maximum and minimum tidal ranges in these estuaries are  $\sim 2.5$  and  $\sim 0.5$

501 meters. According to Andutta et al. (2013), these tidal ranges combined with the relatively the small  
502 depths result in a high rate of change of the potential energy ( $\sim 6.1 \text{ J m}^{-3} \text{ s}^{-1}$ ), which contributes  
503 towards large dispersion. It is valid to compare these results to the Sheldt Estuary, where tidal  
504 oscillation is typically 4-5 meters along the first  $\sim 100$  km, and where the mean water depth is  $\sim 10$   
505 meters. Tidal range in the Sheldt can reach  $\sim 7$  m, which is about 45% of the mean water depth  
506 value for the first  $\sim 25$  km near the estuarine mouth (Soertaert and Herman, 1995; de Brye et al.  
507 2012), and this system is classified as well-mixed due to dispersion prevailing over advection. The  
508 numerical results for the ESCP fit within the timescale ranges estimated using the simple LOICZ  
509 method.

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### Preferred position for figure 10

513 The return coefficient cannot be calculated using the modified LOICZ model. However, it  
514 was computed numerically and compared to the non-dimensional solution obtained using CART.  
515 The return coefficient converges to one at the estuarine mouths and near estuarine heads (Figure 11,  
516 for all scenarios  $S_1$  to  $S_4$  and Figure 12B). However, this is only a direct consequence of the  
517 definition of the residence time, which converges to zero at the entrance, and thus the return  
518 coefficient will always increase towards unity.  $r$  was observed to be smaller upstream, because the  
519 ratio  $(\Theta - \varphi)/\Theta$  is likely to decrease. It can be noticed that the axial variation of the return  
520 coefficient is similar for both CART solution and numerical approach (Figures 11 and 12C). The  
521 return coefficient calculated from CART and from numerical simulations is observed to increase  
522 towards the upstream boundary. This increase towards the estuarine head is due to the boundary  
523 condition assumed in the analytical and numerical solutions, where particles do not re-enter the  
524 domain after crossing the estuarine head, although in a real estuary water particles would re-enter  
525 through the estuarine head due to river flow conditions.



526 Figure 12A shows results of the residence and exposure time and return coefficient for a  
527 range of values of the Péclet number. High values of the Péclet number yield a boundary layer in  
528 the vicinity of the upstream location.

529 The greater the relative importance of advection, the less likely it is that dispersion will  
530 cause a water particle to hit the upstream boundary of the domain ( $x = L_0$ ). In accordance with their  
531 definitions, the exposure time is larger than the residence time for any location in the domain ( $L_1 \leq$   
532  $\xi/L \leq L_0$ ). These idealised results of the return coefficient were used to access results obtained  
533 from our numerical simulations.

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535  
536 **Preferred position for figure 11**  
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538 **Preferred position for figure 12**  
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540 In the illustration shown in Figure 11A, the ratio is simply the difference between times  $t_3$   
541 and  $t_2$ . Evidently this is a simple case where the particle is assumed to have re-entered the domain  
542 only once.

543 Particles are expected to first cross the estuarine mouth during ebb currents, which would be  
544 alternating with flood currents and dispersive processes. Therefore, we could presume that  
545 Lagrangian particles would have a time window of  $\sim 6.5$  hours to cross the entrance (for semi-  
546 diurnal tidal estuaries), and this time window would then close for  $\sim 6.5$  hours (the period of flood  
547 currents).

548 Our simulations were for relatively calm weather conditions, which were predominant over  
549 the region, c.a. wind speeds in the range  $1-4 \text{ m s}^{-1}$  (wind from NE). Andutta et al. (2013) showed  
550 that wind conditions did not affect the water circulation in this estuarine system in January 2008.  
551 However, for stronger wind conditions the results would not be the same. Evidently alongshore  
552 wind-driven currents would reduce the difference between the exposure time and the residence  
553 time, and the return coefficient would thus decrease towards zero. This is because alongshore  
554 currents inhibit the propensity of particles to re-enter the estuarine system. The alongshore shelf  
555 currents are observed to be driven by the N-S migration of the South Atlantic High between  
556 summer and winter. South-southwestward alongshore currents occur between October and January,  
557 while stronger north-northeastward alongshore currents are observed during the fall and winter  
558 months (Lessa and Cirano, 2006).

559

560 **4. Conclusions**

561

562 *Overall goal*

563 This study provides the first estimates of the residence time, exposure time and the return  
564 coefficient for the Caravelas and Peruípe estuaries and might be a reference for future studies  
565 related to the control of pollutants and sediment transport. These transport timescales were  
566 estimated using a Lagrangian model only as a tool, and this model has been properly calibrated and  
567 validated using field data.

568 *Specific conclusions*

569 • *Achievements regarding goals (1 and 2)*

570 The residence time for particles released far upstream in the Caravelas Estuary was found to  
571 be nearly 3 weeks for particles, regardless of whether they are released at high or low tide, and is  
572 driven by tidal dispersion combined with the discharge from the Cupído and Jaburuna Rivers  
573 (typical range of 4 to 9 m<sup>3</sup> s<sup>-1</sup>). These results are consistent with previous estimates derived from  
574 simple analytical solutions (Andutta et al., 2014), see Figure 10. For the Peruípe Estuary, our  
575 estimates of the residence time were for less than one week, due to the tidal dispersion combined  
576 with the larger river input from the Peruípe River (typical range of 20 to 70 m<sup>3</sup> s<sup>-1</sup>).

577 The transport timescales (exposure and residence times) were found to be quite similar for  
578 particles released in high tide under spring and neap tidal conditions, thus confirming previous  
579 estimations made for the Scheldt Estuary (de Brye et al., 2012). In contrast, the transport timescales  
580 were shown to be more sensitive to tidal-phase release time (i.e. high or low tides) in this estuarine  
581 system. Similar observations were made for the Scheldt Estuary (de Brauwere et al., 2011), in  
582 which there was a difference of days for results of residence time using particles released at high  
583 and low tides. This suggests that tidal-phase release time for a meso-tidal shallow estuary forced by  
584 low-moderate river discharge conditions is important for quantification of TTS, especially for water  
585 particles near mouths where larger tidal excursions are expected compared to locations further  
586 upstream, and since their initial movement would be upstream/downstream if released during  
587 low/high tide, respectively.

588 The Lagrangian simulation also showed that the narrow and shallow inter-connecting  
589 channel between the Peruípe and Caravelas estuaries allows little water exchange between the two  
590 estuaries, and only a few particles were capable of crossing the inter-connection passage with  
591 prevailing direction from the Peruípe to the Caravelas, in agreement with Schettini et al. (2013).  
592 Therefore, both exposure time and residence time were large at that location, and the exchange of  
593 water properties is likely to happen through alongshore currents at inner coastal areas.

594 • *Achievements regarding goal (3)*

595 Similarly to the exposure and residence times, the return coefficient was shown to be more  
596 sensitive to tidal phase (high and low tide), than to neap and spring tidal conditions. It may be  
597 summarized as follows: (1) the return coefficient is larger for particles released at high tide than at  
598 low tide; (2) the return coefficient is larger for particles released during spring tides than during  
599 neap tides.

600 For these two estuaries the exposure time was higher than the residence time in all  
601 simulations, thus showing that water may return to the system after having first crossed the mouth.  
602 The propensity of this water to return to the estuary was quantified using the return coefficient,  
603 which depends on the difference between the exposure and residence times, and thus also on the  
604 residual circulation due to river discharge, as well as the circulation in coastal waters. For instance,  
605 swift longshore currents decrease the difference between the exposure and residence times, and  
606 therefore reduce the return coefficient. The wind conditions over our measurement period were  
607 characteristic of calm weather, c.a. a few  $\text{m s}^{-1}$  (see Figure 4), and different scenarios may produce  
608 different results for the transport timescales, for instance under stronger north-northeastward  
609 alongshore currents which are often observed during the fall and winter months Lessa and Cirano  
610 (2006). Due to its definition, the return coefficient is predicted to be larger at the estuarine mouths,  
611 because the residence time tends to zero (see Equation 1). Our results have additionally shown that  
612 for our scenarios the difference between exposure and residence times ( $\Theta - \varphi$ ) is nearly constant  
613 within our domain. This can also be observed from our analytical solution (Figure 12C).

614

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616

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625

626 **References**

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Figure 1

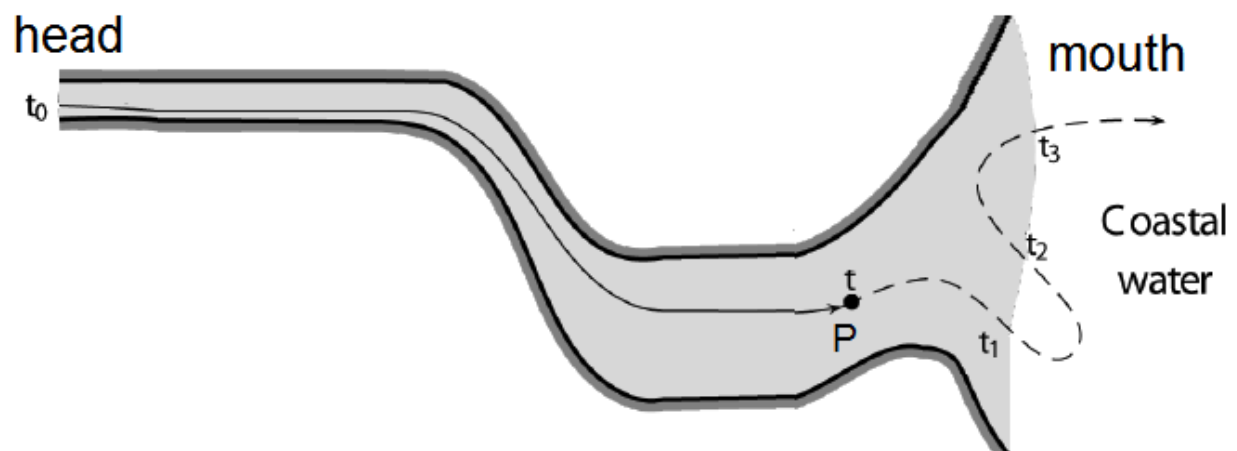


Figure 1 –Path of a particle in the estuary from the upstream boundary (head) to the downstream boundary (mouth). For a particle initially at position P at time  $t$ , the residence time is  $t_1 - t$ , the exposure time is  $(t_3 - t_2) + (t_1 - t)$ .



Figure 2

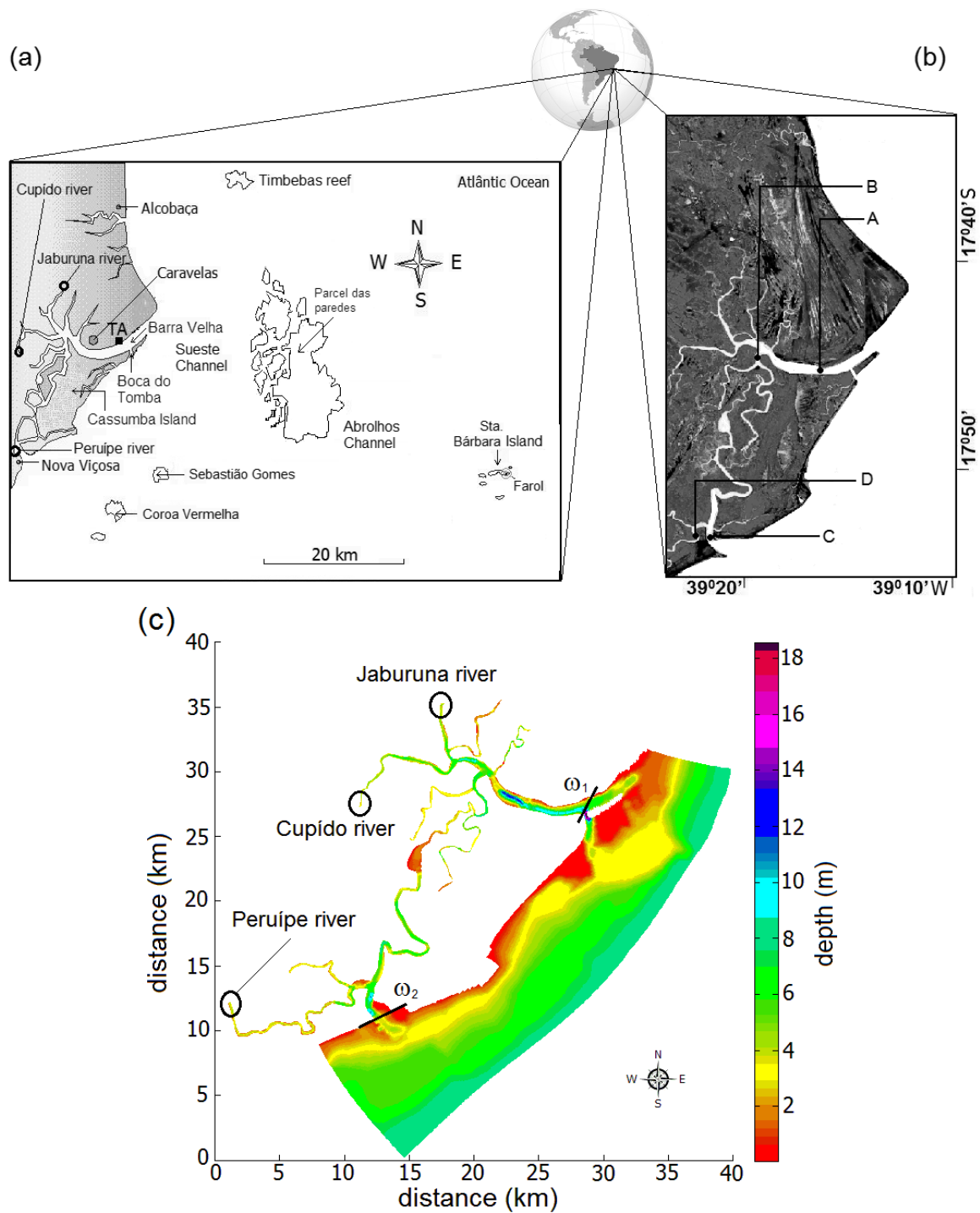


Figure 2 – (a) Geographic location of the estuarine system comprising the Caravelas and Peruípe rivers. Aracruz terminal harbour – TA, and the Sueste and Abrolhos channels, the Parcel das paredes and the National Marine Park of Abrolhos. (b) Detailed image of the estuarine system, and location of the oceanographic mooring sites A and B in Caravelas area, and C and D in Nova Viçosa area, where D is referred as site E at Andutta et al., 2013b. (c) numerical domain with  $\omega_1$  and  $\omega_2$  denoting the limit of the control domain  $\omega$  to compute the transport timescales.

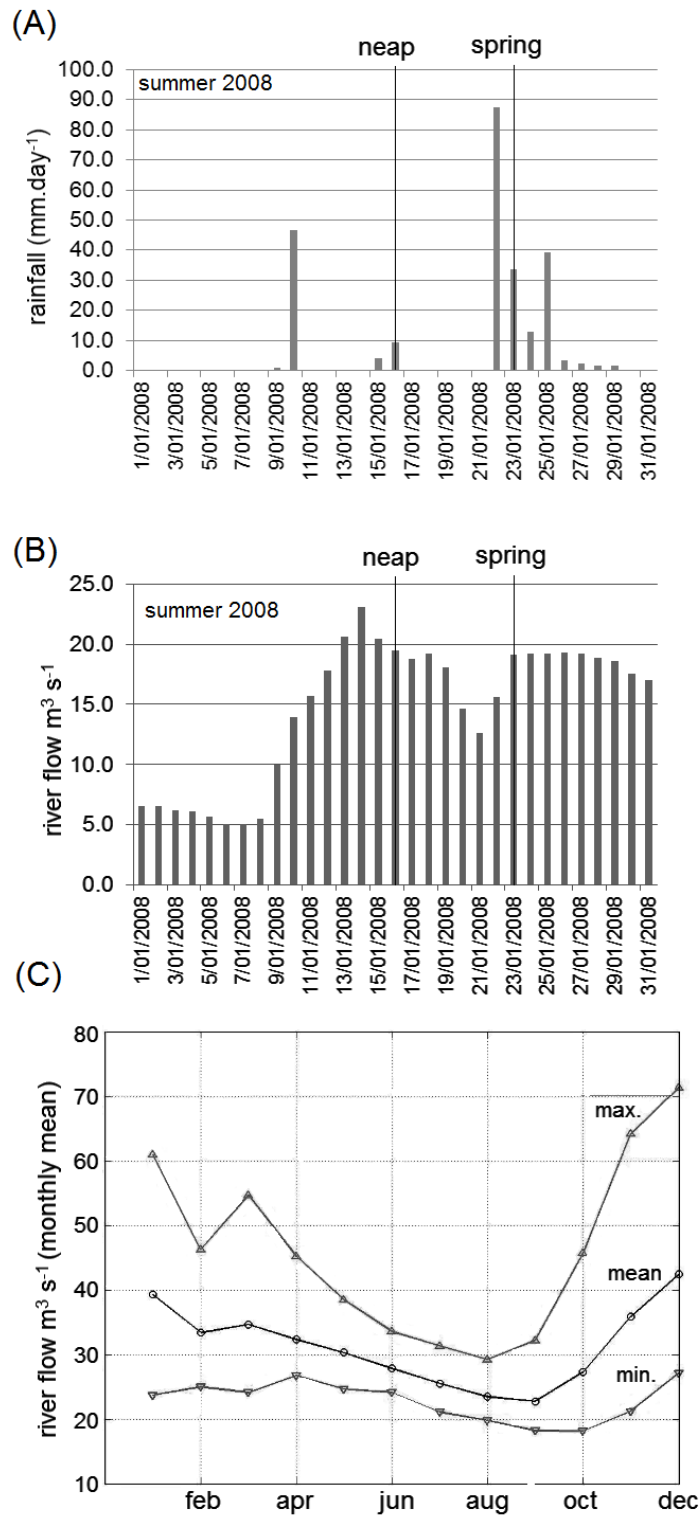


Figure 3 – Daily variation of the rainfall (A), and river discharge (B) during January (2008), observations were made at the gauge station *Helvécia* n° 55510000 (código 1739006) – National Agency of Waters. (C) Climatological estimate of the mean, minimum (min.) and maximum (max.) monthly river discharge using data from 1975 to 2008 (34 years of measured river flow) and corrected using the factor 1.6 to account for the entire drainage basin area of the *Peruípe* River.

Figure 4

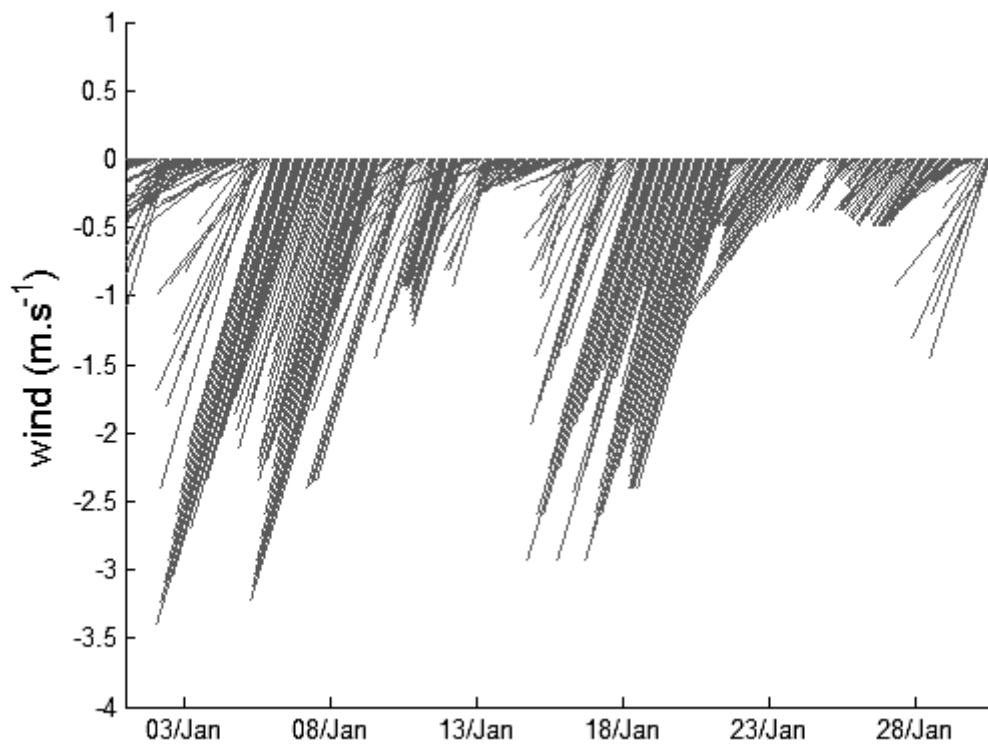


Figure 4 – Wind data obtained from the Instituto Nacional de Meteorologia INMET. Data during January 2008 at Caravelas station, code INMET A405, and coordinates (Lat. 17°43'48.0" S; Long. 39°15'00.0" W).

Figure 5

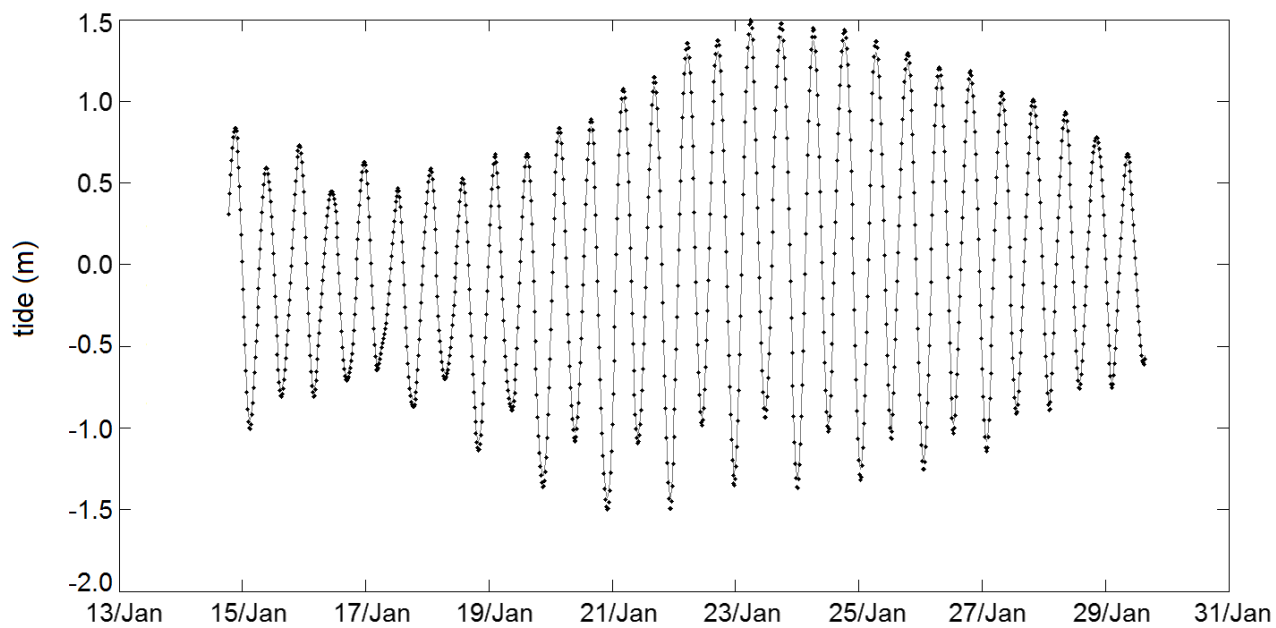


Figure 5 – Modelled water column (m) at station A compared to measured tides, from 14<sup>th</sup> to 29<sup>th</sup> of January 2008. Dots denote observations, and line denotes model result.

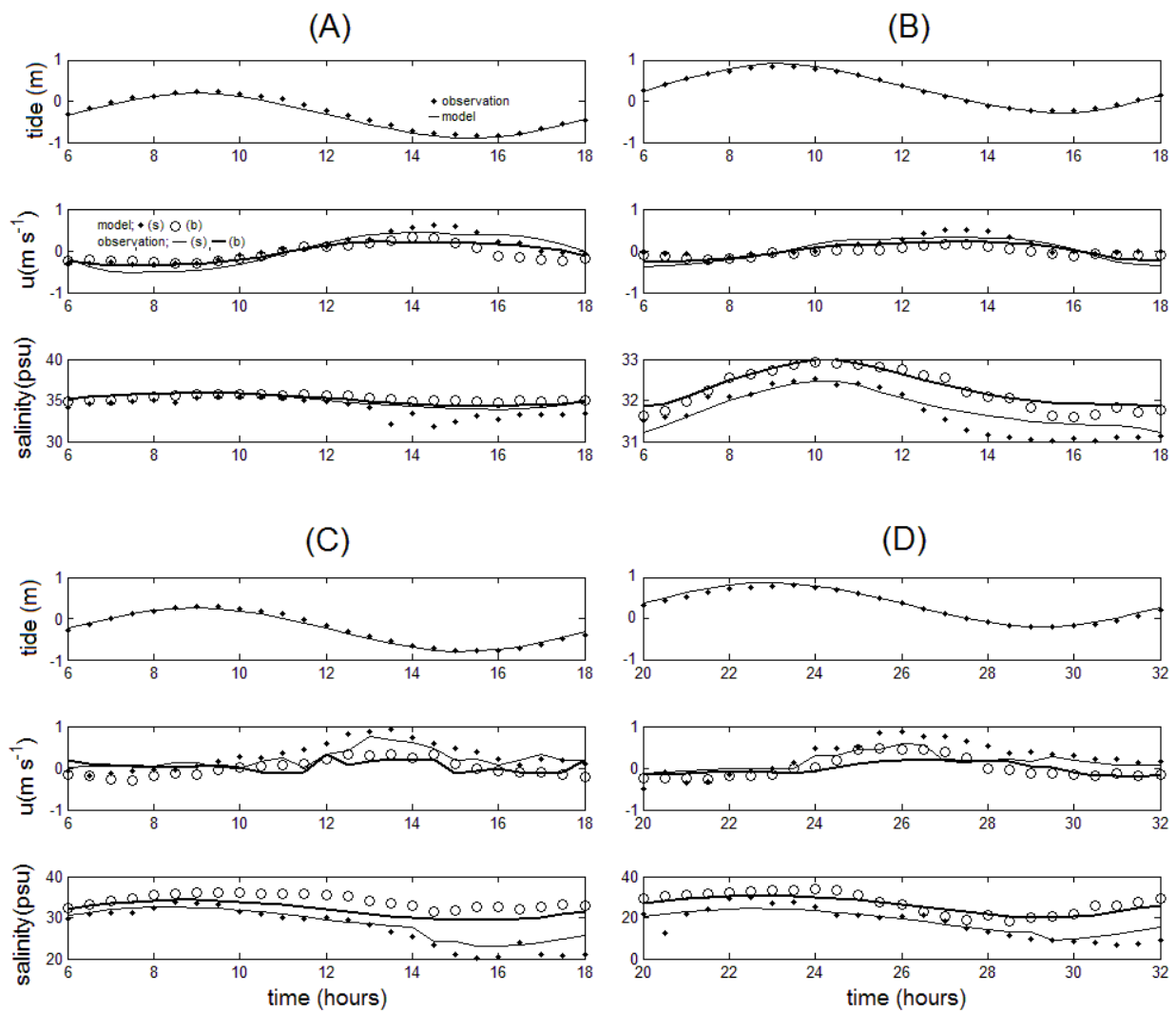


Figure 6 – Modelled tide (m), axial channel velocity  $u$  ( $\text{m s}^{-1}$ ) and salinity (psu) compared to measured time series at stations A, B, C, and D, during neap tides. Measurements and simulation represented at the surface and bottom layers. Skill values are synthesised in Table 4.

Figure 7

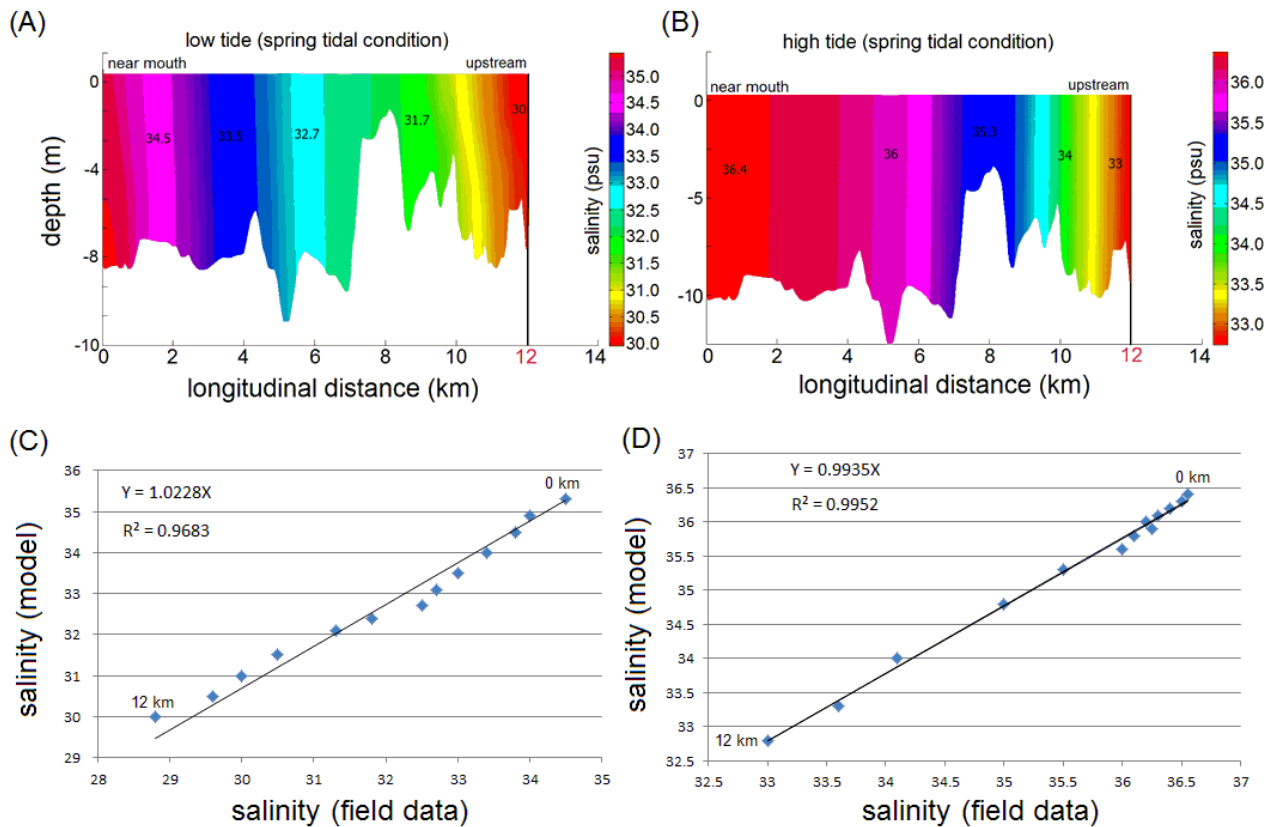


Figure 7 – Axial distribution of salinity ( ) in the Caravelas Estuary in spring tidal conditions, at low (A) and high (B) tide. Correlation of axial distribution of the mean water column salinity between model and observation at low (C) and high (D) tide in spring tide, where Y and X denote model results and measurement, respectively. First dot on left denotes position at estuarine mouth (0 km), while last dot denotes a position 12 km further upstream, the increment of 1 km is applied from first to last dot. Observations obtained from Schettini and Miranda (2010).

Figure 8

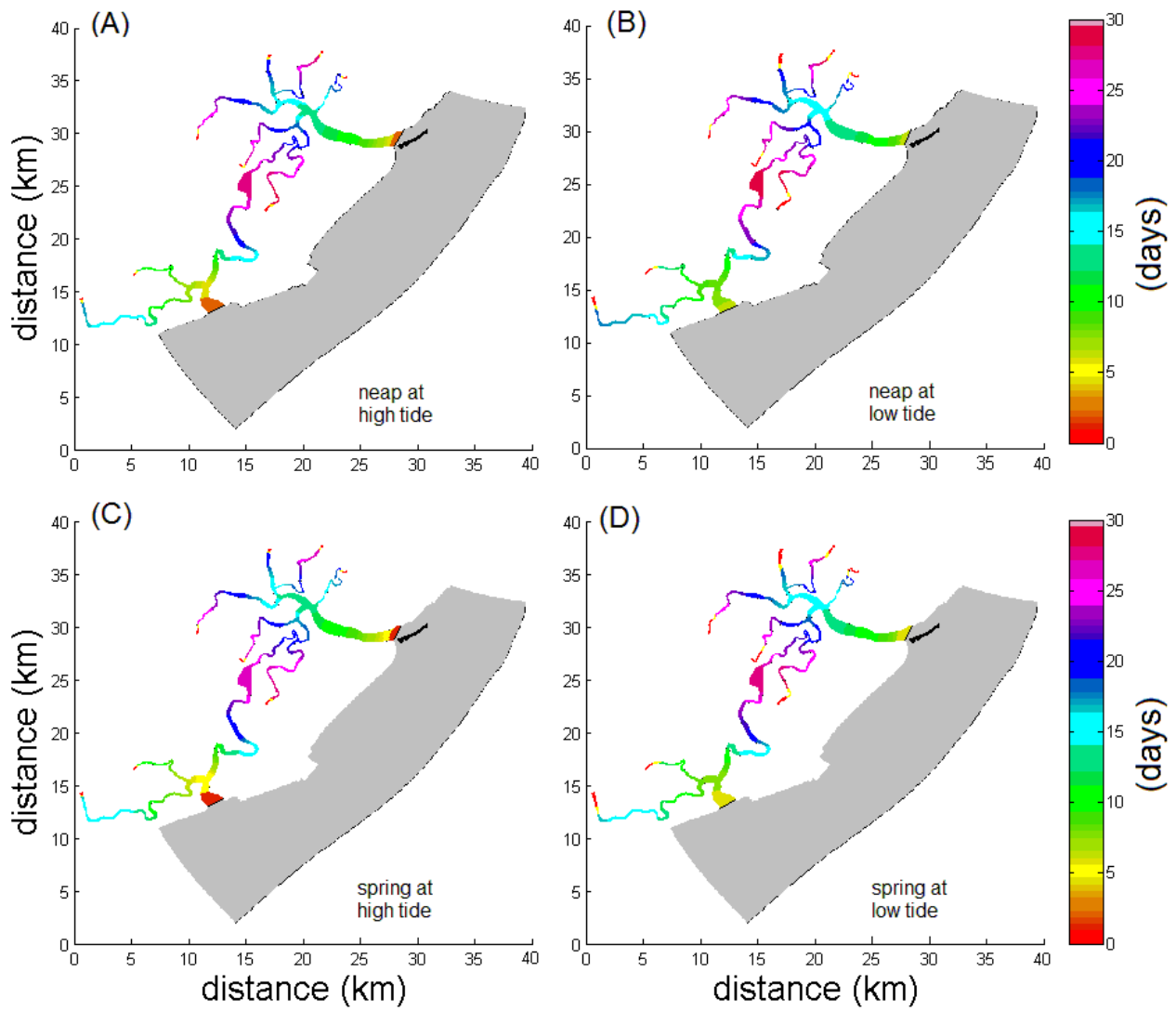


Figure 8 – Verically averaged residence time spatial distribution ( $\varphi$ ), for scenarios  $S_1$  (A),  $S_2$  (B),  $S_3$  (B) and  $S_4$  (C). Colored bar indicates the timescales in days.

Figure 9

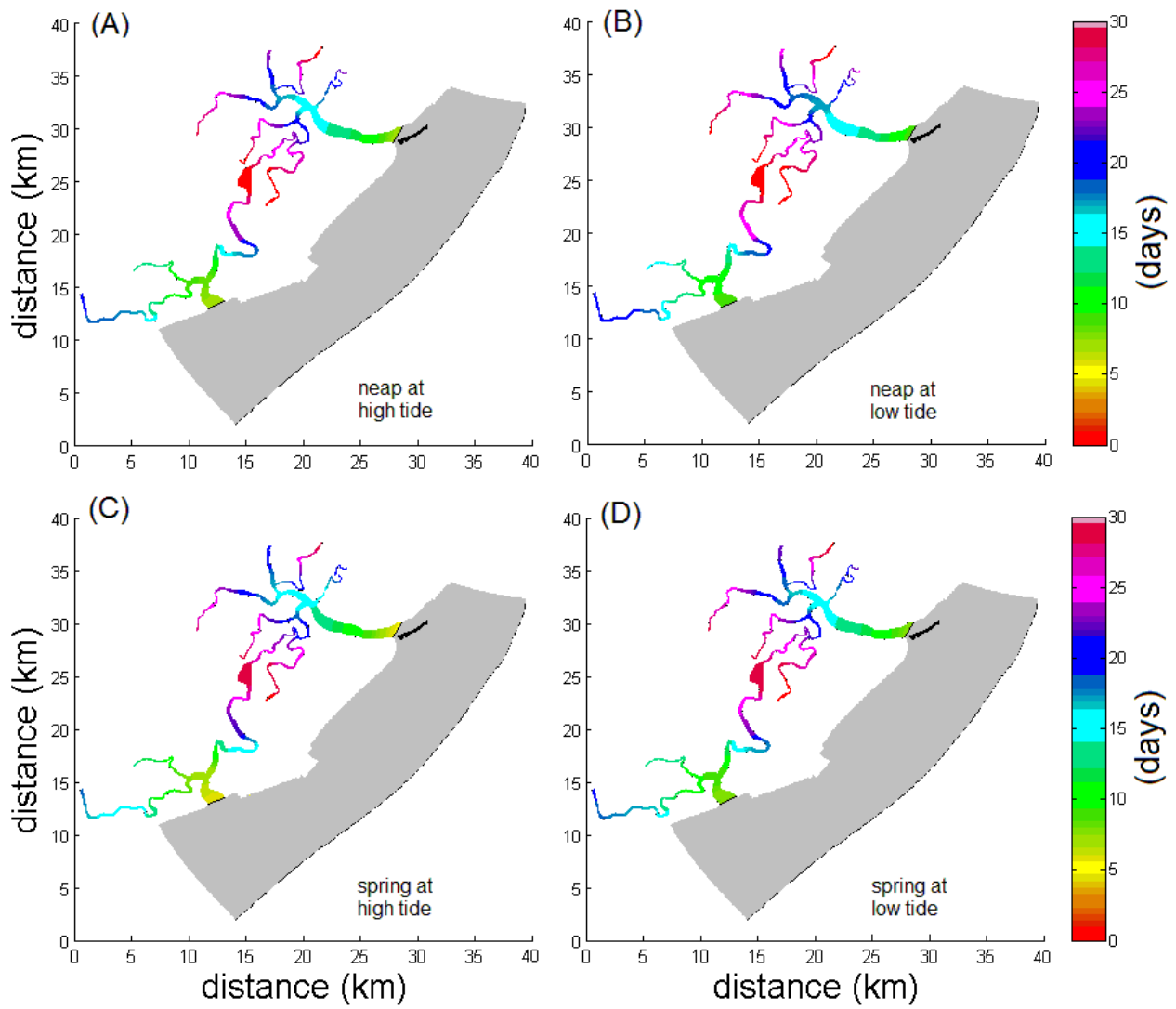


Figure 9 – Vertically averaged exposure time spatial distribution ( $\Theta$ ), for scenarios  $S_1$  (A),  $S_2$  (B),  $S_3$  (B) and  $S_4$  (C). Colored bar indicates the timescales in days.



Figure 10

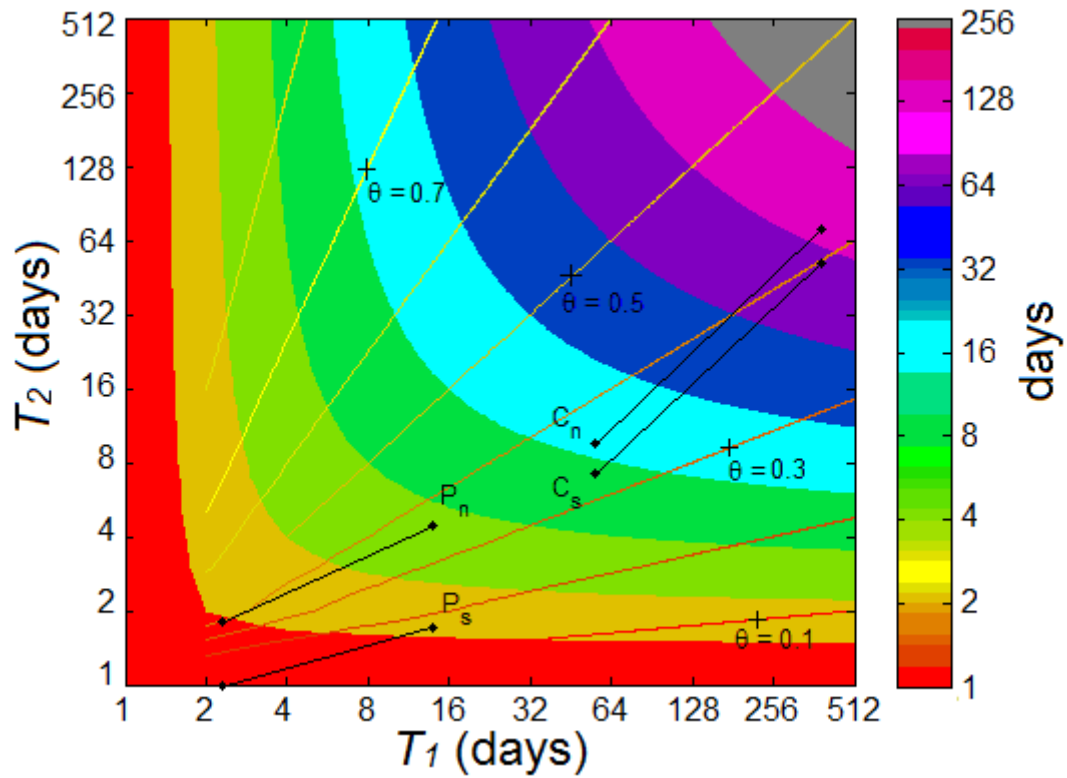


Figure 10 – The position of Caravelas (CA) and Peruípe (P) estuaries on the advection-diffusion diagram to indicate the relative contribution to the water renewal  $T_P$  by the advective ( $T_1$ ) and dispersive ( $T_2$ ) timescales using a logarithmic scale. Subscript (n) and (s) indicate neap and spring tide conditions.

Figure 11

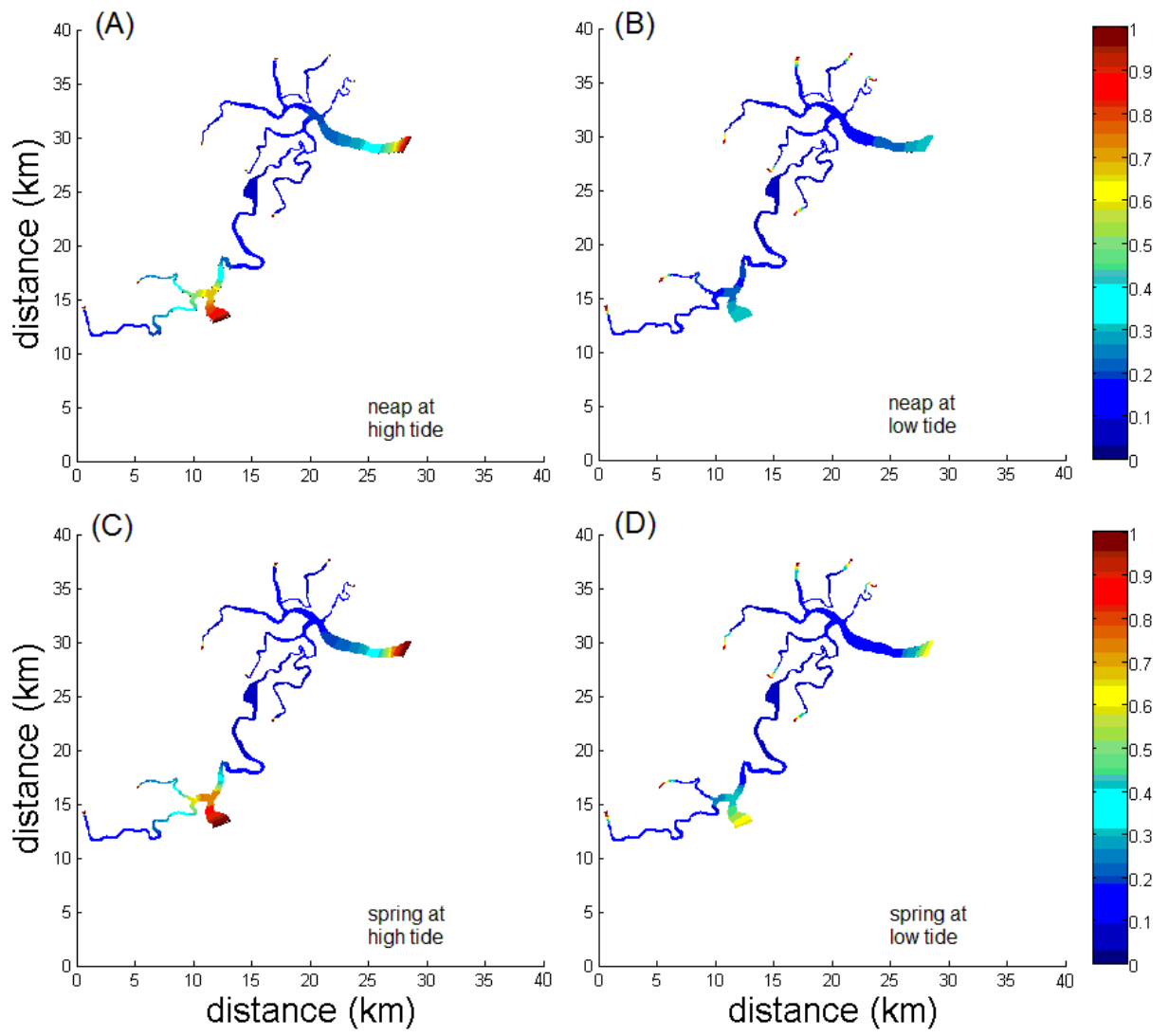


Figure 11 – Return coefficient spatial distribution ( $r$ ), for scenarios  $S_1$  (A),  $S_2$  (B),  $S_3$  (B) and  $S_4$  (C). Colored bar indicates the timescales in days.

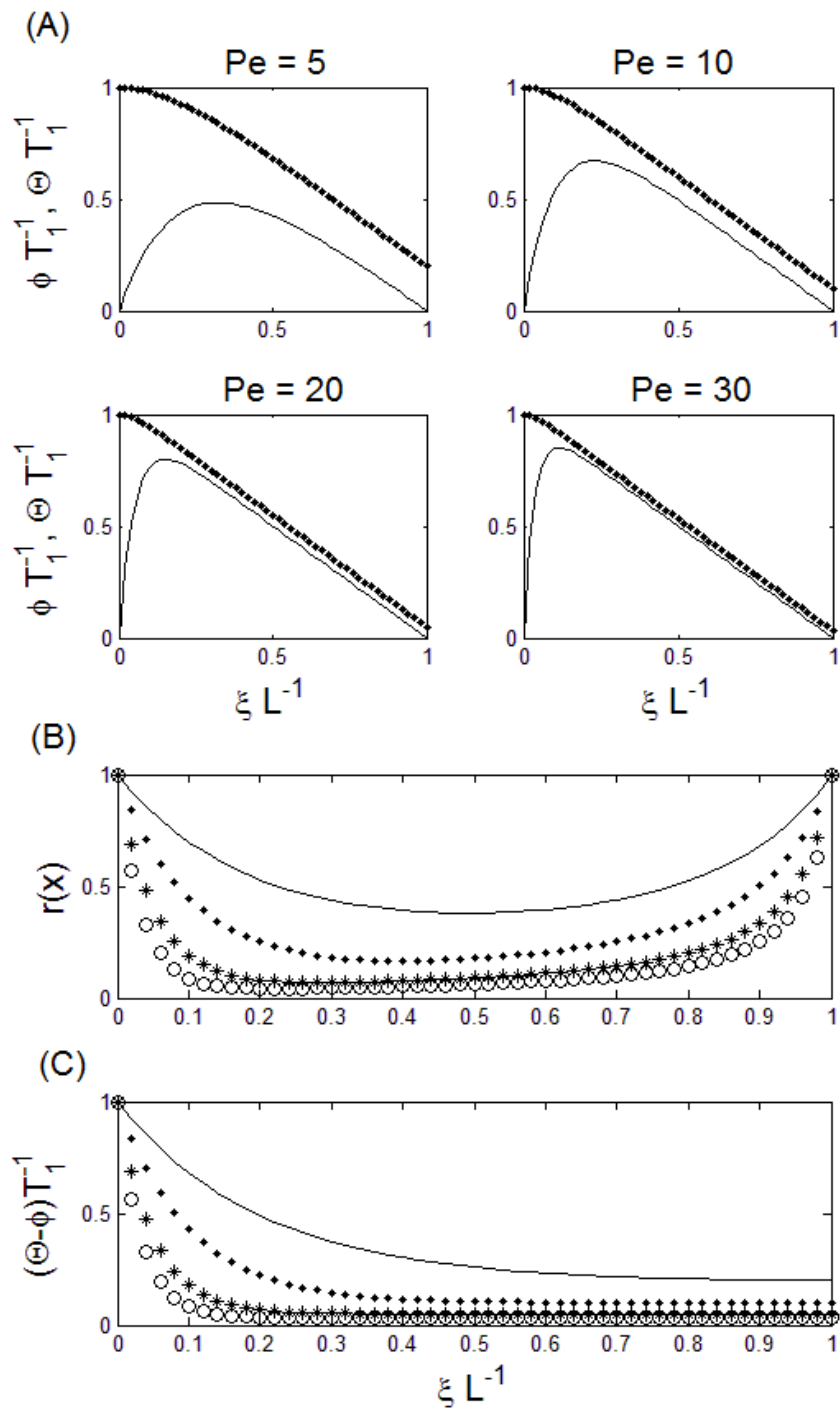


Figure 12 – (A) Representation of the exposure time  $\Theta$  (dots) and residence time  $\phi$  (line) as a function of the distance  $x$  from the upstream boundary of the domain. (B) Return coefficient and (C) and the difference between the exposure and residence time  $(\Theta - \phi)$  calculated for different values of Peclet number,  $Pe = 5$  (line),  $Pe = 10$  (dot),  $Pe = 20$  (star), and  $Pe = 30$  (circle). The timescales are normalised by means of the advective timescale  $T_1$ .

Table 1 – Summary of flow conditions in the simulations for the Peruípe, Cupído, and Jaburuna rivers. Data from ANA.

river	flow ( $\text{m}^3 \text{s}^{-1}$ )	typical range of flow ( $\text{m}^3 \text{s}^{-1}$ )	Salinity applied to
	January 2008	in wet season	boundary cells
Peruípe	~5-20	17 to 70	0
Cupído	2	2 to 9	6
Jaburuna	2		4

Table 2 – Amplitude and frequency of the main tidal components recorded at Terminal Aracruz - TA.

Component	Amplitude (cm)	Frequency (degree hr <sup>-1</sup> )
O <sub>1</sub>	8.89	13.94
K <sub>1</sub>	5.76	15.04
P <sub>1</sub>	1.91	14.96
Q <sub>1</sub>	1.62	13.40
M <sub>2</sub>	75.10	28.98
S <sub>2</sub>	33.48	30.00
L <sub>2</sub>	15.06	29.53
N <sub>2</sub>	13.45	28.44
K <sub>2</sub>	9.11	30.08

Table 3 – Sensitivity analysis of the salinity to the value of the horizontal diffusivity  $K_h$  using the Skill method from Wilmott (1981). Skill values are in the range 0 to 1. The factor  $f$  was used in the sensitivity analyses following formulae by Okubo (1971).

Parameter	Site A (Skill)	Site B (Skill)	Site C (Skill)	Site D (Skill)
<b><math>f = 2</math></b>				
Salinity (neap)	0.78	0.58	0.55	0.70
Salinity (spring)	0.85	0.62	0.60	0.75
<b><math>f = 100</math></b>				
Salinity (neap)	0.86	0.72	0.68	0.74
Salinity (spring)	0.90	0.76	0.75	0.82
<b><math>f = 150</math></b>				
Salinity (neap)	0.80	0.76	0.64	0.72
Salinity (spring)	0.95	0.80	0.80	0.88
<b><math>f = 200</math></b>				
Salinity (neap)	0.85	0.80	0.73	0.78
Salinity (spring)	0.97	0.85	0.83	0.93
<b><math>f = 250</math></b>				
Salinity (neap)	0.81	0.77	0.72	0.74
Salinity (spring)	0.94	0.81	0.78	0.89
<b><math>f = 400</math></b>				
Salinity (neap)	0.81	0.74	0.66	0.65
Salinity (spring)	0.85	0.78	0.70	0.79
<b><math>f = 2000</math></b>				
Salinity (neap)	0.64	0.56	0.50	0.60
Salinity (spring)	0.66	0.60	0.54	0.65

Table 4 – Results of the validation using the Skill method from Wilmott (1981).

Parameter	Site A (Skill)	Site B (Skill)	Site C (Skill)	Site D (Skill)
Tidal height (neap)	0.99	1	0.99	0.99
Tidal height (spring)	1	0.99	1	0.98
Velocity (neap)	0.68	0.65	0.62	0.65
Velocity (spring)	0.77	0.93	0.84	0.88
Salinity (neap)	0.85	0.80	0.73	0.78
Salinity (spring)	0.97	0.85	0.83	0.93
Parameter	Site A (Skill)	Site B (Skill)		
Velocity (14 <sup>th</sup> to 26 <sup>th</sup> Jan 2008)	0.72	0.78		





