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**DOI**

[10.1016/j.jcp.2020.109286](https://doi.org/10.1016/j.jcp.2020.109286)

**Publication date**

2020

**Document Version**

Final published version

**Published in**

Journal of Computational Physics

**Citation (APA)**

He, X., & Vuik, C. (2020). Efficient and robust Schur complement approximations in the augmented Lagrangian preconditioner for the incompressible laminar flows. *Journal of Computational Physics*, 408, Article 109286. <https://doi.org/10.1016/j.jcp.2020.109286>

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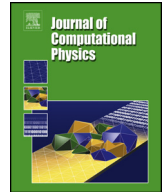
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# Efficient and robust Schur complement approximations in the augmented Lagrangian preconditioner for the incompressible laminar flows

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## ARTICLE INFO

### Article history:

Received 12 November 2018

Received in revised form 17 January 2020

Accepted 25 January 2020

Available online 7 February 2020

### Keywords:

Navier-Stokes equations

Stabilized finite element method

Block structured preconditioners

Schur complement approximations

Augmented Lagrangian preconditioner

## ABSTRACT

This paper introduces three new Schur complement approximations for the augmented Lagrangian preconditioner. The incompressible Navier-Stokes equations discretized by a stabilized finite element method are utilized to evaluate these new approximations of the Schur complement. A wide range of numerical experiments in the laminar context determines the most efficient Schur complement approximation and investigates the effect of the Reynolds number, mesh anisotropy and refinement on the optimal choice. Furthermore, the advantage over the traditional Schur complement approximation is exhibited.

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## 1. Introduction

In this paper we consider the numerical solution of the steady, laminar and incompressible Navier-Stokes equations as follows

$$\begin{aligned} -\nu \Delta \mathbf{u} + (\mathbf{u} \cdot \nabla) \mathbf{u} + \nabla p &= \mathbf{f} \quad \text{on } \Omega, \\ \nabla \cdot \mathbf{u} &= 0 \quad \text{on } \Omega. \end{aligned} \quad (1)$$

Here  $\mathbf{u}$  is the velocity,  $p$  is the pressure, the positive coefficient  $\nu$  is the kinematic viscosity and  $\mathbf{f}$  is a given force field.  $\Omega$  is a 2D or 3D bounded and connected domain with the boundary  $\partial\Omega$ . On the boundaries of the computational domain, either the Dirichlet boundary condition  $\mathbf{u} = \mathbf{g}$  or Neumann boundary condition  $\nu \frac{\partial \mathbf{u}}{\partial \mathbf{n}} - \mathbf{n}p = 0$  is imposed, where  $\mathbf{n}$  denotes the outward-pointing unit normal to the boundary.

After the Picard linearization and FEM discretization [1], the incompressible Navier-Stokes equations convert to the following linear system in saddle-point form

$$\begin{bmatrix} A & B^T \\ B & -C \end{bmatrix} \begin{bmatrix} \mathbf{u} \\ p \end{bmatrix} = \begin{bmatrix} \mathbf{f} \\ g \end{bmatrix} \quad \text{with } \mathcal{A} := \begin{bmatrix} A & B^T \\ B & -C \end{bmatrix}, \quad (2)$$

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where the matrices  $B$  and  $B^T$  correspond to the divergence and gradient operators, respectively. Picard linearization leads to the matrix  $A$  in block diagonal structure, and each diagonal block corresponds to the convection-diffusion operator. Due to the presence of the convective term,  $A$  is not symmetric. For the finite element discretization satisfying the LBB ('inf-sup') stability condition [1], no pressure stabilization is required and  $C = 0$  is taken. When LBB unstable finite elements are applied, the nonzero matrix  $C$  corresponds to a stabilization operator.

Block structured preconditioners [1–3] are often utilized to accelerate the convergence of the Krylov subspace solvers for saddle point systems as (2). They are based on the block  $\mathcal{LDU}$  decomposition of the coefficient matrix given by

$$\mathcal{A} = \mathcal{LDU} = \begin{bmatrix} A & B^T \\ B & -C \end{bmatrix} = \begin{bmatrix} I_1 & O \\ BA^{-1} & I_2 \end{bmatrix} \begin{bmatrix} A & O \\ O & S \end{bmatrix} \begin{bmatrix} I_1 & A^{-1}B^T \\ O & I_2 \end{bmatrix}, \quad (3)$$

where  $S = -(C + BA^{-1}B^T)$  is the so-called Schur complement. A combination of this block factorization with a suitable approximation of the Schur complement is utilized to successfully design the block structured preconditioners, which are given as follows

$$\mathcal{P}_F = \begin{bmatrix} A & O \\ B & \tilde{S} \end{bmatrix} \begin{bmatrix} I_1 & \tilde{A}^{-1}B^T \\ O & I_2 \end{bmatrix}, \quad (4)$$

$$\mathcal{P}_L = \begin{bmatrix} A & O \\ B & \tilde{S} \end{bmatrix}, \quad \mathcal{P}_U = \begin{bmatrix} A & B^T \\ O & \tilde{S} \end{bmatrix}. \quad (5)$$

Multiplying the  $\mathcal{LD}$  and  $\mathcal{DU}$  factors of (3) results in the block lower- and upper-triangular preconditioners  $\mathcal{P}_L$  and  $\mathcal{P}_U$ , respectively. Preconditioner  $\mathcal{P}_F$  is based on the multiplication of the  $\mathcal{LDU}$  factors. The term  $\tilde{A}^{-1}$  denotes some approximation of the inverse action of  $A$ , which is given either in an explicit form or implicitly defined via an iterative solution method with a proper stopping tolerance.

It is not practical to explicitly form the exact Schur complement due to the action of  $A^{-1}$ , typically when the size is large. This implies that the most challenging task is to find the spectrally equivalent and numerically cheap approximation of the Schur complement, which is denoted by  $\tilde{S}$  in (4) and (5). There exist several state-of-the-art approximations of the Schur complement, e.g. the least-square commutator (LSC) [4,5], pressure convection-diffusion (PCD) operator [6,7] and the approximations from the SIMPLE(R) [8–10] and augmented Lagrangian (AL) preconditioner [11,12] etc. Among them, the AL preconditioner exhibits attractive features with stable finite element methods (FEM) used for the discretization, e.g. the purely algebraic and simple construction of the Schur complement approximation and robustness with respect to the mesh refinement and Reynolds number, at least for academic benchmarks. Motivated by these advantages, the further extension to the context of finite volume method (FVM) [13] and the modified variant [14] with reduced computational complexities are promoted. Recently, the authors of this paper propose a new variant of the AL preconditioner [15] for the Reynolds-Averaged Navier-Stokes (RANS) equations discretized by a stabilized FVM, which are widely used to model turbulent flows in industrial computational fluid dynamic (CFD) applications.

The role of the AL term for preconditioning is very simple: by varying parameter  $\gamma$  it puts more weight on either the (1,1) or the (2,2) block of the AL preconditioner. If one cannot afford larger values of  $\gamma$ , then finding a suitable (more complicated) preconditioner for  $S_\gamma$  becomes important again, where  $S_\gamma$  denotes the Schur complement for the augmented system. More discussions on  $S_\gamma$  and the involved parameter  $\gamma$  are given in Section 3 of this paper. Known representations for  $S_\gamma$  [11,14] suggest ways to utilize earlier developed preconditioners for the non-augmented problem. The paper is built on this simple observation and the original idea as given in [11]. This observation is already exploited, for example, in [14,16]. The challenges encountered in the turbulent calculations [17–19] are inevitable factors which could cause the breakdown of the AL preconditioner, including the high Reynolds number, high-aspect ratio cells near the very thin boundary layer and the significant variation in the value of viscosity due to the presence of the eddy-viscosity. To overcome these challenges, an alternative method to approximate the Schur complement for the AL preconditioner is introduced in [15], which leads to a new variant of the AL preconditioner. This new method approximates the Schur complement through its inverse form and facilitates the utilization of the existing Schur complement approximations. Among the available candidates, the Schur complement approximation from the SIMPLE preconditioner [8,20] is chosen and substituted into the inverse Schur complement approximation for the AL preconditioner. This choice is motivated from the notion that it reduces to a scaled Laplacian matrix [8,20] with the considered FVM and its promising efficiency on the turbulent applications of the maritime industry [8,21]. Consequently, the so-arising new variant of the AL preconditioner reduces the number of Krylov subspace iterations by a factor up to 36 compared to the original one [15].

Since the new method to approximate the Schur complement for the AL preconditioner use the existing Schur complement approximations, the following questions straightforwardly raise. Does the utilization of other existing Schur complement approximations deliver a better performance than that from the SIMPLE preconditioner? If so, which Schur complement approximation is the most efficient one? Does the optimal choice depend on the test problem and parameters arising from the physics and discretization, e.g. the Reynolds number and grid size? To answer these questions, in this paper we utilize the existing Schur complement approximations not only from the SIMPLE preconditioner but also from the LSC and PCD operators to construct the new Schur complement approximation in the AL preconditioner. Moreover, extensive comparisons between the considered Schur complement approximations are carried out on a wide range of numerical experiments to evaluate the effect of the Reynolds number, mesh anisotropy and refinement on the optimal choice.

These numerical evaluations are considered in the context of laminar flows, which is motivated by the expectation that the obtained results can provide a fundamental guideline for the more complicated turbulent flow calculations.

The structure of this paper is given as follows. The utilized stabilization method and a brief survey of the existing approximations of the Schur complement are introduced in Section 2. Section 3 illustrates the method using these existing Schur complement approximations to construct the new approximation of the Schur complement in the AL preconditioner. Section 4 includes numerical results on varying laminar benchmarks. Conclusions and future work are outlined in Section 5.

## 2. Stabilization method and survey of Schur complement approximations

### 2.1. Stabilization

In this paper we use the mixed FEM which does not uniformly satisfy a discrete inf-sup condition [1] to discretize the Navier-Stokes equations governing laminar flows, which is chosen by the following considerations. Firstly, the existing Schur complement approximations are originally designed with finite element methods used for discretization. Therefore, it is expected to apply the new Schur complement approximation for the AL preconditioner in the FEM context. In addition, this closes a gap in the application of the new Schur complement approximation. Secondly, both the stabilized FEM [1] and FVM [17] lead to saddle point system with a nonzero (2,2) block which arises from the pressure stabilization. Thanks to this similarity, a minor adaption is required to extend the new variant of the AL preconditioner from the stabilized FVM to the stabilized FEM. Finally, the utilization of stabilized FVM degrades the generality to some extent since the Schur complement approximation in the SIMPLE preconditioner reduces to a special formation [8,20]. However, this special formation can not be obtained with other stabilization and discretization methods. Using stabilized FEM, all Schur complement approximations considered in this paper are expressed in their defined manners, including that from the SIMPLE preconditioner. In this way, a convincing evaluation of the novel Schur complement approximation for the AL preconditioner can be expected.

Based on the above motivations, in this paper we use the  $Q_1$ - $Q_1$  mixed finite element approximation where the equal first-order discrete velocities and pressure are specified on a common set of nodes. Among the available stabilization methods [22–27] specified for the  $Q_1$ - $Q_1$  discretization, we choose the approach introduced in [25]. The main motivation is that there are few stabilization parameters required in the following operator

$$C^{(proj)}(p_h, q_h) = \frac{1}{\nu}(p_h - \Pi_0 p_h, q_h - \Pi_0 q_h), \quad (6)$$

where  $\Pi_0$  is the  $L^2$  projection from the pressure approximation space into the space  $P_0$  of the piecewise constant basis function. This projection is defined locally:  $\Pi_0 p_h$  is a constant function in each element  $\square_k \in T_h$ . It is determined simply by the following local averaging

$$\Pi_0 p_h|_{\square_k} = \frac{1}{|\square_k|} \int_{\square_k} p_h, \quad \text{for all } \square_k \in T_h, \quad (7)$$

where  $|\square_k|$  is the area of element  $k$ . Due to the locality as illustrated by equation (7), the stabilization matrix  $C$  can be assembled from the contribution matrices on macroelements in the same way as assembling a standard finite element mass matrix. Taking the 2D rectangular grid as an example, the  $4 \times 4$  macroelement contribution matrix  $C^{(macro)}$  is given by

$$C^{(macro)} = \frac{1}{\nu}(M^{(macro)} - qq^T|\square_k|), \quad (8)$$

where  $M^{(macro)}$  is the  $4 \times 4$  macroelement mass matrix for the bilinear discretization and  $q = [1/4, 1/4, 1/4, 1/4]^T$  is the local averaging operator. The null space of the macroelement matrix  $C^{(macro)}$  and assembled stabilization matrix  $C$  consist of constant vector, see [1,25] for more details.

Contrary to other pressure stabilization methods [27,28] which utilize the viscosity and velocity fields to derive the scaling parameter in front of the stabilization matrix, the alternative employed in this paper only involves the viscosity coefficient. Results in numerical experiment section demonstrate that the utilized stabilization method results in a reasonable and smooth calculation of the velocity and pressure unknowns ranging from the moderate to large Reynolds numbers. The assessment of other pressure stabilization methods and their effects on the proposed preconditioning techniques by this paper is included in future research plan.

### 2.2. Survey of Schur complement approximations

As follows we briefly introduce several state-of-the-art Schur complement approximations which are utilized to construct the new approximation of the Schur complement for the AL preconditioner. We refer for more details of the Schur complement approximation to the surveys [2,3,29,30] and the books [1,31].

In the following illustration, we use the notation  $p$  to indicate the operators defined on the pressure space and the notation  $u$  for the operators defined on the velocity space.

(1) **The pressure convection-diffusion operator  $\tilde{S}_{PCD}$ .**

This approximation, denoted by  $\tilde{S}_{PCD}$ , is proposed by Kay et al. [6] and defined as

$$\tilde{S}_{PCD} = -L_p A_p^{-1} M_p, \quad (9)$$

where  $M_p$  is the pressure mass matrix, and  $A_p$  and  $L_p$  are the discrete pressure convection-diffusion and Laplacian operators, respectively. Although the PCD Schur complement approximation (9) is originally proposed for stable finite element methods, it is straightforwardly applicable for the discretizations needing a stabilization term, e.g. the  $Q_1$ - $Q_1$  pair. For more details about this extension we refer to [1]. On the other hand, this approximation requires users to provide the discrete operators  $A_p$  and  $L_p$  and preset some artificial pressure boundary conditions on them. The boundary conditions could strongly effect the performance so appropriate ones should be carefully selected based on the problem characteristic [32,33]. Applying the PCD Schur complement approximation involves the action of a Poisson solve, a mass matrix solve and a matrix-vector product with the matrix  $A_p$ .

(2) **The least-square commutator  $\tilde{S}_{LSC}$ .**

Elman et al. [4] originally propose this method for stable finite element discretizations and then extend it to alternatives [5] that require stabilization. For system (2) with a nonzero stabilization operator  $C$ , the LSC Schur complement approximation  $\tilde{S}_{LSC}$  is defined as

$$\tilde{S}_{LSC} = -(B\hat{M}_u^{-1}B^T + C_1)(B\hat{M}_u^{-1}A\hat{M}_u^{-1}B^T + C_2)^{-1}(B\hat{M}_u^{-1}B^T + C_1), \quad (10)$$

where  $\hat{M}_u$  denotes the diagonal approximation of the velocity mass matrix  $M_u$ , i.e.  $\hat{M}_u = \text{diag}(M_u)$ . Given the stabilization matrix  $C$  assembled from the macroelement contribution matrix  $C^{(macro)}$  (8), the contribution matrices  $C_1^{(macro)}$  and  $C_2^{(macro)}$  for the associated stabilization matrices  $C_1$  and  $C_2$  are introduced by

$$C_1^{(macro)} = \frac{\nu}{|\square_k|} \cdot C^{(macro)}, \quad C_2^{(macro)} = \frac{\nu^2}{|\square_k|^2} \cdot C^{(macro)}, \quad (11)$$

where  $\nu$  denotes the viscosity parameter. For the derivation of  $C_1^{(macro)}$  and  $C_2^{(macro)}$  we refer to [5]. The implementation of the LSC Schur complement approximation does not require any artificial boundary condition and consists of one matrix-vector product with the middle term in (10) and two solves with the other term. When the LSC Schur complement approximation is applied to stable finite element discretizations, the matrices  $C_1$  and  $C_2$  are set to zero in (10).

(3) **The approximation  $\tilde{S}_{SIMPLE}$  from the SIMPLE preconditioner.**

SIMPLE (Semi-Implicit Pressure Linked Equation) is used by Patanker [18] as an iterative method to solve the Navier-Stokes problem. The scheme belongs to the class of basic iterative methods and exhibits slow convergence. Vuik et al. [9,10] use SIMPLE as a preconditioner in a Krylov subspace method, achieving in this way, a much faster convergence. Regarding the Schur complement  $S = -(C + BA^{-1}B^T)$  of system (2), the SIMPLE preconditioner approximates  $A$  by its diagonal, i.e.  $\text{diag}(A)$ , and obtains the approximation  $\tilde{S}_{SIMPLE}$  as

$$\tilde{S}_{SIMPLE} = -(C + B\text{diag}(A)^{-1}B^T). \quad (12)$$

Substituting  $\tilde{S}_{SIMPLE}$  and  $\tilde{A}^{-1} = \text{diag}(A)^{-1}$  into (4) leads to the so-called SIMPLE preconditioner. For stable finite element discretizations,  $C = 0$  is set in system (2) and correspondingly in the Schur complement approximation (12). The easy implementation and promising performance on the complicated maritime problems [8,21] make the SIMPLE preconditioner and its variants attractive in real world applications.

The main goal of this paper is to utilize the above mentioned Schur complement approximations to construct a new approximation of the Schur complement in the AL preconditioner, with more details presented in the next section. Theoretical analysis and numerical evaluation of the above Schur complement approximations fall out of the scope of this work and we refer to [1,3,34] for more results. Here we summarize the key differences.  $\tilde{S}_{PCD}$  requires the construction of additional matrices on the pressure space while  $\tilde{S}_{LSC}$  and  $\tilde{S}_{SIMPLE}$  rely on matrices which could be easily generated or are readily available. As seen from  $\tilde{S}_{LSC}$ , the stabilization terms  $C_1^{(macro)}$  and  $C_2^{(macro)}$  are easily obtained by substituting the available term  $C^{(macro)}$  into (11). On the other hand,  $\tilde{S}_{PCD}$  easily extends to the stabilized elements and a minor adaption is required by  $\tilde{S}_{SIMPLE}$  for this extension. However,  $\tilde{S}_{LSC}$  does not immediately apply and needs appropriate stabilization terms  $C_1$  and  $C_2$ . We further note that boundary conditions for the pressure unknowns, which have few physical meanings, have to be considered for  $L_p$  and  $A_p$  in  $\tilde{S}_{PCD}$ . What boundary conditions work best with a specific type of problem is usually based on experimental knowledge [32,33].

### 3. Augmented Lagrangian preconditioner

The focus of this section is the new method to approximate the Schur complement in the augmented Lagrangian (AL) preconditioner. In the following, we first briefly recall the AL preconditioner and then introduce the new method followed by a comparison with the old one.

The motivation of applying the AL preconditioner is to circumvent the challenge on finding the efficient approximation of the Schur complement  $S$  for the original system (2), cf., [11,14]. To apply the AL preconditioner, the original system (2) is transformed into an equivalent one with the same solution [13,14], which is of the form

$$\begin{bmatrix} A_\gamma & B_\gamma^T \\ B & -C \end{bmatrix} \begin{bmatrix} \mathbf{u} \\ p \end{bmatrix} = \begin{bmatrix} \mathbf{f}_\gamma \\ g \end{bmatrix} \quad \text{with } \mathcal{A}_\gamma := \begin{bmatrix} A_\gamma & B_\gamma^T \\ B & -C \end{bmatrix}, \quad (13)$$

where  $A_\gamma = A + \gamma B^T W^{-1} B$ ,  $B_\gamma^T = B^T - \gamma B^T W^{-1} C$  and  $\mathbf{f}_\gamma = \mathbf{f} + \gamma B^T W^{-1} g$ . This transformation is obtained by multiplying  $\gamma B^T W^{-1}$  on both sides of the second row of system (2) and adding the resulting equation to the first one. Clearly, the transformed system (13) has the same solution as system (2) for any value of  $\gamma$  and any non-singular matrix  $W$ . The Schur complement of the transformed system (13) is  $S_\gamma = -(C + B A_\gamma^{-1} B_\gamma^T)$ .

The AL preconditioner is applied for the equivalent system (13), which is to be solved. Using the block  $\mathcal{DU}$  decomposition of  $\mathcal{A}_\gamma$ , the ideal AL preconditioner  $\mathcal{P}_{IAL}$  and its variant, i.e. the modified AL preconditioner  $\mathcal{P}_{MAL}$ , are given by

$$\mathcal{P}_{IAL} = \begin{bmatrix} A_\gamma & B_\gamma^T \\ O & \tilde{S}_\gamma \end{bmatrix} \quad \text{and} \quad \mathcal{P}_{MAL} = \begin{bmatrix} \tilde{A}_\gamma & B_\gamma^T \\ O & \tilde{S}_\gamma \end{bmatrix}, \quad (14)$$

where  $\tilde{S}_\gamma$  and  $\tilde{A}_\gamma$  denote the approximations of  $S_\gamma$  and  $A_\gamma$ , respectively.

First we consider the approximation  $\tilde{A}_\gamma$ . Given the original pivot matrix  $A = \begin{bmatrix} A_1 & O \\ O & A_1 \end{bmatrix}$  and the divergence matrix  $B = [B_1 \ B_2]$  in the 2D case, the transformed pivot matrix  $A_\gamma = A + \gamma B^T W^{-1} B$  can be written as

$$A_\gamma = \begin{bmatrix} A_1 + \gamma B_1^T W^{-1} B_1 & \gamma B_1^T W^{-1} B_2 \\ \gamma B_2^T W^{-1} B_1 & A_1 + \gamma B_2^T W^{-1} B_2 \end{bmatrix}.$$

Contrary to  $\mathcal{P}_{IAL}$ ,  $\mathcal{P}_{MAL}$  approximates  $A_\gamma$  by its block upper-triangular part, i.e.  $\tilde{A}_\gamma$  with a zero (2,1) block, such that the difficulty of solving the systems with  $A_\gamma$  is avoided [14]. When applying  $\mathcal{P}_{MAL}$  one needs to solve the sub-systems with the diagonal blocks of  $A_\gamma$ , i.e.  $A_1 + \gamma B_1^T W^{-1} B_1$  and  $A_1 + \gamma B_2^T W^{-1} B_2$ , which do not contain the coupling between two components of the velocity so that standard algebraic multigrid methods can be applied [34]. This advantage motivates us to choose  $\mathcal{P}_{MAL}$  in this paper despite the observation that the performance of  $\mathcal{P}_{MAL}$  is dependent of the values of  $\gamma$ , which is seen in the numerical experiments of this paper and other related references [14]. The above advantage also motives to approximate  $A_\gamma$  by its block lower-triangular part with a zero (1,2) block. Numerical experiments demonstrate that different approximations of  $A_\gamma$  slightly effect the performance of the modified AL preconditioner for the considered benchmarks. For this reason, in this paper we only illustrate the results by applying the block upper-triangular approximation of  $A_\gamma$  in the modified AL preconditioner. Regarding the ideal AL preconditioner  $\mathcal{P}_{IAL}$ , standard multigrid methods are ineffective to solve the systems with  $A_\gamma$ . A specialized multigrid algorithm for  $A_\gamma$  is built in [11] and the extension to the three dimensional applications is recently proposed in [35]. Alternatively, previous work [12] suggests to solve the systems with  $A_\gamma$  by the Krylov subspace methods, which are accelerated by the approximate inverse preconditioner based on the Sherman-Morrison formula. In the related work [34], the comparison between the modified and ideal AL preconditioners is realized by applying the direct solution method for the involved sub-systems. Although fewer Krylov iterations are needed by the ideal AL preconditioner, removing the difficulty to solve the sub-systems with  $A_\gamma$  makes the modified AL preconditioner attractive in practice.

### 3.1. New Schur approximation in the AL preconditioner

Finding an effective approximation of the Schur complement  $S_\gamma$  is the key for the ideal and modified AL preconditioners. This paper is meant to use the available Schur approximations for the original system (2), as introduced in Section 2, to construct a new approximation of  $S_\gamma$ . The new Schur complement approximation is realized by using the following lemma.

**Lemma 3.1.** Assuming that all the relevant matrices are invertible, then the inverse of  $S_\gamma$  is given by

$$S_\gamma^{-1} = S^{-1}(I - \gamma C W^{-1}) - \gamma W^{-1}, \quad (15)$$

where  $S = -(C + B A^{-1} B^T)$  denotes the Schur complement of the original system (2).

**Proof.** For the proof we refer to [13,14].  $\square$

Lemma 3.1 is originally revealed by [14] and used to derive the old approximation of  $S_\gamma$ , which is discussed in the next section. Here, Lemma 3.1 is viewed from another side. Since Lemma 3.1 builds the connection between the Schur complements  $S_\gamma$  and  $S$ , the natural and simple method to approximate  $S_\gamma$  is substituting the approximation of  $S$  into expression (15). In this way, the new approximation of  $S_\gamma$ , denoted by  $\tilde{S}_{\gamma \text{ new}}$ , is derived in the inverse form as



$$\tilde{S}_{\gamma \text{ new}}^{-1} = \tilde{S}^{-1}(I - \gamma C W^{-1}) - \gamma W^{-1}, \quad (16)$$

where  $\tilde{S}$  denotes the approximation of  $S$ .

The novel approach provides a framework to use the known Schur complement approximation  $\tilde{S}$  for the original system (2) to construct  $\tilde{S}_{\gamma \text{ new}}$  in the AL preconditioner, which is applied to the transformed system (13). Substituting the Schur complement approximations demonstrated in Section 2, i.e.  $\tilde{S}_{PCD}$ ,  $\tilde{S}_{LSC}$  and  $\tilde{S}_{SIMPLE}$  into expression (16), three variants of  $\tilde{S}_{\gamma \text{ new}}$  are derived as

- $\tilde{S}_{\gamma \text{ PCD}}^{-1} = \tilde{S}_{PCD}^{-1}(I - \gamma C W^{-1}) - \gamma W^{-1},$
- $\tilde{S}_{\gamma \text{ LSC}}^{-1} = \tilde{S}_{LSC}^{-1}(I - \gamma C W^{-1}) - \gamma W^{-1},$
- $\tilde{S}_{\gamma \text{ SIMPLE}}^{-1} = \tilde{S}_{SIMPLE}^{-1}(I - \gamma C W^{-1}) - \gamma W^{-1}.$

Following other related references [11,14], in this paper we choose the matrix parameter  $W$  to the diagonal approximation of the pressure mass matrix, i.e.  $W = \hat{M}_p = \text{diag}(M_p)$ . It is trivial to obtain the action of  $W^{-1}$  in the transformation (13) and the new Schur complement approximation (16). Applying the new Schur complement approximation  $\tilde{S}_{\gamma \text{ new}}$  converts to solve a system with it and the choice of  $W = \hat{M}_p$  focuses the complexity mainly on the solve of  $\tilde{S}$ . This implies a limited increase of the complexity when implementing the new Schur complement approximation  $\tilde{S}_{\gamma \text{ new}}$  compared to  $\tilde{S}$ . In addition, the considerable efforts to optimize the approximation  $\tilde{S}$  can straightforwardly reduce the computational time of  $\tilde{S}_{\gamma \text{ new}}$ .

When applying stabilized FVM, the inverse of  $S_{\gamma}$  is expressed in a similar manner [15] as Lemma 3.1 and this similarity facilitates the extension of the new Schur complement approximation from the stabilized FVM to the stabilized FEM. Regarding the new Schur complement approximation, there are two main differences between [15] and this work. Firstly, only  $\tilde{S}_{\gamma \text{ SIMPLE}}$  is considered in [15] and in this paper we introduce three variants, i.e.  $\tilde{S}_{\gamma \text{ PCD}}$ ,  $\tilde{S}_{\gamma \text{ LSC}}$  and  $\tilde{S}_{\gamma \text{ SIMPLE}}$ . In this way, the comparison between them is expected to answer the questions raised in the introduction section and find out the optimal choice. Secondly, in [15] finite volume discretization stabilized by the pressure-weighted interpolation method [36] is applied, which leads to  $\tilde{S}_{SIMPLE}$  in a reduced form. The generality is degraded since this special form of  $\tilde{S}_{SIMPLE}$  can not be obtained by using other stabilization and discretization methods in general. In this paper, the approximations  $\tilde{S}_{PCD}$ ,  $\tilde{S}_{LSC}$  and  $\tilde{S}_{SIMPLE}$  are expressed in their defined manners so that a convincing assessment of the new Schur complement approximation can be expected.

Based on the above approach, it is easy to see that there is no extra requirement on the value of the parameter  $\gamma$ . This advantage of the new Schur complement approximation can be more clearly seen in the next section, where the contradictory requirements on the values of  $\gamma$  in the old approach are presented.

### 3.2. Original Schur approximation in the AL preconditioner

The starting point to construct the original approximation of the Schur complement in the AL preconditioner is also Lemma 3.1. However, the strategy is totally different. Choosing  $W_1 = \gamma C + M_p$  and substituting  $W_1$  into expression (15) we have

$$\begin{aligned} S_{\gamma}^{-1} &= S^{-1}(I - (\gamma C + M_p - M_p)(\gamma C + M_p)^{-1}) - \gamma(\gamma C + M_p)^{-1} \\ &= S^{-1}M_p(\gamma C + M_p)^{-1} - \gamma(\gamma C + M_p)^{-1} \\ &= (\gamma^{-1}S^{-1}M_p - I)(C + \gamma^{-1}M_p)^{-1}. \end{aligned}$$

For large values of  $\gamma$  such that  $\|\gamma^{-1}S^{-1}M_p\| \ll 1$ , the term  $\gamma^{-1}S^{-1}M_p$  can be neglected so that we have  $\tilde{S}_{\gamma \text{ orig}}$  as follows

$$\tilde{S}_{\gamma \text{ orig}} = -(C + \gamma^{-1}M_p). \quad (17)$$

As shown above, the choice of  $W_1 = \gamma C + M_p$  is used to derive the original Schur complement approximation  $\tilde{S}_{\gamma \text{ orig}}$ . However, the choice of  $W_1 = \gamma C + M_p$  is not practical since the action of  $W_1^{-1}$  is needed in the transformed system (13). One practical choice is to omit the term  $\gamma C$  in  $W_1$  and replace  $M_p$  by its diagonal approximation, which leads to  $W = \hat{M}_p$ . This modification is only applied to simplify the matrix parameter  $W$  and the original Schur complement approximation  $\tilde{S}_{\gamma \text{ orig}}$  remains the same as given in (17). In summary, the choice of  $W = \hat{M}_p$  and  $\tilde{S}_{\gamma \text{ orig}}$  is used in this paper and other related work, for instance [13,14] where stabilized discretizations are employed.

The contradictory requirements in the above approximation are shown as follows. The approximation  $\tilde{S}_{\gamma \text{ orig}}$  is obtained if and only if  $W_1 = \gamma \hat{C} + M_p$  and large values of  $\gamma$  are chosen. However,  $W = \hat{M}_p$  is spectrally equivalent to  $W_1 = \gamma C + M_p$  only when  $\gamma$  is small. This means that it is contradictory to tune the value of  $\gamma$  so that  $W = \hat{M}_p$  and  $\tilde{S}_{\gamma \text{ orig}}$  could be simultaneously obtained. By contrast, this contradictory requirements are avoided by applying the new Schur complement approximation as given in Section 3.1. This disadvantage of the original Schur complement approximation reflects in the



**Table 1**

Summary of the linear systems to be solved, applied preconditioners and approximations of the Schur complement utilized therein.

Linear system	Preconditioner	Schur complement approximations
Transformed system with $\mathcal{A}_\gamma$	$\mathcal{P}_{MAL}$	$\tilde{\mathcal{S}}_{\gamma PCD}, \tilde{\mathcal{S}}_{\gamma LSC}, \tilde{\mathcal{S}}_{\gamma SIMPLE}, \tilde{\mathcal{S}}_{\gamma orig}$
Original system with $\mathcal{A}$	$\mathcal{P}_U$	$\tilde{\mathcal{S}}_{PCD}, \tilde{\mathcal{S}}_{LSC}, \tilde{\mathcal{S}}_{SIMPLE}$

**Table 2**

Pressure sub-system ‘mass-p’ with  $\tilde{\mathcal{S}}_\gamma$  in  $\mathcal{P}_{MAL}$  and  $\tilde{\mathcal{S}}$  in  $\mathcal{P}_U$ , and the systems involved therein.

‘mass-p’ with $\tilde{\mathcal{S}}_{\gamma new}$	‘mass-p’ with $\tilde{\mathcal{S}}$	Systems involved in $\tilde{\mathcal{S}}$
$\tilde{\mathcal{S}}_{\gamma PCD}$	$\tilde{\mathcal{S}}_{PCD}$	$L_p$ and $M_p$
$\tilde{\mathcal{S}}_{\gamma LSC}$	$\tilde{\mathcal{S}}_{LSC}$	$(B\hat{M}_u^{-1}B^T + C_1)$ twice
$\tilde{\mathcal{S}}_{\gamma SIMPLE}$	$\tilde{\mathcal{S}}_{SIMPLE}$	$C + B\text{diag}(A)^{-1}B^T$
‘mass-p’ with $\tilde{\mathcal{S}}_{\gamma orig}$	–	Systems involved in $\tilde{\mathcal{S}}_{\gamma orig}$
$\tilde{\mathcal{S}}_{\gamma orig}$	–	$C + \gamma^{-1}M_p$

slower convergence rate of the Krylov subspace solvers compared to the new Schur complement approximation. This conclusion is made based on the fact that the performance of the modified AL preconditioner is evaluated by varying the Schur complement approximations. See more results in the numerical section.

The application of the original Schur complement approximation  $\tilde{\mathcal{S}}_{\gamma orig}$  involves the solution of the system with  $C + \gamma^{-1}M_p$ . Since the contribution stabilization matrix  $C^{(macro)}$  on macroelements consists of the macroelement pressure mass matrix as illustrated in (8), the presence of the assembled pressure mass matrix  $M_p$  does not introduce more non-zero fill-in in the stabilization matrix  $C$ .

### 3.3. Summary of the Schur complement approximations

At each Picard iteration, we solve either the transformed system (13) with the coefficient matrix  $\mathcal{A}_\gamma$  or the original system (2) with the coefficient matrix  $\mathcal{A}$ . We apply the modified AL preconditioner  $\mathcal{P}_{MAL}$  (14) and the block upper-triangular preconditioner  $\mathcal{P}_U$  (5) to the transformed and original systems, respectively. The Schur complement approximations applied in  $\mathcal{P}_{MAL}$  and  $\mathcal{P}_U$  are summarized in Table 1.

Due to the small size of test problems and the lack of code optimization, the complexity comparison of preconditioners  $\mathcal{P}_{MAL}$  and  $\mathcal{P}_U$  is done based on the following costs analysis in this paper, instead of reporting the computational time. Firstly, we consider the costs of using the modified AL preconditioner  $\mathcal{P}_{MAL}$  for a Krylov subspace method that solves the system with  $\mathcal{A}_\gamma$ . The preconditioner is applied at each Krylov iteration and the modified AL preconditioner involves the solution of the momentum sub-system ‘mom-u’ with  $\tilde{\mathcal{A}}_\gamma$  and the pressure sub-system ‘mass-p’ with  $\tilde{\mathcal{S}}_\gamma$ . Furthermore, at each Krylov iteration additional costs are expressed in the product of the coefficient matrix  $\mathcal{A}_\gamma$  with a Krylov residual vector  $\mathbf{b}_{res}$ . Thus, the total costs at each Krylov iteration are

- $\mathcal{P}_{MAL}$ : mom-u with  $\tilde{\mathcal{A}}_\gamma$  + mass-p with  $\tilde{\mathcal{S}}_\gamma$  +  $\mathcal{A}_\gamma \times \mathbf{b}_{res}$ .

Clearly, the difference of costs by applying  $\mathcal{P}_{MAL}$  arises from solving the pressure sub-system ‘mass-p’ with different Schur complement approximations. If we ignore the multiplications in the definition of the new Schur complement approximation  $\tilde{\mathcal{S}}_{\gamma new}$ , finding the solution of the pressure sub-system in  $\mathcal{P}_{MAL}$  with three variants derived from  $\tilde{\mathcal{S}}_{\gamma new}$ , i.e.,  $\tilde{\mathcal{S}}_{\gamma PCD}$ ,  $\tilde{\mathcal{S}}_{\gamma LSC}$  and  $\tilde{\mathcal{S}}_{\gamma SIMPLE}$  is reduced to solve the pressure sub-system in  $\mathcal{P}_U$  with  $\tilde{\mathcal{S}}_{PCD}$ ,  $\tilde{\mathcal{S}}_{LSC}$  and  $\tilde{\mathcal{S}}_{SIMPLE}$ , respectively. Systems involved in  $\tilde{\mathcal{S}}_{PCD}$ ,  $\tilde{\mathcal{S}}_{LSC}$  and  $\tilde{\mathcal{S}}_{SIMPLE}$  are shown in Table 2. The costs of applying the original Schur complement approximation  $\tilde{\mathcal{S}}_{\gamma orig}$  are also included in Table 2 for a comparison with the new Schur complement approximation  $\tilde{\mathcal{S}}_{\gamma new}$ . Note that all involved systems are of the same size. If we assume a comparable complexity to solve different involved systems, the analysis in Table 2 shows that the costs of using  $\mathcal{P}_{MAL}$  with  $\tilde{\mathcal{S}}_{\gamma PCD}$  and  $\tilde{\mathcal{S}}_{\gamma LSC}$  are roughly the same and two times of that with  $\tilde{\mathcal{S}}_{\gamma SIMPLE}$  and  $\tilde{\mathcal{S}}_{\gamma orig}$ .

Secondly, we consider the costs of applying the upper block-triangular preconditioner  $\mathcal{P}_U$  with different Schur complement approximations, which are used for the original system. Similar to the analysis of  $\mathcal{P}_{MAL}$ , we obtain the total costs at every Krylov iteration as

- $\mathcal{P}_U$ : mom-u with  $A$  + mass-p with  $\tilde{\mathcal{S}}$  +  $\mathcal{A} \times \mathbf{b}_{res}$ .

Also, varying Schur complement approximations  $\tilde{\mathcal{S}}$  results in the difference of costs by applying  $\mathcal{P}_U$ . Based on the analysis in Table 2 and the assumption of a comparable solution complexity for all involved systems, we find out that the costs of applying  $\mathcal{P}_U$  with  $\tilde{\mathcal{S}}_{PCD}$  and  $\tilde{\mathcal{S}}_{LSC}$  are roughly the same and two times of that with  $\tilde{\mathcal{S}}_{SIMPLE}$ .

Lastly, we compare the costs between  $\mathcal{P}_{MAL}$  and  $\mathcal{P}_U$ . As mentioned before, solving the pressure sub-system with the new Schur complement approximation  $\tilde{S}_{\gamma \text{ new}}$  in  $\mathcal{P}_{MAL}$  can be reduced to calculate the solution of the pressure sub-system with  $\tilde{S}$ , which is the Schur complement approximation used in  $\mathcal{P}_U$ . Thus, the difference of costs between  $\mathcal{P}_{MAL}$  and  $\mathcal{P}_U$  focuses on the solution of the momentum sub-system and the product of the coefficient matrix with the Krylov residual vector. More non-zero fill-in in  $A_\gamma$  and  $\mathcal{A}_\gamma$  [13], compared to  $A$  and  $\mathcal{A}$ , results in a heavier matrix-vector product when applying  $\mathcal{P}_{MAL}$  at each Krylov iteration. However, the heavier complexity of  $\mathcal{P}_{MAL}$  could be paid off by a reduced number of Krylov iterations. In this paper we obtain a faster convergence rate preconditioned by  $\mathcal{P}_{MAL}$  with the new Schur complement approximations, compared to  $\mathcal{P}_U$  used for the original system. The time advantage of  $\mathcal{P}_{MAL}$  needs a further assessment which is included in future research plan.

#### 4. Numerical experiments

In this section, we carry out numerical experiments on the following 2D laminar benchmarks:

##### (1) Flow over a finite flat plate (FP)

This example, known as Blasius flow, models a boundary layer flow over a flat plate on the domain  $\Omega = (-1, 5) \times (-1, 1)$ . To model this flow, the Dirichlet boundary condition  $u_x = 1, u_y = 0$  is imposed at the inflow boundary ( $x = -1; -1 \leq y \leq 1$ ) and also on the top and bottom of the channel ( $-1 \leq x \leq 5; y = \pm 1$ ), representing walls moving from left to right with speed unity. The plate is modeled by imposing a no-flow condition on the internal boundary ( $0 \leq x \leq 5; y = 0$ ), and the Neumann condition is applied at the outflow boundary ( $x = 5; -1 < y < 1$ ), i.e.,  $\nu \frac{\partial \mathbf{u}}{\partial \mathbf{n}} - \mathbf{n}p = \mathbf{0}$ . The Reynolds number is defined by  $Re = UL/\nu$  and the reference velocity and length are chosen as  $U = 1$  and  $L = 5$ . On the FP flow, we consider four Reynolds numbers as  $Re = \{10^2, 10^3, 10^4, 10^5\}$ , which correspond to the viscosity parameters  $\nu = \{5 \cdot 10^{-2}, 5 \cdot 10^{-3}, 5 \cdot 10^{-4}, 5 \cdot 10^{-5}\}$ , respectively.

Since stretched grid is typically needed to compute the flow accurately at large Reynolds numbers, stretched grid is generated based on the uniform Cartesian grid with  $12 \times 2^n \cdot 2^n$  cells. The stretching function is applied in the  $y$ -direction with the parameter  $b = 1.01$  [cf. [8]]:

$$y = \frac{(b+1) - (b-1)c}{(c+1)}, \quad c = \left(\frac{b+1}{b-1}\right)^{1-\bar{y}}, \quad \bar{y} = 0, 1/n, 2/n, \dots, 1. \quad (18)$$

##### (2) Flow over backward facing step (BFS)

The L-shaped domain is known as the backward facing step. A Poiseuille flow profile is imposed on the inflow ( $x = -1; 0 \leq y \leq 1$ ). No-slip boundary conditions are imposed on the walls. The Neumann condition is applied at the outflow ( $x = 5; -1 < y < 1$ ) which automatically sets the outflow pressure to zero. Using the reference velocity and length  $U = 1$  and  $L = 2$  and the viscosity parameters  $\nu = \{2 \cdot 10^{-2}, 2 \cdot 10^{-3}\}$ , the corresponding Reynolds numbers are  $Re = UL/\nu = \{10^2, 10^3\}$ .

The BFS flow is more complicated than the flat-plate flow as it features separation, a free shear-layer and reattachment. On the BFS flow we do not consider the Reynolds number  $Re > 10^3$  since the increase of the Reynolds number by an order of magnitude will transfer the flow to be turbulent. On this case we only consider uniform Cartesian grid with  $11 \times 2^n \cdot 2^n$  cells.

##### (3) Lid driven cavity (LDC)

This problem simulates the flow in a square cavity  $(-1, 1)^2$  with enclosed boundary conditions. A lid moving from left to right with a horizontal velocity as:

$$u_x = 1 - x^4 \quad \text{for} \quad -1 \leq x \leq 1 \quad y = 1.$$

In order to accurately resolve the small recirculations, we consider stretched grid around the four corners. Stretched grid is generated based on the uniform Cartesian grid with  $2^n \cdot 2^n$  cells. The stretching function is applied in both directions with parameters  $a = 0.5$  and  $b = 1.01$  [8]

$$x = \frac{(b+2a)c - b + 2a}{(2a+1)(1+c)}, \quad c = \left(\frac{b+1}{b-1}\right)^{\frac{\bar{x}-a}{1-a}}, \quad \bar{x} = 0, 1/n, 2/n, \dots, 1. \quad (19)$$

The reference velocity and length  $U = 1$  and  $L = 2$  and the viscosity parameters  $\nu = \{2 \cdot 10^{-2}, 2 \cdot 10^{-3}, 2 \cdot 10^{-4}\}$  result in the following Reynolds numbers  $Re = \{10^2, 10^3, 10^4\}$ . For the same reason as BFS, a larger Reynolds number  $Re > 10^4$  is not considered on this case.

In order to explore the performance of  $\mathcal{P}_{MAL}$  and  $\mathcal{P}_U$  with varying Schur complement approximations as summarized in Table 1 and Table 2, numerical evaluations are classified into four categories as follows.

##### (C1) On small Reynolds number and uniform grid

In this category we consider the FP, BFS and LDC cases on the small Reynolds number  $Re = 10^2$  and uniform Cartesian grid.

**(C2) On moderate Reynolds number and uniform grid**

In this category we apply the moderate Reynolds number  $Re = 10^3$  on the FP, BFS and LDC cases. Similar to the first class of experiments, uniform Cartesian grid is used here to check the variation of performance when increasing the Reynolds number by an order of magnitude.

**(C3) On moderate Reynolds numbers and stretched grid**

This category contains the tests carried out on the FP and LDC cases with stretched grid. The stretching functions for the FP and LDC cases are (18) and (19), respectively. Still, the moderate Reynolds number  $Re = 10^3$  is employed for the two tests. Comparing with the second class of experiments, this category is meant to investigate the effect of mesh anisotropy.

**(C4) On large Reynolds numbers and stretched grid**

The LDC case with  $Re = 10^4$  and FP case with  $Re = \{10^4, 10^5\}$  are included in this class of tests to assess how the Krylov subspace solver behaves at relatively large Reynolds numbers. Here stretched grid is employed to accurately resolve the problem characteristics.

In this paper all experiments are carried out based on the blocks  $A$ ,  $B$ ,  $C$ ,  $C_1$ ,  $C_2$ ,  $A_p$ ,  $M_p$ ,  $L_p$  and  $M_u$  and the right-hand side vector  $rhs$ , which are obtained at the middle step of the whole nonlinear iterations. Numerical experiments in [13] show that the number of linear iterations varies during the nonlinear procedure. The motivation of choosing the middle step of the nonlinear iterations to export the blocks and vector is that a representative number of linear iteration can be obtained, compared to the averaged number of linear iterations through the whole nonlinear procedure. The relative stopping tolerance to solve the linear system by GMRES is chosen equal to  $10^{-8}$ . The restart functionality of GMRES is not used in this paper. Since the preconditioners  $\mathcal{P}_{MAL}$  and  $\mathcal{P}_U$  involve various momentum and pressure sub-systems, all these sub-systems are directly solved in this paper to avoid the sensitiveness of iterative solvers on the varying solution complexities.

As pointed out in Section 2, the application of the Schur complement approximation  $\tilde{S}_{\gamma PCD}$  needs to preset boundary conditions for the pressure Laplacian  $L_p$  and convection-diffusion  $A_p$  operators. In this paper, we follow the suggestions of [32,33] to use Dirichlet boundary conditions along inflow boundaries to define  $L_p$  and  $A_p$ . This means that the rows and columns of  $L_p$  and  $A_p$  corresponding to the pressure nodes on an inflow boundary are treated as though they are associated with Dirichlet boundary conditions. For the enclosed flow, we algebraically add  $h^2 I$  to  $L_p$  and  $A_p$  to make them non-singular, where  $h$  denotes the grid size and  $I$  is the identity matrix of proper size. Such artificial pressure boundary conditions are only imposed on the preconditioner. The coefficient matrix and right-hand side vector are not affected by these boundary node modifications.

**4.1. On small Reynolds number and uniform grid**

In this subsection we carry out experiments on the FP, BFS and LDC cases with uniform Cartesian grid and small Reynolds number  $Re = 10^2$ . The number of Krylov iterations to solve the transformed system preconditioned by the modified AL preconditioner  $\mathcal{P}_{MAL}$  is given in Table 3. The Schur complement approximations  $\tilde{S}_{\gamma PCD}$ ,  $\tilde{S}_{\gamma LSC}$ ,  $\tilde{S}_{\gamma SIMPLE}$  in  $\mathcal{P}_{MAL}$  are derived from the new method  $\tilde{S}_{\gamma new}$  (16) and the approximation  $\tilde{S}_{\gamma orig}$  corresponds to the original Schur complement approximation (17). In this paper, the reported number of Krylov iterations preconditioned by  $\mathcal{P}_{MAL}$  is obtained by using the optimal value of  $\gamma$ , which results in the fastest convergence rate of the Krylov subspace solver. The following observations are made from Table 3.

Except  $\tilde{S}_{\gamma SIMPLE}$ , we see that the other Schur complement approximations result in the independence of Krylov iterations on the mesh refinement at the three test cases. In terms of the number of Krylov iterations,  $\tilde{S}_{\gamma LSC}$  is superior to the other Schur complement approximations on the FP and BFS cases by the reduced number of iterations and equally efficient as  $\tilde{S}_{\gamma PCD}$  and  $\tilde{S}_{\gamma orig}$  on the LDC case. To understand this advantage, we take the FP case as an example and plot the eigenvalues of the preconditioned Schur complement matrix  $\tilde{S}_{\gamma}^{-1} S_{\gamma}$  in Fig. 1. As can be seen,  $\tilde{S}_{\gamma LSC}$  leads to more clustered eigenvalues and the smallest eigenvalue further away from zero. Such a distribution of eigenvalues is favorable for the Krylov subspace solver and a faster convergence rate can be expected. We know that there can be matrices where there is no relation between the spectrum and the convergence of GMRES [37], especially if the matrix is strongly non normal. We include the spectrum because in our examples the properties of the spectrum are in line with the convergence properties of GMRES. In addition, the field-of-values type estimates for the augmented Lagrangian preconditioned matrix are provided by [38].

As analyzed in Section 3.3, at each Krylov iteration the costs of applying  $\mathcal{P}_{MAL}$  with  $\tilde{S}_{\gamma LSC}$  are roughly the same as  $\tilde{S}_{\gamma PCD}$  and two times of that using  $\tilde{S}_{\gamma SIMPLE}$  and  $\tilde{S}_{\gamma orig}$ . If we assume the computational expense of applying  $\mathcal{P}_{MAL}$  with  $\tilde{S}_{\gamma orig}$  to be unit at each iteration, the total costs by using all Schur complement approximations on the finest grid are presented in Table 4 and calculated by multiplying the expense per iteration by the number of iterations. In the other classes of evaluations we also use this method to calculate the total computational costs.

Results in Table 4 show that the minimal computational costs are achieved by using  $\tilde{S}_{\gamma orig}$  in  $\mathcal{P}_{MAL}$ . Although fewer Krylov iterations are needed by using  $\tilde{S}_{\gamma LSC}$  in  $\mathcal{P}_{MAL}$  seen from Table 3, the reduced number of iterations does not pay off

**Table 3**

**Re = 10<sup>2</sup> and uniform grid:** the number of GMRES iterations to solve the transformed system with  $\mathcal{A}_\gamma$  preconditioned by  $\mathcal{P}_{MAL}$  with different Schur complement approximations and the optimal value of  $\gamma$  in parentheses.

	$\tilde{S}_\gamma PCD$	$\tilde{S}_\gamma LSC$	$\tilde{S}_\gamma SIMPLE$	$\tilde{S}_\gamma orig$
FP case:				
$n = 5$	26(1.e-1)	17(8.e-2)	43(2.e-1)	38(2.e-1)
$n = 6$	25(1.e-1)	25(8.e-2)	67(2.e-1)	38(2.e-1)
$n = 7$	25(1.e-1)	26(8.e-2)	100(2.e-1)	38(2.e-1)
BFS case:				
$n = 5$	34(2.e-2)	17(2.e-2)	42(1.e-1)	36(1.e-1)
$n = 6$	42(3.e-2)	21(2.e-2)	60(1.e-1)	36(1.e-1)
$n = 7$	45(3.e-2)	22(2.e-2)	87(1.e-1)	36(1.e-1)
LDC case:				
$n = 6$	17(2.e-2)	17(2.e-2)	34(1.e-1)	19(1.e-1)
$n = 7$	18(2.e-2)	20(2.e-2)	48(1.e-1)	19(1.e-1)
$n = 8$	18(2.e-2)	22(2.e-2)	63(1.e-1)	19(1.e-1)

**Table 4**

**Re = 10<sup>2</sup> and uniform grid:** the total costs of applying  $\mathcal{P}_{MAL}$  with different Schur complement approximations on the finest uniform Cartesian grid.

	$\tilde{S}_\gamma PCD$	$\tilde{S}_\gamma LSC$	$\tilde{S}_\gamma SIMPLE$	$\tilde{S}_\gamma orig$
FP case:	50	52	100	38
BFS case:	90	44	87	36
LDC case:	36	44	63	19

the heavier costs of  $\tilde{S}_\gamma LSC$ . In this class of experiments, it seems that the original Schur complement approximation  $\tilde{S}_\gamma orig$  is more efficient than the other approximations due to the fewer computational costs in total.

#### 4.2. On moderate Reynolds number and uniform grid

In this subsection we choose the moderate Reynolds number  $Re = 10^3$  to evaluate the performance of the Schur complement approximations used in the modified AL preconditioner  $\mathcal{P}_{MAL}$  and compare with the evaluations at  $Re = 10^2$  in Section 4.1. Based on the number of Krylov iterations presented in Table 5, we see that the independence of Krylov iterations on the mesh refinement is achieved by using the Schur complement approximations  $\tilde{S}_\gamma PCD$  and  $\tilde{S}_\gamma LSC$  in  $\mathcal{P}_{MAL}$ , which is also observed in Section 4.1. Contrary to the observations in Section 4.1, the original Schur complement approximation  $\tilde{S}_\gamma orig$  does not result in the mesh independence of Krylov iterations at  $Re = 10^3$ . With the utilization of  $\tilde{S}_\gamma SIMPLE$  the number of Krylov iterations is dependent of the grid size at both  $Re = 10^2$  and  $10^3$ .

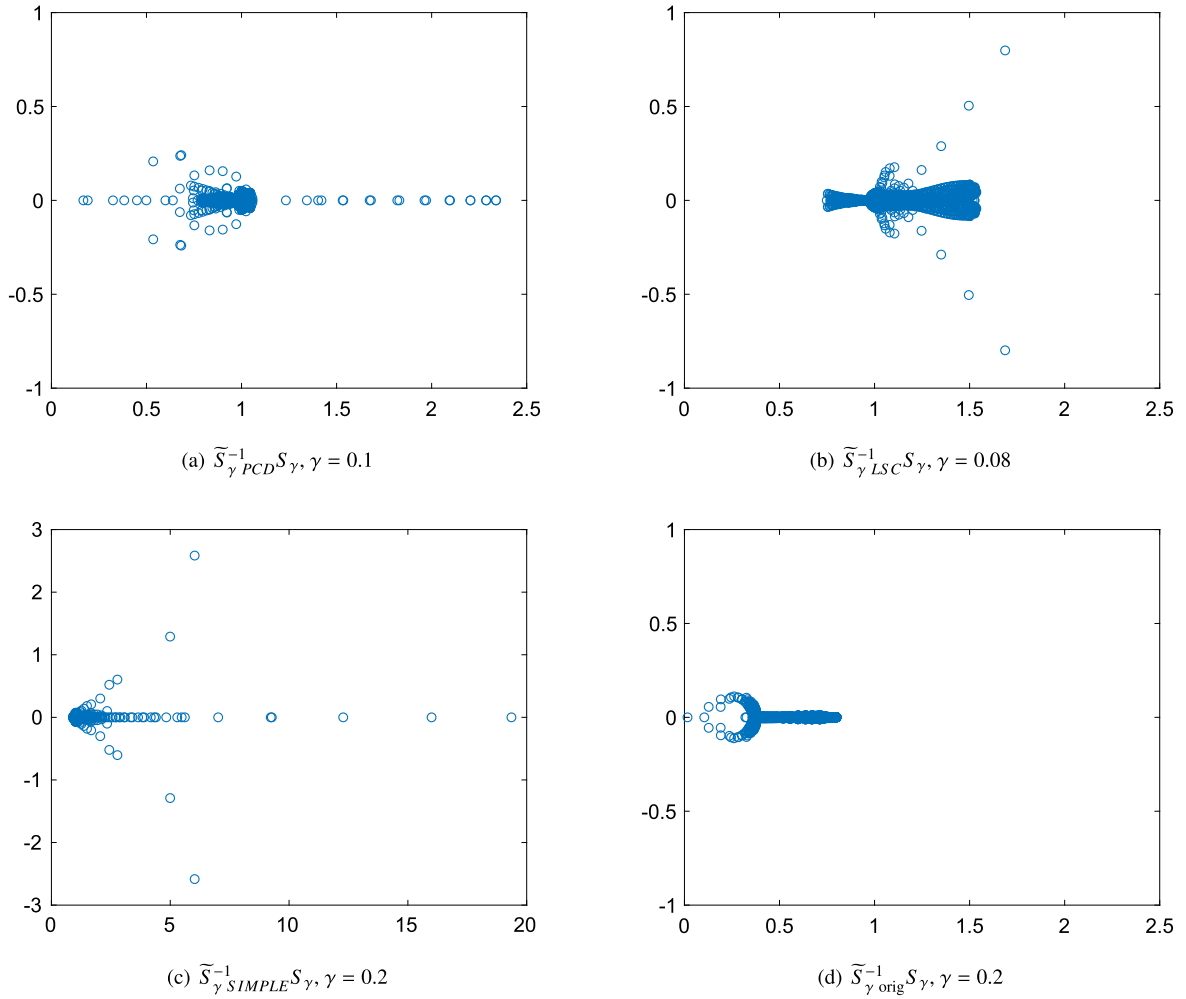
Results in Table 5 show that the smallest number of Krylov iterations is obtained by using  $\tilde{S}_\gamma LSC$  in  $\mathcal{P}_{MAL}$ , which also results in the minimal total costs in Table 6. The total costs are calculated by using the same method as Section 4.2. Taking the mesh independence into account, the utilization of  $\tilde{S}_\gamma LSC$  will lead to a further reduction of total costs on finer grids over  $\tilde{S}_\gamma SIMPLE$  and  $\tilde{S}_\gamma orig$ , which require more iterations with mesh refinement. Compared to  $\tilde{S}_\gamma PCD$  which also results in the mesh independence of Krylov iterations, the application of  $\tilde{S}_\gamma LSC$  reduces the total computational costs at least two times on the FP and BFS cases, and this reduction factor can also be expected on finer grids. On the LDC case  $\tilde{S}_\gamma LSC$  is equally efficient as  $\tilde{S}_\gamma PCD$ .

For the tests at  $Re = 10^3$  it shows that  $\tilde{S}_\gamma LSC$  is superior to the other Schur complement approximations by the reduction of Krylov iterations and total computational costs. In the previous tests with  $Re = 10^2$ , the superiority of  $\tilde{S}_\gamma orig$  is seen. This implies that the optimal Schur complement approximation depends on the Reynolds number.

#### 4.3. On moderate Reynolds number and stretched grid

This subsection is meant to investigate the influence of mesh anisotropy on the performance of the modified AL preconditioner  $\mathcal{P}_{MAL}$ . To compare with Section 4.2, we apply the stretched grid and moderate Reynolds number  $Re = 10^3$  on the FP and LDC cases. The number of Krylov iterations and total computational costs are presented in Table 7 and Table 8, respectively. From Table 7 we note that only  $\tilde{S}_\gamma PCD$  results in the mesh independence and the minimal number of Krylov iterations. Although the total costs of applying  $\tilde{S}_\gamma PCD$  are more than that by using  $\tilde{S}_\gamma SIMPLE$  and  $\tilde{S}_\gamma orig$  on the considered finest grid, as seen from Table 8, fewer costs in total by using  $\tilde{S}_\gamma PCD$  can be expected on finer grids due to the mesh independence. Therefore, we think that  $\tilde{S}_\gamma PCD$  is superior to the other Schur complement approximations on the tests with  $Re = 10^3$  and stretched grid.

Note that on the FP and LDC cases with stretched grid,  $\mathcal{P}_{MAL}$  with  $\tilde{S}_\gamma LSC$  is not mesh independent any more and performs the worst. This is contrary to the observations with uniform Cartesian grid seen in Section 4.2. Considering the



**Fig. 1.** FP and  $\text{Re} = 10^2$ : plot of eigenvalues of the preconditioned matrices  $\tilde{S}_{\gamma}^{-1} S_{\gamma}$  at the uniform Cartesian grid with  $12 \times 2^5 \cdot 2^5$  cells.

**Table 5**

**$\text{Re} = 10^3$  and uniform grid:** the number of GMRES iterations to solve the transformed system with  $\mathcal{A}_{\gamma}$  preconditioned by  $\mathcal{P}_{MAL}$  with different Schur complement approximations and the optimal value of  $\gamma$  in parentheses.

	$\tilde{S}_{\gamma PCD}$	$\tilde{S}_{\gamma LSC}$	$\tilde{S}_{\gamma SIMPLE}$	$\tilde{S}_{\gamma orig}$
FP case:				
$n = 5$	54(8.e-3)	29(8.e-3)	34(2.e-2)	76(6.e-2)
$n = 6$	55(8.e-3)	18(8.e-3)	51(2.e-2)	90(6.e-2)
$n = 7$	56(8.e-3)	17(8.e-3)	99(2.e-2)	95(6.e-2)
BFS case:				
$n = 5$	66(4.e-3)	45(3.e-3)	49(1.e-2)	71(3.e-2)
$n = 6$	63(4.e-3)	27(3.e-3)	77(1.e-2)	76(3.e-2)
$n = 7$	65(3.e-3)	29(3.e-3)	142(1.e-2)	84(3.e-2)
LDC case:				
$n = 6$	30(4.e-3)	54(1.e-3)	66(7.e-3)	36(2.e-2)
$n = 7$	28(4.e-3)	29(4.e-3)	52(1.e-2)	42(2.e-2)
$n = 8$	29(4.e-3)	29(4.e-3)	85(1.e-2)	48(2.e-2)

FP case as an example, on the finest stretched grid of  $n = 7$  the number of Krylov iterations preconditioned by  $\mathcal{P}_{MAL}$  with  $\tilde{S}_{\gamma LSC}$  increases by a factor about 7 compared to the finest uniform grid. This can be seen by comparing the corresponding results in Table 5 and Table 7. The less efficiency of  $\mathcal{P}_{MAL}$  with  $\tilde{S}_{\gamma LSC}$  arising from the mesh anisotropy is also seen on the LDC case. On the other hand, the number of Krylov iterations preconditioned by  $\mathcal{P}_{MAL}$  with the other Schur complement approximations seems robust with respect to mesh anisotropy on the FP and LDC cases.

**Table 6**

**Re = 10<sup>3</sup> and uniform grid:** the total costs of applying  $\mathcal{P}_{MAL}$  with different Schur complement approximations on the finest uniform Cartesian grid.

	$\tilde{S}_{\gamma}^{PCD}$	$\tilde{S}_{\gamma}^{LSC}$	$\tilde{S}_{\gamma}^{SIMPLE}$	$\tilde{S}_{\gamma}^{orig}$
FP case:	112	34	99	95
BFS case:	130	58	142	84
LDC case:	58	58	85	48

**Table 7**

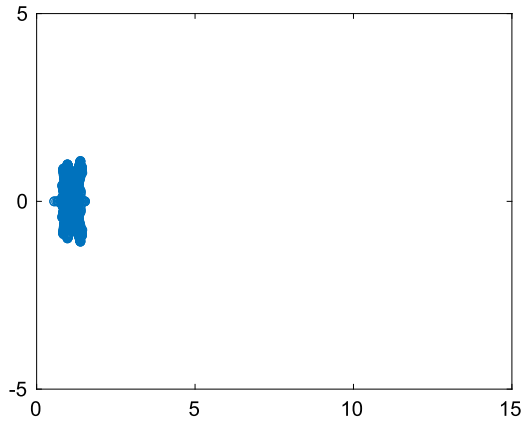
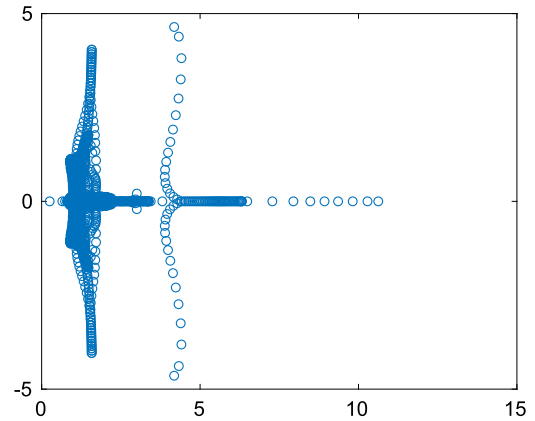
**Re = 10<sup>3</sup> and stretched grid:** the number of GMRES iterations to solve the transformed system with  $\mathcal{A}_{\gamma}$  preconditioned by  $\mathcal{P}_{MAL}$  with different Schur complement approximations and the optimal value of  $\gamma$  in parentheses.

	$\tilde{S}_{\gamma}^{PCD}$	$\tilde{S}_{\gamma}^{LSC}$	$\tilde{S}_{\gamma}^{SIMPLE}$	$\tilde{S}_{\gamma}^{orig}$
FP case:				
$n = 5$	59(8.e-3)	90(7.e-3)	37(2.e-2)	69(6.e-2)
$n = 6$	66(8.e-3)	89(7.e-3)	63(2.e-2)	85(6.e-2)
$n = 7$	62(8.e-3)	117(6.e-3)	119(2.e-2)	92(6.e-2)
LDC case:				
$n = 6$	65(2.e-3)	98(2.e-3)	57(7.e-3)	69(1.e-2)
$n = 7$	41(2.e-3)	58(2.e-3)	46(7.e-3)	40(1.e-2)
$n = 8$	38(2.e-3)	84(2.e-3)	75(7.e-3)	54(1.e-2)

**Table 8**

**Re = 10<sup>3</sup> and stretched grid:** the total costs of applying  $\mathcal{P}_{MAL}$  with different Schur complement approximations on the finest stretched grid.

	$\tilde{S}_{\gamma}^{PCD}$	$\tilde{S}_{\gamma}^{LSC}$	$\tilde{S}_{\gamma}^{SIMPLE}$	$\tilde{S}_{\gamma}^{orig}$
FP case:	124	234	119	92
LDC case:	76	168	75	54

(a) uniform grid,  $\gamma = 8.e-3$ (b) stretched grid,  $\gamma = 7.e-3$ 

**Fig. 2.** FP and **Re = 10<sup>3</sup>**: plot of eigenvalues of the preconditioned matrices  $\tilde{S}_{\gamma}^{-1} S_{\gamma}$  at the uniform and stretched grids with  $12 \times 2^5 \cdot 2^5$  cells.

The less efficiency of  $\tilde{S}_{\gamma}^{LSC}$  on the stretched grid can be explained by the results in Fig. 2, where we consider the FP case at  $Re = 10^3$  and plot the eigenvalues of the preconditioned matrix  $\tilde{S}_{\gamma}^{-1} S_{\gamma}$  for both uniform and stretched grids. As seen from Fig. 2, stretching the grid considerably spreads the distribution of the eigenvalues of the preconditioned Schur complement  $\tilde{S}_{\gamma}^{-1} S_{\gamma}$ , which makes the convergence of the Krylov subspace solver more difficult.

#### 4.4. On large Reynolds number and stretched grid

In this subsection we apply large Reynolds numbers  $Re \geq 10^4$  and stretched grids on the LDC and FP cases. Results in Table 9 and Table 10 illustrate that the fastest convergence rate of the Krylov subspace solver and the minimal computational costs in total are achieved by using  $\tilde{S}_{\gamma}^{SIMPLE}$  in  $\mathcal{P}_{MAL}$  on the two tests. Taking the FP case at  $Re = 10^4$  as an example, from Table 10 we see that the utilization of  $\tilde{S}_{\gamma}^{SIMPLE}$  reduces the total costs at least two times with respect to the other Schur approximations. The reduction factor turns to five at least when applying an even larger Reynolds number  $Re = 10^5$

**Table 9**

**Re = 10<sup>4</sup>** and **stretched grid**: the number of GMRES iterations to solve the transformed system with  $\mathcal{A}_\gamma$  preconditioned by  $\mathcal{P}_{MAL}$  with different Schur complement approximations and the optimal value of  $\gamma$  in parentheses.

	$\tilde{S}_\gamma$ PCD	$\tilde{S}_\gamma$ LSC	$\tilde{S}_\gamma$ SIMPLE	$\tilde{S}_\gamma$ orig
FP case:				
$n = 5$	363(8.e-4)	369(6.e-4)	35(2.e-3)	93(1.e-2)
$n = 6$	334(8.e-4)	336(6.e-4)	53(3.e-3)	128(2.e-2)
$n = 7$	346(8.e-4)	374(6.e-4)	83(4.e-3)	192(2.e-2)
LDC case:				
$n = 6$	113(3.e-4)	97(2.e-4)	34(1.e-3)	46(5.e-3)
$n = 7$	143(3.e-4)	235(2.e-4)	45(1.e-3)	65(5.e-3)
$n = 8$	159(4.e-4)	309(2.e-4)	80(2.e-3)	106(5.e-3)

**Table 10**

**Re = 10<sup>4</sup>** and **stretched grid**: the total costs of applying  $\mathcal{P}_{MAL}$  with different Schur complement approximations on the finest stretched grid.

	$\tilde{S}_\gamma$ PCD	$\tilde{S}_\gamma$ LSC	$\tilde{S}_\gamma$ SIMPLE	$\tilde{S}_\gamma$ orig
FP case:	692	748	83	192
LDC case:	318	618	80	106

**Table 11**

**FP** and **Re = 10<sup>5</sup>**: the number of GMRES iterations and total costs to solve the transformed system with  $\mathcal{A}_\gamma$  preconditioned by  $\mathcal{P}_{MAL}$  with different Schur complement approximations and the optimal value of  $\gamma$  in parentheses. The stretched grid is applied.

	$\tilde{S}_\gamma$ PCD	$\tilde{S}_\gamma$ LSC	$\tilde{S}_\gamma$ SIMPLE	$\tilde{S}_\gamma$ orig
iterations:				
$n = 5$	1000+	1000+	26(1.e-4)	136(1.e-3)
$n = 6$	1000+	1000+	35(2.e-4)	192(2.e-3)
$n = 7$	1000+	1000+	58(3.e-4)	310(2.e-3)
total costs:				
$n = 7$	2000+	2000+	58	310

on the FP case, which is seen from Table 11. In the context of large Reynolds numbers, it appears that  $\tilde{S}_\gamma$  SIMPLE is the optimal Schur complement approximation in the modified AL preconditioner  $\mathcal{P}_{MAL}$ . In contrast to the previous tests, at large Reynolds numbers none of the considered Schur complement approximations lead to the mesh independence of  $\mathcal{P}_{MAL}$ . The advantage of  $\tilde{S}_\gamma$  SIMPLE on finer grids needs a further assessment, which is included in future research.

To investigate the effect of the Reynolds number, we take the FP case as an example and in Fig. 3 plot the number of Krylov iterations preconditioned by  $\mathcal{P}_{MAL}$  at varying Reynolds numbers. It appears that only  $\tilde{S}_\gamma$  SIMPLE results in the robustness of  $\mathcal{P}_{MAL}$  with respect to the Reynolds number. To understand the reasons, we compute the extremal eigenvalues of the preconditioned Schur complement matrix  $\tilde{S}_\gamma^{-1} S_\gamma$  and present them in Table 12.  $R_{min}$  and  $R_{max}$  denote the smallest and largest real parts of the eigenvalues and  $I_{max}$  corresponds the largest imaginary part. These extremal values correspond to the boundaries of the rectangular domain containing all eigenvalues. Regarding  $\tilde{S}_\gamma^{-1} S_\gamma$ , the values of  $R_{min}$  slightly decrease and remain the same order of magnitude. Together with the decrease of  $R_{max}/R_{min}$  and  $I_{max}$ , the eigenvalues are further clustered. However, fewer clustered eigenvalues are yielded by using the other Schur complement approximations. This explains the robustness of  $\mathcal{P}_{MAL}$  with  $\tilde{S}_\gamma$  SIMPLE with respect to the Reynolds number.

To investigate the computed solutions at large Reynolds numbers, we choose the FP case. In the inviscid limit  $Re \rightarrow \infty$  the solution is simply  $u_x = 1$ ,  $u_y = 0$  and  $p = \text{constant}$ . Since the shear boundary layer is of width proportional to  $\sqrt{\nu}$  and within the layer the horizontal velocity increases rapidly from zero to unity, the plate seems “invisible” as  $Re \rightarrow \infty$  [1]. To check this feature, in Fig. 4 we illustrate the calculated pressure and equally spaced contours of the horizontal velocity between 0 and 0.95 at different Reynolds numbers. The stretched grid with  $12 \times 2^6 \cdot 2^6$  cells is utilized. At  $Re = 10^3$ , the contours of the horizontal velocity show the evolution of the boundary layer as the fluid passing from the leading edge of the plate to the outflow. The parabolic shape of the velocity contours seems consistent with asymptotic theory [39] and the reported results in [1]. When increasing the Reynolds numbers to  $Re = 10^5$ , we see that the plate “disappears” and the difference between the pressure values decreases by one order of magnitude compared to the case of  $Re = 10^3$ . Results in Fig. 4 demonstrate that the computed solutions, ranging from the moderate to large Reynolds numbers, seem reasonable.

#### 4.5. Summary of the Schur complement approximations in $\mathcal{P}_{MAL}$

Based on the above four classes of numerical evaluations, in Table 13 we summarize the optimal Schur complement approximation in the modified AL preconditioner  $\mathcal{P}_{MAL}$ . It shows that the optimal Schur complement approximation, which leads to the fastest convergence rate of the Krylov subspace solver, depends on the Reynolds number and mesh anisotropy.



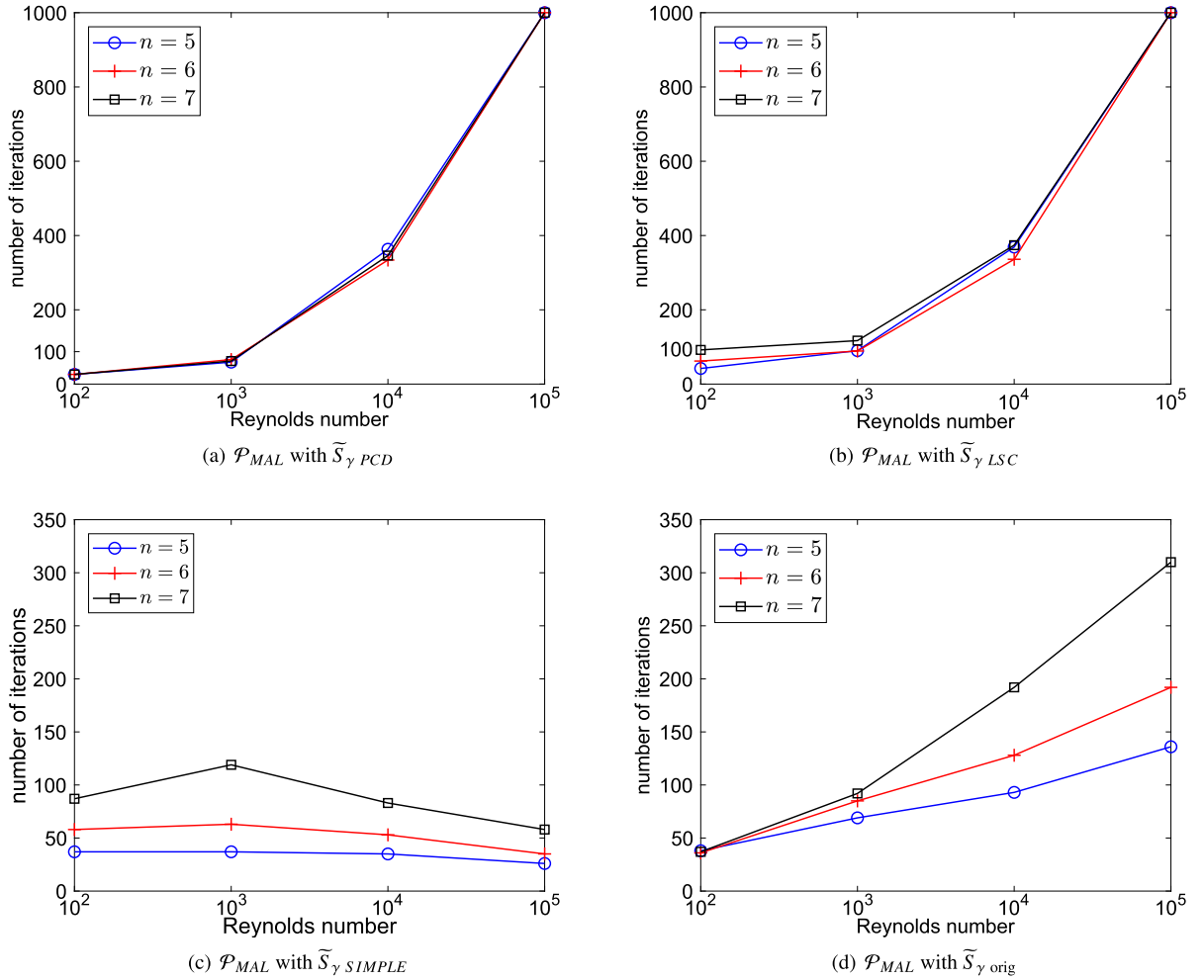


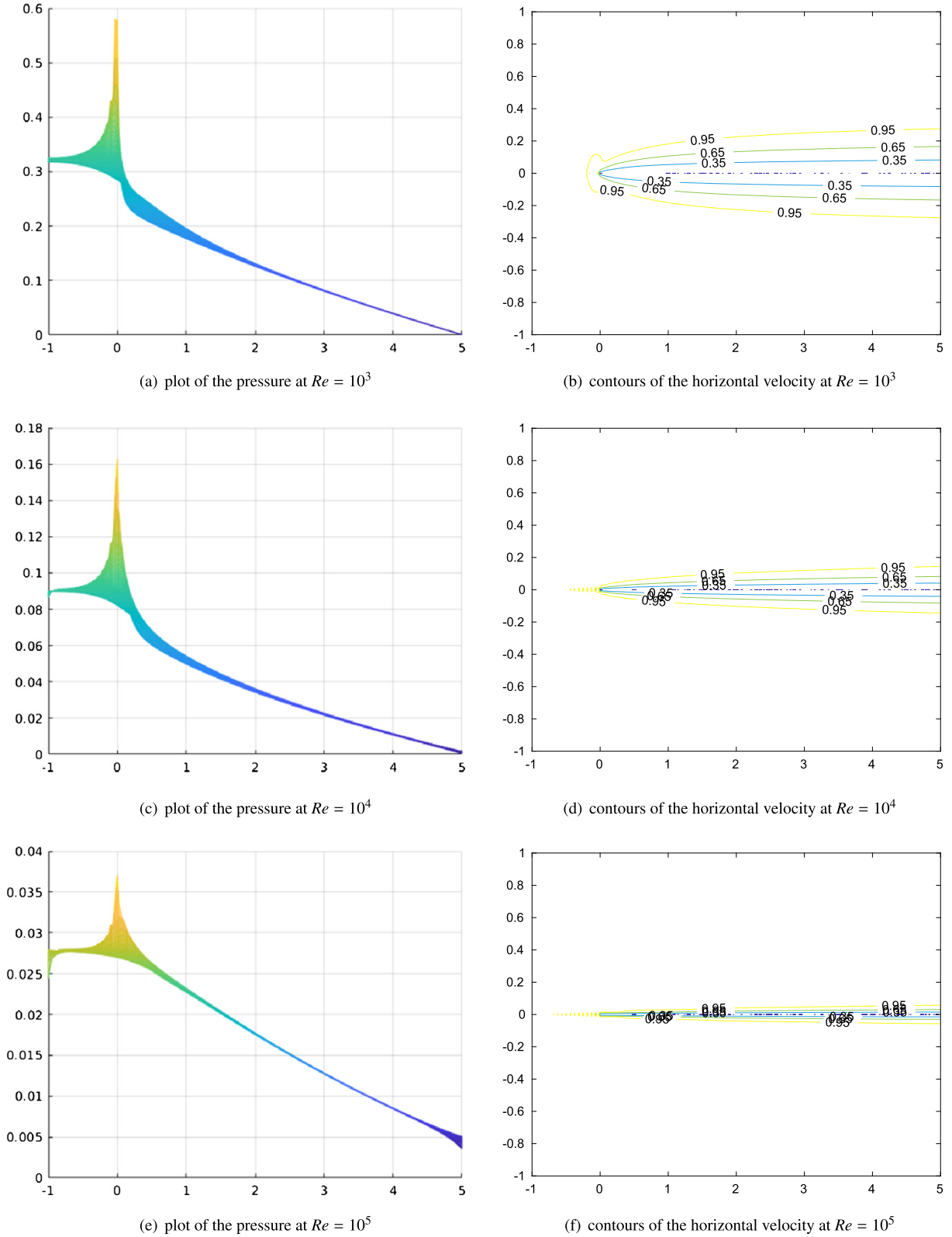
Fig. 3. FP and stretched grid: plot of the number of GMRES iterations preconditioned by  $\mathcal{P}_{MAL}$  at varying Reynolds numbers.

At every class of evaluations, the optimal Schur complement approximation is problem independent. Numerical evaluations in this paper show that  $\tilde{S}_{\gamma orig}$  is suitable for the calculations with small Reynolds numbers and  $\tilde{S}_{\gamma SIMPLE}$  delivers a better performance for large Reynolds numbers due to its Reynolds robustness. In the context of moderate Reynolds numbers,  $\tilde{S}_{\gamma LSC}$  is more efficient with uniform grids but sensitive to mesh anisotropy. When stretched grids are employed,  $\tilde{S}_{\gamma PCD}$  turns out to be the optimal choice in the moderate Reynolds number context. Except the calculations at small Reynolds numbers and uniform grids, the optimal Schur complement approximations on other classes of tests are derived from the new method  $\tilde{S}_{\gamma new}$  proposed in this paper. This demonstrates the advantage of the new approach over the traditional one  $\tilde{S}_{\gamma orig}$ . The mesh independence of Krylov iterations is not achieved by using the optimal Schur complement approximation only for the class of tests with large Reynolds numbers. The reason and possible improvement on this issue are to be considered in future research.

#### 4.6. Comparison between $\mathcal{P}_{MAL}$ and $\mathcal{P}_U$ .

To apply the modified AL preconditioner  $\mathcal{P}_{MAL}$ , one needs to transform the original system (2) to an equivalent one (13) with the coefficient matrix  $\mathcal{A}_{\gamma}$ . This transformation consumes additional costs. Furthermore, at each Krylov iteration extra costs arise from the product of  $\mathcal{A}_{\gamma}$  with a Krylov residual vector due to more fill-in in  $\mathcal{A}_{\gamma}$  [13]. In this sense, the heavier complexities of  $\mathcal{P}_{MAL}$  could be paid off only by a reduced number of Krylov iterations, compared to the block upper-triangular preconditioner  $\mathcal{P}_U$  applied to the original system. In this section, we consider the comparisons between  $\mathcal{P}_{MAL}$  and  $\mathcal{P}_U$  on the LDC and FP cases at the large Reynolds number  $Re = 10^4$  and stretched grid which represent stiff tests on the considered preconditioners.

It is revealed in Section 4.4 that  $\tilde{S}_{\gamma SIMPLE}$  turns out to be the most efficient Schur complement approximation for the modified AL preconditioner  $\mathcal{P}_{MAL}$  in this class of evaluations. Therefore, the comparison is carried out between  $\mathcal{P}_{MAL}$  with



**Fig. 4.** FP and stretched grid: plot of the calculated pressure unknown (left) and contours of the horizontal velocity between 0 and 0.95 (right) at different Reynolds numbers.

**Table 12**

**FP and stretched grid:** the extremal eigenvalues of the preconditioned Schur complement  $\tilde{S}_Y^{-1} S_Y$  at varying Reynolds numbers. The stretched grid with  $12 \times 2^5 \cdot 2^5$  cells is used.  $R_{\min}$  and  $R_{\max}$  denote the smallest and largest real parts of the eigenvalues and  $I_{\max}$  corresponds the largest imaginary part.

	$Re = 10^2$	$Re = 10^3$	$Re = 10^4$	$Re = 10^5$
$\tilde{S}_Y^{-1} PCD S_Y$				
$R_{\min}$	0.2062	0.1283	0.1129	0.1992
$R_{\max}$	2.3315	4.2868e+1	4.1574e+2	1.3059e+3
$R_{\max}/R_{\min}$	1.1621e+1	3.3412e+2	3.6824e+3	6.5557e+3
$I_{\max}$	0.2567	1.2106	1.1109e+1	1.2598e+2
$\tilde{S}_Y^{-1} LSC S_Y$				
$R_{\min}$	0.2537	0.2530	0.8865	0.5652
$R_{\max}$	2.1509e+1	1.0623e+1	1.0973e+1	1.1309e+2
$R_{\max}/R_{\min}$	8.4782e+1	4.1991e+1	1.2378e+1	2.0009e+2
$I_{\max}$	2.2301e+1	4.6429	4.6264e+1	8.8363e+2
$\tilde{S}_Y^{-1} SIMPLE S_Y$				
$R_{\min}$	0.6714	0.4075	0.1949	0.1541
$R_{\max}$	2.9729e+1	9.8786	3.1976	1.4942
$R_{\max}/R_{\min}$	4.4280e+1	2.4241e+1	1.6406e+1	9.6963
$I_{\max}$	5.3308	1.0578	0.1630	0.1755
$\tilde{S}_Y^{-1} orig S_Y$				
$R_{\min}$	0.161e-1	0.167e-1	0.3423e-2	0.1315e-3
$R_{\max}$	0.8000	0.9231	0.9524	0.9524
$R_{\max}/R_{\min}$	4.9689e+1	5.5275e+1	2.8011e+2	7.2382e+3
$I_{\max}$	0.1081	0.2458	0.3078	0.3404

**Table 13**

The optimal Schur complement approximation  $\tilde{S}_Y$  opt in the modified AL preconditioner on varying classes of evaluations.

Class of evaluations	$\tilde{S}_Y$ opt	Mesh independence	Problem independence
$Re = 10^2$ and uniform grid	$\tilde{S}_Y$ orig	Yes	Yes
$Re = 10^3$ and uniform grid	$\tilde{S}_Y$ LSC	Yes	Yes
$Re = 10^3$ and stretched grid	$\tilde{S}_Y$ PCD	Yes	Yes
$Re \geq 10^4$ and stretched grid	$\tilde{S}_Y$ SIMPLE	No	Yes

**Table 14**

**$Re = 10^4$  and stretched grid:** the number of GMRES iterations to solve the transformed system with  $\mathcal{A}_Y$  preconditioned by  $\mathcal{P}_{MAL}$  and the number of GMRES iterations to solve the original system with  $\mathcal{A}$  preconditioned by  $\mathcal{P}_U$ .

	$\mathcal{P}_{MAL}$ for $\mathcal{A}_Y$	$\mathcal{P}_U$ for $\mathcal{A}$		
	$\tilde{S}_Y$ SIMPLE	$\tilde{S}_{PCD}$	$\tilde{S}_{LSC}$	$\tilde{S}_{SIMPLE}$
LDC case:				
$n = 6$	34(1.e-3)	130	147	83
$n = 7$	45(1.e-3)	246	307	119
$n = 8$	80(2.e-3)	364	560	182
FP case:				
$n = 5$	35(2.e-3)	879	661	62
$n = 6$	53(3.e-3)	1000+	599	122
$n = 7$	83(4.e-3)	1000+	809	229

$\tilde{S}_Y$  SIMPLE and  $\mathcal{P}_U$  and presented in Table 14. As seen, fewer iterations are needed when applying  $\mathcal{P}_{MAL}$  with  $\tilde{S}_Y$  SIMPLE. Considering the LDC case on the finest grid, the application of  $\mathcal{P}_{MAL}$  with  $\tilde{S}_Y$  SIMPLE reduces the number of Krylov iterations by a factor about four, seven and two, compared to that by using  $\mathcal{P}_U$  with  $\tilde{S}_{PCD}$ ,  $\tilde{S}_{LSC}$  and  $\tilde{S}_{SIMPLE}$ , respectively. On the FP case, a further reduction of Krylov iterations is obtained by using  $\mathcal{P}_{MAL}$  with  $\tilde{S}_Y$  SIMPLE. One direction of future research is to verify whether the reduced number of Krylov iterations could convert to the advantage of  $\mathcal{P}_{MAL}$  with  $\tilde{S}_Y$  SIMPLE in terms of the total computational costs.

## 5. Conclusion and future work

In this paper we introduce three variants based on the new method to approximate the Schur complement for the AL preconditioner. To evaluate their performance, we classify the numerical experiments to four categories according to the Reynolds number and mesh anisotropy. At every class of evaluations we consider different test problems. The optimal Schur

complement approximation for every class of tests is determined and given in Table 13. It is seen that the most efficient Schur complement approximation is dependent of the Reynolds number and mesh anisotropy, but problem independent. Furthermore, we find out that, except the experiments at  $Re = 10^2$  and uniform grid, the optimal Schur complement approximations on the other three classes of tests are the variants derived from the new method to approximate the Schur complement in the modified AL preconditioner. This demonstrates the advantage of the new approach over the traditional Schur complement approximation.

In this paper we observe that for large Reynolds numbers  $Re \geq 10^4$  none of the considered Schur complement approximations can make the modified AL preconditioner independent of the grid size. One planned future research is on the improvement which allows the mesh independence. Another direction of future work is to evaluate whether the advantage of the modified AL preconditioner by the reduced number of Krylov iterations, which is shown in this paper, can convert to the wall-clock time benefit with respect to the preconditioner applied to the original system.

### Declaration of competing interest

Both authors are only paid by the institutes mentioned in the affiliations given in the manuscript.

### Acknowledgements

We would like to thank the anonymous reviewers for their helpful comments.

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