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# Transparent Transfer-Free Ultrasmall Multilayer Graphene Microelectrodes Enable High Quality Recordings in Brain Slices

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## ABSTRACT

Resolving the underlying mechanisms of complex brain functions and associated disorders remains a major challenge in neuroscience, largely due to the difficulty in mapping large-scale neural network dynamics with high spatiotemporal resolution. Multimodal neural platforms that integrate optical and electrical modalities offer a promising approach that surpasses resolution limits. Over the last decade, transparent graphene microelectrodes have been proposed as highly suitable multimodal neural interfaces. However, their fabrication commonly relies on the manual transfer process of pre-grown graphene sheets which introduces reliability and scalability issues. In this study, multilayer graphene microelectrode arrays (MEAs) with electrode sizes as small as 10–50  $\mu\text{m}$  in diameter, are fabricated using a transfer-free process on a transparent substrate for in vitro multimodal platforms. For the first time, the capability of transparent graphene electrodes with a diameter of just 10  $\mu\text{m}$  to reliably capture extracellular spiking activity with high signal-to-noise ratios (up to  $\sim 25$  dB) is demonstrated. The recorded signal quality is found to be more limited by the electrode-tissue coupling than the MEA technology itself. Overall, this study shows the potential of transfer-free multilayer graphene MEAs to interface with neural tissue, paving the way to advancing neuroscientific research through the next-generation of multimodal neural interfaces.

## 1 | Introduction

The human brain is one of the most complex biological systems, comprising billions of neurons that communicate through intricate neural networks. These networks are the basis of essential functions, such as cognition, memory, and behavior, as well as neurological disorders such as epilepsy, Parkinson's disease, and schizophrenia [1–3]. Unraveling the mechanisms of these networks is a fundamental challenge in neuroscience, requiring advanced tools capable of mapping neural activity with high spatial and temporal resolution [4].

Neural interfaces have emerged as powerful tools for interacting with the nervous system, enabling the detection and modulation of electrical signals from excitable cells [5]. Conventional electrophysiological techniques, such as patch-clamp recordings and metal-based microelectrode arrays (MEAs), have been the gold standard for studying neuronal activity and have significantly advanced our understanding of neural circuits [6, 7]. However, these technologies are limited in their ability to capture the dynamics of large-scale neural networks across extended fields of view, hindering progress in understanding complex brain functions.

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Recently, there has been a growing interest in optical techniques in neuroscience due to their ability to record and manipulate neural activity with increased spatial resolution. Methods such as calcium imaging and optogenetics allow researchers to simultaneously monitor the activity of hundreds to thousands of neurons, providing insights into neural connectivity and network dynamics [8–10]. Despite their advantages, optical techniques alone often lack the temporal resolution required to capture fast electrophysiological events, such as action potentials, with millisecond precision. Multimodal neural platforms that integrate optical and electrical modalities offer the potential to further advance the depth of understanding of our nervous system by offering greater spatiotemporal resolution [11, 12].

Graphene has emerged as a highly attractive material for such neural interfaces owing to its unique combination of biophysical, electrical, mechanical, biological, and optical properties [13–19]. This 2D material exhibits flexibility and mechanical resilience, which allows it to be integrated into highly conformable soft interfaces, conforming closely to the complex geometries of neural tissues and reducing the mechanical mismatch. Furthermore, the biocompatibility of graphene, which was initially controversial, has been given more clarity in recent studies. Toxicity is not an intrinsic property of “graphene” but depends on lateral size, defect density, and surface chemistry, with high-purity, minimally functionalized few-layer graphene generally exhibiting low toxicity and limited inflammatory response [20]. In particular, continuous CVD graphene films used as neural electrodes in retinal and cortical implants have been reported to integrate stably *in vivo*, with minimal glial activation and no major adverse events over implantation periods of weeks to months, supporting their promising integration in chronic neural interfacing applications [21–23]. Due to its intrinsic optical transparency, monolayer CVD graphene has been explored for simultaneous electrophysiological recordings and optical imaging [24]. However, the inherent quantum capacitance of graphene poses a challenge when scaling down electrode sizes, as it limits the impedance of the electrodes. To address this limitation, researchers have explored various strategies, including the chemical doping of graphene [25], and surface modifications based on the integration of platinum nanoparticles [14, 16]. These approaches have successfully achieved lower impedance and higher charge storage capacity (CSC) values, enhancing the performance of graphene-based neural interfaces.

Despite their potential, the widespread adoption of graphene-based neural interfaces has been hindered by challenges in fabrication, particularly the need to transfer pre-grown graphene layers onto target substrates. This transfer process often introduces defects, contamination, and scalability issues, limiting the reliability and performance of graphene electrodes [26, 27]. CVD graphene electrodes have been developed using a transfer-free process, while enabling their integration into flexible substrates, as we have previously reported [13]. The suitability of these transfer-free graphene electrodes for multimodal applications was successfully demonstrated, showing no photo-induced artifacts and compatibility with MRI, further highlighting their potential for advanced neural interfacing technologies.

In this study, we describe lithography-compatible transfer-free multilayer graphene MEAs directly fabricated on transparent

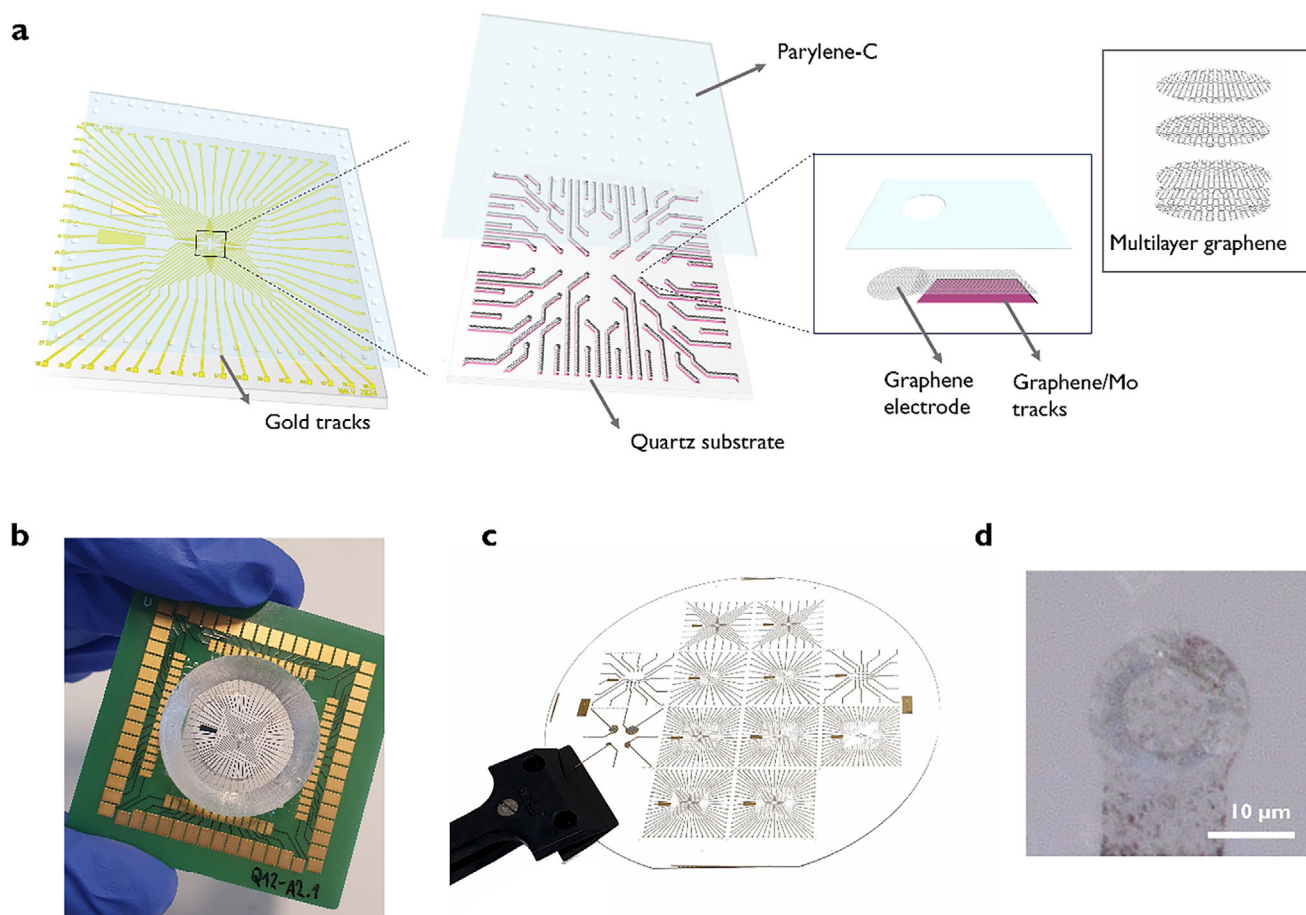
wafer substrates, with electrode sizes as small as 10–50  $\mu\text{m}$  in diameter, comparable to or smaller than state-of-the-art transparent microelectrodes [28–31], for *in vitro* multimodal platforms. We show that transfer-free multilayer graphene achieved impedance values lower than those of previously reported CVD monolayer or few-layer graphene electrodes. This could be attributed to an increase in the intrinsic graphene quantum capacitance with the number of layers, in accordance with previous work [25, 32]. Most importantly, the proposed MEAs with electrodes as small as 10  $\mu\text{m}$  in diameter enabled electrophysiological recordings of spiking activity from brain slices with high signal quality. To our knowledge, this is the first demonstration of extracellular recordings with graphene electrodes at this scale, overcoming longstanding challenges posed by impedance and signal quality. This demonstration at the 10  $\mu\text{m}$  scale is particularly relevant for next-generation multimodal neural interfaces, as such ultrasmall electrodes enable higher-density transparent arrays capable of single-cell spatial resolution while maintaining compatibility with optical imaging. Overall, the obtained results show that transfer-free multilayer graphene can be effectively integrated into *in vitro* MEA platforms and offers a great promise for advanced multimodal neural interfaces.

## 2 | Results and Discussion

### 2.1 | Fabrication and Characterization of Transfer-Free Graphene MEAs

To enable multimodal recordings, we designed and fabricated graphene-based MEAs on transparent fused silica substrates. Several electrode arrays with varying electrode sizes, numbers of electrodes, and pitches were designed to meet diverse experimental requirements and explore their technological limits. The primary designs included a 60-electrode MEA with 10  $\mu\text{m}$  diameter electrodes arranged in an  $8 \times 8$  grid with a 100  $\mu\text{m}$  pitch, a 60-electrode MEA with 50  $\mu\text{m}$  diameter electrodes arranged in an  $8 \times 8$  square grid with a 200  $\mu\text{m}$  pitch, and a 32-electrode MEA with 30  $\mu\text{m}$  diameter electrodes arranged in a  $6 \times 6$  grid with a 100  $\mu\text{m}$  pitch. Additionally, a MEA with various electrode diameters, in the range of 10–500  $\mu\text{m}$ , was included for a more direct and efficient characterization of the electrodes’ performance with respect to their sizes. In our device architecture, the active recording sites consisted exclusively of transfer-free multilayer graphene, whereas the inner tracks located within the transparent imaging region were formed by a graphene/Mo bilayer to reduce sheet resistance while preserving optical access (see Figure 1a). Outside this region, a highly conductive and biocompatible metal, Ti/Au, was used to form the outer tracks and contact pads. A custom-designed printed circuit board (PCB) electrically interconnected to the MEA pads ensures efficient interfacing with commercially available electrophysiology recording systems, as shown in Figure 1b and Figure S1.

The microfabrication process for transfer-free graphene MEAs was initiated by the deposition and patterning of a molybdenum (Mo) layer on a fused silica wafer. Mo acts as the catalyst layer for the subsequent multilayer graphene growth via chemical vapor deposition (CVD) [26]. To ensure the integrity of the graphene recording sites during the subsequent processing steps, a protective Ti/Al layer was deposited and patterned using a lift-off



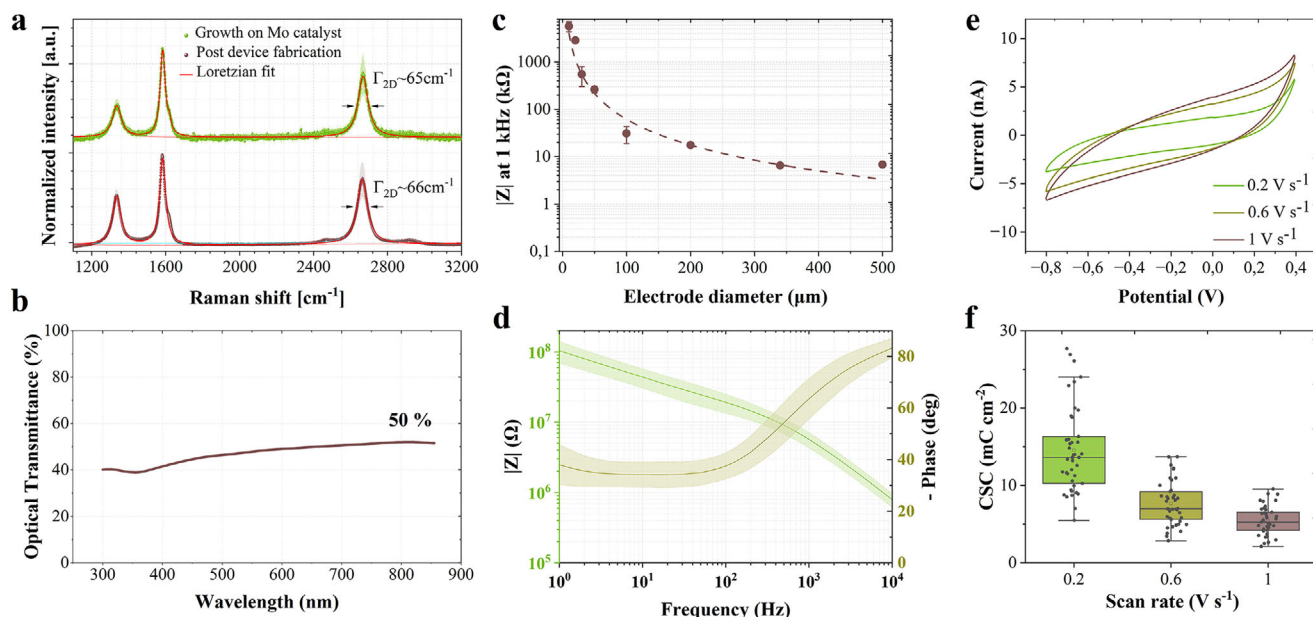
**FIGURE 1** | Transfer-free multilayer graphene microelectrode arrays. (a) Schematic of the MEA device architecture and material layers, showing multilayer graphene electrodes interfacing with graphene/Mo inner tracks for optical access, and connecting to gold outer tracks and pads. (b) Graphene MEA device used for the in vitro recording experiments. (c) Photograph of a 4 in. fused silica wafer containing 12 MEAs with different array designs. (d) Optical image (using ring illumination) of a 10 μm multilayer graphene electrode.

technique. We also attempted deposition via sputtering followed by wet etching. However, this often resulted in a non-uniform etching process, leading to overetched structures, severely compromising the final MEA device functionality. Ti/Au tracks and contact pads were then formed via evaporation and lift-off. The devices were encapsulated with a 1–2 μm-thick parylene-C film, deposited via CVD, and patterned to expose the recording sites and contact pads. The fabrication process was completed with the removal of the Ti/Al protective layer and underlying Mo layer, leaving only graphene exposed on the electrodes. A photograph of a 4-inch fused silica wafer containing 12 microfabricated MEA arrays and an optical image of the multilayer graphene electrode are shown in Figure 1c,d, respectively. Additional details on the microfabrication process are provided in the Experimental Section, and a schematic representation is provided in Figure S2.

Raman spectroscopy revealed the multilayer and turbostratic nature of the CVD grown graphene films. Turbostratic graphene refers to a type of multilayer graphene where the layers are rotationally misaligned, leading to weaker interlayer interactions and electronic decoupling [33]. The characteristic G, 2D, and D peaks of graphene (~1582, 2660, 1335 cm<sup>-1</sup>, respectively) were observed, with an I<sub>2D</sub>/I<sub>G</sub> ratio lower than 1, confirming the presence of the multilayer graphene (see Figure 2a). Additionally,

spatially resolved Raman mapping over the 10 μm electrodes (Figure S3) showed that the 2D band remained single-peaked across the exposed area. Maps of 2D peak position ( $\omega_{2D}$ ), FWHM ( $\Gamma_{2D}$ ), and I<sub>2D</sub>/I<sub>G</sub> ratios, along with histograms (Figure S3), show smooth spatial gradients across the electrode without domain-like features or 2D splitting, consistent with turbostratic stacking [33]. This interpretation is further supported by a previous work illustrating independent TEM analysis of Mo-grown multilayer graphene produced using the same catalyst system, which shows an enlarged interlayer spacing (> 0.34 nm), a structural hallmark of turbostratic multilayer graphene [34]. The I<sub>D</sub>/I<sub>G</sub> ratio, indicative of the amount of defects, was low, I<sub>D</sub>/I<sub>G</sub> = 0.35, right after graphene growth on the Mo catalyst layer on a quartz substrate. The number of defects slightly increased as the graphene layer was post-processed. Additional Raman spectra at different stages of the fabrication process are provided in Figure S4, and the corresponding intensity ratios of D, G, and 2D bands are summarized in Table S1.

Optical transparency within the field of view of the microelectrode array is a critical requirement for enabling multimodal studies. To address this, our design employed multilayer graphene grown on a Mo catalyst layer to define the inner tracks within the field of view rather than traditional gold tracks. Gold, while



**FIGURE 2** | Materials characterization and electrochemical properties of graphene-based MEA electrodes. (a) Averaged Raman spectra ( $n = 5$ ) of transfer-free multilayer graphene obtained immediately after chemical vapor deposition (CVD) growth on the Mo catalyst and after completing the MEA microfabrication process, confirming the structural integrity and quality of the graphene throughout the fabrication steps. Additional Raman spectra at different stages of the fabrication process are provided in the Supporting Information. (b) Optical transmittance measurements of transferred graphene sheets, with the contribution from the glass substrate subtracted. (c) Electrochemical impedance spectroscopy (EIS) magnitude at 1 kHz of various electrode sizes, ranging from 10 to 500  $\mu\text{m}$ . The dotted line represents the power fitting function of the data points. Circles represent the mean impedance values, with error bars indicating the standard deviation for electrode sizes with 42 measurements (10  $\mu\text{m}$ ) and 10 measurements (30, 50, and 100  $\mu\text{m}$ ). For electrode sizes with only two measurements (20, 200, 340, and 500  $\mu\text{m}$ ), the error bars were omitted because of insufficient data. (d) Averaged impedance spectra ( $n = 42$ ), including magnitude and phase, for 10  $\mu\text{m}$  diameter electrodes. Shaded regions show standard deviation. The impedance magnitude at 1 kHz is  $5.68 \pm 1.37 \text{ M}\Omega$ . (e) Averaged cyclic voltammetry (CV) curves ( $n = 42$ ) for 10  $\mu\text{m}$  diameter electrodes at scan rates of 0.2, 0.6, and 1  $\text{V s}^{-1}$ . (f) Cathodic CSC values extracted from the CV curves depicted in (e).

highly conductive, exhibits photoelectric effects that can interfere with optical modalities, whereas multilayer graphene does not suffer from such limitations [13]. Optical transmittance analysis of the multilayer graphene in this work revealed transparency levels of approximately 50% across the entire spectrum, as shown in Figure 2b. A transmittance of 47.5% was obtained at a wavelength of 550 nm, corresponding to an absorbance of 52.5%. Based on the typical absorption of  $\sim 2.3\%$  per graphene layer [35], this corresponds to roughly 20–25 layers, assuming a linear approximation. While such approximations are less accurate at higher layer counts due to interlayer optical effects, they provide a useful estimate of the film's thickness. Though this transparency is lower than that of monolayer graphene or ITO-based systems (typically  $> 80\%$ ), it remains within a workable range for in vitro imaging modalities, and can be further optimized by tuning the CVD growth process. Notably, while the Mo layer was completely etched away from the electrode sites, it remained beneath the inner tracks, which could slightly impact the overall transparency within the field of view. Ongoing efforts are focused on developing methods to completely remove the Mo layer after graphene growth, thereby further enhancing the optical performance for multimodal applications.

The electrochemical properties of the transfer-free MEAs are detailed in Figure 2c–f. The impedance dependency on the electrode size was studied by measuring the electrical impedance response of graphene electrodes of different sizes, ranging from

10 to 500  $\mu\text{m}$  in diameter. Figure 2c shows the average impedance magnitude at 1 kHz plotted against the electrode diameter. The impedance magnitude decreased with increasing electrode size, as expected, following an inverse relationship. The corresponding numerical values are summarized in Table S2.

Impedance spectra ( $n = 42$ ), including magnitude and phase, are featured in Figure 2d for electrodes with a diameter of 10  $\mu\text{m}$ . The average impedance magnitude at 1 kHz was  $5.68 \pm 1.37 \text{ M}\Omega$  ( $4.46 \pm 1.08 \Omega \text{ cm}^2$ ). The EIS magnitude follows the typical impedance behavior of neural recording electrodes, with an inverse relationship between the impedance and frequency. The phase response behaves as a non-ideal capacitor at higher frequency regime (approaching  $-90^\circ$ ), and stabilizes around  $-35^\circ$  at lower frequencies, reflecting the interaction of multiple impedance elements, including capacitive and diffusive components. The cutoff frequency is  $\sim 250 \text{ Hz}$ , above which, the interface is dominated by a mainly capacitive charge-transfer mechanism, where signal components are transferred with minimal amplitude attenuation and phase distortion [36, 37]. A plausible explanation for deviations from capacitive behavior at lower frequencies is the presence of Faradaic processes, potentially arising from the residual Mo, which by design remains still beneath the graphene interconnect tracks but not under the recording sites. Although not directly exposed, the Mo, being electrochemically active, may still interact with the electrolyte through exposed track edges or defects in the graphene, thereby

enabling redox activity [38]. While this does not compromise the ability of the electrodes to record high-quality neural signals, removing Mo from beneath the tracks remains a priority for future process optimization.

We then studied the reversibility of the electrochemical reactions on the electrodes and the amount of charge that can be stored reversibly, i.e., charge storage capacity (CSC), through cyclic voltammetry (CV). The CV curves for 10  $\mu\text{m}$  diameter electrodes at scan rates of 0.2, 0.6, and 1  $\text{V s}^{-1}$  are shown in Figure 2e. With the increase of the scan rate, the diffusion layer at the electrode-electrolyte interface becomes thinner, resulting in greater current densities. The water window was maintained between -0.8 and 0.4 V to prevent undesirable electrochemical reactions. The CSC for each electrode was calculated based on the time integral of the CV curve and normalizing it to the electrode area. The average CSC values of the fabricated electrodes are shown in Figure 2f. Future work could more systematically investigate the full electrochemical stability window of this multilayer graphene material to further identify its limits.

## 2.2 | Electrophysiological Recordings of Neuronal Activity from Brain Slices

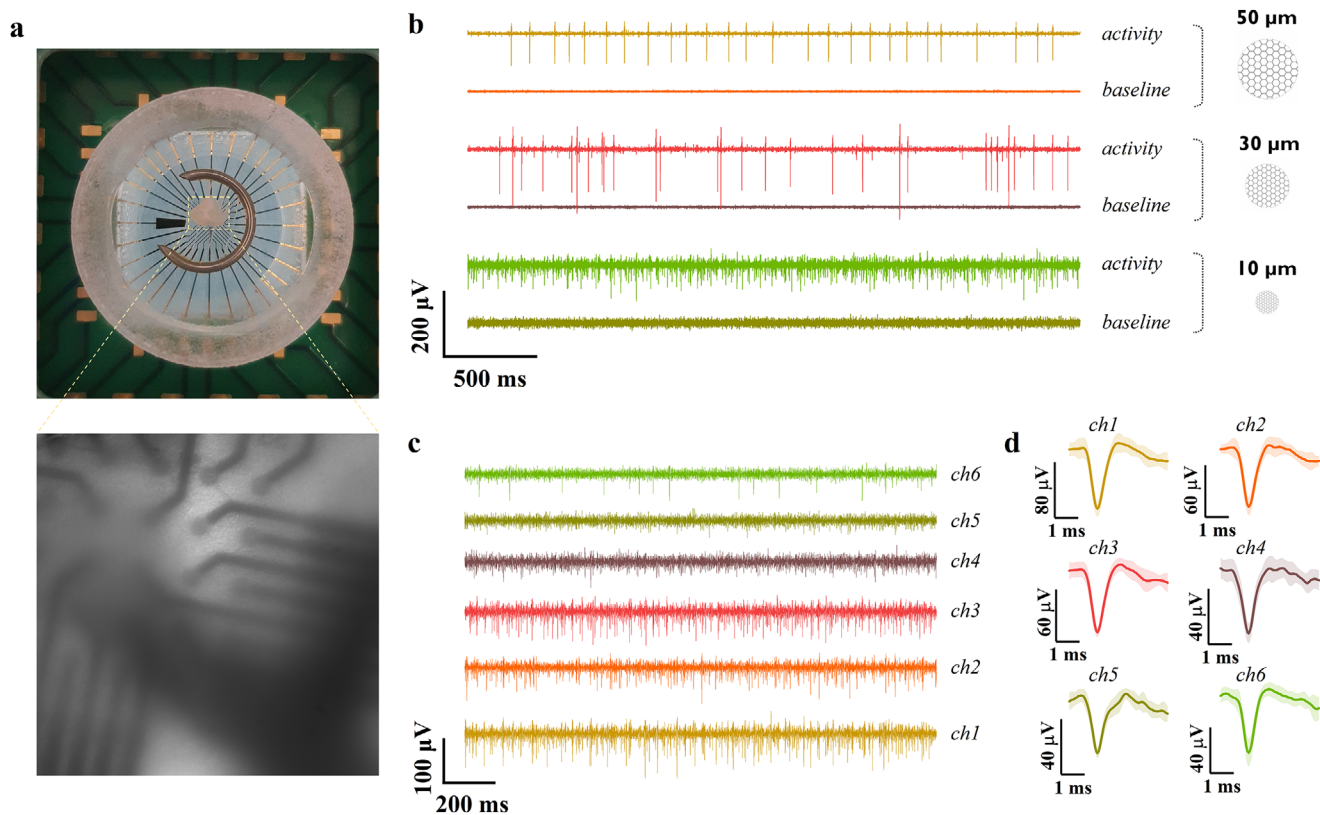
The *in vitro* performance of transfer-free multilayer graphene MEAs, with 10, 30, and 50  $\mu\text{m}$ -diameter electrodes, was evaluated by recording neural activity from acute mouse cerebellar brain slices. The cerebellum was selected as the model system because of its well-characterized spontaneous spiking activity patterns, which are dominated by the firing of Purkinje cells. These cells exhibit regular and rhythmic spikes at a relatively constant and high frequency of around 30–50 Hz [39]. The preparation of cerebellar slice culture is described in the Experimental Section. The tissue slices were carefully positioned on the MEA surface and secured using a slice anchor with parallel nylon fibers to ensure close contact (see Figure 3a). Artificial cerebrospinal fluid (aCSF) was manually perfused over the slice to maintain tissue viability. We developed a custom-designed interface to facilitate the connection between the graphene MEAs and the Intan recording system (Intan Technologies, Los Angeles, CA). Further information regarding the acquisition setup is provided in the Experimental Section.

Prior to recording from a slice, a baseline signal was acquired for several minutes to assess the noise level of the system. The recorded filtered signals exhibited a root mean square (rms) noise of 2–7  $\mu\text{V}$ , with smaller electrodes showing a higher noise floor. Spontaneous extracellular spiking activity of neuronal cells within the cerebellar slice was successfully detected across electrodes of 10, 30, and 50  $\mu\text{m}$  in diameter (Figure 3b). Despite their considerably smaller surface area and inherently higher impedance ( $5.68 \pm 1.37 \text{ M}\Omega$  at 1 kHz), the 10  $\mu\text{m}$  electrodes captured spikes with amplitudes up to  $\sim 140 \mu\text{V}$ . Representative cerebellar brain slice activity signals and their corresponding averaged spike waveforms are shown in Figure 3c,d. Across all tested electrode sizes, spike amplitudes reached up to 100–270  $\mu\text{V}$ . The amplitude variation can be attributed to several factors: (1) electrode size and spatial averaging—larger electrodes capture signals averaged over a broader area, potentially diluting contributions from individual neurons, whereas smaller elec-

trodes resolve higher-amplitude signals from localized sources [40, 41]; and (2) neuron-electrode proximity—tight coupling between the tissue and electrode surface enhances signal amplitude. Additionally, variations in spike amplitude were observed within individual electrode recordings, indicating that multiple nearby neurons were being captured simultaneously, with each contributing spikes of different magnitudes. Moreover, different neurons are expected to have different spike waveforms [42].

The quality of the recorded electrophysiological signals was quantified by the signal-to-noise ratio (SNR), following the methodology described in the Experimental Section. The average SNR values of the filtered signals were found to be  $18.6 \pm 2.7 \text{ dB}$  for the 10  $\mu\text{m}$  electrodes,  $24.4 \pm 6.2 \text{ dB}$  for the 30  $\mu\text{m}$  electrodes, and  $24.2 \pm 4.3 \text{ dB}$  for the 50  $\mu\text{m}$  electrodes. The distribution of the obtained SNR values is depicted in Figure 4a. For the 30 and 50  $\mu\text{m}$  electrodes, the SNR values were found to be similar despite the size difference. The slightly lower SNR observed for the 10  $\mu\text{m}$  electrodes is likely governed by their higher impedance. It should be noted that the comparison of the SNR with previously reported values in the literature for transparent recording electrode arrays is challenging, as there is no standardized approach to compute the SNR. While some reports use peak-to-peak spike amplitudes relative to the baseline noise standard deviation, others employ RMS calculations or different filtering approaches. Moreover, electrophysiological signal characteristics vary substantially depending on the experimental paradigm, whether drug-induced, evoked, or spontaneous activity. To contextualize the performance of our devices, we provide a direct comparison of impedance and SNR metrics with previously reported transparent electrode technologies in Table S3. Our results demonstrate the capability of transfer-free graphene MEAs to reliably detect extracellular neural activity even with electrodes as small as 10  $\mu\text{m}$ . The achieved SNR values, particularly considering that the recordings were obtained from spontaneous activity, validate the potential of the technology for neurophysiological research applications.

Notably, the signal quality was found to be predominantly governed by the electrode impedance and neuron-electrode coupling. Electrode impedance is traditionally regarded as a primary benchmark for neural recording performance [43]. However, in practice, electrode impedance only needs to be sufficiently low such that its thermal noise and voltage-divider effects do not dominate over the intrinsic characteristics of the recording electronics. Beyond this threshold, further reductions in impedance yield diminishing returns in signal quality. Compared to CVD monolayer or few-layer graphene, the transfer-free multilayer graphene microelectrodes presented here exhibit reduced impedance due to their increased effective surface area, while also eliminating fabrication variability and defects associated with the graphene transfer process. Other transparent electrode materials, such as PEDOT:PSS, indium tin oxide (ITO), and MXenes, have been explored for multimodal neural interfacing [18, 28–30]. Among these, PEDOT:PSS has demonstrated exceptionally low impedance owing to its volumetric capacitive behavior; however, its long-term chemical and mechanical stability remain significant challenges, particularly in complex biological environments. Although the impedance of our multilayer graphene electrodes remains higher than that of PEDOT:PSS-coated devices, it is



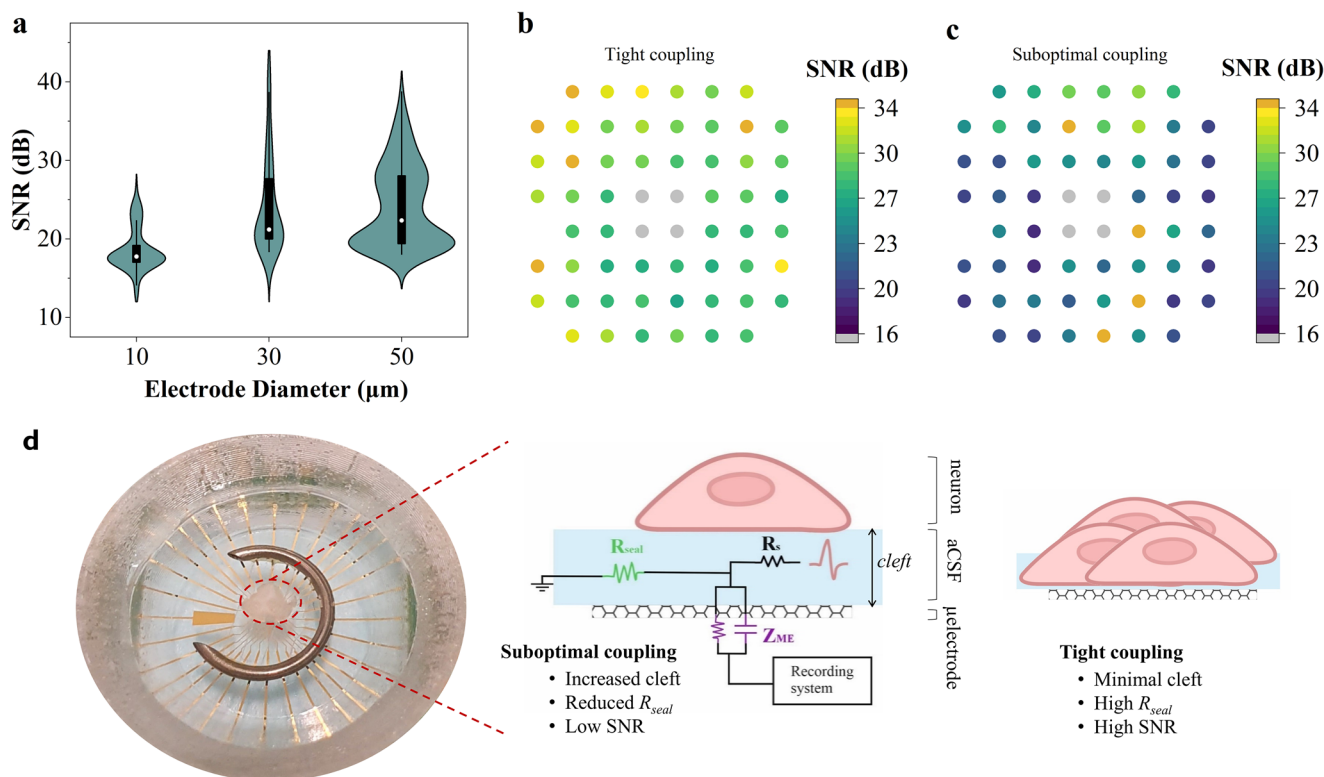
**FIGURE 3** | Electrophysiological recordings of neuronal activity from cerebellar brain slices. (a) Photograph (Top view) of a mouse cerebellar brain slice mounted on a graphene-based MEA device and an optical image of the positioned brain slice (captured with an epifluorescence microscope). To ensure close contact between the slice and the MEA, a slice anchor with parallel nylon fibers was gently pressed onto the tissue. (b) Recorded baseline and neural activity from graphene MEA devices with electrode diameters of 10, 30, and 50  $\mu\text{m}$ . (c) Neural activity recorded by graphene MEA electrodes with a diameter of 10  $\mu\text{m}$ , showing the activity of six distinct channels. (d) Averaged detected spike waveforms corresponding to the recording in (c). Shaded regions represent the standard deviation.

comparable to or lower than values reported for ITO and MXene-based electrodes. More importantly, we demonstrate that these multilayer graphene electrodes achieve high-fidelity recordings of spontaneous extracellular activity in acute brain slices, with spike amplitudes up to  $\sim 140 \mu\text{V}$ , and signal-to-noise ratios reaching 25 dB for ultrasmall 10  $\mu\text{m}$  electrodes. To the best of our knowledge, this is the first demonstration of successful neural spike recording using graphene microelectrodes of this size, highlighting a significant advantage of our transfer-free fabrication process in achieving reliable device miniaturization.

Optimal recordings in our experiments were achieved when electrodes were positioned in close proximity to active neurons and maintained tight contact with the tissue (Figure 4b). Conversely, during perfusion with CSF, we observed gradual tissue detachment from the electrode surface, which increased the cleft distance and degraded recording quality (Figure 4c). This detachment likely resulted from the expansion of the fluid-filled gap between cells and electrodes, reducing the effective coupling. This relationship between physical proximity and signal quality can be understood through the concept of neuron–electrode coupling, commonly described by the well-established point-contact model of neuron–electrode interaction [44–47]. A key parameter in this model is the seal resistance ( $R_{\text{seal}}$ ), which represents the electrical resistance to current leakage through

the extracellular cleft between the neuronal membrane and the electrode surface (Figure 4d).  $R_{\text{seal}}$  exhibits a strong inverse dependence on the cleft distance: tighter contact yields higher seal resistance and, consequently, improved signal fidelity. To further refine the understanding of neuron–electrode coupling and its influence on signal quality, future work could incorporate in situ impedance spectroscopy measurements or computational modeling approaches. Such methods would enable a more quantitative characterization of the coupling dynamics, particularly the contribution of seal resistance, and could help clarify how these mechanisms shape the observed SNR across recordings.

While various noise sources contribute to signal degradation, including thermal noise associated with electrode impedance, biological noise from neural tissue, and electronic noise from recording instrumentation [48], in our in vitro recordings, we found that the dominant factor determining signal quality was the quality of neuron–electrode coupling, rather than absolute impedance alone. These findings underscore that achieving high quality neural recordings requires optimization of both electrode properties and neuron–electrode electrical coupling for in vitro experiments. In this context, we demonstrate that excellent neural signal acquisition is achievable without ultra-low impedance, as long as electrode design, tissue coupling, and recording chain are appropriately matched. Our transfer-free multilayer graphene



**FIGURE 4** | The electrical coupling between the neuronal cells and the microelectrodes. (a) Obtained signal-to-noise ratio (SNR) values per each tested electrode size and considering various activity recording sessions with different brain slices. (b) Colormap representation of SNR values obtained with 50  $\mu\text{m}$ -diameter electrodes overlaid on the MEA, for recordings performed with a low aCSF volume. Electrodes marked in grey indicate damaged ones, defined by an impedance magnitude greater than 1 M $\Omega$  at 1 kHz. (c) Colormap representation of SNR values, similar to (b), for recordings performed with standard aCSF volume. (d) Simplified contact model of the neuron-electrode coupling, adapted from Spira and Hai [44]. The recorded signal quality largely depends on the electrode impedance ( $Z_{\text{ME}}$ ) and on the seal resistance ( $R_{\text{seal}}$ ).

electrodes reliably capture spontaneous extracellular activity with high signal-to-noise ratios. This establishes transfer-free multilayer graphene as a robust and high-performance platform for transparent neural interfacing.

### 3 | Conclusion

In this study, we developed transfer-free graphene MEAs for interfacing with neural tissue and demonstrated their capability for electrophysiological recording. Our transfer-free fabrication approach represents a significant advancement in graphene-based neural technology, addressing the reliability and scalability challenges associated with state-of-the-art CVD graphene wet transfer methods. We showed that transfer-free graphene can be miniaturized to the micrometer scale, down to 10  $\mu\text{m}$  in diameter, and integrated into transparent in vitro substrates, while preserving the integrity of the graphene film.

The electrochemical characterization revealed impedance values at 1 kHz between 263 k $\Omega$  and 5.68 M $\Omega$  for electrodes with diameters from 50 to 10  $\mu\text{m}$ , which enabled the detection of spontaneous neural activity from acute cerebellar brain slices. Our experiments revealed that the neuron-electrode coupling strength was the main limiting factor for signal fidelity. Optimizing the coupling between the neural tissue and the electrode surface in in vitro platforms remains a critical aspect for achieving

high-quality neural recordings. Despite this limitation, several electrodes recorded neural signals with exceptional signal quality (SNR up to 25–40 dB), including unprecedented recordings with 10  $\mu\text{m}$  electrodes, which represents a significant milestone in transparent neural interface technology, enabling higher density arrays and improved spatial resolution for mapping neural circuits.

In addition to advancing the understanding of electrophysiological recording capabilities, this study emphasizes the broader potential of transfer-free graphene MEAs for multimodal neural interfacing. Their compatibility with optical imaging is ensured by restricting the field of view to non-photoelectric materials (e.g., graphene grown on a Mo layer and transparent substrates), paving the way toward fully transparent electrode arrays. Furthermore, prior work [13] has demonstrated that transfer-free graphene electrodes exhibit no photo-induced artifacts and remain MRI-compatible, highlighting their suitability for multimodal applications. These properties position transfer-free graphene MEAs as a promising platform for integrating electrical and optical modalities, providing high spatiotemporal resolution for comprehensive neural network analysis.

Overall, this work demonstrates that transfer-free graphene MEAs offer an innovative approach to neural interfacing by overcoming current fabrication limitations and providing reliable, high-quality electrophysiological recordings. By validating

reliable neuronal recordings at a 10  $\mu\text{m}$  electrode scale, this work overcomes a longstanding barrier in transparent graphene interfaces and lays the foundation for high-density multimodal MEAs capable of mapping complex neural dynamics with single-cell spatial resolution. Furthermore, the integration of electrical and optical modalities within a single transparent platform opens new avenues for advancing neuroscientific research. Future research directions should focus on optimizing neuron-electrode coupling, exploring bidirectional functionalities, and translating this technology to *in vivo* settings, by integrating it into soft, flexible substrates to record from the more challenging biological environments. Ultimately, these advancements will contribute to the next-generation of multimodal neural interfaces for a deeper understanding of complex brain functions and associated disorders.

## 4 | Experimental Section

### 4.1 | Device Fabrication and Assembly

Fused silica quartz wafers were used as transparent starting material due to their ability to withstand the high temperatures required for graphene growth, their superior resistance to graphene delamination compared to sapphire substrates and their ease of dicing in comparison to sapphire [49]. The microfabrication process of the graphene MEAs is illustrated in Figure S2.

The fabrication started with a 50 nm molybdenum (Mo) layer deposition at 50°C on the frontside of the wafer via sputtering. Mo serves as the catalyst layer for the subsequent graphene growth. Next, a temporary 50 nm Ti layer was sputtered at 50°C at the backside for the wafer to be optically detected in the metal etcher equipment. After both sputtering processes, standard lithography steps defined the pattern in the Mo layer using a positive photoresist (SPR3012, Shipley Megaposit) (Figure S2b). The lithography process required adaptation, such as extended bake times, to account for the lower thermal conductivity of quartz. The defined pattern was then transferred by plasma etching of the Mo layer in an ICP-RIE etcher. The etching was performed at 40°C with no RF platen power, 500 W ICP power, 5 mTorr pressure, and SF<sub>6</sub> gas at 25 sccm flow. Following this, the ion bombarded photoresist was stripped using a bath with NI555 solvent solution. Ultrasonication at 80 kHz and elevated temperatures (50°C–60°C) were employed to accelerate the process. The Ti layer in the backside was then fully wet etched using HF 0.55% bath to avoid any contributions from it during the graphene growth process. Graphene was then selectively grown on the Mo structures. The growth was done via chemical vapor deposition (CVD) process at 935°C with 960, 40, and 25 sccm of Ar, H<sub>2</sub>, and CH<sub>4</sub> gases for 20 min at 25 mbar.

A Ti/Al metal layer protected the graphene electrodes throughout the fabrication process and in particular, during the plasma etching of the Parylene-C encapsulation layer. After the lithography using a negative photoresist (nLOF-2020, Microchemicals GmbH, Germany), a stack composed of 10 nm Ti and 100 nm pure Al was evaporated. For the patterning of the metal layer via lift-off, NI555 stripper was used to remove the photoresist and along with the evaporated metal on top, leaving the protective Al structures on the electrodes revealed (Figure S2d).

Before preparing the wafers for Au evaporation to form the outer MEA tracks and contact pads, a 200 nm Ti layer was evaporated in the backside. The Ti layer enabled the electrostatic clamping in the ICP-RIE plasma etcher process step to come. The Au layer was e-beam evaporated and defined via a lift-off process by using a negative photoresist (nLOF-2020, Microchemicals GmbH, Germany) (Figure S2e). The photoresist was stripped with NI555 solvent solution overnight.

The wafers were then coated with a 1–2  $\mu\text{m}$  parylene-C layer (Figure S2f), which was CVD deposited at room temperature. Parylene-C served as the insulating coating of the MEAs. 3-(trimethoxysilyl)propyl methacrylate (A-174 Silane) was used as an adhesion promoter for parylene on the substrate. A patterned thick positive photoresist coating (AZ10XT, Microchemicals GmbH, Germany) was used as the masking layer to expose electrodes and contact pads in the parylene layer. A plasma etching step created the openings in the parylene-C, landing on the Al protective layer. O<sub>2</sub> and SF<sub>6</sub> gases were used at 185 sccm and 15 sccm flows respectively, and with 40 W LF power. The photoresist mask was removed with acetone followed by IPA. Additional cleaning with NI555 was performed to ensure that the ion bombarded photoresist was completely removed.

Prior to dicing, the whole wafer surface was coated with a thick positive photoresist layer (AZ3027, Microchemicals GmbH, Germany) to protect it from the dicing procedure. The quartz wafers were then diced with a dedicated diamond blade. The microfabricated dies were cleaned in acetone followed by IPA. Thereafter, the Al protective layer on the electrodes as well as the backside Ti layer were fully etched in 0.55% HF solution. Finally, Mo was wet etched by gently covering the electrode area with 31% H<sub>2</sub>O<sub>2</sub> forming a puddle (Figure S2i). An etching time of 3 min was sufficient to remove almost completely the Mo layer underneath without causing graphene detachment. The microfabricated dies were left in vacuum overnight at 80°C to remove any moisture and ensure a better adhesion in between layers.

The microfabricated dies were attached and electrically interconnected to a custom-designed PCB via wire bonding to facilitate electrode characterization and ensure efficient interfacing with commercially available electrophysiology recording systems. The design of the PCB, including the pads' placement, size, and pitch, was specifically optimized to be compatible with Multichannel Systems MEAs featuring 60 electrodes. This configuration also ensured compatibility with other commercial electrophysiology systems, such as the MZ60 MicroElectrode Array interface from TDT.

To contain phosphate-buffered saline (PBS) or culture medium during experiments, inverted cone-shaped wells were designed and fabricated using an Asiga3D printer. A biocompatible resin, Detax Freeprint Ortho, was selected for 3D printing the wells to minimize the risk of cytotoxicity or other adverse biological responses when in contact with cells or tissue slice cultures [50]. The 3D-printed wells were securely adhered to the surface of the MEA device using the same non-conductive epoxy (EPO-TEK 301-2FL), which also served to cover the wirebonds, providing additional mechanical protection against physical damage during handling and use. Figure 1b shows a completely fabricated and assembled graphene MEA device.

## 4.2 | Device Characterization

### 4.2.1 | Raman Analysis

Raman spectroscopy was employed to confirm the presence of graphene, and extract information about the type of graphene, quality and amount of defects present in the grown layer. Raman spectra were obtained using a Renishaw inVia Raman system with a laser of 633 nm. The spectrum was acquired with 50% laser power and 20 s of exposure time to achieve an adequate signal-to-noise ratio. Several point measurements from each sample were taken and then analyzed with a custom Matlab script.

### 4.2.2 | Optical Transmission

To investigate the level of transparency of the final device, optical transmittance measurements were conducted. For these measurements, a cm-scale graphene layer was transferred onto a glass substrate. PerkinElmer Lambda 1050+ UV/VIS/NIR spectrometer was used to evaluate the optical transmittance of graphene samples. Transmittance data over a wide range of wavelengths, from 300 to 860 nm, were obtained. Measurements were taken for graphene and glass samples, allowing the isolation of the glass's contribution.

### 4.2.3 | Electrochemical Characterization

Standard electrochemical measurements were conducted to characterize the microelectrodes' performance. Electrochemical impedance spectroscopy (EIS) and cyclic voltammetry (CV) were performed in a three-electrode setup and using a phosphate buffered saline (PBS), PBS 1X pH 7.4, as the electrolyte solution. The three-electrode setup consisted of: a Pt electrode (3 mm diameter (BASI Inc.)) serving as the counter electrode (CE), a leakless miniature silver/silver chloride (Ag/AgCl) (eDAQ) as reference electrode (RE), and the fabricated graphene microelectrodes as the working electrodes (WE). All the electrodes were connected to a potentiostat (Autolab PGSTAT302N) and kept inside a Faraday cage. For the EIS, a 10 mV sine-wave voltage was applied between the WE and RE, and the current between the WE and CE was measured. The impedance magnitude and phase over a range of frequencies (from 0.1 Hz to 100 kHz) was recorded. For the CV, the water window, defined as the potential range where water remains stable and avoids electrolysis, was set from  $-0.8$  to  $0.4$  V for the 50  $\mu\text{m}$ -diameter electrodes. CV measurements at several scan rates were taken: 0.2, 0.6, and  $1 \text{ V s}^{-1}$ .

## 4.3 | MEA Acquisition Setup

Neural activity was acquired and amplified using Intan RHD amplifier chips (RHD2132) and digitized by the Intan RHD USB Interface Board (Intan Technologies, Los Angeles, CA). To facilitate the connection between the MEA devices and the Intan recording system, a custom-designed interface was developed. This setup, illustrated in Figure S1, included a custom-printed circuit board (PCB) that interfaced the MEA pads with Omnetics connectors, which were linked to two 32-channel Intan recording headstages (containing RHD2132 chips). The RHD USB

Interface Board was connected to a computer running RHX Data Acquisition Software, enabling real-time data collection and analysis.

The custom PCB was designed to support up to 60 channels (59 recording electrodes and one internal reference electrode), ensuring compatibility with both the fabricated graphene-based MEAs and standard 60-channel commercial MEAs from Multichannel Systems GmbH. Spring-loaded pins, soldered to the custom PCB, ensured reliable electrical contact with the MEA pads. To maintain stable mechanical coupling between the MEA and the custom PCB, laser-cut components were fabricated from 2 mm-thick plexiglass sheets. These components were designed to securely host the MEA while maintaining proper alignment between the MEA pads and the spring-loaded pins on the PCB. By applying pressure through screws mounted on the assembly, the spring-loaded pins were pressed against the MEA pads, ensuring reliable and consistent electrical contact (Figure S1c).

## 4.4 | Acute Cerebellar Slice Preparation

All animal experiments were approved by the national Central Commissie Dierproeven and the institutional animal welfare committee of Erasmus MC. A male C56/BL6 mice of 3 months old, bred at the in-house animal facility of Erasmus MC, were decapitated under isoflurane anesthesia. Subsequently, the cerebellum was removed and transferred into ice-cold slicing medium containing (in mM): 240 sucrose, 5 KCl, 1.25  $\text{Na}_2\text{HPO}_4$ , 2  $\text{MgSO}_4$ , 1  $\text{CaCl}_2$ , 26  $\text{NaHCO}_3$ , and 10 D-glucose, bubbled with 95%  $\text{O}_2$  and 5%  $\text{CO}_2$ . Parasagittal slices 250  $\mu\text{m}$  thick of the cerebellar vermis were cut using a Leica vibratome (VT1000S, Nussloch, Germany) and kept in artificial cerebrospinal fluid (aCSF) containing (in mM): 124 NaCl, 5 KCl, 1.25  $\text{Na}_2\text{HPO}_4$ , 2  $\text{MgSO}_4$ , 2  $\text{CaCl}_2$ , 26  $\text{NaHCO}_3$ , and 20 D-glucose, bubbled with 95%  $\text{O}_2$  and 5%  $\text{CO}_2$  for  $> 1$  h at  $34^\circ\text{C}$  before the experiments started.

## 4.5 | Electrophysiological Recordings

Extracellular activity from cerebellar brain slices was acquired at a 20 kHz sampling rate, using the MEA-to-Intan interface system described in section 4.3. The complete acquisition setup was placed inside a Faraday cage, with the ground pin of the Intan RHD USB Interface Board connected to it, establishing a common ground reference. ACSF was manually perfused over the slice to maintain tissue viability. To ensure close contact between the slice and the MEA, a slice anchor with parallel nylon fibers was gently pressed onto the tissue. Prior to recording from a slice, a baseline signal was acquired for several minutes to assess the noise level of the system.

## 4.6 | Data Analysis

Recordings were post-processed with a custom Matlab script using Signal Processing Toolbox. The data processing technique was based on previous work [42, 51]. The first step involved filtering the signals using a second-order IIR bandpass filter from 200 to 2000 Hz, effectively isolating the frequency components relevant to spiking activity. Because IIR filters can largely

distort the spike shapes due to phase nonlinearities, a zero-phase digital filtering was applied. After filtering, spikes were detected using an amplitude thresholding method based on the median absolute deviation (MAD) of the filtered signal. The detection threshold was initially set at 6 times the MAD. For the averaged detected spike waveforms depicted in Figure 3d, this threshold was readjusted by visual inspection to isolate higher amplitude spikes typically corresponding to neurons located closer to the recording electrode. This approach, while requiring manual intervention, provided a fast and straightforward method to minimize contributions from distant neurons, ensuring a more accurate representation of nearby neural activity. Additionally, to avoid detecting multiple spikes within the same action potential event, a refractory period of 2.5 ms was applied.

Finally, the signal-to-noise ratio (SNR) was computed by calculating the ratio of the maximum peak-to-peak amplitude of the neural spikes,  $V_{pp,signal}$ , to the standard deviation of the noise in the baseline signal,  $\sigma_{noise}$ , as shown in the expression below:

$$SNR=20 \log \frac{V_{pp,signal}}{\sigma_{noise}} \quad (1)$$

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### Conflicts of Interest

The authors declare no conflicts of interest.

### Data Availability Statement

The data that support the findings of this study are available from the corresponding author upon reasonable request.

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### Supporting Information

Additional supporting information can be found online in the Supporting Information section.

**Supporting File:** advs73844-sup-0001-SuppMat.pdf.