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# High-dynamic baseline determination for the Swarm constellation

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#### Abstract

Baseline determination for the European Space Agency Swarm magnetic field mission is investigated. Swarm consists of three identical satellites -A, -B and -C. The Swarm-A and -C form a pendulum formation whose baseline length varies between about 30 and 180 km. Swarm-B flies in a higher orbit, causing its orbital plane to slowly rotate with respect to those of Swarm-A and -C. This special geometry results in short periods when the Swarm-B satellite is adjacent to the other Swarm satellites. Ten 24-hr periods around such close encounters have been selected, with baseline lengths varying between 50 and 3500 km. All Swarm satellites carry high-quality, dual-frequency and identical Global Positioning System receivers not only allowing precise orbit determination of the single Swarm satellites, but also allowing a rigorous assessment of the capability of precise baseline determination between the three satellites. These baselines include the high-dynamic baselines between Swarm-B and the other two Swarm satellites.

For all orbit determinations, use was made of an Iterative Extended Kalman Filter approach, which could run in single-, dual-, and triple-satellite mode. Results showed that resolving the issue of half-cycle carrier phase ambiguities (present in original release of GPS RINEX data) and reducing the code observation noise by the German Space Operations Center converter improved the consistency of reduced-dynamic and kinematic baseline solutions for both the

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Swarm-A/C pendulum pair and other combinations of Swarm satellites. All modes led to comparable consistencies between the computed orbit solutions and satellite laser ranging observations at a level of 2 cm. In addition, the consistencies with single-satellite ambiguity fixed orbit solutions by the German Space Operations Center are at comparable levels for all the modes, with reduced-dynamic baseline consistency at a level of 1-3 mm for the pendulum Swarm-A/C formation and 3-5 mm for the high-dynamic Swarm-B/A and -B/C satellite pairs in different directions.

Keywords: Precise Baseline Determination, Precise Orbit Determination, Swarm, Ambiguity fixing, Half-cycle ambiguity

#### 1. Introduction

Satellite formations and constellations have been increasingly utilized to ful-

fill various research objectives [1]. Data collected by their on-board instruments

4 offer adequate information to satisfy complex scientific and operational tasks.

5 For instance, two Low Earth Orbiting (LEO) satellites in close formation are

6 used for observing the temporal and spatial variations of Earth's gravity field

[2] or for producing digital elevation maps [3]. As a prerequisite for these state-

of-the-art applications, satellite orbits and especially also baselines have to be

9 precisely determined, the latter with (sub-)mm level precision. Precise baseline

solutions are crucial for e.g. interferometric Synthetic Aperture Radar (SAR)

missions [4] and have the potential benefit of supporting gravity field research

12 [5].

Formation flying LEO satellites typically make use of high precision, dual-

frequency multi-channel GPS receivers for Precise Orbit Determination (POD)

<sub>15</sub> [6]. By forming Double-Differenced (DD) carrier phase observations, common

6 errors are strongly mitigated and so-called integer ambiguities can be resolved

[7]. With the advent of the GRACE mission [2], it has been proved that Precise

Baseline Determination (PBD) at 1-mm level is feasible by fixing DD carrier

phase ambiguities [8]. Further improvements are obtained by making use of

relative dynamics constraints and GPS receiver antenna patterns. Nowadays, sub mm level baseline precision is achievable for in-line or along-track forma-21 tions like the Gravity Recovery and Climate Experiment (GRACE) mission [9, 10, 11]. For a more complex side-by-side or radial/cross-track formation such as the TanDEM-X/TerraSAR-X mission, it is claimed that a precision in each direction of 3-8 mm can be achieved [4]. On 22 November 2013, the European 25 Space Agency (ESA) geomagnetic field mission Swarm was launched and soon the three Swarm satellites entered their preferred orbits by a series of dedicated maneuvers [12]. It is an unprecedented three-identical-satellite constellation equipped with the same space-borne instruments. All Swarm satellites fly in near-polar orbits, with Swarm-A/C in a pendulum formation and Swarm-B at 30 a higher altitude [12]. The distance between the Swarm-A and -C satellites is 31 varying between 30 and 180 km. When Swarm-B is in view of the other Swarm satellites, the distance can be as small as about 50 km. For the pendulum part of Swarm, PBD has already been studied in detail, showing that consistencies between reduced-dynamic and kinematic solutions under different in-flight envi-35 ronment can be achieved that are of the order of 5-40 mm in different directions [13, 14]. At present, no successful consistently high-precision high-dynamic PBD research has been done for such kind of constellation. 38

Obtaining very precise baseline solutions for LEO satellites that do not fly
in stable formation is still an open issue. For example, the work described in
[15] shows that it is not straightforward to achieve precise baseline solutions
between the CHAMP and GRACE satellites when these satellites are in view
of each other. The CHAMP-GRACE baselines grow easily from hundreds of
kms to thousands of kms in one day and these are therefore referred to as highdynamic baselines. The same applies to the Swarm-B satellite with respect to
the Swarm-A and -C satellites. As the baseline - or distance - between two
LEO satellites grows, the number of GPS satellites that are simultaneously in
view of two GPS receivers drops, resulting in a smaller number of possible DD
combinations. Moreover, LEO satellites experience different perturbing forces
when at different altitudes, especially atmospheric drag due to different density

1 levels [16].

The three-identical-satellite Swarm constellation will be used as a test bed for high dynamic baseline determination between LEO satellites. The results in [15] are based on 24-hr orbital arcs that start and end at midnight, which leads to significantly different CHAMP-GRACE orbital geometries for each arc. Moreover, CHAMP and GRACE carry GPS BlackJack receivers with different 56 performance and also have different antenna installation geometries [17]. For CHAMP and occasionally for GRACE, also so-called cross-talk signal interference between the POD and radio occultation antenna's took place leading to different multi-path patterns [18, 11]. For Swarm, this is not the case. Compared to the work described in [15], a different approach is adopted for defining 61 the orbital arcs. A total of 10 days are identified in the period from mid-July to mid-September in 2014 when the Swarm satellites are frequently in view of each other. The time of closest approach is then determined and a 24-hr orbital arc is defined starting 12 hr before and ending 12 hr after this time. This leads to comparable and more stable geometries for each selected orbital arc.

The RUAG Space Swarm GPS receiver exhibits half- and full-cycle ambiguities due to the tracking issue with its Numerically Controlled Oscillator (NCO) [19, 14]. Systematic 180° phase rotation frequently happens during the tracking process [20]. This makes carrier phase integer ambiguity fixing more challenging. Fixing half-cycle ambiguities erroneously to full-cycle will 71 significantly downgrade the baseline solution precision for the lower pair [10]. This receiver characteristic has thus to be properly dealt with. The German Space Operations Center (GSOC/DLR) has implemented an algorithm to correct the half-cycles into full-cycles by checking a certain bit of each carrier phase tracking record in the raw data [20]. In addition, a systematic GPS 76 RINEX converter software issue existed for code observations, leading to larger code noise at the early stage of the Swarm mission and was fixed by ESA on 11 April 2016 (https://earth.esa.int/web/guest/missions/esa-79 operational-eo-missions/swarm/news/-/article/swarm-software-issue-in-rinexconverter-fixed, last accessed: 9 January 2019). ESA has been re-creating these old Swarm RINEX files with both issues removed (the 8th Swarm Data Quality Workshop, https://earth.esa.int/web/guest/missions/esa-eo-missions/swarm/activities/conferences/8th-data-quality-workshop, last accessed: 9 January 2019). The resulting GPS data lead to significantly more precise single-satellite POD [21] and dual-satellite PBD solutions for the Swarm-A/C formation [14, 13]. Their impacts on the high-low satellite pairs will be investigated in this research.

For the Swarm mission, it is not possible to validate PBD solutions by comparison with independent data coming from for example a K-band Radar Ranging system as on board the GRACE twin satellites [22]. A quality check can typically be done by assessing the consistency between kinematic and reduced-92 dynamic baseline solutions [5, 10, 13]. Moreover, external POD and PBD solutions are available and can be used for a quality assessment. An interesting development is single receiver ambiguity fixing, leading to enhanced POD solutions [23, 20]. [23] propose a scheme of ambiguity fixing based on the ionosphere-free wide-lane model developed by [24], while [20] make use of the wide-lane phase 97 bias estimate products provided by [25]. Such single-satellite ambiguity fixed POD solutions have been made kindly available by GSOC/DLR for Swarm and will be used for assessing the quality of both POD and PBD orbit solutions in 100 this research [21]. Details of the single-satellite ambiguity fixed POD solutions 101 can be found in [20] for the Sentinel-3A satellite, which carries a GPS receiver 102 with similar characteristics when comparing with those flown by Swarm. An 103 external validation of the individual satellite orbit solutions is offered by the availability of Satellite Laser Ranging (SLR) observations, which will form part 105 of the analysis and quality assessments [26]. 106

The structure of this paper is as follows. Section 2 includes a description of the Swarm constellation data selection and corresponding quality assessment.

Section 3 introduces the kinematic and reduced-dynamic POD and PBD algorithms. Section 4 describes results and orbit comparisons for the Swarm constellation. This paper is concluded by Section 5, which includes a summary and outlook.

#### 2. Observations

#### 2.1. Data selection

Representative data have been selected to test PBD for all three Swarm 115 satellites. Table 1 includes three selected Keplerian orbital elements for Swarm 116 satellites at a representative epoch. The Swarm-A/C formation flies in two 117 almost identical polar orbits with only  $1.5^{\circ}$  difference in the right ascension of 118 the ascending node (RAAN). These two satellites form a so-called pendulum 119 formation. During the analyzed period the Swarm-B satellite flies about 50 km 120 higher, which slightly differs with the early designed orbit scheme [12, 27], and 121 the RAAN difference on average is about 10°. Baseline lengths of high-low 122 Swarm satellite pairs thus vary dramatically due to the different orbital planes 123 and altitudes. It is found that the period July-September 2014 includes days 124 for which the Swarm-A/B/C geometry is favorable, i.e. all three satellites are 125 in view of each other. During this period, the baseline lengths between the 126 Swarm-B satellite on the one hand and the Swarm-A and -C satellites on the 127 other hand reach a local minimum every 6.1 days.

To evaluate the PBD methods used in this research, a sliding 24-hr orbit arc 129 selection is done. Each selected orbit arc centers around the epoch of minimum 130 distance, see e.g. Figure 1. The Swarm-A/C formation baseline length varies 131 consistently between 30 and 180 km. For the Swarm-B/A and Swarm-B/C pairs, the two satellites approach each other from an approximate 3500 km 133 to a minimum of around 50 km. Ten orbit arcs are selected and recorded in 134 Table 2. The used GPS ephemeris products are separate 24-hr GPS satellite 135 orbits and 5-sec clock biases files [28]. Before making use of them, a tool is used 136 to interpolate the adjacent three consecutive 24-hr GPS satellite orbits into 5 seconds and then a merged orbit and clock file is created. The influence of GPS 138 orbit and clock bias gaps crossing midnight is reduced. 139

Figure 2 shows that the Swarm-A/C pendulum formation has on average > 7 common GPS satellites in view. This number is not yet influenced by the antenna field of view modification and is approximately equal to the number of

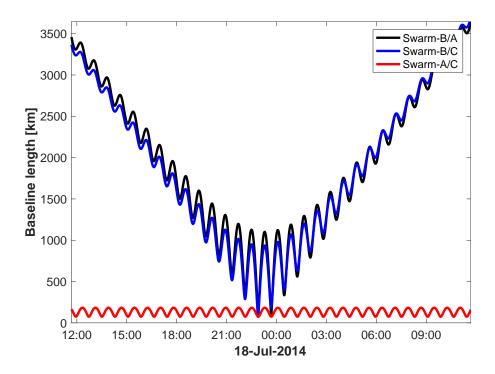


Figure 1: Length variations for each Swarm dual-satellite formation during one representative 24-hr orbit arc.

Table 1: The crucial Keplerian orbital elements determining the relation between Swarm orbital planes during mid-July to mid-September 2014. a represents the semi-major axis, i means the orbit inclination and  $\Omega$  is the right ascension of the ascending node (Credit: satellite two line elements data is obtained from www.space-track.org).

Satellite	a  (km)	i  (deg)	$\Omega$ (deg)
Swarm-A	6842.06-6840.75	87.35-87.36	197.53-175.66
Swarm-C	6842.05-6840.75	87.35-87.36	198.70-177.03
Swarm-B	6890.98-6890.41	87.75-87.76	206.28-188.59

Table 2: Ten selected 24-hr orbit arcs for Swarm constellation. Please note that DOY specifies the day of the center of the arc. This DOY number will be used as orbit arc identifier in this research.

Date	DOY	Middle of	Minimum
(YYYY-MM-DD)		the arc	distance (km)
2014-07-17	198	23:40:30	112.57
2014-07-24	205	02:50:40	85.69
2014-07-30	211	06:00:40	82.85
2014-08-05	217	08:23:30	120.39
2014-08-11	223	11:33:00	56.14
2014-08-17	229	13:55:10	51.84
2014-08-23	235	16:17:20	52.51
2014-08-29	241	18:39:10	70.62
2014-09-04	247	20:13:40	58.99
2014-09-10	253	21:47:50	64.91

GPS receiver tracking channels [13]. For the high-low Swarm satellite pairs, this
number drops from 6-8 to 4-6 as the baselines become longer. A low number
of common GPS satellites in view has a big impact on the achievable PBD
precision, especially for kinematic solutions. For high-quality PBD, at least 5
GPS satellites are required to be simultaneously tracked by two GPS receivers
[8]. If less than 5 GPS satellites are commonly in view, no kinematic PBD
solution will be generated for the associated epochs. Reduced-dynamic baseline

solutions will then however still be available.

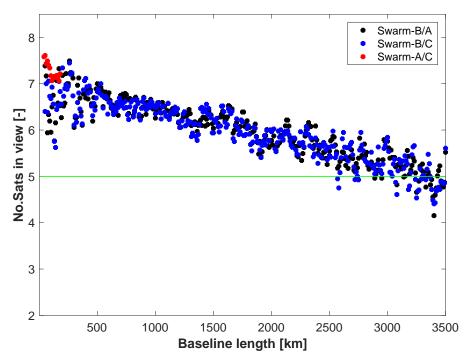


Figure 2: The number of GPS satellites simultaneously tracked by two GPS receivers as a function of distance (every 10 kms) for each Swarm dual-satellite formation (analysis for 10 24-hr orbit arcs).

# 2.2. Data quality assessment

GPS code and carrier phase observations are affected by several error sources, including thermal noise and multi-path. For the relevant Swarm data used in this research, the original GPS code observations suffer additionally from systematic errors due to sub optimal RINEX converter software leading to large noise levels. The code noise level has a clear impact on the ambiguity fixing success rate. The original carrier phase observations experience half-cycle ambiguity issues as mentioned above. A new version of Swarm GPS data was kindly provided by GSOC/DLR. For this version, the converter code error was removed and in addition the half-cycle carrier phase ambiguities were corrected to full-cycles.

The quality of in-flight GPS code observations can be assessed by analyzing 162 their multi-path effects by using the multi-path evaluation models that are in-163 troduced in [18, 29]. Thus, the multi-path represents an independent evaluation 164 of misfit caused by the systematic errors from the RINEX converter on the one 165 hand and the code observation noise on the other hand. The Root-Mean-Square 166 (RMS) of multi-path is displayed in Figure 3 for Swarm-A as a function of the 167 elevation of the GPS satellites as seen from the GPS receiver antenna installed 168 on the zenith surface of each Swarm satellite. The results displayed in Figure 3 hold for 17 July 2014, when the Swarm-A GPS antenna had an antenna field of 170 view of 80° (improved to 88° in October, 2014, [30]). The tracked GPS observa-171 tions below 10° antenna cut-off angle are obtained by the tracking performance 172 of GPS receiver antenna in its aft direction, as reported by [30]. 173

In general, the observation residual level drops with increasing elevation angle, which is in agreement with anticipated noise levels of GPS observations [18]. Modifications in the new version of data clearly reduce the code noise level. This analysis indicates a reduction from 0.34/0.37 m to 0.18/0.20 m in terms of global RMS for the  $L_1/L_2$  frequencies. Code noise on the  $L_1$  frequency is slightly smaller than on the  $L_2$  frequency. It is anticipated that the ambiguity fixing will improve when using the new batch of data.

Research in [14, 13] confirms that the GPS observation correction process 181 implemented by GSOC/DLR has a clear impact on the ambiguity fixing process, 182 as also shown in Figure 4 in this research. This figure is representative for a 183 triple-satellite PBD (see Section 3.1) and displays the ambiguity fixing success 184 rate as a function of the number of iterations completed by the IEKF (with a 185 maximum of 20). In the IEKF procedure, the ambiguities for the pendulum 186 formation Swarm-A/C pair are fixed first (requiring around 6 iterations until 187 convergence), after which as many as possible ambiguities are fixed for the 188 Swarm-B/A and Swarm-B/C pairs. It can be observed that the ambiguity fixing is clearly enhanced by using the new version of the data. For the Swarm-A/C 190 formation, the success rate for the first iteration is improved from 37% to 97%. 191 The final fixing success rate increases from 88% to 98%. For the Swarm-B/A

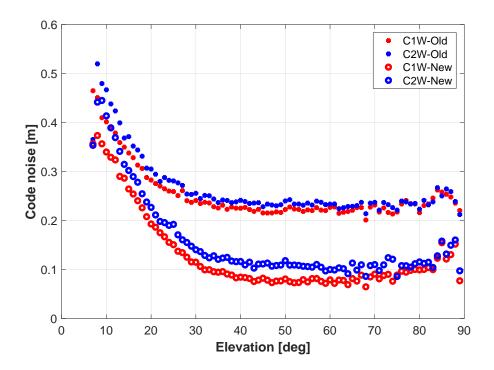


Figure 3: RMS of code multi-path as a function of elevation for the GPS  $L_1$  and  $L_2$  frequencies for two versions of Swarm-A GPS receiver RINEX data: Old indicates the ESA original file with RINEX converter software issues, New indicates the one corrected by GSOC/DLR and used in this research (selected day: DOY 198, 2014).

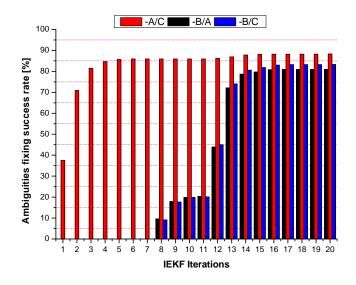
and Swarm-B/C combinations, fixing starts at iteration 8 for the old version of 193 the data and iteration 7 for the new version of the data. It can also be clearly 194 seen that for the starting iteration, the success rate improves from merely 9% 195 and 8% to a much higher level of 64% and 64% for the Swarm-B/A and Swarm-B/C combinations, respectively. The final success rates reach about 97% and 97%, respectively, which is much higher than 81% and 83% when using the old 198 version of the data. 199

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Swarm dual-satellite PBD (again, please see Section 3.1) is done to evaluate the influence of half-cycle vs. full-cycle inter ambiguity fixing. As shown in table 3, the ambiguity fixing success rate is improved by more than 10% when full-cycle ambiguities are to be fixed. The new version of the data also im-



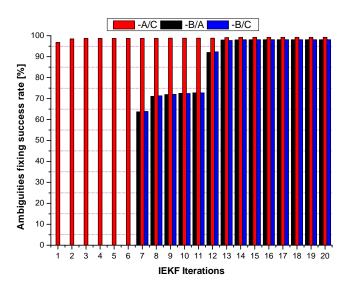


Figure 4: Integer ambiguity fixing success rate versus IEKF iterations for the triple-satellite Swarm PBD. Two sets of data, original version (top) and new version with corrections (bottom) are used (selected day: DOY 198, 2014).

 $_{204}$  proves the kinematic and reduced-dynamic baseline consistency, especially for two high-dynamic Swarm-B/A and Swarm-B/C satellite pairs. Therefore, for

the remainder of this paper, results will be based on the new version of the data (Section 4).

Table 3: Mean of daily RMS differences between kinematic and reduced-dynamic baseline solutions, and ambiguity fixing success rate for Swarm constellation (dual-satellite PBD solutions). Two sets of Swarm GPS RINEX data are used.

Solution	Radial	Along-track	Cross-track	Amb.fix.
	(mm)	(mm)	(mm)	(%)
		Swarm-A/	C	
Half-cycle	15.0	7.8	4.1	86.9
Full-cycle	12.4	5.5	3.6	98.1
		Swarm-B/	A	
Half-cycle	24.9	11.2	5.3	84.2
Full-cycle	22.9	9.8	5.6	97.3
${f Swarm-B/C}$				
Half-cycle	24.9	11.4	6.5	83.9
Full-cycle	22.6	10.4	5.7	97.5

## 3. Methodology

### 209 3.1. Single-, dual- and triple- POD/PBD

When solely using dual-frequency high-precision GPS tracking data and GPS satellite orbit/clock products, instantaneous satellite positions can be determined at the observation epochs when a sufficient number of GPS satellites is in view. This approach is referred to as kinematic approach [31] and obviously leads to gaps in the position time series when there are gaps in the GPS observation data or when not enough GPS satellites are in view. Dynamic and reduced-dynamic orbit determination, which include force models to solve equations of motion, result in continuous time series of satellite positions [6]. Force

models are typically divided in (1) gravitational force models including the non-218 spherical gravity field, perturbations from  $3^{rd}$  bodies (Sun and the Moon), and 219 solid-earth and ocean tides, and (2) non-gravitational force models including the Sun radiation pressure, the Earth albedo pressure, and atmospheric drag. How-22 ever, the associated models are not perfect, and model errors can be absorbed 222 by so-called empirical accelerations [17]. 223

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The Multiple Orbit Determination using Kalman filtering (MODK, [15]) tool is an in-house developed add-on tool to the GPS High Precision Orbit Determination Software Tools (GHOST) [32]. MODK has the capability to provide reduced-dynamic single-, dual- and triple-satellite orbit solutions, where for the dual- and triple-satellite mode ambiguity fixing as well as further kinematic 228 baseline determination can be done. The core of the MODK tool is based on an Iterative Extended Kalman Filter (IEKF) process, where the GPS observations are used and modeled for each frequency, i.e.  $L_1$  and  $L_2$  [11]. A comprehensive description of the MODK tool and underlying method can be found in 232 Chapter 3.3 of [15]. 233

Compared to single-satellite POD, PBD in case of dual- and triple-satellite 234 orbit determination includes the possibility to constrain differential empirical 235 accelerations, which is especially relevant if two satellites fly in almost iden-236 tical orbits (as is the case for Swarm-A and -C). This constraining proved to 237 be very beneficial for estimating high-precision baselines for the GRACE tan-238 dem and for the Swarm-A/C pendulum formations [10, 13]. In this study the frequency-dependent antenna Phase Center Variation (PCV) maps created by so-called residual approach are included [33, 11]. Our proposed Code Residual 241 Variation (CRV) maps are not modelled since the used GSOC/DLR processed 242 data have lower noise levels than the original data. Besides, no significant sig-243 nal interference exists for Swarm when comparing with GRACE as described in [11].245

The MODK tool first computes reduced-dynamic orbit solutions, after which kinematic solutions are generated. The latter are based on the same modeled GPS observations, where use is made of the ambiguity fixing of the reduced-

dynamic solution. In order to minimize gaps in the kinematic satellite position time series, all available fixed integer ambiguities and otherwise float ambigu-250 ities are used. No kinematic solutions are computed for epochs for which less than 5 GPS satellites are simultaneously in view of each combination of two 252 GPS receivers, or epochs for which the RMS of GPS observation phase residu-253 als is above 5 cm. A Least Squares Method (LSM) is adopted for the kinematic 254 PBD. More detailed information and the data flow chart regarding the kinematic and reduced-dynamic approaches can be found in [13]. The MODK tool includes the option to define a preferred baseline, i.e. a pair of satellites for 257 which the ambiguity fixing is done first, after which the fixing is invoked for the 258 other baselines. For the Swarm triple-satellite PBD, this option is used and the 259 preferred baseline is the one for the pendulum Swarm-A/C satellite pair. 260

The DD ambiguities are resolved by the Least-squares Ambiguity De-correlation Adjustment (LAMBDA) algorithm [7]. It has been widely used for different 262 satellite formations PBD [8, 10, 11]. To maximize the ambiguity fixing success 263 rate, a subset fixing process is implemented. It allows for part of a set of integer 264 ambiguities to be fixed while for the remaining the associated float values are 265 used. This is not a conventional use of the LAMBDA algorithm, which nominally only accepts epochs when the entire set of ambiguities is fixed [8]. A strict 267 ambiguity fixing validation scheme is adopted and integrated in the MODK 268 tool [34, 11]. Moreover, an additional outlier detection check is included: if 269 the absolute value of GPS carrier phase observation residuals (after fixing) is above 5 cm, the associated ambiguity will be kept at its float value and sent into 27 IEKF for further fixing in the next iterations. It was found that this resulted in 272 a reduced chance of wrongly fixed integer ambiguities and thus a more robust 273 PBD by the IEKF as used by the MODK tool. 274

#### 275 3.2. Parameter settings

Due to the different orbit altitudes for the Swarm satellites (Table 1), especially uncertainties in the modeling of non-gravitational accelerations can be different for Swarm-A and -C on the one hand and Swarm-B on the other hand.

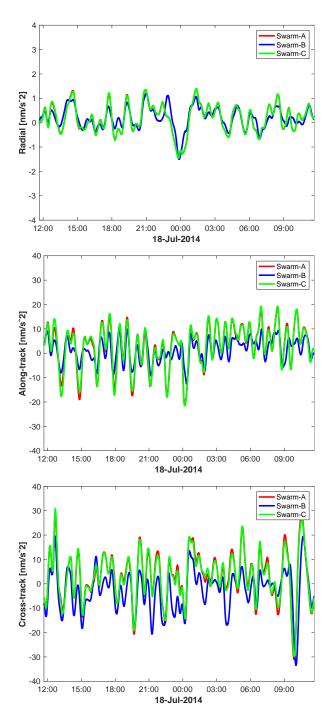


Figure 5: Time series of estimated empirical accelerations in the radial (top), along-track (middle) and cross-track (bottom) directions for each Swarm satellite based on triple-satellite PBD. Please note different scales are set for the vertical axes (DOY 198, 2014). Please note that the curves for Swarm-A and -C almost completely overlap.

This will lead to differences in the estimated empirical accelerations that are used to absorb modeling errors. Figure 5 shows typical levels of estimated em-280 pirical accelerations for the three Swarm satellites on a representative day. The statistics of them are shown in Table 4. The mean of estimates of empirical 282 accelerations represents the level of constant correction to the adopted dynamic 283 models in certain direction. Although for all three Swarm satellites, the val-284 ues seems to overlap to quite a significant extent, the empirical acceleration 285 differences for the Swarm-A/C pair are significantly smaller than for the other pairs. It can be observed that the empirical accelerations (mean and RMS-287 about-mean) are larger in the along-track direction, which is the direction for 288 which atmospheric drag is predominant, and the cross-track direction, which 289 is the direction for which mis-modeling of solar radiation pressure forces is the largest (also due to the simplified canon ball satellite model that is used by the MODK tool, the scaling factors of the associated non-gravitational forces can 292 not compensate the in-flight perturbations completely [13, 35]). 293

Table 4: Empirical acceleration estimate statistics for each Swarm satellite and satellite pair (mean and RMS-about-mean, DOY 198, 2014).

Sat/Pair	Radial	Along-track	Cross-track
	$(nm/s^2)$	$(nm/s^2)$	$(nm/s^2)$
Swarm-A	$0.2 \pm 0.6$	$2.9 \pm 8.2$	$3.2 \pm 9.8$
Swarm-B	$0.2\pm0.4$	$1.2\pm4.6$	$-2.6\pm8.2$
Swarm-C	$0.2 \pm 0.6$	$3.0\pm 8.3$	$3.2 \pm 9.5$
Swarm-A/C	$0.0\pm0.0$	$-0.0\pm1.1$	$-0.0\pm1.2$
Swarm-B/A	$0.0\pm0.3$	$-1.7 \pm 5.3$	$-5.8 \pm 6.5$
Swarm-B/C	$0.0\pm0.3$	$-1.7 \pm 5.4$	$-5.8 \pm 5.9$

The correlation time  $(\tau)$ , STandard Deviation (STD) of a-priori values  $(\sigma_a)$ and process noise  $(\sigma_p)$  of empirical accelerations have been tuned to reflect the typical level for these parameters, both in an absolute and relative sense. The adopted values are included in Table 5. It can be seen that the values for the STD for the difference between empirical accelerations is specified to be smaller for the Swarm-A/C pendulum satellite pair, reflecting their similarity of orbit (especially altitude).

Both GPS carrier phase and code observations are used by MODK to produce orbit solutions. The carrier phase weight is set inversely proportional to its claimed noise level, which is 3 mm for each frequency in POD and 5 mm in PBD as in that case single-differences are used. The code observation weight is set as 0.3 m for each frequency in POD and 0.5 m in PBD. The same force models and standards are used as specified in [13].

Table 5: Empirical acceleration parameter settings in three directions (radial/along-track/cross-track) for each Swarm satellite and each pair of satellites in IEKF. The correlation time  $\tau$  is equal to 600 s.

Sat/Pair	$\sigma_a$	$\sigma_p$
	$(nm/s^2)$	$(nm/s^2)$
Swarm-A	5/15/15	1/3/3
Swarm-B	5/15/15	1/3/3
Swarm-C	5/15/15	1/3/3
Swarm-A/C	2/5/5	0.2/1/1
Swarm-B/A	5/15/15	1/3/3
Swarm-B/C	5/15/15	1/3/3

# <sup>7</sup> 4. Results and discussion

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This section includes the results of the Swarm precise orbit and baseline determination for the selected 10 orbit arcs. The single-satellite ambiguity fixed GSOC/DLR kinematic and reduced-dynamic POD solutions serve as reference both for the absolute and baseline solutions, where the latter is referred to as the GSOC/DLR Differential POD or DPOD solution. Results for both dual-satellite (Section 4.2) and triple-satellite (Section 4.3) PBD will be provided

and discussed, followed by SLR validation (Section 4.4). However, this section starts with a brief result regarding the detection of GPS observation outliers.

#### 316 4.1. GPS data outliers

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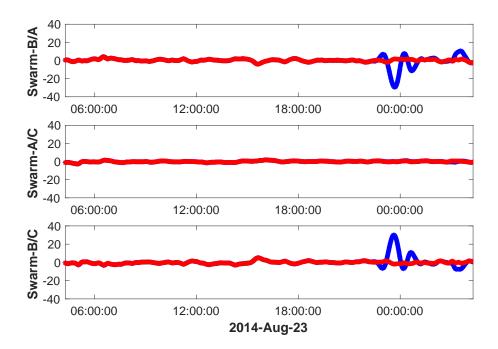


Figure 6: Consistency (unit:cm) between triple-satellite Swarm baseline solutions and baselines derived from the reference GSOC/DLR orbits in the along-track direction, both for including (blue) and excluding (red) the identified G04 outliers (22:50 to 23:50, on 23 August 2014). The consistency is included for the Swarm-B/A (top), Swarm-A/C (middle) and Swarm-B/C (bottom) satellite pairs.

GPS observation outliers are in principle detected automatically by the MODK tool (Section 2.2). It is important to report that for a few GPS satellite tracking passes very large observation residuals were obtained, *i.e.* after the automated outlier detection. This resulted in an unstable IEKF process. Therefore, these observations were excluded manually. To be precise, the following passes were eliminated: GPS Block IIA G04 for Swarm-B from 22:50 to 23:50 on 23 August 2014 (DOY 235) and GPS Block IIR-M G17 for Swarm-A from

23:50 on 04 September (DOY 247) to 00:50 on 05 September 2014. Block IIA GPS satellites are sometimes in eclipse affecting their yaw attitude motion [36]. 325 The outliers for 23 August can be attributed to G04 being in eclipse. The cause for the outliers during the other pass might be the inconsistency of GPS satellite 327 clock corrections spanning midnight. The impact of removing the outlying pass 328 is shown for 23 August 2014 in Figure 6. It can be seen that the impact of the 329 outlying pass reaches a level of 20 centimeters. The eliminated data accounts 330 for less than 0.5% of all GPS available observations. It has to be noted that for PBD the relevant GPS tracking passes are excluded for all three satellites when 332 forming DD combinations. 333

#### 334 4.2. Dual-satellite PBD

Three dual-satellite PBD solutions can be obtained for Swarm. For each 335 possible pair of Swarm satellites, selected parameter settings are included in 336 Table 5. An ephemeris comparison is done for each satellite between its MODK 337 dual-satellite PBD solution and external GSOC/DLR solutions (Table 6). As for 338 reduced-dynamic POD, two edges of each orbit often show large inconsistency when comparing with adjacent orbits. These edge effects will be exaggerated 340 by differentiating two GSOC/DLR orbits directly. Therefore two 15 min edges 341 of each MODK or GSOC/DLR orbit are neglected for all baseline comparisons 342 in this research, namely 23-hr baseline comparisons are done instead of 24hr. An example is shown in Figure 7 for 5 August 2014 (DOY 217), which indicates that the edge effects cause clearly larger inconsistency between two 345 solutions. Therefore these influence will be excluded for the following ephemeris 346 comparisons. 347

In general the different reduced-dynamic orbit solutions show a good level of consistency: the RMS-about-mean of orbit differences is about 5-7 mm for the radial and cross-track directions. For the along-track direction, this is around 12 mm level, which corresponds to a larger dynamic modeling difference between two institutes. Moreover, the comparison shows mean orbit differences of about 2-5 mm in the radial and cross-track directions. They again indicate

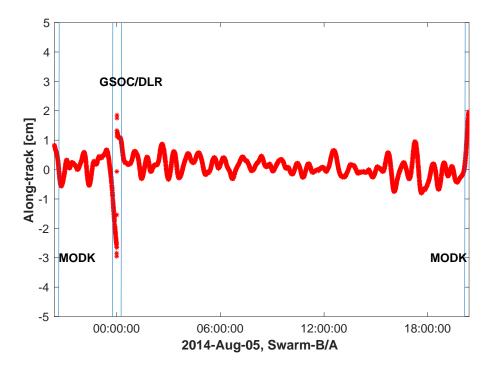


Figure 7: Ephemeris comparison between MODK reduced-dynamic solution and GSOC/DLR single receiver ambiguity fixed reduced-dynamic orbits in along-track direction for the Swarm-B/A baseline (DOY 217, 2014). The excluded edge effects of MODK solution and GSOC/DLR solution are indicated by the legends and blue vertical lines: for the MODK solution, the first and last 15 minutes of an orbit arc are excluded; for the GSOC/DLR solution, the 30 minutes around midnight of an orbit arc are excluded.

the differences between the satellite cannon-ball model used in this research and the panel box-wing macro-model used in [21]. The mean of differences in the radial direction can be attributed to the missing Earth albedo modeling in this research. More sophisticated dynamic modeling of satellite is beneficial for POD and PBD [35, 37], however it goes beyond the scope of this research.

Results of the ephemeris comparisons in terms of baseline are displayed in Table 7. It has to be noted that the GSOC/DLR solutions are provided from midnight to midnight, which differs with the 24-hr arc in this research. The comparisons have been done for both the reduced-dynamic and kinematic MODK baseline solutions. It can be observed that the mean of baseline differences is

Table 6: Ephemeris comparison between different dual-satellite reduced-dynamic MODK baseline solutions and GSOC/DLR single receiver ambiguity fixed reduced-dynamic orbits (mean and RMS-about-mean, 10 orbit arcs).

Satellite	PBD solution	Radial	Along-track	Cross-track
		(mm)	(mm)	(mm)
Swarm-A	Swarm-A/C	$4.8 \pm 6.0$	$-2.8 \pm 12.8$	$1.4 \pm 7.1$
	Swarm-B/A	$4.9 \pm 6.0$	$-2.7\pm12.4$	$3.1 \pm 7.1$
Swarm-B	Swarm-B/A	$5.0 \pm 5.3$	$-0.7\pm11.1$	$3.3 \pm 6.7$
	$\operatorname{Swarm-B/C}$	$5.0 \pm 5.4$	$-0.4\pm11.5$	$3.2 \pm 7.1$
Swarm-C	Swarm-A/C	$4.7 \pm 5.9$	$-1.3\pm12.8$	$1.3 \pm 7.2$
	$\operatorname{Swarm-B/C}$	$4.8 \pm 5.7$	$-0.4 \pm 12.1$	$2.9 \pm 7.1$

very small, typically below 1 mm for the radial and cross-track directions, and below 2.5 mm for the along-track direction. It is clear that common single-365 satellite orbit errors are canceled to a large extent when forming baselines, cf. 366 Table 6. For the reduced-dynamic solutions, a 1-3 mm level consistency is ob-367 tained for the Swarm-A/C baseline. This is slightly worse than the level of consistency as reported in [13], in which only a comparison for the Swarm-A/C pair was done and the GSOC/DLR baselines were also DD ambiguity fixed so-370 lutions. [13] selected a more quiet ionospheric activity period (January 2016) 371 for comparison. Stronger ionospheric activities bring more challenging issues for precise baseline determination [38]. For the other two reduced-dynamic base-373 lines, larger differences are obtained, which is due to the less favorable geometry 374 between the associated two satellites. 375

For the kinematic baselines, the consistency between the MODK and the reference GSOC/DLR orbit solutions is worse (Table 7). The consistency level is comparable to the consistency between the MODK reduced-dynamic and kinematic orbit solutions (Table 3). The consistency for Swarm-A/C is better than for Swarm-B/A and Swarm-B/C, which can be attributed to the less favorable

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geometry when these satellites are at larger distances. Kinematic solutions will not be computed when less than 5 GPS satellites are in view by two Swarm 382 satellites, therefore the percentage of epochs with available kinematic solutions drops as the distance gets longer for satellite pairs. Another comparison is done 384 between baselines derived from GSOC/DLR kinematic and reduced-dynamic 385 DPOD solutions. It is interesting to observe that for the GSOC/DLR kine-386 matic baseline comparison, a similar level of consistency is obtained for all 387 three baselines, thus including Swarm-A/C. The MODK kinematic baselines display better consistency with the GSOC/DLR DPOD reduced-dynamic refer-380 ence orbits than the associated GSOC/DLR DPOD kinematic orbits, even for 390 Swarm-B/A and Swarm-B/C formations for which the lengths are varying up to 391 3500 km. This can be explained by considering that in single-satellite POD, no advantage can be taken of e.g. constraining relative dynamics, as are done for Swarm-A/C with the MODK tool. Nevertheless, the GSOC/DLR kinematic so-394 lutions for the high-dynamic satellite pairs have around 10% higher availability 395 than the MODK solutions. 396

#### 397 4.3. Triple-satellite PBD

When comparing the kinematic and reduced-dynamic baseline consistency 398 obtained by dual-satellite and triple-satellite PBD, respectively, slightly down-399 graded consistency can be seen for the triple-satellite case in Table 8. Table 9 400 shows the direct comparison between satellite orbits computed using the triplesatellite PBD mode and the GSOC/DLR single-satellite reference orbit solu-402 tions. This in general also corresponds to the results in Table 6. The results 403 indicate that by including a third Swarm satellite leading to high-dynamic base-404 lines does not significantly degrade the baselines solution for the Swarm-A/C 405 pendulum pair.

Table 10 shows the results of comparison between Swarm triple-satellite PBD solutions and baselines derived from the reference GSOC/DLR orbits. When comparing with dual-satellite mode, in general around 2.6% less kinematic solutions are created for Swarm-A/C baseline due to more data editing for three

Table 7: Comparison between different MODK baseline solutions (dual-satellite PBD) and baselines derived from the GSOC/DLR DPOD reduced-dynamic reference orbits (mean and RMS-about-mean, 10 orbit arcs), another comparison is done between the GSOC/DLR DPOD kinematic and reduced-dynamic reference orbits. The percentage of epochs with available kinematic solutions is also shown.

Solution	Radial	Along-track	Cross-track	Perc.	
	(mm)	(mm)	(mm)	(%)	
MODK Red	MODK Reduced-dynamic				
Swarm-A/C	$-0.0\pm1.6$	$2.1\pm2.9$	$-0.1\pm1.4$	100	
Swarm-B/A	$0.7 \pm 4.7$	$1.6 \pm 6.7$	$0.2\pm3.5$	100	
Swarm-B/C	$-0.2\pm2.9$	$0.7 \pm 4.3$	$-0.2\pm3.0$	100	
MODK Kin	ematic				
Swarm-A/C	$-0.1\pm11.9$	$2.2 \pm 5.7$	$-0.1\pm3.5$	97.7	
Swarm-B/A	$-0.2\pm22.8$	$2.0\pm12.0$	$0.4 \pm 6.3$	80.2	
Swarm-B/C	$0.9 \pm 21.3$	$0.3\pm10.0$	$-0.4 \pm 5.9$	81.3	
DLR DPOI	) Kinematic				
Swarm-A/C	$0.2\pm21.2$	$0.1\pm8.3$	$-0.1 \pm 6.3$	93.7	
Swarm-B/A	$-0.1\pm25.0$	$1.0\pm11.6$	$0.0\pm7.6$	91.7	
Swarm-B/C	$0.2\pm25.4$	$-1.0 \pm 11.6$	$-0.1 \pm 7.6$	91.8	

satellites. Compared to the dual-satellite mode, more single-differenced combi-411 nations have to be established and pass the data editing because of the involve-412 ment of Swarm-B [15]. It is found that the single-differenced clock offset editing - highly determined by the relative ionospheric changes between two satellites is the dominant impact factor which discards more than 1% data for each 415 satellite. However for especially Swarm-B/A baseline a slight improvement of 416 1% is obtained, which can be attributed to more kinematic solutions passing 417 the residual assessment. Dual-satellite PBD mode lacks constraint from the third satellite, therefore more solutions at larger distance will fail to pass this 419 test. The baseline consistency between the MODK kinematic solutions and the 420

Table 8: Comparison between MODK kinematic and reduced-dynamic baseline solutions, and ambiguity fixing success rate for dual- and triple-satellite PBD (mean of RMS-about-mean statistics of 10 orbit arcs).

Solution	Radial	Along-track	Cross-track	Amb.fix.	
	(mm)	(mm)	(mm)	(%)	
		Swarm-A/	$^{\prime}\mathbf{C}$		
Dual-	12.4	5.5	3.6	98.1	
Triple-	13.9	6.4	4.0	98.4	
		Swarm-B/	<b>'A</b>		
Dual-	22.9	9.8	5.6	97.3	
Triple-	23.4	10.0	5.8	97.3	
	${f Swarm-B/C}$				
Dual-	22.6	10.4	5.7	97.5	
Triple-	23.5	10.4	5.9	97.4	

Table 9: Comparison between the Swarm triple-satellite reduced-dynamic PBD orbits of each satellite and the reference GSOC/DLR reduced-dynamic orbit (mean and RMS-about-mean, 10 orbit arcs).

Solution	Radial	Along-track	Cross-track
	(mm)	(mm)	(mm)
Swarm-A	$4.8 \pm 5.7$	$-2.7\pm12.0$	$3.8 \pm 7.2$
Swarm-B	$4.9 \pm 5.4$	$-0.6 \pm 11.6$	$3.9 \pm 7.1$
Swarm-C	$4.7 \pm 5.7$	$-0.5\pm12.3$	$3.6 \pm 7.3$

reference solutions is similar compared to the result for dual-satellite PBD (Ta-

 $_{422}$  ble 7), which corresponds to the results in Tables 8 and 9. Nevertheless, for the

triple-satellite PBD, the reduced-dynamic baseline solutions, especially baselines

involving Swarm-A, have slightly better agreement with the GSOC/DLR orbits.

For the Swarm-A/C pair an improvement from 1.6/2.9/1.4 to 1.5/2.6/1.4 mm is obtained, for the Swarm-B/A pair 4.7/6.7/3.5 to 3.3/4.7/3.3 mm, and for the Swarm-B/C pair a slight degradation from 2.9/4.3/3.0 to 3.1/4.6/3.1 mm. It will be assessed in Section 4.4 if the absolute orbit solutions are influenced by the triple-satellite PBD.

Table 10: Comparison between different MODK baseline solutions (triple-satellite PBD) and the baselines derived from the reduced-dynamic GSOC/DLR reference orbits (mean and RMS-about-mean, 10 days). The percentage of epochs with available kinematic solutions is also shown.

Solution	Radial	Along-track	Cross-track	Perc.	
	(mm)	(mm)	(mm)	(%)	
MODK Red	MODK Reduced-dynamic				
Swarm-A/C	$-0.1\pm1.5$	$2.2\pm2.6$	$-0.1\pm1.4$	100	
Swarm-B/A	$0.6\pm3.3$	$1.5\pm4.7$	$0.1\pm3.3$	100	
$\operatorname{Swarm-B/C}$	$-0.2\pm3.1$	$0.7 \pm 4.6$	$-0.2\pm3.1$	100	
MODK Kin	MODK Kinematic				
Swarm-A/C	$-0.0 \pm 13.0$	$2.2 \pm 6.2$	$-0.1\pm3.8$	95.1	
Swarm-B/A	$-0.6\pm22.2$	$2.3\pm10.0$	$0.5 \pm 6.2$	81.5	
Swarm-B/C	$1.1\pm22.5$	$0.1\pm10.8$	$-0.6 \pm 6.3$	81.2	

Figure 8 depicts a one day comparison between two kinematic solutions and 430 the GSOC/DLR-derived reduced-dynamic baseline solution for three satellite 431 pairs. It shows periodic peaks, especially for the Swarm-A/C pair whose baseline 432 length is varying between 30 to 180 km. They fly simultaneously over two poles with the smallest distance. However, they also experience the worst consistency 434 in the polar areas. [39, 13, 14] all report that ionospheric activities clearly 435 deteriorate the POD and PBD solutions above the geomagnetic poles. The 436 ionospheric activity became stronger as the 11-year solar cycle was approaching 437 its peak at the end of 2014.

Figure 9 takes one example and shows the baseline consistency between the

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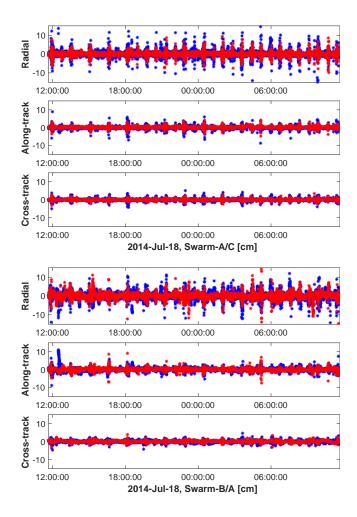


Figure 8: Ephemeris comparison (unit:cm) for the GSOC/DLR(blue) and MODK(red) kinematic baselines for the Swarm-A/C (top), Swarm-B/A(bottom) satellite pairs, the GSOC/DLR DPOD reduced-dynamic baselines are set as reference (DOY 198, 2014). The comparison for Swarm-B/C pair is similar with Swarm-B/A pair.

MODK kinematic and reduced-dynamic solutions as a function of the distance between two associated satellites for a representative day. This consistency is displayed for each individual direction, where the direction is defined by the local-horizontal, local-vertical reference frame (*i.e.* radial, along-track and crosstrack direction) of a reference satellite (Swarm-A for Swarm-B/A and SwarmA/C formations, and Swarm-B for Swarm-B/C formation). Baseline consistency for the radial direction is the worst, which can be explained by geometry, *i.e.* the largest component of Geometric Dilution Of Precision (GDOP) is in this direction.

Figure 9 also shows that the availability of kinematic solutions drops when 449 the distance between the two associated satellites increases. As shown in Fig-450 ure 2, the number of simultaneously tracked GPS satellites by two on-board 451 GPS receivers drops when the distance increases. Eventually, there will not be 452 sufficient satellites simultaneously in view to compute a kinematic baseline so-453 lution. Apparently the spatial geometry for the more dynamic Swarm-B/A and 454 Swarm-B/C pairs deteriorates more quickly. In general the Swarm-B/A and 455 Swarm-B/C satellite pairs have only 81.5% and 81.2% of epochs with kinematic solutions, respectively, compared to 95.1% for the Swarm-A/C satellite pair (see Table 10). It can be observed in Figure 9 that the consistency between kinematic 458 and reduced-dynamic baselines solutions become slightly worse with increasing 459 distance. The consistency statistics are shown in Table 10, which indicate that 460 13.0/6.2/3.8 mm is achievable for the Swarm-A/C satellite pair in respectively 461 the radial, along-track and cross-track directions. For the Swarm-B/A satellite 462 pair, a degraded consistency level of 22.2/10.0/6.2 is obtained, similar to the 463 Swarm-B/C satellite pair. 464

## 4.4. Satellite Laser Ranging

The availability of SLR observations for the Swarm constellation allows for 466 an independent validation of orbit solutions in the line-of-sight direction between 467 the SLR ground stations and each LEO satellite [40]. An editing threshold of 468 30 cm is applied, which is more than an order of magnitude above the RMS of fit 469 levels. In addition, observations below a  $10^{\circ}$  elevation cut-off angle are excluded to eliminate observations with relatively large atmospheric delay correction er-471 rors. An SLR retro-reflector correction map from the German Research Center 472 for Geosciences (GFZ) is included [41]. Furthermore, four SLR stations (Are-473 quipa, Hartebeest, Kiev, Simeiz) with large mean offsets are excluded for the

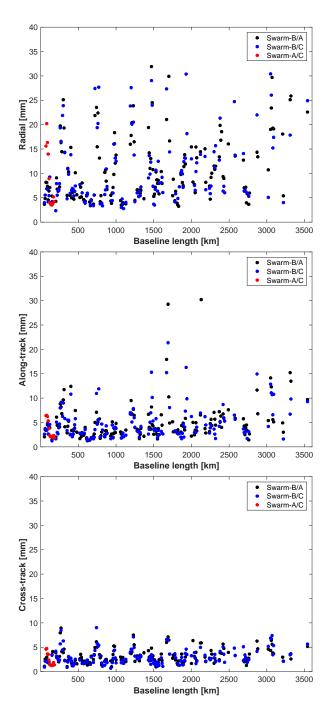


Figure 9: RMS of differences between kinematic and reduced-dynamic solutions as a function of distance (every 10 kms) in the radial (top), along-track (middle) and cross-track (bottom) directions for the three Swarm baselines (DOY 198, 2014).

75.3%(510/677) of the SLR observations are used for orbit validation of Swarm-476 A, -B and -C respectively (Table 11). It can be observed that for the MODK POD single-satellite orbits the RMS-478 about-mean of fit of SLR validation is quite close to the reference ESA reduced-479 dynamic Precise Science Orbits (PSO) [39]. In general, a consistency level 480 (RMS-about-mean) of around 20 mm is achieved for the three Swarm satellites. 481 The best performance is obtained for Swarm-B, which flies at the highest alti-482 tude. The best accuracy is found for the GSOC/DLR single-receiver ambiguity 483 fixed solutions. Similar to the analysis in [29, 15], the dual-satellite PBD results 484 in slightly worse SLR consistency levels. Note that for the Swarm-B satellite, 485 the consistency improves for the Swarm-B/C PBD, but not for the Swarm-B/A PBD solution. For the Swarm triple-satellite MODK PBD solution, similar levels are obtained. This indicates good consistency between dual-satellite and 488 triple-satellite modes of MODK. 489

Swarm SLR validations. Eventually 76.5%(649/848), 80.2%(1385/1726) and

Table 11: Mean and RMS-about-mean of fit of SLR observations for different reduced-dynamic orbit solutions for the 10 selected orbit arcs.

Solution	Swarm-A	Swarm-B	Swarm-C
	(mm)	(mm)	(mm)
ESA	$1.5 \pm 18.4$	$-2.8 \pm 14.7$	$1.9 \pm 21.0$
$\operatorname{GSOC}/\operatorname{DLR}$	$1.1\pm17.5$	$1.0\pm11.1$	$1.6\pm21.2$
POD	$-1.1\pm20.8$	$-4.0\pm14.1$	$0.8 \pm 21.6$
PBD Swarm-A/C	$-0.7\pm21.0$	NA	$0.7 \pm 22.1$
PBD Swarm-B/A	$-0.8 \pm 19.2$	$-2.2\pm14.3$	NA
PBD Swarm-B/C	NA	$-3.7\pm12.7$	$1.1\pm22.3$
PBD Swarm-A/B/C	$-0.9 \pm 19.7$	$-3.5 \pm 12.9$	$1.3\pm22.2$
No.	649	1385	510

The Swarm-A/C satellites fly in formation with a baseline below 180 km.

Therefore it is possible that an SLR station switches between these two Swarm

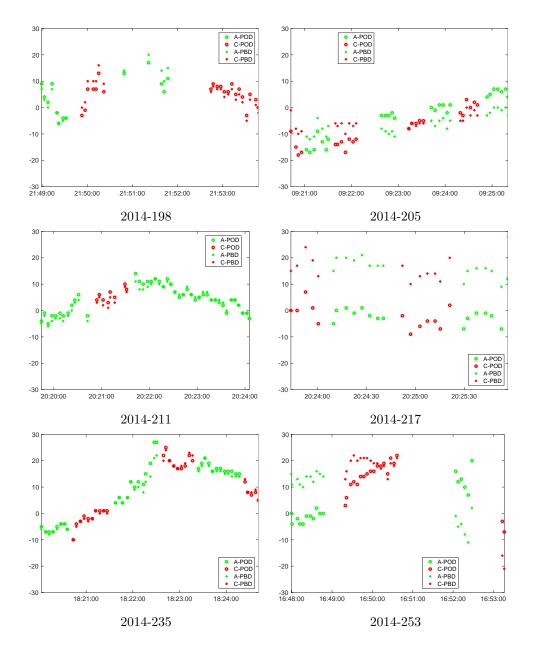


Figure 10: SLR residuals (unit:mm) for the Swarm-A/C single-satellite POD (reference) and dual-satellite PBD orbit solutions by using the well-performing Yarragadee station in Australia. Six tracking passes with more than 27 points are selected. For each pass the DOY in 2014 is indicated.

satellites during one overpass. This offers an additional opportunity to assess the consistency in terms of time series between the two different orbit solutions and the SLR observations. The Yarragadee station in Australia offers the largest number of such overpasses and is therefore selected for this analysis.

When tracking the Swarm-A and C satellites, normally the Yarragadee tracking switches happen 1 to 6 times during the satellite overpass, which typically has a duration of only a few minutes. Figure 10 shows that for DOY 205 in 2014, the SLR residuals are better aligned in time when using the Swarm-A/C dual-satellite PBD solution. For other passes displayed in Figure 10, consistency is at the same level for the PBD solutions as compared to the POD solutions. This result agrees well with results reported in [14] and also similar analysis for the TanDEM-X/TerraSAR-X formation as reported in [42].

Another assessment is done to check the alignment of Swarm-A and -C satellite orbits based on the Swarm-B/A and Swarm-B/C PBD on DOY 205 in 2014. 505 The STDs of all Swarm-A and -C SLR residuals for a tracking pass are com-506 puted. A smaller STD means two satellite orbits align closer with the same 507 reference SLR ground station, or in other words, it represents better alignment 508 between two orbits. The STDs of Swarm-A and -C satellite SLR validation resid-509 uals for this orbit pass are 7.78, 3.36, 3.12 and 2.48 mm for the single-satellite 510 POD, Swarm-A/C dual-satellite PBD, triple-satellite PBD and the Swarm-A/C 511 baseline based on the Swarm-B/A and Swarm-B/C PBD, respectively. Clearly 512 the alignments for the latter three solutions are very close and are better than the single-satellite POD orbits. The PBD seems to improve the SLR consis-514 tency between the Swarm-A and -C satellites for this day. This demonstrates 515 the benefits of relative dynamics constraints between the higher Swarm-B and 516 either of the lower Swarm satellites. 517

#### 5. Conclusions and Recommendations

The three-satellite Swarm constellation has been used as test bed for Swarm dual- and triple-satellite orbit determination, where two of the satellites are fly-

ing in formation and the third one flies in a different orbit. Thus, in addition to relatively slowly varying baselines, also fast changing or high-dynamic baselines 522 are included in the tests. Three different Swarm satellite pairs and thus baselines can be defined: the pendulum baseline (Swarm-A/C) and two high-low base-524 lines (Swarm-B/A and Swarm-B/C), where the high-low baselines can typically 525 be formed during limited periods every 6.1 days. For the latter, the baseline 526 varies from 50 km to 3500 km for orbital arcs with a duration of 24-hr centered 527 around the time of closest approach. Precise Baseline Determination (PBD) for Swarm involving the Swarm-B satellite is challenging because of different 520 levels of dynamic force modeling uncertainty, where it is expected that this is 530 different for Swarm-A and -C. An Iterative Extended Kalman Filter (IEKF) in 531 combination with subset ambiguity fixing is used to compute reduced-dynamic 532 PBD solutions for Swarm. Kinematic PBD solutions are then obtained by using the fixed ambiguities obtained from the reduced-dynamic solutions. 534

Results show that the GPS receiver RINEX converter and half-cycle to full-535 cycle ambiguities corrections are very beneficial for PBD. The Swarm reduced-536 dynamic baseline comparisons with external orbits from the German Space Op-537 erations Center (GSOC/DLR) show good baseline consistency at a level of only 538 1-3 mm for the pendulum Swarm-A/C satellite pair. For the other two pairs, a 539 consistency at a level of 3-5 mm is achieved for different directions. The overall 540 MODK kinematic baseline consistences with its reduced-dynamic baseline are 541 at a level of 13/6/4 mm for Swarm-A/C and a level of 23/11/7 mm for the other two pairs (radial/along-track/cross-track). They are better than the internal consistences between two GSOC/DLR solutions and again indicate the 544 benefits of constraining relative dynamics and fixing Double-Difference (DD) 545 carrier phase ambiguities. However it has to be noted that these consistencies 546 deteriorate when baselines increase.

The research in this paper has shown that triple-satellite PBD including high-dynamic baselines leads to comparable performance in terms of kinematic/reduced-dynamic baseline consistencies and SLR observation fits as dual-satellite PBD.

The inclusion of high-dynamic baselines does thus not degrade the quality of the

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orbit solutions as was the case in *e.g.* [15]. Compared to single-satellite POD, it was shown that a better Swarm-A/C consistency can be obtained in the time series of SLR observation residuals.

It has also been shown that the consistency between kinematic and reduced-555 dynamic baseline solutions deteriorates with growing distance, which can be 556 explained to a large extent by a less favorable geometry. A possibility for im-557 provement might be to combine the single-satellite ambiguity fixed method with 558 the PBD ambiguity fixing method used in this paper. This is a nice topic for 559 future research. The single-satellite ambiguity fixed solutions lead to larger 560 kinematic/reduced-dynamic consistency levels at short distance (Table 7), but 561 might suffer less from a deteriorated geometry for longer distances. 562

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