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**DOI**

[10.3390/electronics10040433](https://doi.org/10.3390/electronics10040433)

**Publication date**

2021

**Document Version**

Final published version

**Published in**

Electronics (Switzerland)

**Citation (APA)**

Sun, Y., Kang, X., Deng, S., Zheng, Y., Wei, K., Xu, L., Wu, H., & Liu, X. (2021). First demonstration of I-band high-power limiter with gan schottky barrier diodes (Sbds) based on steep-mesa technology. *Electronics (Switzerland)*, 10(4), 1-8. Article 433. <https://doi.org/10.3390/electronics10040433>

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## Communication

# First Demonstration of L-Band High-Power Limiter with GaN Schottky Barrier Diodes (SBDs) Based on Steep-Mesa Technology

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**Abstract:** Gallium nitride (GaN) has attracted increased attention because of superior material properties, such as high electron saturation velocity and high electrical field strength, which are promising for high-power microwave applications. We report on a high-performance vertical GaN-based Schottky barrier diode (SBD) and its demonstration in a microwave power limiter for the first time. The fabricated SBD achieved a very low differential specific on-resistance ( $R_{ON,sp}$ ) of  $0.21 \text{ m}\Omega\cdot\text{cm}^2$ , attributed to the steep-mesa technology, which assists in reducing the spacing between the edge of the anode and cathode to  $2 \mu\text{m}$ . Meanwhile, a low leakage current of  $\sim 10^{-9} \text{ A}/\text{cm}^2$  at  $-10 \text{ V}$ , a high forward current density of  $9.4 \text{ kA}/\text{cm}^2$  at  $3 \text{ V}$  in DC, and an ideality factor of 1.04 were achieved. Scattering parameter measurements showed that the insertion loss ( $S_{21}$ ) was lower than  $-3 \text{ dB}$  until  $3 \text{ GHz}$ . In addition, a microwave power limiter circuit with two anti-parallel diodes was built and measured on an alumina substrate. The input power level reached  $40 \text{ dBm}$  (10 watts) in continuous-wave mode at  $2 \text{ GHz}$ , with a corresponding leakage power of  $27.2 \text{ dBm}$  (0.5 watts) at the output port of the limiter, exhibiting the great potential of GaN SBD in microwave power limiters.

**Keywords:** vertical; GaN SBD; L band; Schottky diode limiter; high power



**Citation:** Sun, Y.; Kang, X.; Deng, S.; Zheng, Y.; Wei, K.; Xu, L.; Wu, H.; Liu, X. First Demonstration of L-Band High-Power Limiter with GaN Schottky Barrier Diodes (SBDs) Based on Steep-Mesa Technology. *Electronics* **2021**, *10*, 433. <https://doi.org/10.3390/electronics10040433>

Academic Editor: Geok Ing Ng

Received: 13 January 2021

Accepted: 8 February 2021

Published: 10 February 2021

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## 1. Introduction

Microwave power diode limiters have been widely used in the RF (Radio Frequency) front-end in a variety of wireless communication systems [1], such as cellular infrastructure (including 5G) and microwave radio communications [2]. A diode limiter prevents the damage of sensitive receiver components by allowing RF signals below a certain threshold to pass through, but larger signals exceeding the threshold are attenuated [3]. The development of modern RF receivers requires a high-performance diode limiter [4] that can operate in a wide bandwidth and at a high-input power level with compactness, easy integration and low cost. Many studies have been carried out on Si-based diode limiters in recent years [5–7]; however, they showed scant room for further improvement as the silicon reached its theoretical limitations. Gallium nitride (GaN) has the superior material properties of high electron saturation velocity, high electrical field strength, and high operating temperature [8,9], which makes it well suited for high-power microwave limiter applications.

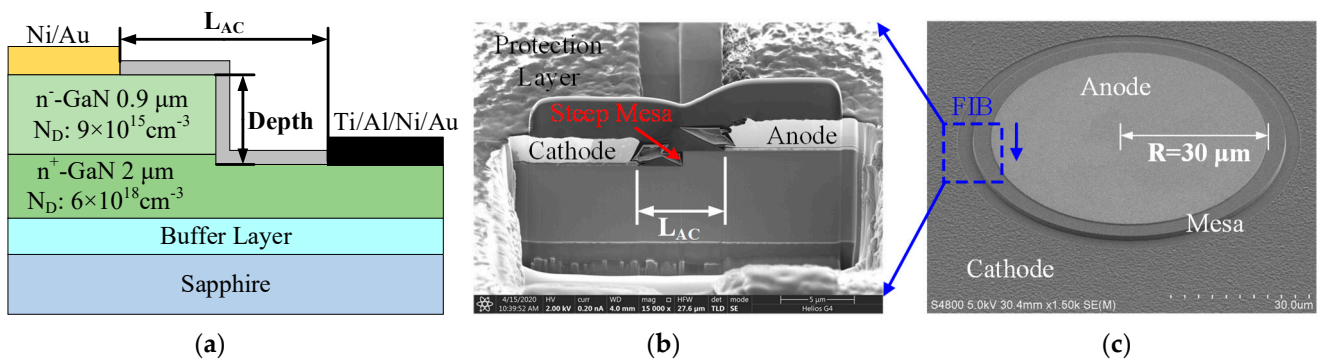
High performance vertical GaN p-n diodes [10–12] and SBDs [13,14] have been demonstrated for high breakdown and good thermal properties. Most of the GaN diodes have

been reported in high-voltage applications [15,16], microwave rectifiers [17,18] and frequency doublers [19]. A GaN microwave power SBD limiter has rarely been reported to date.

In this work, we have experimentally demonstrated a vertical GaN SBD for L-band microwave power limiters for the first time. By using steep-mesa technology, the spacing between the anode and cathode can be reduced to 2  $\mu\text{m}$ , leading to a further reduction of differential on-resistance ( $R_{\text{on}}$ ) of the SBD. The fabricated SBD has a low differential  $R_{\text{ON,sp}}$  of 0.21  $\text{m}\Omega\cdot\text{cm}^2$  and a very high forward current density of 9.4  $\text{kA}/\text{cm}^2$  at 3 V. The insertion loss of the SBD was increased from  $-20$  dB to  $-3$  dB over a frequency range of 0.1–3 GHz. The GaN SBD power limiter has shown a peak input power of 40 dBm with a leakage power of 27.2 dBm at 2 GHz.

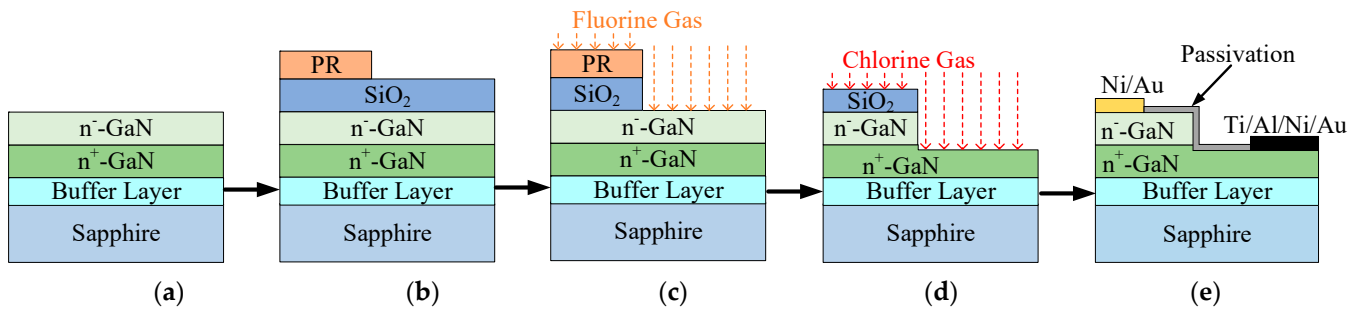
## 2. Materials and Methods

Figure 1a–c shows the cross-section schematic, a cross-section SEM image, and a top-view SEM image of the fabricated vertical GaN SBD. The epitaxial structure was grown on c-plane sapphire substrates by metalorganic chemical vapor deposition (MOCVD), and consisted of a buffer layer, a 2  $\mu\text{m}$   $\text{n}^+$ -GaN conducting layer ( $N_{\text{D}}: 6 \times 10^{18} \text{ cm}^{-3}$ ), and a 0.9  $\mu\text{m}$   $\text{n}^-$ -GaN drift layer ( $N_{\text{D}}: 9 \times 10^{15} \text{ cm}^{-3}$ ). The spacing between the anode and cathode ( $L_{\text{AC}}$ ) was varied from 2  $\mu\text{m}$  to 10  $\mu\text{m}$ .



**Figure 1.** (a) Cross-section schematic; (b) cross-section of the SEM image; and (c) top view of the SEM image of the vertical GaN-on-sapphire SBD.

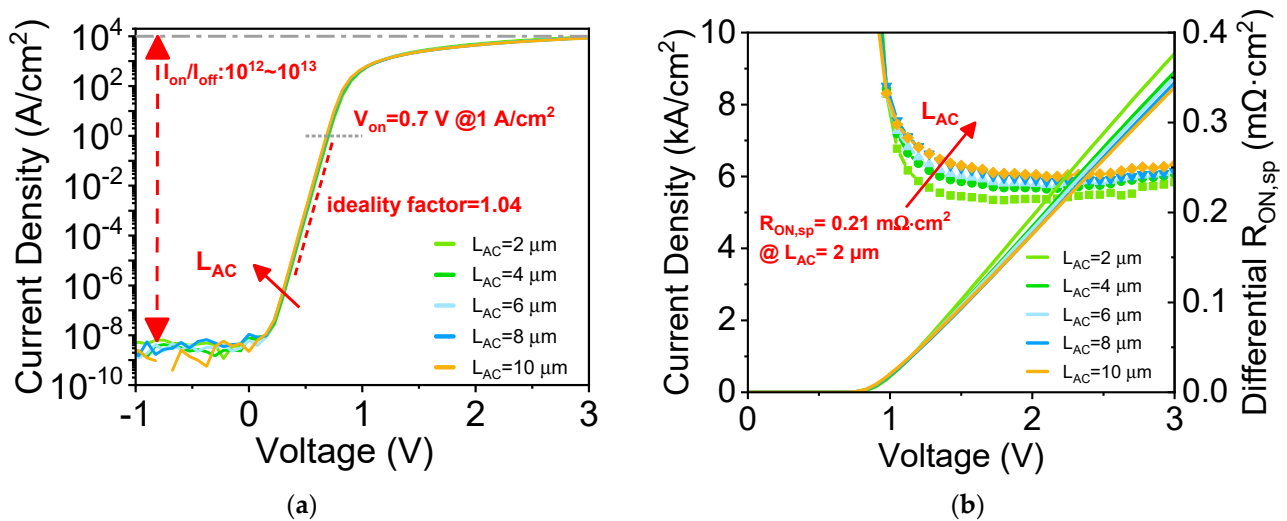
Figure 2a–e describes the fabrication steps for the vertical GaN SBD. First, the 1  $\mu\text{m}$  mesa was formed by a combination of inductively coupled plasma (ICP) dry etching with  $\text{Cl}_2/\text{BCl}_3$  gas mixture and tetramethylammonium hydroxide (TMAH) wet etching. Both a photoresist (PR) and a silicon oxide ( $\text{SiO}_2$ ) hard-mask were employed for the mesa etch. The ICP etching conditions were optimized to form a steep-mesa structure with the following parameters [20]: 360 W ICP power, 42 W RF (radio frequency) power, and 100 sccm/10 sccm  $\text{Cl}_2/\text{BCl}_3$  flow rates. Second, the ohmic metal (Ti/Al/Ni/Au) was deposited on the  $\text{n}^+$ -GaN layer and annealed at 650  $^\circ\text{C}$  for 1.5 min. A specific contact resistivity as low as  $1.08 \times 10^{-6} \Omega\cdot\text{cm}^2$  was obtained for ohmic contact, extracted from the circular transmission line method (CTLTM) measurements. Then, the Schottky metal (Ni/Au) was formed on  $\text{n}^-$ -GaN layer with a radius of 30  $\mu\text{m}$ . Finally, the  $\text{SiO}_2$  passivation layer was deposited by plasma-enhanced chemical vapor deposition (PECVD).



**Figure 2.** Simplified fabrication steps of the vertical GaN SBD. (a) Epitaxy structure of vertical GaN SBD on sapphire substrate; (b) photoresist (PR) and SiO<sub>2</sub> mask on GaN; (c) fluorine-based hard mask etching; (d) chlorine-based mesa etching; (e) electrode deposition and SiO<sub>2</sub> passivation.

### 3. Results and Discussion

Figure 3a shows the forward I-V characteristics in the semi-log scale for the vertical GaN-on-sapphire SBDs with various  $L_{AC}$ . A high on/off current ratio ( $I_{on}/I_{off}$ ) of  $10^{13}$ , ideality factor ( $\eta$ ) of 1.04, and low turn-on voltage ( $V_{on}$ ) of 0.7 V (extracted at 1 A/cm<sup>2</sup>) were extracted from the forward I-V curves of the GaN SBDs with various  $L_{AC}$ . Figure 3b shows the forward I-V characteristics in linear scale and differential  $R_{ON,sp}$  for the GaN SBD. The GaN SBD with a small  $L_{AC}$  of 2  $\mu$ m had a high forward current density (defined as the total current divided by the anode area) of 9.4 kA/cm<sup>2</sup> at 3 V, and a low differential  $R_{on,sp}$  of 0.21 m $\Omega$ ·cm<sup>2</sup>. The differential  $R_{on,sp}$  of the SBD with a large  $L_{AC}$  of 10  $\mu$ m was 1.16 times higher than that with a small  $L_{AC}$  of 2  $\mu$ m, which was attributed to the additional resistance introduced by increasing  $L_{AC}$ . A steep-mesa etching technology was expected to form a near-90° mesa structure and add sufficient freedom to reduce the spacing between the anode and cathode, enabling a low differential  $R_{on}$  in the vertical GaN SBD.



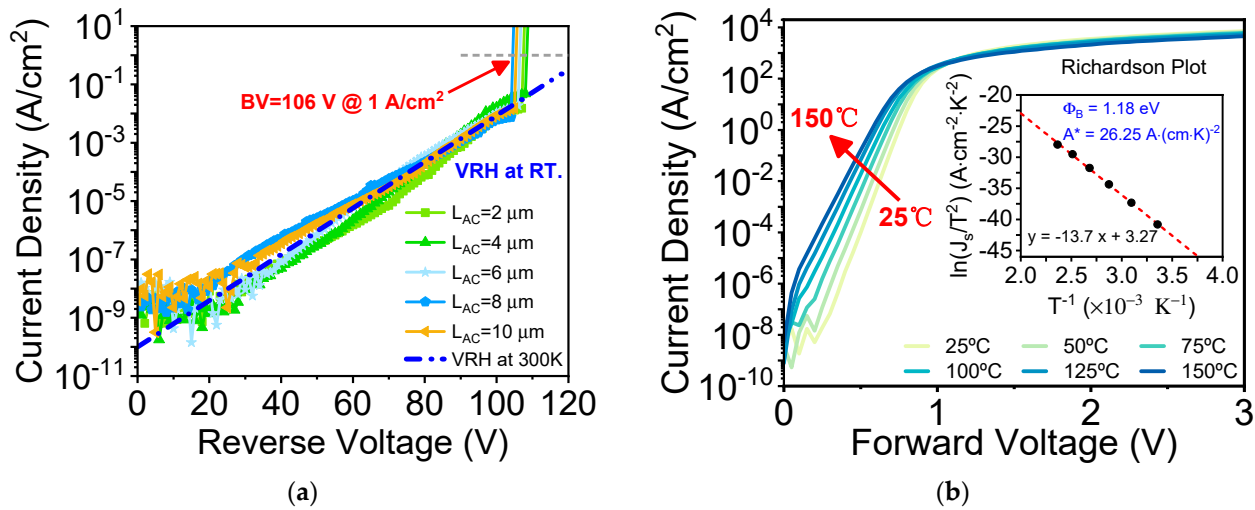
**Figure 3.** (a) Forward I-V characteristics in semi-log scale, and (b) in linear scale (left) and differential  $R_{ON,sp}$  vs. voltage (right) for vertical GaN SBDs with different spacing between the anode and cathode ( $L_{AC}$  = 2, 4, 6, 8, 10  $\mu$ m).

Figure 4a shows the reverse I-V characteristics of the GaN SBDs with various  $L_{AC}$  at room temperature. The GaN SBDs with various  $L_{AC}$  showed a similar breakdown voltage (BV) of 106 V at 1 A/cm<sup>2</sup> and a similar leakage density of  $10^{-8}$  A/cm<sup>2</sup> until  $-30$  V.  $L_{AC}$  had minor impact on reverse BV, which can be explained by the electric field distributed mostly in the drift layer. When the reverse bias exceeded 30 V, the leakage behavior showed a variable range-hopping (VRH) process, which could be attributed to the threading dislocation in the bulk [21]. Figure 4b shows the temperature-dependent

I-V characteristics of the SBDs, which ranged between 300 and 425 K. With increasing temperature, the current density increased from 300 K (room temperature) to 425 K when the forward voltage was below 1 V, which was attributed to the thermionic emission (TE) behavior. However, the current density decreased with temperature at high forward bias (>1 V), mainly attributed to a decrease of electron mobility in the drift region. Thermionic emission behavior can usually be proved by a Richardson plot as follows [22,23]:

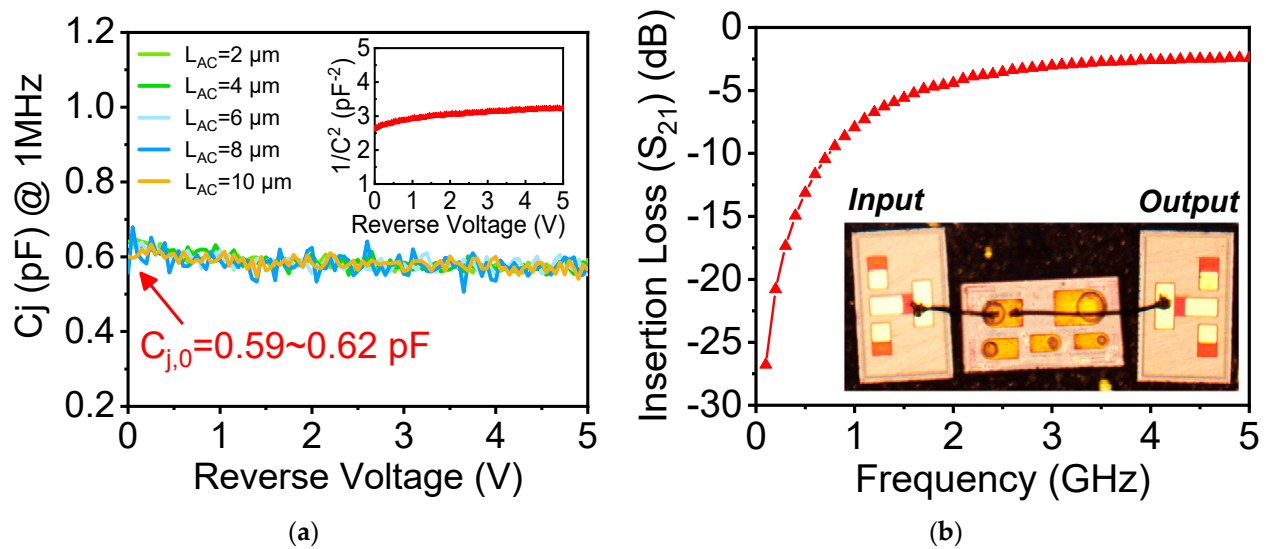
$$\ln J_s/T^2 = \ln A^* - \frac{q\phi_{B0}}{kT} \quad (1)$$

where  $J_s$ ,  $k$ , and  $A^*$  are the saturation current density, Boltzmann's constant, and Richardson's constant, respectively. In the inset of Figure 4b, the Richardson plot of  $\ln(J_s/T^2)$  versus  $1000/T$  is linear, and the calculated  $A^*$  is about  $26.25 \text{ A} \cdot (\text{cm} \cdot \text{K})^{-2}$ , which are very close to the theoretical value of  $26.64 \text{ A} \cdot (\text{cm} \cdot \text{K})^{-2}$  [22]. As a result, the temperature-dependent I-V characteristic of our GaN SBD can be well explained by the TE model.



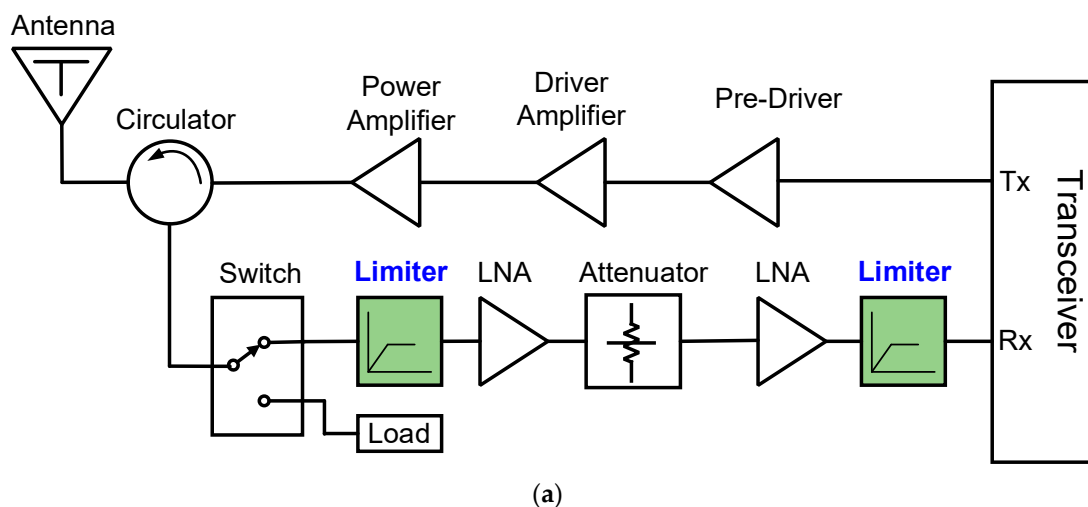
**Figure 4.** (a) Reverse I-V characteristics of the vertical GaN SBDs with various  $L_{AC}$ . (b) Temperature-dependent I-V characteristics of the GaN SBD with  $L_{AC}$  of  $2 \mu\text{m}$  in semi-log scale at temperatures ranging from  $25^\circ\text{C}$  to  $150^\circ\text{C}$  and corresponding Richardson plot (inset).

Figure 5a shows the junction capacitance of the GaN SBD varied with the applied reverse voltage from 0 V to 5 V at a measurement frequency of 1 MHz. The junction capacitance ( $C_{j,0}$ ) at zero bias was between 0.59 and 0.62 pF with various  $L_{AC}$ . The extracted  $C^{-2}$ -V plot shows a normal linearity, which indicates the relatively uniform net donor concentration along the depth direction. Figure 5b shows the transmission characteristics of the GaN SBD with a  $L_{AC}$  of  $2 \mu\text{m}$  over a frequency range of 0.1–5 GHz. The anode and cathode were wire-bonded to co-planar waveguide transmission line test fixture modules, as shown in the inset of Figure 5b. The measured results showed that the insertion loss ( $S_{21}$ ) was lower than  $-3 \text{ dB}$  from 0.1 GHz to 3 GHz when the diode was in an off-state. The insertion loss increased with increasing input frequency, which was attributed to the off-state junction capacitance of the GaN SBD [24]. For an ideal limiter, the output power should have no attenuation when a low power signal is incidentally added to the input port. Therefore, a low junction capacitance is required to realize a low insertion loss for the GaN SBD, which is critical to the limiter performance below the threshold level.



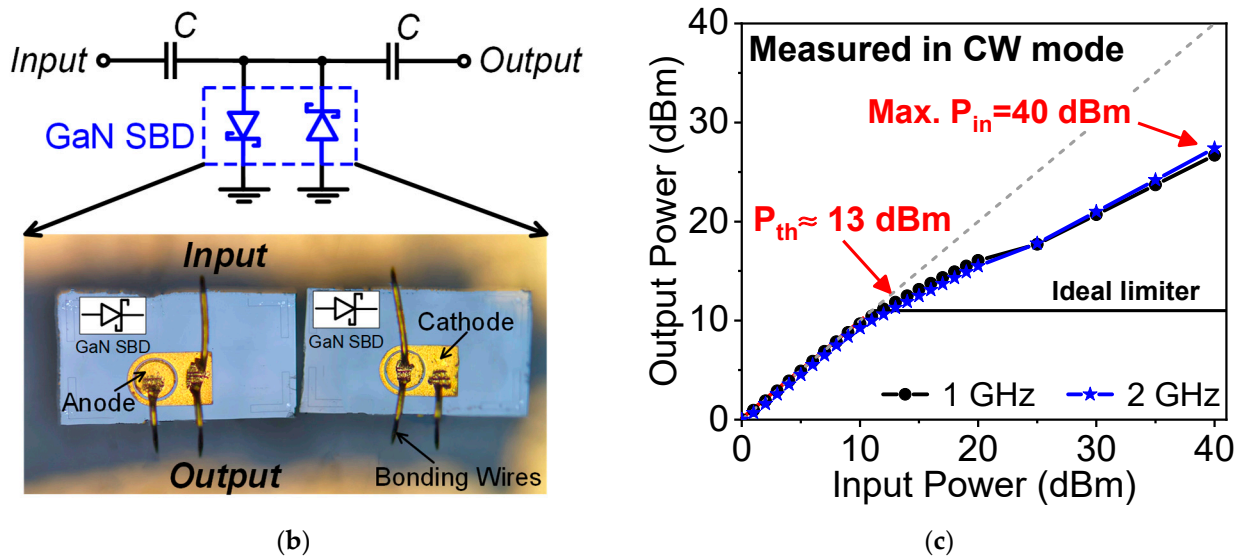
**Figure 5.** (a) C-V characteristics of the GaN SBD at a measurement frequency of 1 MHz with an anode radius of 30  $\mu\text{m}$  and different  $L_{AC}$  of 2, 4, 6, 8, and 10  $\mu\text{m}$ . Inset is the corresponding  $C^{-2}$ -V plot. (b) Insertion loss ( $S_{21}$ ) of the GaN SBD over a frequency range of 0.1 GHz to 5 GHz in the small-signal S-parameter measurements. Inset is the wire-bonded GaN SBD with two GSG test fixture modules.

Figure 6a shows a typical radio transceiver block diagram. The limiter is located at the receiver stage to protect the low-noise amplifier (LNA) and transceiver from the high-power microwave signal transduced by the antenna. Figure 6b shows the circuit schematic and a photograph of the one-stage anti-parallel diode limiter using the wire-bonded vertical GaN SBD ( $R_{on,diff} = 8 \Omega$ ,  $C_{j,0} = 0.6 \text{ pF}$ ). The two capacitors were used as a DC block (not shown in the photograph). The anti-parallel GaN SBDs were used to clip the input's large signal symmetrically. For a low input power level, the diodes were both in an off-state. When the input power exceeded the threshold level, the diodes were both in an “on-state” and become low impedance, forming a conducting path to ground. Therefore, the peak amplitude of the input power was limited at the threshold level to prevent damage of the LNA stage.



**Figure 6.** Cont.





**Figure 6.** (a) Radio transceiver block diagram. (b) Circuit schematic and microscope image of the one-stage anti-parallel diode limiter using the wire-bonded GaN SBD. (c) Output power versus input power for the GaN SBD limiter at 1 GHz and 2 GHz.

Figure 6c presents the input and output characteristics of the ideal limiter and our GaN SBD limiter. An ideal power limiter has the following characteristics [25]:

$$P_{out} = P_{in} \quad (\text{when } P_{in} < P_{th}) \quad (2)$$

$$P_{out} = P_{th} \quad (\text{when } P_{in} > P_{th}) \quad (3)$$

where  $P_{out}$  is the output power,  $P_{in}$  is the input power, and  $P_{th}$  is the threshold level. The microwave power limiter circuit with an anti-parallel diode was measured on an alumina substrate. The input power was increased from low power (0 dBm) to high power in CW mode at a frequency of 1 GHz and 2 GHz. The measured results showed a limiting threshold level (or input 1-dB compression point) of 13 dBm. The limiter had a negligible loss when the input power was below 13 dBm at 1 GHz and 2 GHz, which we attributed to the low junction capacitance of our GaN SBD. The leakage power was 16.7 dBm and 27.4 dBm when the input power was 20 dBm and 40 dBm at 2 GHz, respectively. The GaN SBD limiter can handle at least 40 dBm of CW input power at 2 GHz without failure. When the input power was beyond the maximum power, the SBD suffered from a catastrophic failure due to a self-heating problem. In sum, the GaN SBD was successfully demonstrated in a microwave power limiter application, and showed great potential for future work.

#### 4. Outlook

To further improve the performance of the GaN SBD limiter, four aspects should be addressed:

First, the junction capacitance ( $C_j$ ) of the diode dominates the insertion loss of the limiter at a low input power, especially for a high-frequency signal. Stacking multiple diodes can reduce the total capacitance but increase the threshold level of the diode limiter. The  $C_j$  of a GaN SBD can be reduced by decreasing the doping level of the drift layer, increasing the width of the drift layer, or reducing the Schottky contact area; however, this leads to an increase of  $R_{on}$ .

Second, a lower  $R_{on}$  of the diode can sufficiently attenuate the output power at a high input power that exceeds the threshold level. For the vertical GaN SBD, a high doping level or thin drift layer result in a low  $R_{on}$ , but with a low breakdown voltage (BV). Diodes with a low  $R_{on}$  and a high BV can be achieved by improving the crystal quality of the GaN, owing to its high electron mobility and low dislocation density in the bulk.

Third, improving the heat dissipation of the GaN diode enhances the power-handling capability of the GaN diode limiter. Advanced thermal management methods are required to cool the GaN SBD, such as using a high thermal conductivity substrate (SiC and diamond) or removing the foreign substrate (sapphire and silicon).

Finally, a multi-stage limiter based on GaN PiN diodes and GaN SBDs can reduce the leakage power and adjust the threshold level [26]. Monolithic and microwave integrated circuits (MMICs) offer the possibility of integrating the multi-stage diode limiter, enabling a better limiting performance with high power handling at a high-frequency band.

## 5. Conclusions

In conclusion, we have experimentally demonstrated a vertical GaN SBD for L-band microwave power limiters for the first time. Thanks to the steep-mesa technology, the spacing between the anode and cathode ( $L_{AC}$ ) could be reduced to 2  $\mu\text{m}$ , leading to a further reduction of  $R_{on}$ . The fabricated vertical GaN SBD had a high forward current density of 9.4  $\text{kA}/\text{cm}^2$  at 3 V, a low differential  $R_{on,sp}$  of 0.21  $\text{m}\Omega\cdot\text{cm}^2$ , a near-unity ideality factor ( $\eta$ ) of 1.04, and a BV of 106 V. The GaN SBD limiter can withstand up to a very high input power of 40 dBm at 2 GHz in CW mode to yield a low leakage power of 27.4 dBm. Therefore, the results suggest great potential for high-power microwave power limiters using a GaN SBD.

**Author Contributions:** Y.S. and X.K. contributed equally to this paper. Y.S., writing—original draft; X.K., writing—review and editing; L.X. and H.W., data curation; X.K., S.D., Y.Z., K.W., and X.L., project administration. All authors have read and agreed to the published version of the manuscript.

**Funding:** This work was supported by the National Key Research and Development Program of China (Grant No. 2017YFB0403000) and the Natural Science Foundation of China (Grant Nos. 61804172 and 61534007), in part by the Youth Innovation Promotion Association of CAS, and in part by the Key-Area Research and Development Program of Guangdong Province (No. 2019B010128001).

**Conflicts of Interest:** The authors declare no conflict of interest.

## References

- White, J.F. *Microwave Semiconductor Engineering*; Springer: Heidelberg, The Netherlands, 2012; pp. 245–313.
- Sardi, A.; Alkurt, F.Ö.; Özkaner, V.; Karaaslan, M.; Ünal, E.; Mohamed, T. Investigation of microwave power limiter for Industrial Scientific Medical band (ISM) applications. *Int. J. RF Microw. Comput. Aided Eng.* **2020**, *30*, e22180. [CrossRef]
- Fan, G.Q.; Xing, H.Y.; Hu, H.Q. K-Ka band schottky diode limiter. In Proceedings of the 2013 IEEE International Conference on Applied Superconductivity and Electromagnetic Devices, Beijing, China, 25–27 October 2013.
- Yang, L.; Yang, L.-A.; Rong, T.; Li, Y.; Jin, Z.; Hao, Y. Codesign of Ka-Band Integrated GaAs PIN Diodes Limiter and Low Noise Amplifier. *IEEE Access* **2019**, *7*, 88275–88281. [CrossRef]
- Seong-Sik, Y.; Tak-Young, K.; Kong, D.K.; Kim, S.S.; Yeom, K.W. A Novel Analysis of a  $\text{K}\mu\text{S}$ -Band Planar p-i-n Diode Limiter. *IEEE Trans. Microw. Theory Tech.* **2009**, *57*, 1447–1460. [CrossRef]
- Wang, H.; Zou, H.; Zhou, Y.; Li, H. Electro-thermal coupled modeling of PIN diode limiter used in high-power microwave effects simulation. *J. Electromagn. Waves Appl.* **2015**, *29*, 615–625. [CrossRef]
- “Limiter Diodes”, Skyworks, Woburn, MA, USA. 2011. Available online: <http://www.skyworksinc.com> (accessed on 9 February 2021).
- Mishra, U.K.; Shen, L.; Kazior, T.E.; Wu, Y.F. GaN-Based RF Power Devices and Amplifiers. *Proc. IEEE* **2008**, *96*, 287–305. [CrossRef]
- Deng, S.; Gao, C.; Chen, S.; Sun, J.; Wu, K. Research on Linearity Improvement of Silicon-Based p-i-n Diode Limiters. *IEEE Microw. Wirel. Compon. Lett.* **2020**, *30*, 62–65. [CrossRef]
- Liu, X.; Chiu, H.-C.; Wang, H.Y.; Hu, C.; Wang, H.C.; Kao, H.L.; Chien, F.T. 2.4 kV Vertical GaN PN Diodes on Free Standing GaN Wafer Using CMOS-Compatible Contact Materials. *IEEE J. Electron Devices Soc.* **2018**, *6*, 825–829. [CrossRef]
- Zhang, Y.; Sun, M.; Piedra, D.; Azize, M.; Zhang, X.; Fujishima, T.; Palacios, T. GaN-on-Si Vertical Schottky and p-n Diodes. *IEEE Electron. Device Lett.* **2014**, *35*, 618–620.
- Fu, H.; Fu, K.; Alugubelli, S.R.; Cheng, C.-Y.; Huang, X.; Chen, H.; Yang, T.-H.; Yang, C.; Zhou, J.; Montes, J.; et al. High Voltage Vertical GaN p-n Diodes with Hydrogen-Plasma Based Guard Rings. *IEEE Electron. Device Lett.* **2019**, *41*, 127–130. [CrossRef]
- Li, L.; Kishi, A.; Liu, Q.; Itai, Y.; Fujihara, R.; Ohno, Y.; Ao, J.-P. GaN Schottky Barrier Diode with TiN Electrode for Microwave Rectification. *IEEE J. Electron. Devices Soc.* **2014**, *2*, 168–173. [CrossRef]



14. Han, S.; Yang, S.; Sheng, K. High-Voltage and High- $I_{on}/I_{off}$  Vertical GaN-on-GaN Schottky Barrier Diode with Nitridation-Based Termination. *IEEE Electron. Device Lett.* **2018**, *39*, 572–575. [[CrossRef](#)]
15. Sun, Y.; Kang, X.; Zheng, Y.; Lu, J.; Tian, X.; Wei, K.; Wu, H.; Wang, W.; Liu, X.; Zhang, G. Review of the Recent Progress on GaN-Based Vertical Power Schottky Barrier Diodes (SBDs). *Electronics* **2019**, *8*, 575. [[CrossRef](#)]
16. Kang, X.; Wang, X.; Huang, S.; Zhang, J.; Fan, J.; Yang, S.; Wang, Y.; Zheng, Y.; Wei, K.; Zhi, J.; et al. Recess-free AlGaN/GaN lateral Schottky barrier controlled Schottky rectifier with low turn-on voltage and high reverse blocking. In Proceedings of the 2018 IEEE 30th International Symposium on Power Semiconductor Devices and ICs (ISPSD), Chicago, IL, USA, 13–17 May 2018.
17. Joseph, S.D.; Hsu, S.S.H.; Alieldin, A.; Song, C.; Liu, Y.; Huang, Y. High-Power Wire Bonded GaN Rectifier for Wireless Power Transmission. *IEEE Access* **2020**, *8*, 82035–82041. [[CrossRef](#)]
18. Dang, K.; Zhang, J.; Zhou, H.; Huang, S.; Zhang, T.; Bian, Z.; Zhang, Y.; Wang, X.; Zhao, S.; Wei, K.; et al. A 5.8-GHz High-Power and High-Efficiency Rectifier Circuit with Lateral GaN Schottky Diode for Wireless Power Transfer. *IEEE Trans. Power Electron.* **2020**, *35*, 2247–2252. [[CrossRef](#)]
19. Liang, S.; Song, X.; Zhang, L.; Lv, Y.; Wang, Y.; Wei, B.; Guo, Y.; Gu, G.; Wang, B.; Cai, S.; et al. A 177–183 GHz High-Power GaN-Based Frequency Doubler with Over 200 mW Output Power. *IEEE Electron. Device Lett.* **2020**, *41*, 669–672. [[CrossRef](#)]
20. Sun, Y.; Kang, X.; Zheng, Y.; Wei, K.; Li, P.; Wang, W.; Liu, X.; Zhang, G. Optimization of Mesa Etch for a Quasi-Vertical GaN Schottky Barrier Diode (SBD) by Inductively Coupled Plasma (ICP) and Device Characteristics. *Nanomaterials* **2020**, *10*, 657. [[CrossRef](#)] [[PubMed](#)]
21. Fu, K.; Fu, H.; Huang, X.; Yang, T.H.; Cheng, C.Y.; Peri, P.R.; Chen, H.; Montes, J.; Yang, C.; Zhou, J.; et al. Reverse Leakage Analysis for As-grown and Regrown Vertical GaN-on-GaN Schottky Barrier Diodes. *IEEE J. Electron. Devices Soc.* **2020**, *8*, 74–83. [[CrossRef](#)]
22. Arehart, A.R.; Moran, B.; Speck, J.S.; Mishra, U.K.; DenBaars, S.P.; Ringel, S.A. Effect of threading dislocation density on Ni/n-GaN Schottky diode I-V characteristics. *J. Appl. Phys.* **2006**, *100*, 023709. [[CrossRef](#)]
23. Luongo, G.; Di Bartolomeo, A.; Giubileo, F.; Chavarin, C.A.; Wenger, C. Electronic properties of graphene/p-silicon Schottky junction. *J. Phys. D* **2018**, *51*, 255305. [[CrossRef](#)]
24. Surdi, H.; Ahmad, M.F.; Koeck, F.; Nemanich, R.J.; Goodnick, S.; Thornton, T.J. RF Characterization of Diamond Schottky p-i-n Diodes for Receiver Protector Applications. *IEEE Microw. Wirel. Compon. Lett.* **2020**, *30*, 1141–1144. [[CrossRef](#)]
25. Katko, A.R.; Hawkes, A.M.; Barrett, J.P.; Cummer, S.A. RF Limiter Metamaterial Using p-i-n Diodes. *IEEE Antennas Wirel. Propag. Lett.* **2011**, *10*, 1571–1574. [[CrossRef](#)]
26. Bera, S.C.; Basak, K.; Jain, V.; Singh, R.V.; Garg, V.K. Schottky diode-based microwave limiter with adjustable threshold power level. *Microw. Opt. Technol. Lett.* **2010**, *52*, 1671–1673. [[CrossRef](#)]