

# **Charge Domain Interlacing CMOS Image Sensor Design**

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## **Abstract**

This thesis presents a CMOS image sensor which can implement the charge domain interlacing principle. Inspired by the shared amplifier pixel structure and based on a pinned photodiode four transistor (4T) structure, two innovative pixel designs combined with two different readout directions are presented. These novel pixels are designed to fit the charge domain interlacing principle, which used the charge binning technology in the field integration mode of interlaced scan to improve the signal-to-noise ratio of the sensor. To realize this working principle and compared it with other working modes, a programmable universal image sensor peripheral circuit is designed for controlling and driving the pixel array in the most flexible and most efficient way. As a result, the designed sensor can be used not only in the progressive scan mode, frame integration interlaced scan, and voltage domain interlacing mode but also in the charge domain interlacing mode. This is a very unique feature for CMOS image sensors, and without the shared pixel concept, charge domain interlacing was only possible with CCDs.

The proposed image sensor is implemented in TSMC 0.18um 1P6M CMOS technology. Some preliminary measurement results of the chip are shown to prove the functional correctness of the image sensor.

**Keywords:** CMOS image sensor, charge binning, interlaced scan

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# Chapter 1

## Introduction

Over the past decade, fueled by the demands of multimedia applications, digital still and video cameras are rapidly becoming widespread. Image sensor being a key component in modern digital cameras, converts the light intensity to electric signals. The purpose of this thesis project is to design a universal image sensor test chip structure and implement CMOS pixel design interlacing in the charge domain.

In this introduction chapter, a brief overview of the history of CMOS image sensor development will be described at first in section 1.1. Secondly, the challenges we faced in designing CMOS images will be analyzed in section 1.2. Finally, the organization of the thesis is presented.

### 1.1 Historical Background

Although the first successful MOS image sensor was invented in 1963 [1], which born nearly the same age as charged couple device(CCD), most of todays CMOS image sensors are based on work done starting around the early 1980's. In the early 60s, most of the photosensitive elements used in the image sensors were either photoresistors or n-p-n junctions(scanistors) [2] [3]. In 1967, Weckler at Fairchild suggested operating p-n junctions in a photon flux integrating mode, which is predominant in the CMOS imagers



used today [4]. This work is the first time that a reverse-biased p-n junction was used for both photosensing and charge integration and also build the foundation of the photo-sensing principle in the modern CMOS imagers. In 1968, based on the method of Weckler, Nobel [5] developed the first  $100 \times 100$  pixel array using an in-pixel source follower transistor for charge amplification which is also being used today. Thus, in the end of 1960s, significant improvements were already achieved in terms of the photosensing principle development and the pixel design. However the applications of these MOS imagers were still limited, due to the immature fabrication technology, e.g. a large non-uniformity between pixels due to the process spread, which introduced extremely high fixed-pattern noise.

On the other hand, the success of the CCD imagers in the years between the late 1970s and 1980s led to a stagnation of research into MOS-based image sensors. From 1970, a new solid-state imaging device, CCD, was introduced by Boyle and Smith from Bell Labs [6]. Compared to MOS imagers, CCDs had the advantage of a simpler structure and a much lower fixed-pattern noise, which made them more suitable for imaging market applications. In the mid-1970s, the CCDs began to appear in the imaging applications. After 10 years of overcoming the fabrication and reliability issues, CCDs technology realized the vast commercialization and quickly dominated almost all digital imaging applications. Although CCDs had excellent imaging performance, their fabrication processes are dedicated to make photosensing elements instead of transistors. Consequently, it is very difficult to integrated the whole peripheral and signal processing circuit on a CCD chip. However, if it were possible to realize an imager in a standard CMOS process, the signal processing could be integrated on a single chip, which could make camera-on-a-chip becoming true.

In the early of 1990s, MOS imagers started to make a comeback [7]. In 1995, the first successful high-performance CMOS image sensor was demonstrated by JPL [8]. It included on-chip timing, control, correlated-double

sampling, and fixed-pattern noise suppression circuitries.

In all, compared with CCDs, the main advantages of the CMOS imagers are:

1. On-chip functionality and compatibility with standard CMOS technology, which means the sensor could integrate signal processing blocks on the same chip. For instance, amplifier, ADC, data compression etc.
2. Lower cost, lower power consumption compared with CCD technology. Estimates of CMOS power consumption range from 1/3 to more than 100 times less than that of CCDs [9].
3. Integrated level of circuit is rather high compared with CCDs.
4. Flexible readout mechanism and high speed imaging.

From then on, the development of CMOS imagers has dramatically improved and has replaced CCDs in many fields. This development was driving by two independently motivated efforts. The first was to design highly integrated single chip imaging systems where low cost, not performance, was the driving factor. The second independent effort was the special need of highly miniaturized, low power, high performance image systems for next generation deep-space exploration spacecraft, the cost was not the concern. These efforts have led to significant improvement of performance of the CMOS image sensor. Since 2000, CMOS image sensors have began their “golden age” due to the fast increasing demand from cameras used in mobilphones. Due to the nature of the CMOS imagers like small size and low power consumption, CMOS image sensors are perfect to meet the needs of portable electronic device application. Now, CMOS imaging is already emerging as a mature technology alongside CCDs. The mobilphone equipped with a CMOS camera have become a standard. However, despite the advantages listed above, there are still significant disadvantages of CMOS image sensors compared to CCD technology [10].

1. Sensitivity: the CMOS Active Pixel Sensors(APS) has a limited fill factor, less quantum efficiency, hence, less sensitivity.
2. CMOS image sensors suffer from several (fixed-pattern) noise sources especially under low illumination.
3. The dynamic range, which will be discussed in detail in next section.

In order to overcome these problems and also to improve the current advantage of CMOS image sensor, the development of CMOS imagers and challenges for these applications are focused on improving image quality which will be discussed in next section.

## 1.2 Challenges and Motivation

After retrospect the history of CMOS image sensors, this section will briefly look into the future. From the micro-fabrication and design point of view, extremely high resolution and small pixel pitch does involve many challenges and technical issues. In this section, a few existing design challenges will be analyzed. To evaluate the performance of the imager we should consider a lot of aspects and constrains. It is difficult to mathematically define the functional relationship between these constrains and it is still no widely accepted figure-of-merit(*FOM*) has been defined for CMOS imagers. Nevertheless, it is still possible to identify a number of parameters that are defining and evaluate CMOS image sensor performance.

In analog circuits, both signal-to-noise ratio (*SNR*) and dynamic range(*DR*) are important parameters and always cause confusing because in many situations, the maximum SNR is nearly equal to DR. *SNR* is defined as the the ratio between the signal and the noise at a given input level and can be given as:

$$SNR = 20\log\left(\frac{\text{Number of signal electrons}}{\text{Number of noise electrons}}\right)[dB] \quad (1.1)$$

The dynamic range( $DR$ ) is defined as the ratio of the maximum and the minimum electron charge measurable by the potential wells corresponding to the pixels [11]. It can be given as:

$$DR = 20\log\left(\frac{\text{Number of signal electrons at saturation}}{\text{Number of noise electrons without exposure}}\right)[dB]. \quad (1.2)$$

However, the noise level of an image sensor is signal dependant because of the existence of photon shot noise and it dominates at higher input signals. When the pixel is saturated with photon-generated electrons, the photon-shot noise level is higher than the noise floor of without exposure, thus from the formula above, for an image sensor the maximum  $SNR$  is less than the its  $DR$ .

To improve the overall quality of the image, a high  $S/N$  ratio and wide dynamic range are desired. To correspond to these requirements, a lot of work has been done. From the definition of the dynamic range in formula 1.2 there are two methods to improve, decreasing the dark noise level or increasing the full-well capacity which is the maximum charge saturation level. For instance wide dynamic range CMOS image sensors with multi-exposure [12], linear-logarithmic exposure [13] [14], are desired to improve the full-well capacity. However these works increasing the pixel full-well capacity either sacrifice the other performances like  $S/N$  ratio or have a significant cost on increased chip area, power consumption, circuit complexity. On the other hand, reducing the noise not only could increase the dynamic range of pixel, but also could benefit the  $S/N$  ratio at the same time when the noise floor of CMOS image sensor could be lowered.

To decrease the noise floor, we should analysis the origins of these noise sources. The origins of noises are complicated and can be classified as 3 types according their different origins. The photon shot noise is fundamental in nature and is always has a root-mean-square value proportional to the signal level. The second type is a technology dependent noise source like dark current noise. The third type of noise is produced by the circuit, for

instance the reset noise, thermal noise, and  $1/f$  noise. These noise sources will be analysis in detail in chapter 2.

From the other aspects, with improvement of the imaging fabrication process scaling, the pitch of pixel keeps shrinking which causes the smaller fill factor and the lower signal level. To increase the signal level under the same lighting condition becomes important and challenging. This is indeed one of the motivation of this thesis: to increase the signal level under the same lighting condition to achieve the high light sensitivity for CMOS image sensor. The other motivation of this thesis is that pixel design work always need the support of the peripheral circuit. So a small and flexible test structure of the CMOS image sensor which can provide the row and column addressing, timing control, data sample and processing... was designed which will be introduced in detail in Chapter 3. Having this test chip will make different pixel designs more easily and quickly to implement on the whole image sensor chip.

In this thesis, we propose some special arrangements of pixel design to try to increasing of pixel sensitivity and then improve the overall image quality.

### 1.3 Thesis Outline

This paper is organized as follow. In the chapter 2, we introduce the interlacing technology and the different modes of interlaced scan, deeply analyze the origin and proposed potential solution to improve the light sensitivity and S/N ratio.

The particular architecture and the working principle of the CMOS image sensor, which combine the peripheral circuit and pixel array, is presented in Chapter 3.

In the chapter 4, the design of the test PCB and relevant measurement

work is introduced, and some measurement results with analysis are given in detail.



## Chapter 2

# Introduction to Interlacing Technology of CMOS Image Sensors

In this section, the principle and the mechanism of interlacing technology in the charge domain is present. The section 2.1 will briefly overview the interlacing technology. The necessity of the interlacing technology and relevant issues caused by it will be discussed in detail. The section 2.2 will analyze the two different modes of interlacing scan. In next section 2.3, the architecture and working principle of 4T pixel structure was presented, and the shared readout pixel structure is introduced. Inspired by the mechanism of the field integration mode, and the shared readout pixel structure, in section 2.5 we propose a charge domain interlacing pixel design for high sensitivity CMOS imagers as a potential solution to deal with the signal noise ratio problem.

### 2.1 Overview of Interlacing Technology

Interlaced cameras are characterized by the interlacing readout mechanism inherited from both European and US television standards. It is a technique for improving the picture quality of a video signal primarily on cathode



ray tube(CRT) devices without consuming extra bandwidth. When you're watching your television, if you go up real close to it and watch carefully you'll notice that the picture sort of "shimmers." That's interlacing at work.

### 2.1.1 Interlaced Scan

Many years ago, some engineers in UK worked on what was then called high-definition television. It had 405 horizontal scan lines and was monochrome only, which offered high definition compared to the television technology that had gone before, and had the high potential to serve as a standard for several decades. But the design presented problems. It needed hundreds of horizontal scan lines each of which required quite a few cycles of detail to achieve the intended resolution. And to meet the standard for eyes to prevent visible flicker, the picture had to update 50 times per second. Consider each line had 250 cycles of horizontal modulation, the system bandwidth would be  $250 \times 50\text{Hz} \times 405$ , which is just over 5MHz. The necessity for an audio carrier and a vestigial lower sideband would increase the required bandwidth to about 6MHz. The requirement was too high for VHF(Very High Frequency) technology of the day and the cost for the system would be very expensive. Interlacing, as the solution to the bandwidth problem, was invented from 1930s. This mechanism does not transmit the scan lines of the frame in their order. Instead, each frame is divided into two parts called fields. The first field carries the odd lines(1,3,5...),and the second field carries the even lines(2,4,6...),which are lines omitted in the first field. Figure 2.1[15] illustrated this process. In the figure, the solid lines represent the scan lines transmitted in the first field, and the dotted line represent the scan lines transmitted in the second field. This reduces flicker by taking advantage of the persistence of vision effect, producing a refresh rate of double the frame rate without the overhead of either transmitting each frame twice or holding it in a buffer so it can be redrawn. The United States developed their TV broadcast systems standard as 525 lines, 60Hz,

2 : 1 interlace(NTSC) which is still used nowadays. When European teams designed a successor to the 405-line scheme, it seemed convenience to select a line rate similar to the US standard which can use same the line-scanning components. So the Europeans increase the number of lines to 625, due to the 50Hz frame rate of European standard(PAL).

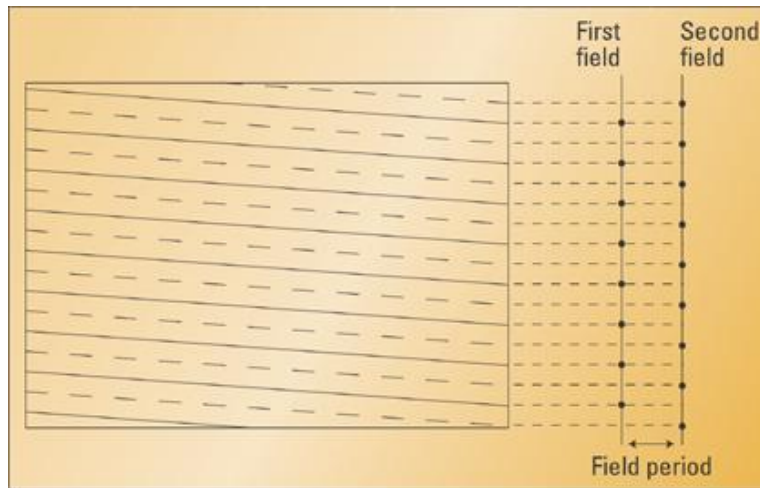


Figure 2.1: Interlacing meshes two subsampled fields together to make a frame

In the other way, the interlaced scan means the odd-number lines are scanned in the first 1/50th second, and then the even lines are scanned. the figure 2.2[16] illustrates the scanning process. This view in (t,y) coordinates illustrates the discredited sampling nature of the scanning process.

### 2.1.2 Interlace Scan Issues

The fast development of television broadcasting was benefit from the interlacing technology. Conventional TV systems use an interlaced scan format because it means good compromise between spatial and temporal resolution as well as flicker reduction on one hand, and bandwidth on the other hand. However, since each frame of interlaced video is composed of two fields that are scanned separately in time by 20ms, the position of a moving object will have changed between the two fields, some times resulting in artifacts when

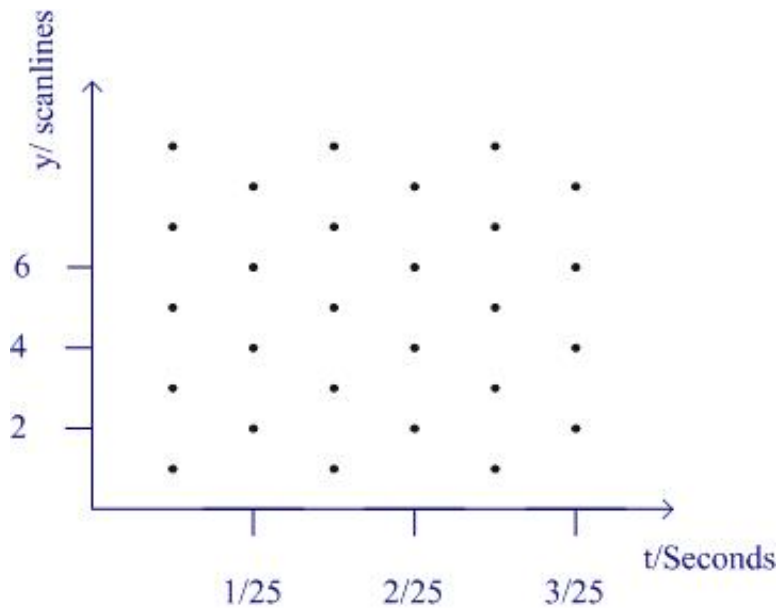


Figure 2.2: Interlace Scan

two fields are combined to the final image.

An other problem is the development of display technology, a lot of display devices, other than CRT, can not support the interlace scanning format but must draw the screen each time. The video must be de-interlaced before it can be displayed. De-interlacing requires the display to buffer one or more fields and recombine them into a single frame. In theory this would be as simple as capturing one field and combining it with the next field to be received, producing a single frame. But also due to the short time difference between two continuous fields, the de-interlace results in a “tearing” effect where alternate lines are slightly displaced from each other. Modern de-interlacing systems therefore buffer several fields and use techniques like edge detection in an attempt to find the motion between the fields. This is then used to interpolate the missing lines from the original field, reducing the “tearing” effect [17].

Due to problems mentioned above, from the 1940s onward, improvements in technology allowed the US and the rest of Europe to adopt systems using

progressively more bandwidth to scan higher line counts, and achieve better pictures. However the fundamentals of interlaced scanning were at the heart of all of these systems.

### **2.1.3 Progressive Scan**

Compared with interlace scan, the other method of scanning –progressive scan means all lines of a video frame are scanned successively and each field has the same number of lines as a frame. The scan lines in a progressive image are scanned from one row to the next, from top to bottom. The whole frame is created in one time, which is different from interlace scan.

Compared with the interlace scan, the progressive scan has a higher vertical resolution under the same frame rate.(Vertical resolution: the number of rows, dots or lines from top to bottom on a printed page, display screen or fixed area such as one inch. Contrast with "horizontal resolution," which is the number of elements, dots or columns from left to right.) It offers fewer artifacts than interlace scan. The main drawback compared with the interlace scan is that it requires higher bandwidth than interlaced video that has the same frame size and vertical refresh rate.

## **2.2 Two Interlacing Modes**

For compatibility reasons, the NTSC/PAL scanning scheme has been carried over to the digital camera employing the CCDs/CMOS image sensor which can record the video. The first work using interlacing technology in CCDs is introduced by Carlo in 1973 [18]. From then on the interlaced CCD cameras was becoming popular. Why is the artifacts disadvantage not simple avoided by switching to a progressive scan? There are 2 reasons for this. One reason is more about economy: extensive modification in the construction of the broadcasting system. This involves a major effort and considerable expenses. Many users would outweigh the advantages. The other reason

is for interlaced scan the sensor could have better light sensitivity than progressive scan sensors. To better understanding this advantage we will introduce the two different modes of interlacing scan.

1. Frame integration mode: This integration mode is shown in figure 2.3[19], during the first field, the odd lines(1,3,5,...)were scanned and output as line 1,3,5,... The second field consists of even lines (2,4,6,...), and also outputs as even line (2,4,6,...) of the new frame. The sensitivity of this mode is the same compared with the progressive scan, and the temporal resolution is also low because it does need two fields to get the whole image information. The advantage of this mode is the relative high vertical resolution and it is easy to implement.

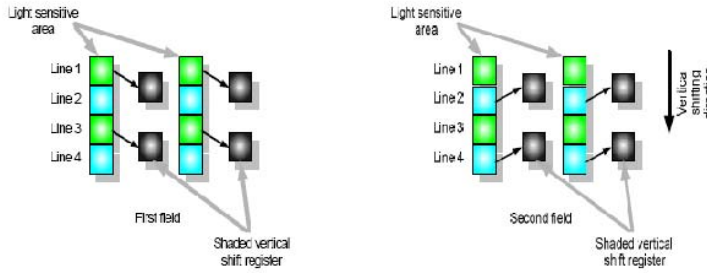


Figure 2.3: Frame Integration mode

2. Field integration mode: In frame integration mode, the photo-generated charges stored in the odd horizontal scanning pixels are readout in the odd field, while the other line charges are read out in the even field. The integration time for the each pixel is equal to the frame time of the broadcasting system (40ms in Europe). In the field integration mode the charges in two adjacent scanning lines are added together, like the first field scan and get the line 1 + 2, 3 + 4, 5 + 6, ... and output as the line 1, 3, 5, .... Using line 2 + 3, 4 + 5, 6 + 7 to make the second field and outputs as the line 2, 4, 6, ... This mechanism will be illustrated in figure 2.4. The integration time is the field time which is half

of the frame time (20ms in Europe). The characteristics of field integration mode of scanning can be concluded as below. First, no field time lag [20]. Due to the lower integration time for field integration mode, charges for the preceding field remain in the photo-diode(called “field time lag”) is much less than frame integration mode. Secondly, reducing the flicker at vertical edges of image. The field integration mode doubles the vertical aperture. Thirdly, the vertical resolution of the field is lower than progressive scan and frame integration mode. And last but not least, it has a high sensitivity, wide dynamic range compared to the frame integration mode. The field integration mode combines two scanning lines together, which is equal to enlarges the pixel size two times and means better the light sensitivity and dynamic range [21]. The design of this thesis is also based on the field integration mode due to its high sensitivity.

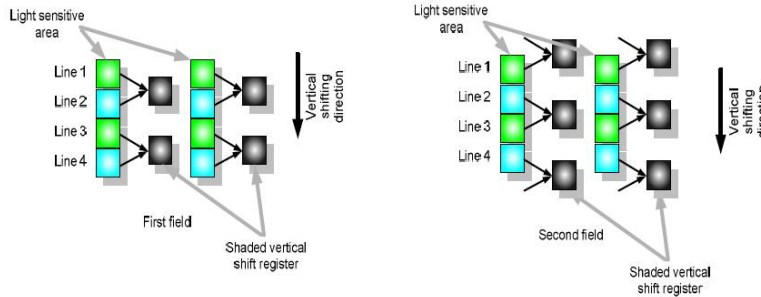


Figure 2.4: Field Integration mode

## 2.3 CMOS Image Sensor Pixel Circuits

### 2.3.1 Photodiode

A photosensitive element is the indispensable part of an image sensor. The basis of photosensitive imaging is the photo-electric effect [22]. When a semiconductor is exposed to light, the incident photons will penetrate into the material generating electron-hole pairs, as long as the incident photons

have energy higher than the bandgap of the semiconductor. In the solid-state imaging, the most widely used semiconductor material is silicon, which has a bandgap low enough (1.1eV) to allow visible light to generate electron-hole pairs.

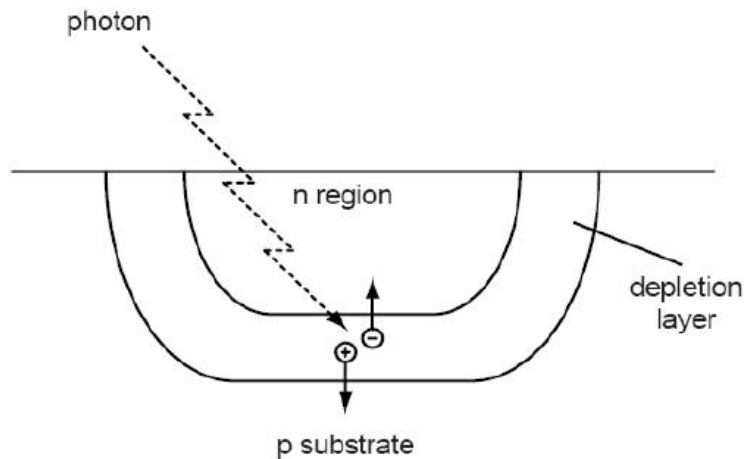


Figure 2.5: Photocurrent Generation in P-N junction

In order to detect the generated electron-hole pairs, a quick separation of the electrons from the holes is necessary to stop the recombination. The simplest method is using a reversed pn junction as a photodiode structure (figure 2.5). The electric field across the depletion region will cause the electrons to drift towards the n-doped region, the holes drift towards the p-doped region. In a word, when a photodiode is exposed to light, the incident light will produce electron-hole pairs that results in a reverse current, often called photocurrent. To accurately measure the photocurrent, all modern solid state imagers work in integrating mode. The photocurrent is integrated onto a capacitance, and the voltage change across the capacitance is read out.

### 2.3.2 Photodiode Three Transistor (3T) Pixel

Normally, we classify CMOS Image Sensor according to their pixel structures. These pixel structures can be classified into two catalogs, which is named the passive pixel sensors(PPSs) and the active pixel sensors(APSs).

PPSs structure consists of a photodiode and a select transistor as shown in figure 2.6[23]. When the access transistor is “on”, the photodiode is connected to a vertical column bus. A charge integrating amplifier readout circuit is arranged at the bottom of the column bus. This pixel is characterized by a large fill factor. The fill factor indicates the size of the light sensitive photodiode relative to the total area of the pixel.

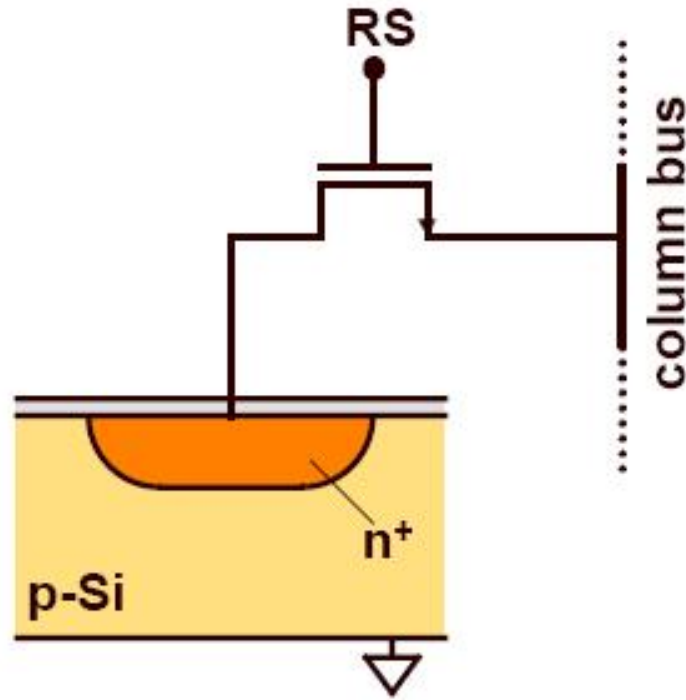


Figure 2.6: Passive Pixel Structure

To improve the PPSs structure, the APSs design was proposed. The APS pixel inserts an amplifier within every pixel. Since each amplifier is



only active during its readout, the power dissipation is minimal. The most common type of the APS is the photodiode three transistor (3T) pixel as figure 2.7 shows. In the schematic below we can see the source follower is the amplifier in the pixel, the two other transistors in pixel are used for addressing (RS), and reset the pixel (RST). The potential of the photodiode is to reset to the highest voltage value through a reset transistor ( $RST = 1$ ), after reset, the photon generated charges are collected and converted to a voltage by the photodiode. After the integration time, the voltage video signal is sensed by the source follower. When particular row was selected ( $RS = 1$ ), the row select transistor operates in the triode/linear region as an analog selection switch. Then the video signal can be accessed on the column bus. The pixel is reset again afterward.

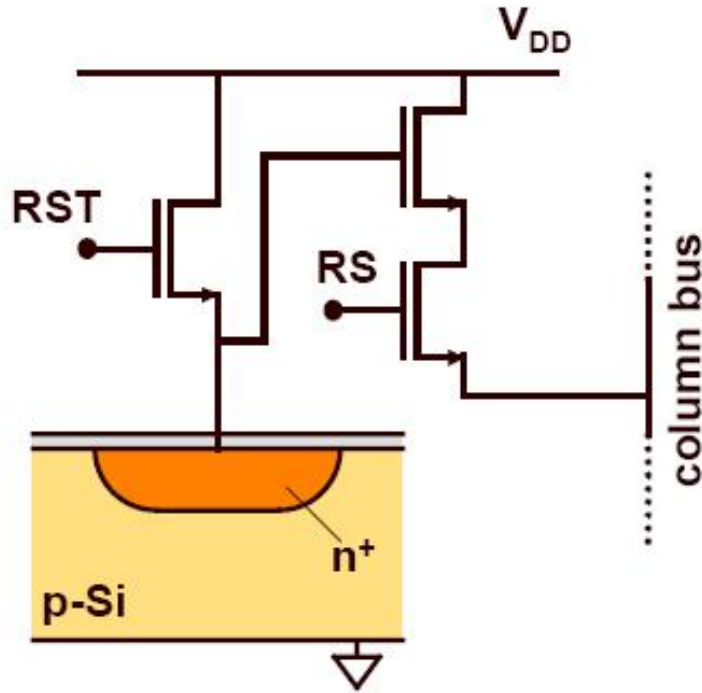


Figure 2.7: Photodiode 3T Pixel

Compared to APSs pixel structure, PPSs has the advantages like high fill factor, high quantum efficiency, and a simple structure. The disadvantages

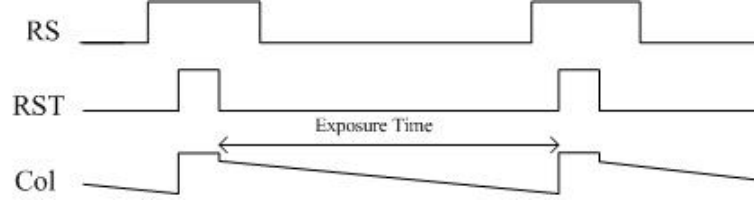


Figure 2.8: Timing of 3T APS pixel

are mainly because its readout noise level and scalability. The passive pixel also does not scale well to larger array sizes and or faster pixel readout rates. This is because increased bus capacitance and faster readout speed both results in higher readout noise. The photodiode capacitance is very small compared to the large vertical column and horizontal bus capacitance. This mismatch in capacitances results in a large noise component added to the signal during readout of the photodiodes. To solve the problem the active pixel inserted a buffer/amplifier into the pixel could potentially isolate the sense node from the column capacitance and improve the performance of pixel. Adding an amplifier to each pixel significantly increases sensor speed and improves its SNR, thus overcoming the shortcomings of PPS. Decrease in detector area is compensated by an increase in conversion gain. The conversion gain (2.1) reveals the relationship between the voltage output of the pixel and the number of electrons stored on the photodiode, which is determined by the photodiode capacitance in 3T APS pixel.

$$CF = \left( \frac{q}{C_{PD}} \times A_{SF} \right) \quad (2.1)$$

$C_{PD}$  : photodiode capacitance;

$A_{SF}$  : gain of source follower;

But 3T APSs still have their own problems. Introducing an amplifier within every pixel increases the mismatch between the different pixels. If uncorrected, this mismatch will cause large offsets which is called Fixed Pattern Noise. Fixed Pattern Noise (FPN) is also one of the main disadvantages of CMOS imagers compared with CCD technology. Canceling FPN can be performed by on-chip or off-chip storage of the offset values while the pixel is

reset. Double sampling (DS) is an effective way to implement this cancellation. During the pixel readout cycle, two samples are taken. One when the pixel is still in the reset state and the other when the video signal (and noise) has been transferred to the read-out node. Although DS reduced the fixed pattern noise to a large extent, for 3T APS, DS will increase the reset noise ( $KT/C$  noise) in the 3T APS pixel. The double sampling operation, the reset signal sampling and integration signal sampling, needs to be completed within a short readout time ( $RS = 1$ ). Thus, the integration signal which contain both the reset noise and the video signal will be sampling at the end of integration period. The reset signal which mainly contains the reset noise will be sampling at the beginning of the next integration period. Since the reset signal in the two samples (two different integration periods) are not correlated with each other, the double sampling, which means subtract between two signals, will make the reset noise increased but not canceled out.

### 2.3.3 Pinned Photodiode Four Transistor (4T)Pixel

Pinned Photodiode 4T pixel, as the mainstream choice of CMOS image sensor nowadays, as shown in figure 2.9 [23] introduces two elements. One is the regular photodiode is replaced by a pinned photodiode PPD. The other is a transfer gate TX is added between PPD and the floating diffusion node. The common purpose of these two elements is to establish charge transfer from the photodiode. As can be seen in band diagram 2.10 [24], the sandwich structure (p-n-p) of PPD can store the charge underneath the surface and into the silicon. An other goal of adding a transfer gate TX is to decouple the PPD region from the sense node and to split two important conversions – photon to charge conversion and charge to voltage conversion. When the transfer gate TX is turned off, the pinned photodiode is insulated from the readout FD node, thus the integration of the photo-generated charge happens at the capacitance  $C_{PD}$  of the the photodiode. If

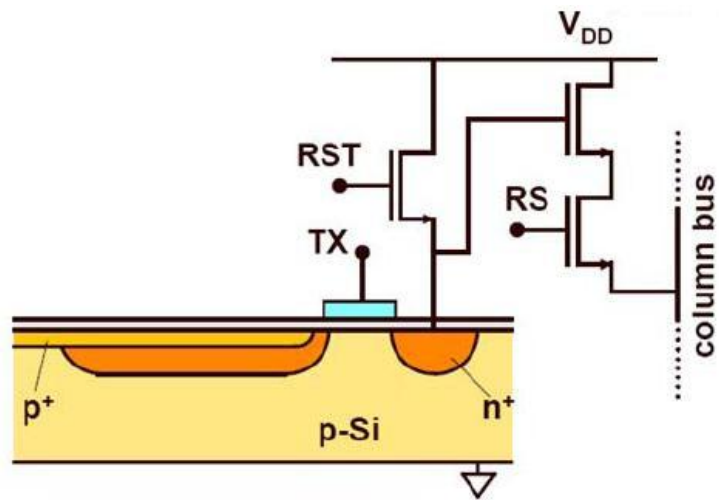


Figure 2.9: The 4T Pinned Photodiode Pixel

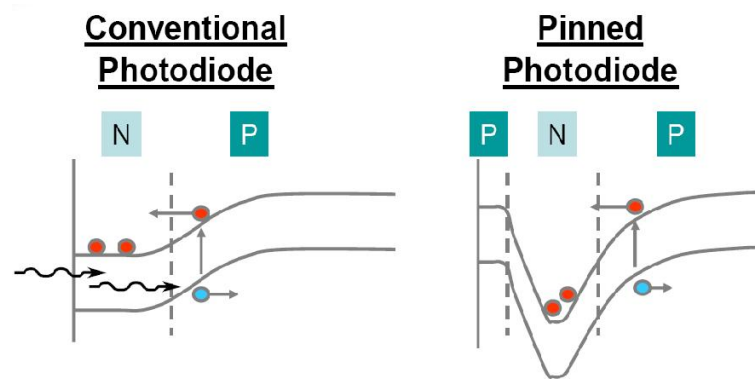


Figure 2.10: Band diagram comparison of two photodiodes

the transfer gate TX is turned on, the accumulated charge is transferred to capacitance  $C_{FD}$  of the floating diffusion node, and the charge is converted into voltage signal. This separation makes two parameters, the full-well capacity and the conversion gain not highly related anymore. In 3T APS, the way to improve conversion gain is decrease the  $C_{PD}$  which will also deteriorate the full-well capacity at same time. After the decoupling in 4T PPD, the conversion gain is related to the  $C_{FD}$ , the full well capacity is related to the  $C_{PD}$ . Thus, compared with a 3T pixel, the conversion gain of 4T pixels is normally higher, which is attractive when obtaining high light sensitivity. On the hand, photon to charge conversion and charge to voltage conversion decoupling also means that read and reset operations can departed with integration period. Thus, correlated double sampling(CDS), as will be discussed in detail in section 2.4.2, can be used in a 4T imager design. Compared with 3T non-correlated double sampling, as explained before, the kTC noise can be eliminated completely in 4T PPD pixel. These aspects are clarified by the timing diagram.

The rest of the pixel components perform the same function as in 3T APS design: reset transistor, source follower, and row select transistor. From the

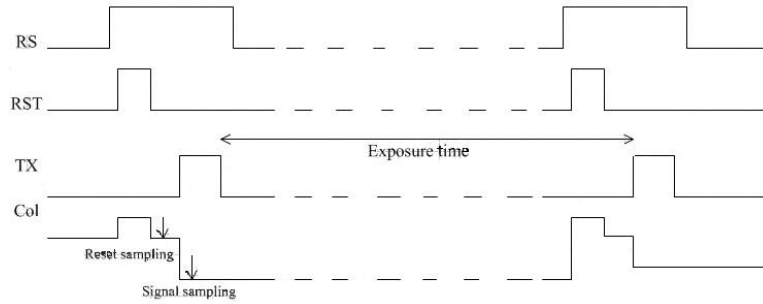


Figure 2.11: Timing diagram of 4T Pinned Photodiode Pixel

timing diagram in figure 2.11 and presents the sequences for three control signals: “RS”, “RST” and “TX”, we can know the working principle of 4T pinned photodiode pixel.

1. When a particular row is addressed, the correspondence “RS” signal of this row is “on”, the readout voltage is accessible on the column bus(Col).
2. Within the line time, the “RST” pulse reset the voltage of the floating diffusion node to the highest voltage value which cleans all the charges left in the sense node. At this time the transfer gate TX is turned off and the signal charge generated by incident light is collected on the photodiode capacitance  $C_{PD}$ . But after reset, the floating diffusion node still has some noise charges which were produced by the  $kT/C$ /reset noise during the reset operation. After the reset pulse is made low, a first sample is taken. This sample contains the  $kT/C$  noise generated with the reset of the floating diffusion as well as offset and  $1/f$  noise of the source follower transistor.
3. After the first sampling, the transfer gate “TX” is pulsed. The photo generated charges were transferred from the pinned photodiode to the floating diffusion. After this transfer is finished, the second sample is taken, which contain the signal,  $KTC$  noise from the floating diffusion, offset and  $1/f$  noise from the source follower.

As mentioned before, the pinned photodiode 4T can quickly transfer the charge to diffusion node, which allows the reset of the floating diffusion to be performed before reading the signal, and the two samplings performed in the same integration period. Thus, the  $kT/C$  noise generated with the reset is correlated between the two subsequent samples, and it will be canceled out together with offset and  $1/f$  noise of source follower by subtracting the two samples.

The significantly lower noise level of 4T pixels compared to the read-out operation with 3T pixel structures make pinned photodiode 4T pixels become the mainstream choice of CMOS image sensor.

## 2.4 Increasing Signal-to-Noise Ratio in CMOS Image Sensor

From the first chapter, the signal-to-noise ratio is defined as equation 1.2. To improve the signal noise ratio, the challenge can be stated as more signal with less noise. In this section, first, the main noise sources in CMOS 4T pixel are analyzed. Secondly, the important noise cancelation mechanism Correlated Double Sampling technology will be introduced in detail. Then the binning technology will be present, which can significantly enhance the signal level.

### 2.4.1 Overview of Main Noise Sources in CMOS 4T Pixel

The noise sources in our image sensor can be classified into 3 categories: input-signal noise, spatial noise, temporal noise sources.

#### Photon Shot Noise

Photon Shot Noise is an important input-signal noise, which relates to fundamental physical laws, rather than circuit design and technology. Photon shot noise is caused by a statistical phenomenon following a Poisson distribution which is resulting from the random variation of the number of discrete electrons generated and captured by the sensor. It is basically due to the quantum nature of light, photon shot noise can not be separated from the signal. Because it appears before any signal processing or output operation, even before the detection.

The photon shot noise is equal to the square root of the mean number of electrons generated by photons like the figure 2.12 [25] shows. From the square relationship of the photon shot noise, doubling the photons will increase the noise by  $\sqrt{2}$ , the signal-to-noise ratio still can increase  $3dB$ .

$$SNR = 20 \log(N_{sig}/n_{shot}) = 20 \log(N_{sig}/\sqrt{N_{sig}}) = 10 \log N_{sig}(dB) \quad (2.2)$$

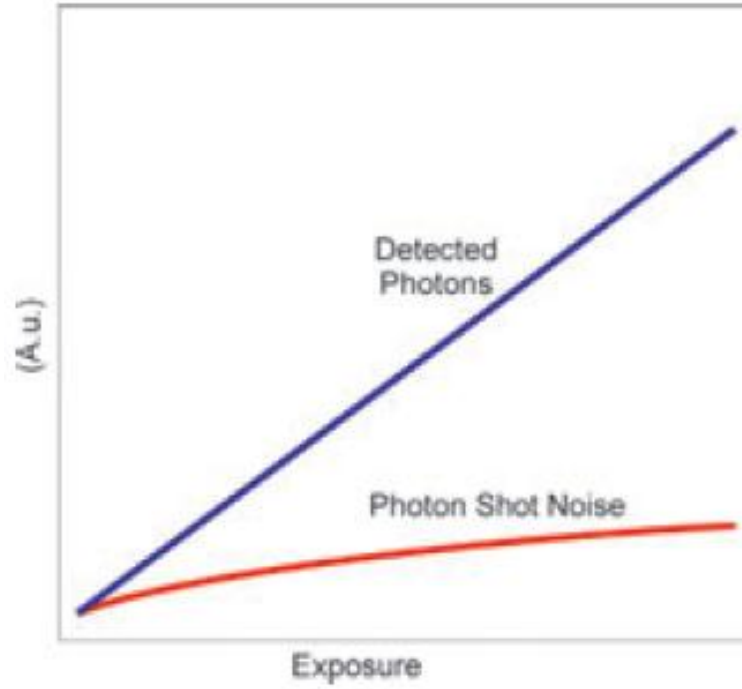


Figure 2.12: The relationship of photon shot noise and collected photon

$N_{sig}$  = Voltage of the video signal;

$n_{shot}$  = Voltage of the photon shot noise;

Therefore, under the limits of the photon shot noise, designers will try to increase the photon-generated electrons under a given level of illumination to improve the performance. With the constraints of the fill factor and pixel pitch, light intensity, and the exposure time, the charge domain interlacing technology in field integration domain is an efficient way to enhance photon-generated electrons. The other solution could be to increase the quantum efficiency of the photodiode.

### Reset/kTC Noise

As mentioned in section 2.3, the “reset” operation in the APS pixel will lead to a kTC or reset noise, which is an important temporal noise source. When a capacitor is charged through a resistor, the uncertainty of the charge



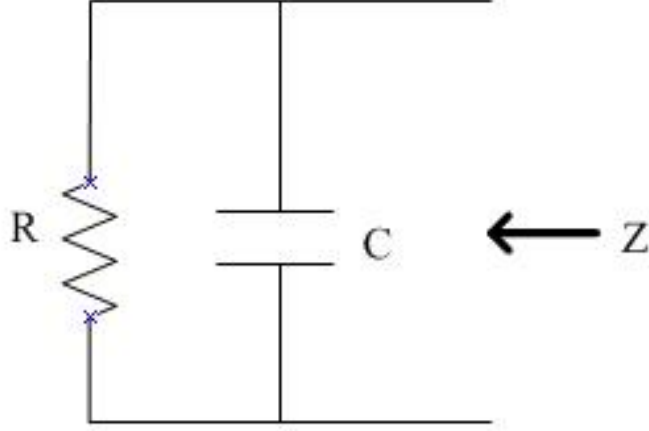


Figure 2.13: kTC noise

stored on the capacitor causes the kTC noise. The figure 2.13 shows the kTC noise model. And from this model we can conclude following formula.

$$\begin{aligned}
 Z &= \frac{R}{(1 + j2\pi fRC)} \\
 \text{Re}(Z) &= \frac{R}{(1 + (2\pi fRC)^2)} \\
 V_t &= \left[ \int_0^\infty 4KT \frac{R}{1 + (2\pi fRC)^2} df \right]^{\frac{1}{2}} = \sqrt{\frac{kT}{C}} \\
 Q_{res} &= C \times U = \sqrt{kTC}
 \end{aligned} \tag{2.3}$$

From the formula listed above we can conclude that if we want to reduce the kTC noise then the capacitor of the floating diffusion in the pixel should be small, because the noise in the floating diffusion is in the charge domain. The capacitor in CDS sample and hold circuit should be large due to the fact that the signal and noise already are converted in the voltage domain.

### Fixed Pattern Noise

Fixed pattern noise(FPN) is a classic spatial noise and it can be divided into dark and light fixed pattern noise. Dark FPN noise is mainly caused by non-uniformities of dark current generation. Light FPN is mainly caused by non-

uniformities of pixel or column response. Therefore, the noise is not related to the fluctuations of the time domain, but affected by the distribution in spatial domain.

The non-uniformity is caused by the offset of the source follower in different pixels which can be decreased by CDS as we already mentioned in last section.

### Others

Except the noise sources discussed before, there still are a lot of noise sources like thermal noise,  $1/f$  noise. These two noises are generated inside the MOS transistors and these two noises are common in a lot of analog circuits.

$$\sigma_R = \sqrt{4KTR \cdot BW} \quad (2.4)$$

Thermal noise is well known as “white” noise, or Johnson noise. It caused by the random thermal motion of the charge carriers in the conductor. According to the formula 2.4, the thermal noise is mainly determined by absolute temperature and noise bandwidth. Therefore, the reduction method for the thermal noise is to reduce the temperature and the bandwidth. In addition, instead of reducing thermal noise in CDS, thermal noise will be increase under the implementation of the CDS mechanism. Because the two thermal noises of reset and signal samples are not correlated with each other. When two noise is not correlated, then the subtraction between two samples will get  $N^2 = N1^2 + N2^2$ .

$1/f$  noise is also an important noise source, which is dominant in the source follower transistor of APS pixel. Revealed by McWhorter [26] in 1955,  $1/f$  noise is mainly caused by lattice defects at the interface of the  $Si - SiO_2$  channel of the MOS transistor. The random current variation raised by these defects trapping and de-trapping the conducting carries is  $1/f$  noise. On one hand, increasing the size of source follower transistor can highly reduce the  $1/f$  noise; on the other hand, the area inside the pixel

is highly limited and it will also affect the fill factor significantly. Thus, increasing transistor size to decrease the noise is not practical at all. In addition,  $1/f$  noise is technology-dependent and just can be fully canceled out under some special conditions using CDS. In conclusion,  $1/f$  noise is hard to be fully eliminated.

The analog signals produced by the light-sensitive elements are apt to be contaminated by the noises mentioned above, causing the lower sensitivity or lower dynamic range of CMOS image sensor, compared to the CCD technology.

#### 2.4.2 Correlated Double Sampling Technology

In previous analysis, Correlated Double Sampling(CDS) technology has been mentioned a lot of times. CDS is a very useful signal processing method for CMOS image sensors. It substrates the reset level from the signal level to suppress the noise. In this subsection we would like to explain CDS in detail. CDS technology is based on the sample/track and hold circuits. Track-and-hold circuits consist of a switch and a capacitor as shown in figure 2.14. A capacitor is used to store the analog voltage, and the switch is used to control the connection between input signal and capacitor. When the switch is “on”, the output signal will track the input signal; when “off”, the output signal is insulated with input change, the voltage on the capacitor will be hold until next track phase begins. This holding allows more processing to be done to the output signal. In most system, Track and Hold circuit produce the time-discrete samples from the time continuous input. But for the CDS of a CMOS image sensor, the input of the CDS readout circuit is already time-discrete. In the figure 2.15, we can show the working principle of CDS technology.

The input of the CDS can be classified into 3 phases. 1)The sensitive node was reset to a predetermined value. 2) A “zero-signal” $V_r$  was sampled

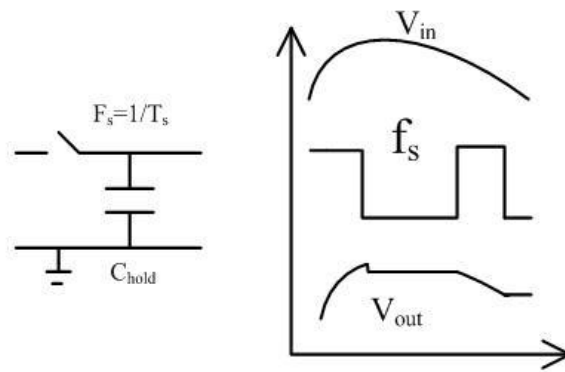


Figure 2.14: Track and Hold circuit

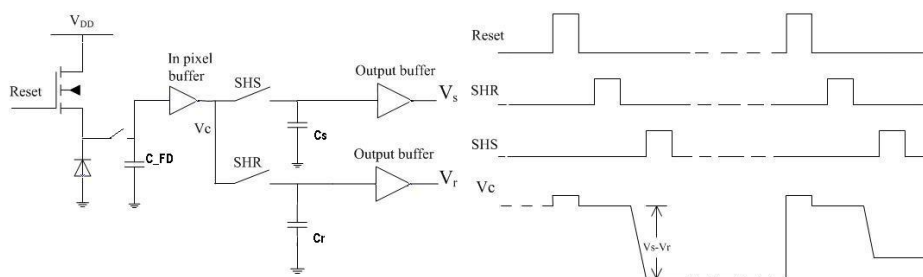


Figure 2.15: The correlated double sampling technology

by SHR, and stored  $V_r$  on a capacitors  $C_r$  and 3) The transfer gate is open, the charge accumulated in the specific integration time was transferred to  $C_{FD}$ . Then SHS trigger the sampling process, the sampled voltage  $V_s$  is stored on the signal capacitor  $C_s$  for the readout. The resetting of the sensitive node introduces a number of unwanted noise components:  $kT/C$  noise,  $1/f$  noise components, etc. The correlated double sampling technology eliminates a number of these components by first sampling the "zero-signal" level, then together with the sample from the signal sample period, and subtract these two samples with each other. The transfer function for the unwanted noise components is:

$$|H(w)| = |2\sin(wT_d/2)| = |2\sin(\Pi f T_d)| \quad (2.5)$$

$T_d$  is the delay between the two sample moments. From the transfer function (2.5)[27] we know that CDS acts as a high pass filter and shows a great suppression to low frequency noise. On the other hand, the noise at higher frequencies is increased. The circuit implementation of the CDS technology will be discussed in next chapter.

Except decreasing noise components like mentioned above in this section, improving the signal-to-noise ratio of the CMOS image sensor, can also be done by increasing the signal. Charge-domain binning technology is an effective way to increase the signal level specially in low light level application. It will be introduced in detail in next section.

## 2.5 Charge Domain Interlacing Pixel Design for High Sensitivity CMOS Image Sensor

Improvement of sensitivity or dynamic range becomes a critical challenge of CMOS image sensor design, this section intends to present some special pixel design arrangements to increase pixel sensitivity and to improve the overall image quality.

In this section we first introduce the charge binning technology. Then based on this technology and combined with the interlace scan to improve the performance of the CMOS image sensor, this project propose two different pixel structures.

### **2.5.1 Binning Techniques Increase Signal-to-Noise Ratio in CMOS Image Sensor**

The binning technology in the charge domain is based on the idea from sharing the readout circuitry among pixels. In 2004, Matshushita [28] and Canon [29] both presented shared readout circuit pixels. The concept of sharing the readout circuit by 4 pixels is time-division multiplex readout. In rolling shutter or global shutter mode, at one time, just have one pixel was readout by one amplifier. But the readout structure in pixels can be shared by different photo-sense elements. In figure 2.16, we can see four photodiodes controlled by 4 separate transfer gates, and shared one common floating diffusion which accepts the transferred charge with single readout circuit(“reset” transistor, source follower, and row selector). Thus, 7 transistors are required to readout 4 pixels, which means that only 1.75 transistor/pixel is necessary. These shared readout structure pixels were intended to produce small pixels with a high fill factor.

### **2.5.2 Two Photodiodes Shared Amplifier Structure**

Inspired by this shared amplifier structure and combined with the field integration mode, we can add the readout of neighboring lines in the charge domain through special pixel design. It allows the charge from multiple pixels to be measured in a single read operation, reducing the total noise in the final image and increasing the sensitivity of the sensor when it is operated in this mode. In field integration mode, each row will be scanned twice(both odd field and even field), not only the readout structure will be shared by two photodiodes placed in two rows, but also the individual photodiodes

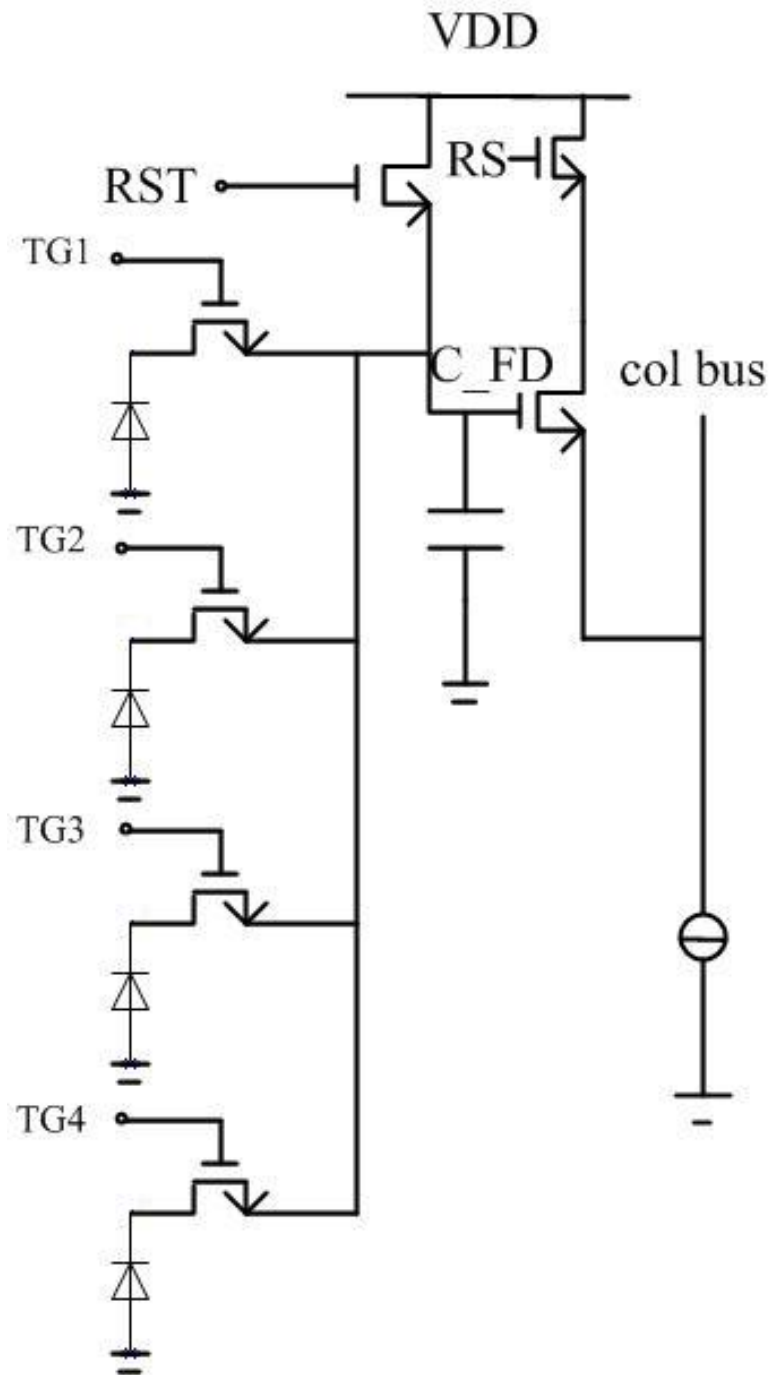


Figure 2.16: Schematic of shared pixel circuitry

will be connected and readout by two neighboring readout structures.

Figure 2.17 contains two graphs. (A) is the normal arrangement of the pixel column. This arrangement can only realize the progressive scan and this 4T pinned photodiode structure has 4 transistor/pixel. (B) is the designed pixel which has the vertical two photodiode shared amplifier structure. Every photodiode controlled by two transfer gates TX. For example, photodiode 2 was connected to  $T2\langle 0 \rangle$  and  $T2\langle 1 \rangle$  separately. It can realize both the interlacing scan in field integration mode and progressive scan.

1. With progressive scan and display, every photodiode was readout by corresponding readout structure in turn. photodiode“1” was readout by first source follower and get the output at “1’”; “2”was readout at “2’”, “3”was readout at “3’”...
2. When this design was used in an interlace scan application with repeated scan of the same photodiode row for both odd and even fields. In addition, the neighboring photodiode are sensed in combination. In the odd field scan, charges accumulated in “1”and “2” are transferred to one common floating diffusion by turning on  $T1_0$  and  $T2_0$  at same time. The corresponding output voltage“1’”is the combination of the signal produced by “1” and “2”(“1’”=“1”+“2”), which significantly enhances the sensitivity of the pixel by a factor of roughly two as compared with progressive scan in figure 2.17(A). The scanning sequence is photodiode(1,2),(3,4),(5,6)(7,8),...by driving transfer gates TXs on turn ( $T1\langle 0 \rangle, T2\langle 0 \rangle$ ), ( $T1\langle 2 \rangle, T2\langle 2 \rangle$ ), ( $T1\langle 4 \rangle, T2\langle 4 \rangle$ ),... and getting the readout signal in odd rows like “1’”, “3’”, “5’”, “7’”... In the even field, the photodiode(2,3), (4,5), (6,7),... combination was readout by turning on the transfer gates in turn like ( $T1\langle 1 \rangle, T2\langle 1 \rangle$ ), ( $T1\langle 3 \rangle, T2\langle 3 \rangle$ ), ( $T1\langle 5 \rangle, T2\langle 5 \rangle$ ), ( $T1\langle 7 \rangle, T2\langle 7 \rangle$ )...The output gives the even rows like “2’”, “4’”, “6’”,... The detail timing diagram can be seen in figure 2.18



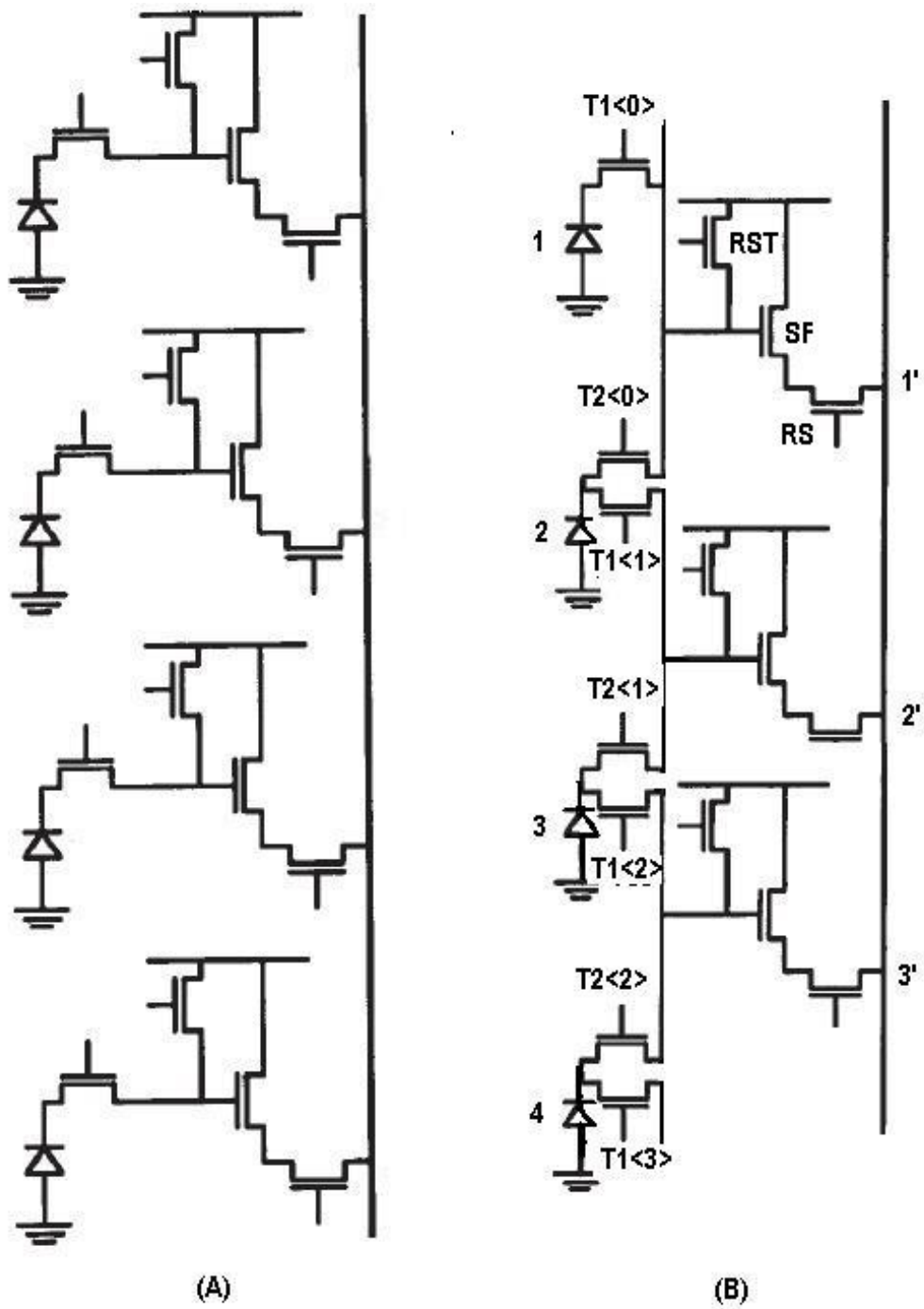


Figure 2.17: (A):Normal CMOS image column (B): Vertical two photodiodes shared amplifier structure

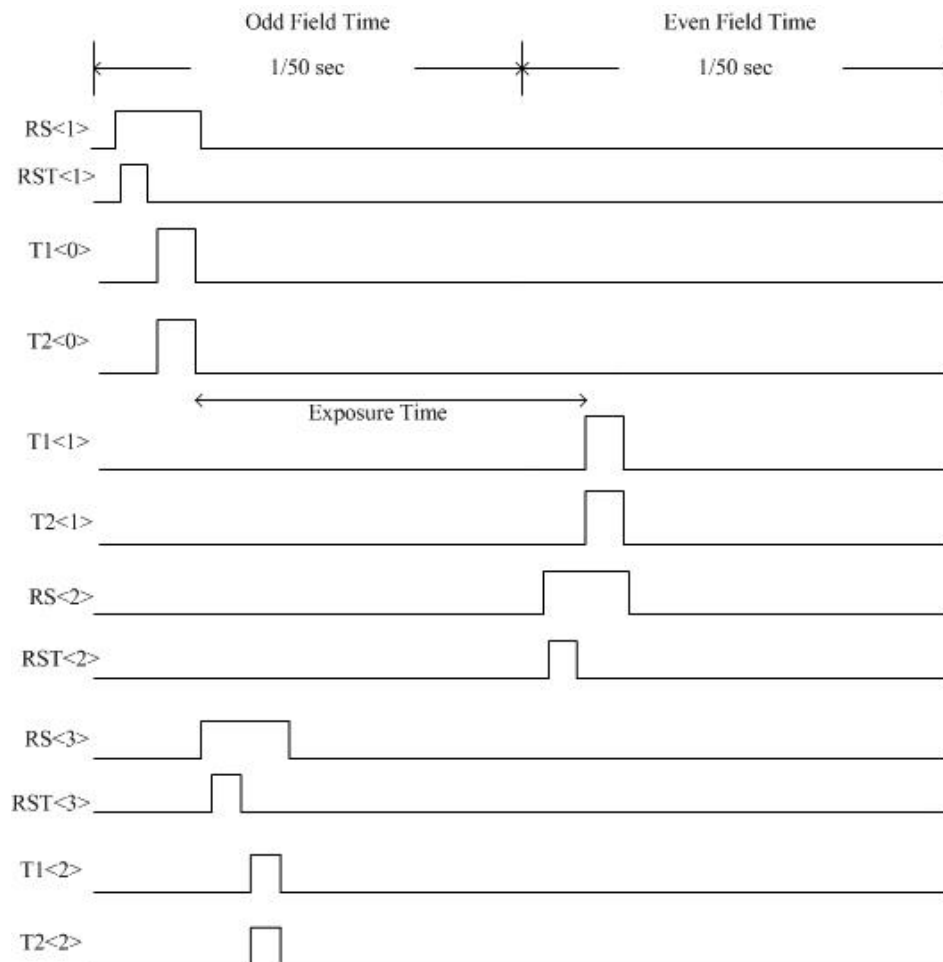


Figure 2.18: Timing Diagram of Vertical two photodiode shared amplifier structure

This structure adds one more transfer gate per pixel which achieves 5 transistor/pixel(photodiode), so the fill factor is lower than a 4T pixel. The advantage of this structure is the two signals(for example:signal produced by photodiode in Row 1 and Row 2) are combined in charge domain at the front end but not in the voltage domain or digital domain like traditional interlace. For instance, two real signals  $S_1$ ,  $S_2$ , with total noises in two photon sense element like the dark current noise and photon shot noise which produced in the photon-charge conversion as  $N_{c1}$ ,  $N_{c2}$ , the signal we get in the common floating diffusion will be  $S_1 + S_2 + N_{c1} + N_{c2}$ . For this shared readout structure, adding the noise like reset noise,  $1/f$  noise which produced in the pixel readout phase just  $N_r$ , the total readout signal is  $S_{total1} = S_1 + S_2 + N_{c1} + N_{c2} + N_r$ . If we combine the signal after the readout in the voltage domain, the combination of signal after readout could be  $S_{total2} = S_1 + S_2 + N_{c1} + N_{c2} + N_{r1} + N_{r2}$  which has much more severe noise contamination than  $S_{total1}$ , even if we do not consider the Fixed Pattern Noise produced by mismatch.

The other special arrangement of the two shared pixel design is shown in figure2.19. The characteristic of this arrangement is a different readout direction for the odd and the even field. In the odd field scan, the signal output( $1', 3', 5', \dots$ ) was read at column  $(x, x + 1, x + 2, \dots)$ . In the even field scan, the signal output( $2', 4', 6', \dots$ ) was read at column  $(x - 1, x, x + 1, \dots)$ . One particular column line is shared by pixels both left and right, both odd and even field. Due to the interlacing scan, there will be an vertical offset between odd and even fields, but this can be compensated in the read out chain.

### 2.5.3 Three Photodiodes Shared Amplifier Structure

Base on the same idea of two photodiodes shared amplifier structure and in order to improve the fill factor of two photodiodes shared amplifier structure, a three photodiodes shared readout structure is presented here [30].

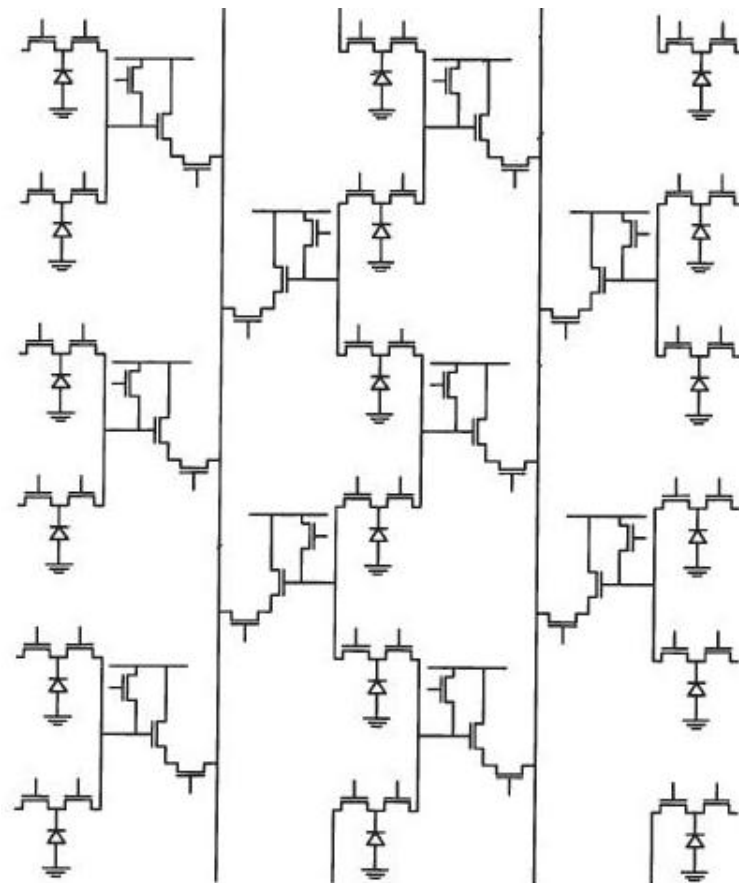


Figure 2.19: Vertical two photodiodes shared structure: mirror column read-out version

This structure also can be used in both progressive and interlace scan. The difference is it reuses the readout structure in odd and even field. The schematic of this pixel design is shown in figure 2.20. For this structure, every odd number photon sense element (like photodiode 1,3,5,7...) is connected with two transfer gates like photodiode 3 was connected to transfer gates  $T2\langle 0 \rangle, T1\langle 1 \rangle$ . All of the transfer gates T2 are use in even field scan. And all T1 are used in transfer charges in odd field scan. These two transfer gates belong to two readout circuits respectively. The even numbered photon sense elements (like photodiode 2,4,6...) are not shared but belong to one particular pixel readout circuit no matter in the odd field scan or even field scan. The photodiodes connected with transfer gates  $T2\langle n \rangle$  ( $n = \text{row number}$ ), which will turn on not only when  $T1\langle n \rangle = 1$  in odd field scan; but also  $T2\langle n \rangle = 1$  in even field scan.

The working principle of this structure for interlace scan were:

1. When the odd field time begins, transfer gate pairs turn on in sequence like  $(T1\langle 0 \rangle, T3\langle 0 \rangle), (T1\langle 1 \rangle, T3\langle 1 \rangle), (T1\langle 2 \rangle, T3\langle 2 \rangle) \dots$ , the output in the odd field gets “1’”=“1”+“2”, “3’”=“3”+“4”, “5’”=“5”+“6”...
2. When the even field time begins, activated transfer gates pairs change to  $(T2\langle 0 \rangle, T3\langle 0 \rangle), (T2\langle 1 \rangle, T3\langle 1 \rangle), (T2\langle 2 \rangle, T3\langle 2 \rangle) \dots$  Using the same readout circuit as for the odd field scan, the output was changed to “2’”=“2”+“3”, “4’”=“4”+“5”, “6’”=“6”+“7”... Because this structure reuses the readout circuit in the two fields, the number of readout circuits will be reduced to the half. Considering the extra transfer gate, this structure could improve the fill factor significantly and achieve 3 transistors/pixel(photodiode) which is lower than normal 4T pixel.

The disadvantage of this three photodiode shared amplifier structure is about the mismatch. It is hard to layout three photodiodes connected to one readout amplifier exactly the same with each other. This will cause the mismatch between pixels and produce fixed pattern noise.

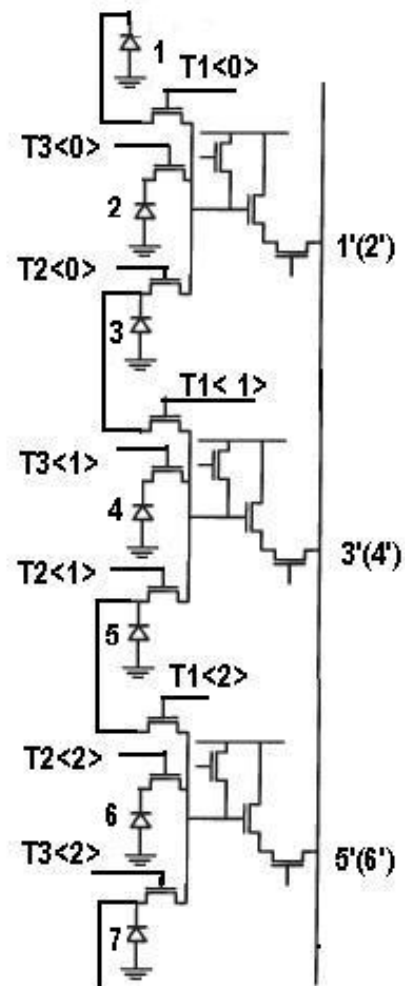


Figure 2.20: Vertical three photodiodes shared amplifier structure

In addition, all of these shared amplifier structures use the common floating diffusion which will be larger than normal 4T APS pixel. This means the associated capacitance  $C_{FD}$  will be larger and reduce the conversion gain. The other problem caused by large  $C_{FD}$  is its effect for kTC noise, however it can be eliminated by CDS.

## 2.6 Chapter Summary

In this chapter, based on the understanding of the interlace scan principle, the introduction of basic 4T APS structure, and analyzing the origins of the main noise sources in pixel, we propose some charge domain interlace pixel structures to enhance the signal-to-noise ratio and light sensitivity, which can improve the overall image performance.

## Chapter 3

# Sensor Architecture

In the last chapter, the working principle of a charge domain interlacing CMOS image sensor is explained. In this chapter, the circuit level implementation of the charge domain image sensor will be introduced into detail. In section 3.1, an overall architecture of this test chip will be presented. In the following, from section 3.2 to section 3.6 the sensor design will be divided into different functional blocks to be discuss individually. In the section 3.7, the overview of the designed sensor will be concluded.

### 3.1 Architecture of the Charge Domain Interlacing Image Sensor

The figure 3.1 is the whole architecture of the sensor, which contains several parts. I will introduced them as follow:

**Pixel Array:** the light sensitive part of the image sensor. It contain  $96 \times 128$  pixels, converting the light signal into a voltage signal.

**Current Source Array:** a current source is needed on every column bus. The current source is used to bias the source follower in the pixel and charge the parasitic capacitor of each column.

**Column Multiplexer:** according to the even or the odd field to select the column bus processed by the column analog chain.



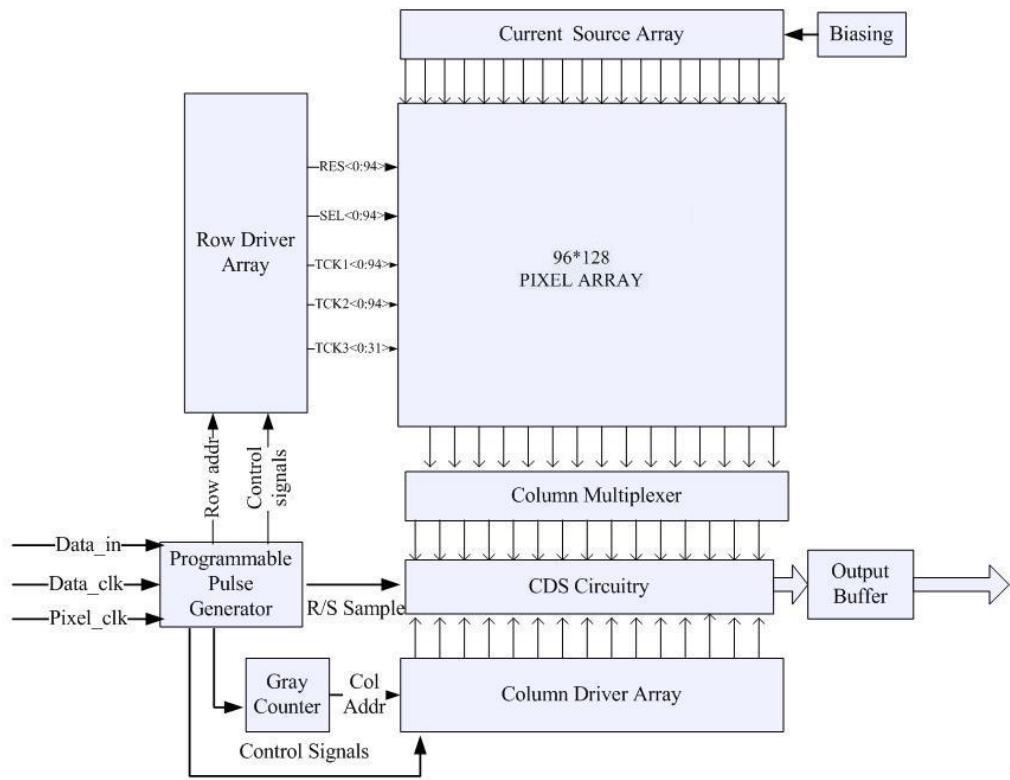


Figure 3.1: Architecture of charge domain interlacing CMOS image sensor

Column readout circuit: implementing the CDS (correlated double sampling) and analog signal processing chain to readout the column bus and output the processing signal.

Row Driver Array: decoding the gray code row address and providing driving signals for the specific addressing pixel row.

Column Driver Array: when a specific row is addressed by the row driver array(decoded from the row address), the column driver array will decode the gray code to drive the column readout circuit column by column.

Programmer Pulse Generator: buffers the series input signals and use different clock domain transfers from the series input signals to the parallel control signals. These control signals contain the row addressing signals, the pixel control signals, the column bus readout control signals and so on.

Gray Code Counter: when the counter is triggered, 7 bits gray address code is produced with the rising edge of the CLK. This code will be used to address and readout the column readout circuits.

Output buffer: the output stage of the sensor, buffers the analog output signal to enhance the driving capability of the sensor output.

## **3.2 Pixel Array**

### **3.2.1 Pixel Design**

The pixel array contains two type of pixel designs which are introduced in the chapter 2. And both two pixel designs can be organized into two different readout directions. For figure 3.2, from row 0 to row 62, there is the two photodiode shared amplifier structure pixel. From row 63 to row 94, there is the three photodiode shared amplifier structure pixel. From the Column line 0 to Column line 48, these pixels use the mirror column readout direction structure to readout.

As mentioned in last chapter and shown in figure 3.3, a basic cell of

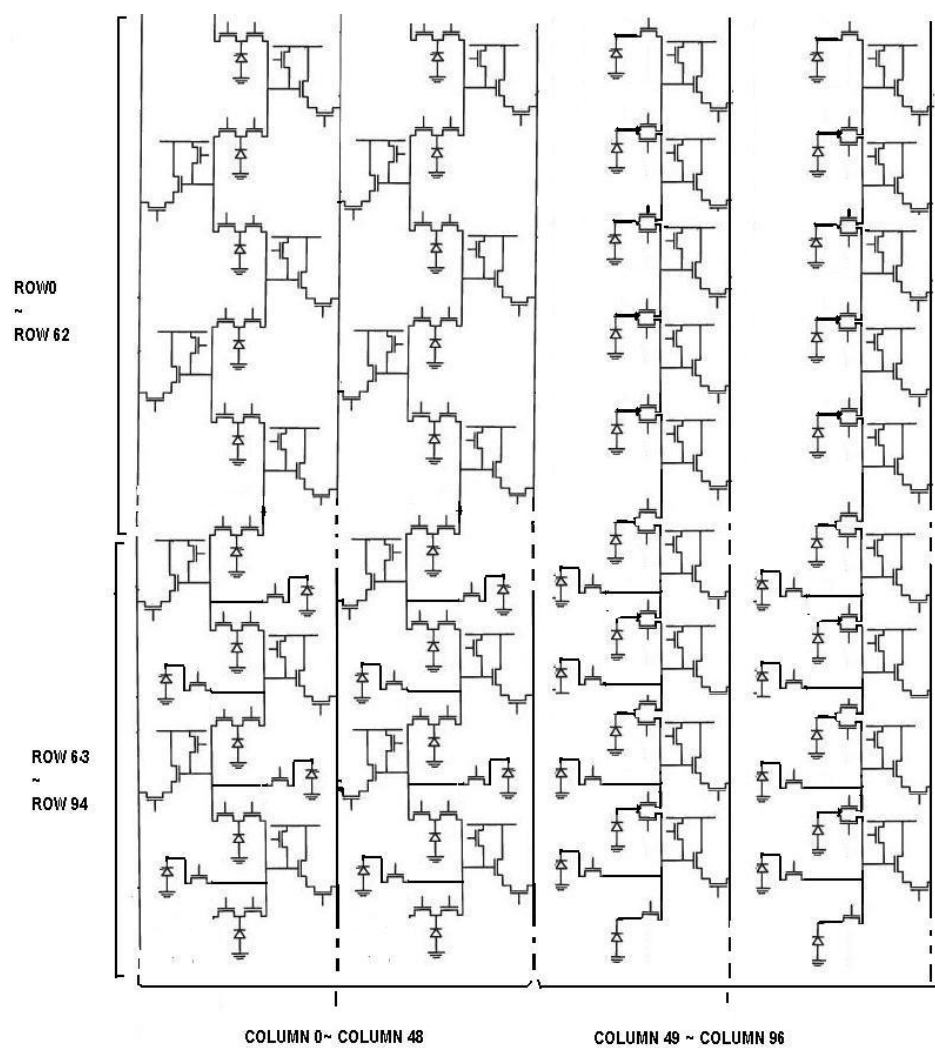


Figure 3.2: Pixel Array of Sensor

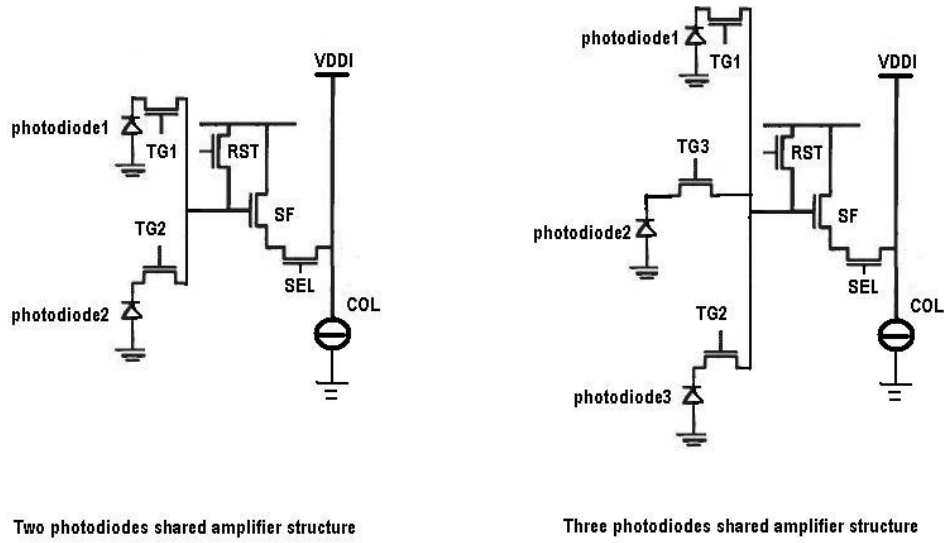


Figure 3.3: Schematic of two different pixel designs

two shared photodiodes amplifier structure includes two photodiode parts and two transfer gates(TG1 and TG2), a reset transistor(RST), a source follower(SF), and a row selector(SEL). Because these two photodiodes can have a shared readout, every photodiode is divided in two parts which have the same shape and were placed in two basic cells. This project use the pinned photodiode which is composed of a p+ implantation, n implantation and p substrate. All of other transistors in this cell are NMOS transistor which are placed in the p-well(ground). The control signals of this structure are explained in the table 3.1 below :

Signal	Description
VDDI	pixel array power supply (3.3V)
GND	Analog Ground
RST	Reset signal, high and low voltage level can be adjusted
SEL	Row select signal, high voltage level can be adjusted, low level is ground
COL	Column bus
TG	transfer gate, high and low voltage level can be adjusted

Table 3.1: 4T pixel signals description

### 3.2.2 Layout Considerations

Figure 3.4 and Figure 3.5 are layouts of the basic cell of two photodiodes, and three photodiodes shared amplifier structure respectively. The basic cell of “two photodiodes shared amplifier structure” contains two photodiode parts, but one is just the half of the actual photodiode size. The pitch of this structure is  $10\mu m \times 10\mu m$ . The fill factor of this pixel design is 46.37%. The other type “three shared photodiodes amplifier” structure contains one more photodiode and one more transfer gate. Because this three shared structure is used in both even and odd field, and contains one independent photodiode and 2 shared photodiodes, the area of this basic cell is  $20\mu m \times 10\mu m$ . The fill factor of this structure pixel is 47.8% which improves the fill factor compared with two photodiode shared amplifier structure. As shown in figure 3.4, the big red area is the pinned-photodiode part. Along every photodiode there is a blue rectangular structure which is the transfer gate of the 4T pixel structure. The readout structure is located in the middle of structure, which makes two photodiodes having the same distance to the readout structure. The three transistors in readout structure is reset transistor(RST), source follower transistor(SF), row select transistor(RS).

In this particular project, the pixel design should consider two aspects, first of all, symmetric requirement. These pixels are used in charge domain interlacing design. Some photodiodes will be shared by different readout circuits and charges stored in the photodiode will be transferred in two different directions. Even for column 0 to column 48, the readout direction is different in neighboring rows. Thus, the two photodiodes share one readout circuit should be fully symmetric with respect to the readout structure of the pixel. For the three photodiode shared amplifier structure(figure 3.5), the photodiode 2 is just being readout by one readout circuit, and controlled by one transfer gate. But the other two photodiodes 1 and 3 are shared individually by two readout structures in neighboring rows and controlled by

two transfer gates. In this situation, the layouts of the three photodiode are hard to be exactly the same to each other. But if we just consider the charge domain interlacing scan mode, the output signal is from the integration voltage of charges produced by photodiode 1 and 2 together, or charge produced by photodiode 2 and 3 together. No matter which combination, the photodiode 2 is always included. Considering the photodiode 1 and 2 together as a readout unit, photodiode 2 and 3 together as a readout unit, these two units should be symmetric.

To control the transfer gate for photodiode2, there is a metal line connected with TG3 of all the pixels in one particular row. In order to keep the metal away from the photodiode, we just could connect this TG3 at one end of the gate TG3. But for the symmetry of the layout and to avoid the non-even electrical potential across the gate of TG3, a second metal TG3 should be added to balance the electrical potential in the poly of TG3.

Second, to reduce the kTC noise, the capacitance of the floating diffusion should be small, specially for this project, the floating diffusion of two or three photodiode connected together for one readout circuit, which will be larger than normal design. In this situation, the layout should try to control the area of the floating diffusion to reduce the kTC noise.

### 3.3 Current Source Array

#### 3.3.1 Column Current Source Design

From the pixel operation, we know that a current source is necessary for each column bus. The current column source  $I_{col}$  is not required continuously during an imaging cycle, but only when the pixel values require to be reset for integration and readout. On one hand, the column current source is used to bias the source follower of pixel. On the other hand, for every pixel connected in one column bus, the row select transistor introduces a parasitic capacitor to the column bus, the column current source was used to charge

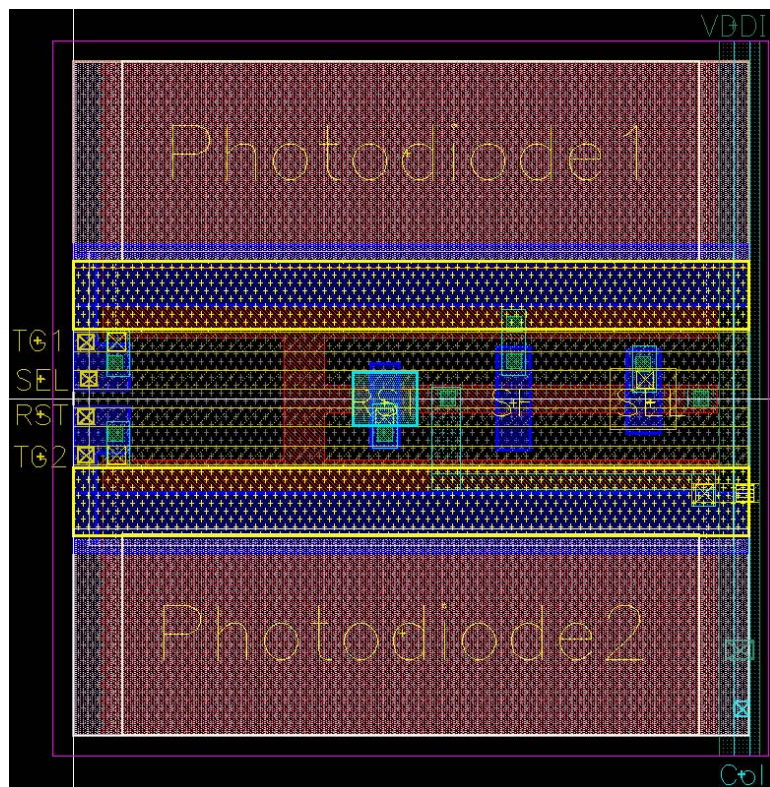


Figure 3.4: Layout of the two photodiodes shared amplifier basic cell



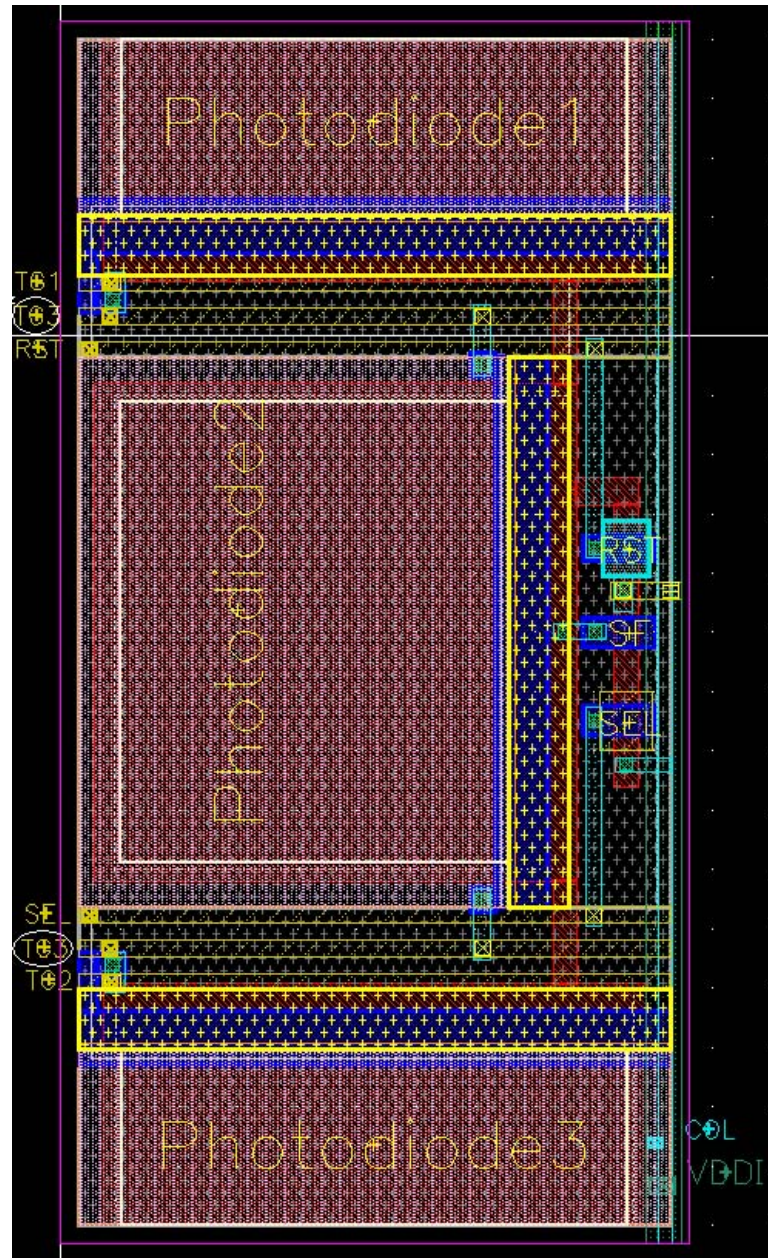


Figure 3.5: Layout of the three photodiodes shared amplifier basic cell



or discharge these capacitors to the stable value.

The figure 3.6 shows the circuit of one column current source. It can be divided into two parts according to the function. The first part is the current source (M5 and M9). Saturated PMOS transistor M9 and NMOS M5 is operated as current sources. The source ends of two transistor are connected together, which could improve the Power-Supply Rejection Ratio(PSRR) to reduce the influence of the jitter from power and ground. A stable current reference for current mirror can be provide by this structure. The second part is the current mirror (M3 and M4). The same W/L ratio of M3 and M4 makes the current  $I_{d(M3)}$  mirroring the  $I_{d(M4)}$  which is equal to 12uA. The last part M2 and M11 are used to allocate the current value for column bus. When  $CS = 2.7V$ , the NMOS M2 is “on”, nearly the total output current of M3 is concentrated to  $I_{col}(I_{d(M2)})$ . When  $CS = 1.4V$ , the total current is flow into the PMOS transistor M11, the NMOS M2 is turn “off”. When the CS is adjusted in between, the column current can be changed between 0 to 12uA. Thus, based on this current source circuit, the current ratio of PMOS and NMOS can be relocated easily, then the column current value can be controlled by input bias. But combined with the control mechanism, in this sensor, CS just can choose 2.7V or 1.4V by the digital control signal NSEL. This limitation can be improved in the future design to give more choices for column current.

VDDI	pixel array power supply (3.3V)
gnd	Analog Ground
Biasn	Bias voltage produce by Biasing Part(3.3V)
Biasp	Bias voltage produce by Biasing Part(855mV)
CS	switch of the col current which is controlled by one of the input control signal(NSEL) of the sensor. When digital signal NSEL=“1”(1.8V), CS=2.7V; when NSEL=“0”(ground), CS=1.4V
COL	Corresponding column bus

Table 3.2: Current source signal description

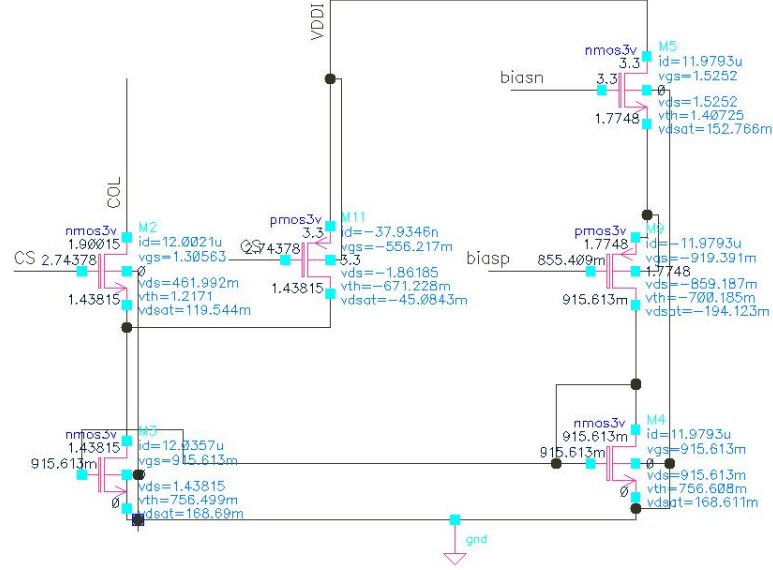


Figure 3.6: Schematic of column current sensor

### 3.3.2 Design Considerations

To design of the column current source is a tradeoff between the speed of the pixels and the noise performance. From the speed consideration, the large column current results in a the fast speed for charging and discharging the parasitic capacitance. From the noise consideration, a large current also means a large  $g_m$  of the source follower, and means a large thermal noise contribution to the output signal. So a compromise between these two aspects is made for the column current.

The design of the column current source is critical because the transfer gain of the in-pixel source follower is sensitive to this column current source. Even the small variation on the current value would change the source follower gain, which is one of origins of the non-linearity of the pixel.

This current source structure is repeated in every column, so the layout of the current source in each column must fits the pixel pitch 10um.

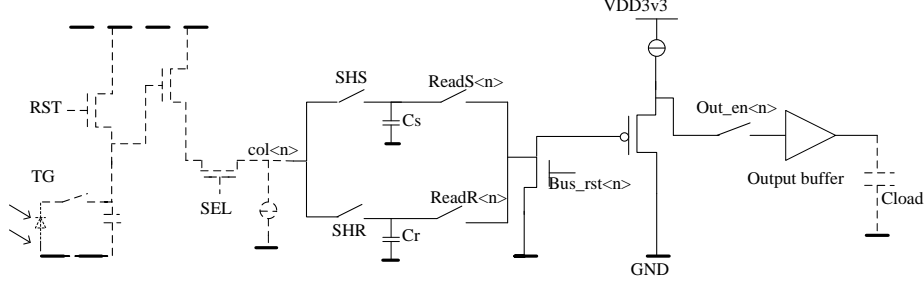


Figure 3.7: Column signal processing chain

### 3.4 Column Readout Circuit

Since the pixel array design and the current source array design are introduced in last two sections, we can get the signal and reset voltage from the column bus. To implement the CDS technology and get the output signals of the whole pixel array with good driving capability and correct timing sequence, an signal processing chain is needed for every column bus. Figure 3.7 is the schematic of the whole signal processing chain for one column, which shows the whole course from light input to the sensor analog output. This signal processing chain can be divided into two parts, the sample and hold(S/H), the readout timing control, and the output buffer.

#### 3.4.1 Sample-hold and Readout Circuit

This part will describe how to sample and hold the output signals and readout for every column bus when a particular pixel row is addressed. As figure 3.7 shows, every column bus has two 1pf capacitors ( $C_s$  and  $C_r$ ) which are used to store the reset level and the signal level respectively. The timing diagram of control signals of the column readout circuit is shown in figure 3.8.

1. When a row is addressed, all of the pixel output signals in that row

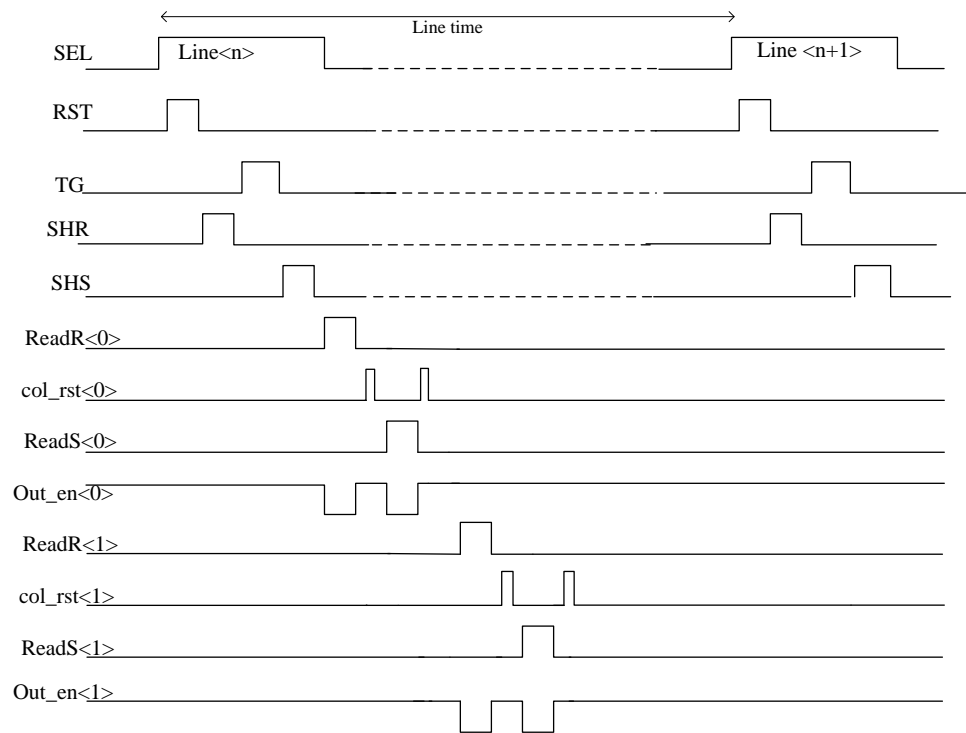


Figure 3.8: Timing diagram of 4T pixel and CDS readout

should be sampled and stored in  $C_s$  or  $C_r$  at the same time. Thus, the sample signal SHS and SHR are global signals for all the column readouts. When the row select signal SEL is high, that row is addressed. Then after the reset, the reset levels of all pixels in that row are sampled and stored in corresponding column  $C_r$  by  $SHR = 1$ ; after charges which are accumulated in the photodiode were transferred to the floating diffusion ( $TG = 1$ ), the signal levels of all pixels are sampled and stored in the corresponding  $C_s$  by  $SHS = 1$ . Until now, signals of all columns are stored in their corresponding capacitor.

2. After sample and hold the signal in capacitors  $C_r$  and  $C_s$ , readout circuits will be driving one by one from column 0 to column 96 and finished one row readout in one line time. For instance, when driving column readout circuit of column  $\langle 0 \rangle$ , switches of  $ReadR\langle 0 \rangle$  and output enable( $out\_en$ ) will open to transfer the stored reset signal to the output bus. Then the bus was reset by  $col\_rst\langle 0 \rangle = 1$ . After the reset( $col\_rst\langle 0 \rangle = 0$ ), the video signal stored in the  $C_s\langle 0 \rangle$  will be transferred to output bus ( $ReadS\langle 0 \rangle = 1 \& out\_en\langle 0 \rangle = 1$ ). When both reset signal and video signal were readout, the output bus will reset again by  $col\_rst\langle 0 \rangle = 1$ . Finished the readout of column line 0, the column line 1, 2,... will be readout at the same principle until the last column line 96. It is important to notice that the necessary subtraction of the two signals to complete the CDS action is done off-chip.
3. Then the next row is addressed, the readout process depicted in 1 and 2 will be repeated again until the whole pixel array was scanned.

These readout control signals are listed in the table 3.3 below.

For this particular application, some columns (from column line 0 to column line 48) have different readout directions for odd and even fields. For example column line  $\langle 1 \rangle$  is not only connected the odd field output of the first column, but is also connected with the even field output of the

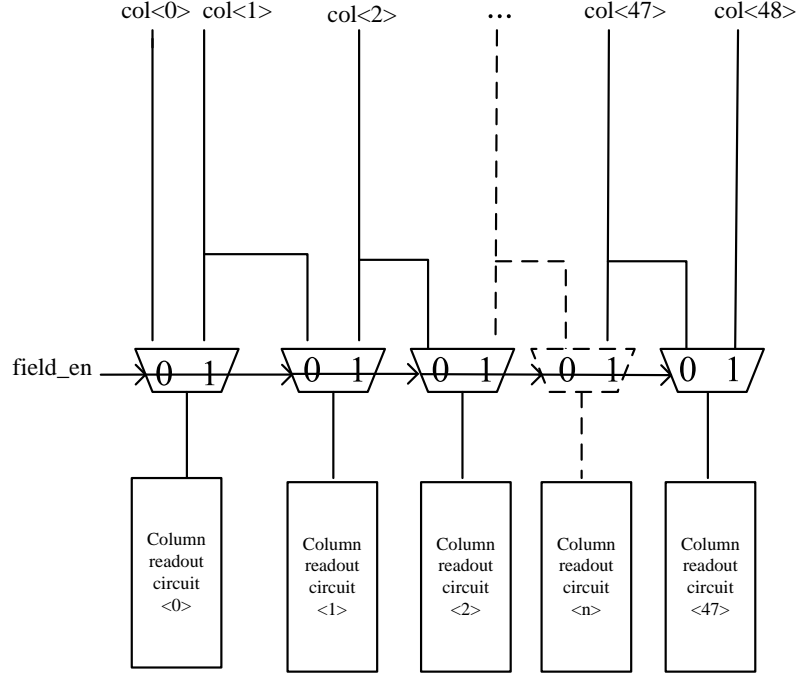


Figure 3.9: Principle of column multiplexer

Signal	Type	Sensitivity	Description
SHS	input	active high	Global sample signal for the Signal level. High is 3.3V, low is ground
SHR	input	active high	Global sample signal for Reset level. High is 3.3V, low is ground
ReadR<n>	input	active high	Readout switch for the reset signal from $C_r$ of the column. High is 3.3V , low is ground
ReadS<n>	input	active high	Readout switch for the video signal from $C_s$ of the column. High is 3.3V, low is ground
col_rst<n>	input	active high	Reset pulse for the column readout bus. If $col\_rst = 1$ , then the readout bus was reset. High is 1.8V, low is ground
out_en<n>	input	active low	Output enable signal, when reset signal or video signal were readout in column n, then $out\_en<n> = "0"$ . High is 3.3V, low is analog ground
field_en	input	level	$field\_en = 1$ means odd field scan, and $field\_en = 1$ means even field scan

Table 3.3: Column Readout Control Signals

second column. Then, to process these readout signal, the column bus will be selected by different column signal processing chains. In figure 3.9 we can see the *field\_en* signal to select a field. When the scan field is the odd field(*field\_en* = 1), the output direction of these pixels is the right, the 2 to 1 multiplexer will choose the column line  $\langle 1 \rangle$  for column readout circuit  $\langle 0 \rangle$ , column line  $\langle 2 \rangle$  for column readout circuit  $\langle 1 \rangle$ ... When the scan field is the even field(*field\_en* = 0), the output direction changes to the left. The 2 to 1 multiplexer will choose the column line  $\langle 0 \rangle$  to be processed by column readout circuit  $\langle 0 \rangle$ , choose column line  $\langle 1 \rangle$  to be processed by readout circuit  $\langle 1 \rangle$ , and so on.

### 3.4.2 Output Buffer

The output stage of the sensor should satisfy a number of special requirements. One of the most important is to minimize the output impedance so that the output voltage will not be affected by the load impedance. An analog buffer which has a low output resistance, high driving capability can satisfy the requirement. Another requirement for the output stage in this sensor is the wide dynamic range. In this project, a CMOS buffer with a wide dynamic range and a capacitive load driving capability is needed. This buffer is connected to the output of all 96 column readout circuits which can buffer and delivery the reset signal and video signal of column 1 to column 96 in turn. This amplifier will use a differential pair with an active current mirror structure and implement as a unity gain feedback topology. In figure 3.10, the M0 and M2 are identical, M3,M1 are identical too. The input range of output buffer should tolerate the reset signal and the minimum video signal. The minimum input voltage for this buffer is equal to  $V_{DS4} + V_{GS3,min}$ , and the maximum allowable input voltage will put input transistor M3 at the edge of the triode region which is

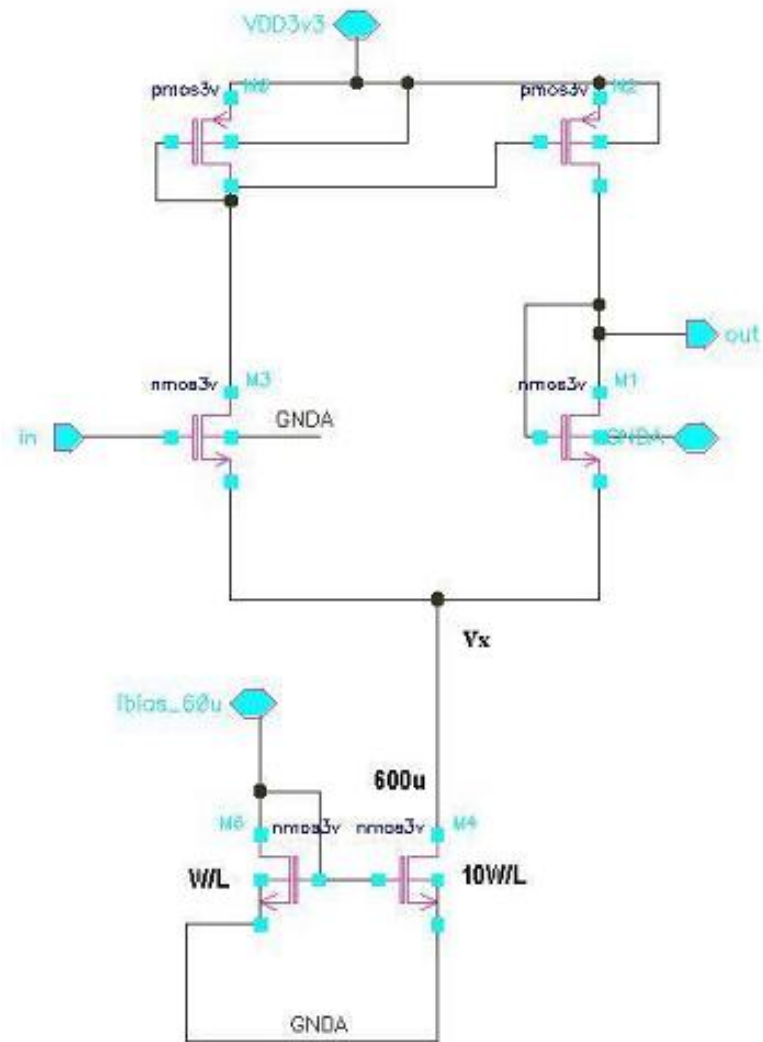


Figure 3.10: Schematic of output buffer



$$\begin{aligned}
V_{in} - V_{th} &= V_{G3} = V_{DD3v3} - |V_{GS3}| \\
V_{in,max} &= V_{DD3v3} - |V_{GS3}| + V_{th}
\end{aligned}
\tag{3.1}$$

Suppose  $V_{th}$  is about 0.7V in this technology, and the overdriver  $V_{GS} - V_{th} = 0.3V$ . Then  $V_{in,max} = 3.3 - 1 + 0.7 = 3V$ , and  $V_{in,min} = 0.3 + 0.3 + 0.7 = 1.3V$ . From the simulation of the analog chain, we can know the reset voltage is around 2.7V. And the maximum pixel voltage swing was estimated to be 1V. Then the minimum video signal we get is about  $2.7 - 1 = 1.7V$ , which is higher than the minimum voltage of the buffer. So this buffer design is enough for this application.

Another concern about the buffer is the settling time. From transient simulation we can see the step response of the amplifier in figure 3.11. And if we define the error less than -50dB (0.3% accuracy), then the settling time is 81.3ns. In this project, the pixel clock for one column readout is 416kHz, and sample frequency of off chip ADC is about 800kHz, which is about the two times of the pixel clock. This settling time could satisfy the requirements of this application. From the AC response of the close loop amplifier 3.12, we can see the united gain bandwidth is about 10MHz, which is far beyond the requirement of the output stage.

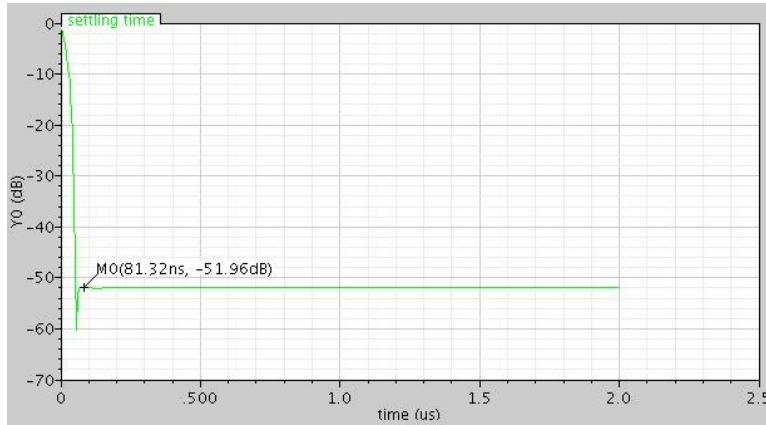


Figure 3.11: Buffer settling time with the accuracy

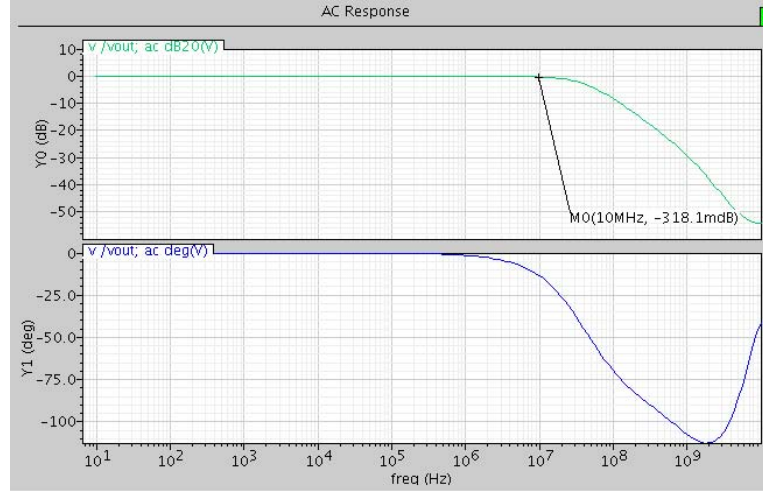


Figure 3.12: Close loop AC response of buffer

## 3.5 Row and Column Driver

In this part, the row and column driver design will be introduced. There are two basic functions for the row driver and column driver. One is the addressing and decoder. The other one is according the decoding signal to produce driving signals for the target row or column. The structure of the column and row driver are shown in figure 3.13. These row and column drivers are basically digital circuits. Normally, they can be easily designed in hardware description language and automatically generated by CAD tools. In the image sensor design, the row and column driver should fit the pixel pitch which is 10um for the column and row driver (some of the row drivers should fit the 20um due to the three photodiode shared amplifier structure). No software tools can do the layout fitting to the pixel pitch. Then the column and row driver should be designed and layout at gate level.

### 3.5.1 Gray Code Addressing

In this project, we use a Gray code as the address signal to addressing the column or row. The Gray Code is unweighed and is not an arithmetic

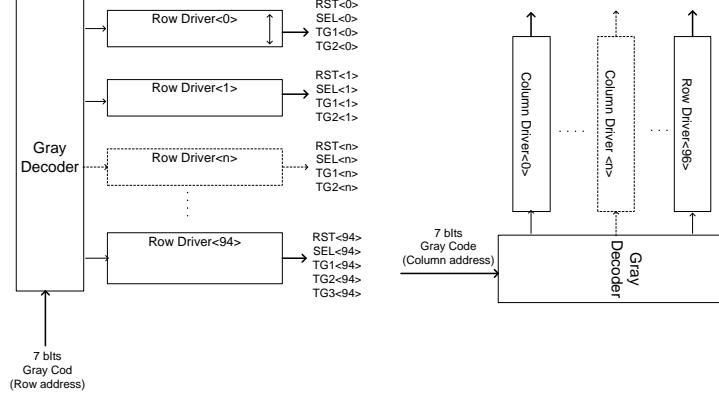


Figure 3.13: Structure of Column and Row Driver

code which means there are no specific weights assigned to the bit positions. It is a cyclic binary code, and specifically designed for position information [31]. A gray code sequence is a set of numbers represented as combination of digits “1” and “0” in which contiguous numbers have only one bit difference. Inspired by this characteristic of the Gray code, we use a switchable two way bus to deal with the addressing problem. The metal 3 was used to transmit the invert state of the address code, and metal 2 was used to transmit the address code. And the bit state will invert by exchanging the metal 2 and metal 3 with each other. Figure 3.14 depicted a 5 bits Gray code bus example. From this example we can see the lowest bit  $D\langle 0 \rangle$  of the Gray code convert its state in every two column/rows, and the  $D\langle 1 \rangle$  converts state in every four columns/rows. With increasing bit position, the conversion frequency is decreased by a factor of two. In reality, the column and row bus are 7 bits and for every column driver, a 7 bits address signal is connected to a 7-input NAND. For example, if we want addressing the row No. 10, the gray code address is 0001111. After the transition in the bus line, the address will becoming 1111111 at the corresponding column driver. The

NAND in the addressed row driver will output a falling edge as the decode signal. The other NAND for non-addressed columns drivers will still be “1”. When the load row address is 111111, then without any transition in this switchable address bus, the row 128 was addressed. The decoder part

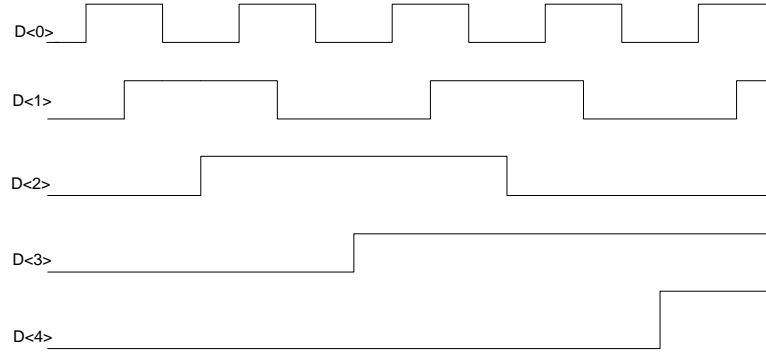


Figure 3.14: 5 bits gray code bus

in both row and column driver are the same Gray code addressing bus with 7-input NAND corresponding to every column/row. But for row addressing, the row address signal is produced by FPGA on the PCB, then the driving sequence for the row is flexible. For column addressing, the column address is produced by a Gray code counter in the sensor. This gray counter can be reset by the input control signal. If the reset signal is not active, the counter will keep counting to produce the column address in turn.

### 3.5.2 Row and Column Driver Array

A row driver is necessary for every pixel row. For a 4T pixel, signal like “ $RST\langle n \rangle$ ”, “ $TGs\langle n \rangle$ ” and “ $SEL\langle n \rangle$ ” are generated by row driver  $\langle n \rangle$  according to the decode signal. The figure 3.15 above is the schematic of the row driver. When address present in 7-input NAND is 111111, then this row is addressed. The following table 3.4 describes the input signal behav-

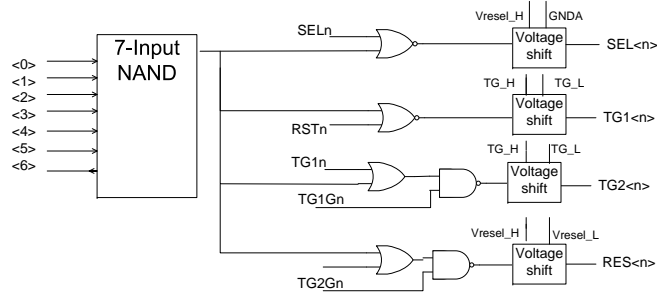


Figure 3.15: Schematic of Row Driver

Signal	Type	Sensitivity	Description
SELn	input	active low	The row select pulse, which can produce a row select signal for the selected 4T pixel row, the signal comes from the programmable pulse generator.
RSTn	input	active low	The reset pulse, which can produce RST signal for the selected 4T pixel row, this signal comes from the programmable pulse generator.
TG1n	input	active low	The transfer gate pulse which will produce TG1 signal for the selected pixel row.
TG2n	input	active low	This is the transfer gate pulse which will produce TG2 signal for the selected pixel row.
TG1Gn	input	active low	This is the global signal for the transfer gate pulse produced by programmable pulse generator. When this signal is active, then TG1 of all rows will be open.
TG2Gn	input	active low	This is the global signal for the transfer gate pulse produced by programmable pulse generator. When this signal is active, then TG2 of all rows will be open.
Vresel_H	input	n.a	High voltage for pixel reset (RST) and row select (SEL) signal.
Vresel_L	input	n.a	Low voltage for reset signal (RST)
TG_H	input	n.a	High voltage for transfer gate (TG1/TG2)
TG_L	input	n.a	Low voltage for transfer gate (TG1/TG2)

Table 3.4: Row driver input signals

Signal	Type	Sensitivity	Description
ReadRn_i	input	active low	A programmable readout pulse that is going to generate a reset signal readout signal for selected column readout
ReadSn_i	input	active low	A programmable readout pulse that is going to generate a video signal readout for selected column readout
En_out_i	input	active high	A programmable readout pulse that is going to generate enable readout for selected column readout
resetn_i	input	active low	A programable readout pulse that is going to generate col_rst (table 3.3) for selected column readout

Table 3.5: Column Driver input signals

ior of the row driver, and the output signals of the row driver were already introduced in table 3.1.

These input signal are digital pulses which has the 1.8V as the high level, 0V for the low level. In order to driving transistors in the analog circuit, a voltage shift from 1.8V to power supply for every output driving signal is needed. The power supply for every driving signal is independent and can be adjusted around 3.3V.

The Column Driver has a similar structure as the row driver, and all the column driver output signals (ReadS, ReadR, out\_en, and col\_rst ) have been introduced in table 3.3. Table 3.5 introduce the input signals of the column driver. These signals are digital pulses (*high* = 1.8V) which are generated from programmable pulse generator.

### 3.6 Programmable Pulse Generator

The programmable pulse generator is a purely digital circuit which buffers the series input data and uses different clock domain transfer from the series input signals to the parallel control signals. These control signals contain the row addressing signals, the pixel control signals, the column bus readout

control signals and so on.

First, DATA\_CLK is 24 times of the frequency of the pixel clock(CLK). Then DATA\_CLK can shift 11 bits valid DATA\_IN in the last 11 DATA\_CLK pulses of one pixel CLK cycle. In one pixel CLK can write one 7 bit register. These are eight different 7 bit registers to generate the different control signals. In this 11 bits data, the first 4 bits are the address for addressing the target register. The next 7 bits represent the data we want to write into the register. The timing diagrams of the DATA\_IN, CLK, and DATA\_CLK are shown in the figure 3.16. DATA\_IN is the only control signal input pad for the sensor. DATA\_CLK is the data clock to write into the register. CLK is the main clock for the pixel readout. At the rising edge of the DATA\_CLK, the DATA\_IN were shifted into the register, because of the limited depth of the input register, only during the last 11 cycles, DATA\_IN will be written into the register. In this example, a bitstream “01111000000” was shifted into sensor. Then we can know the first 4 bits are referring to the address “1110”, then  $\text{reg11}\langle 6 : 0 \rangle$  was write into “0000001”. The detailed allocation of the register will be explained in table 3.6.

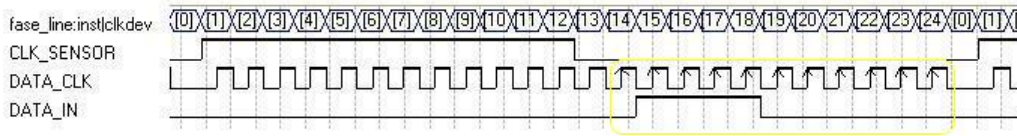


Figure 3.16: Timing Diagram of Sensor Input

The programmable value of Reg1 was related to the timing of setting the ReadR signal. The programmable value of Reg4 was related to the timing of resetting the ReadR signal. And the programmable value of Reg7 was related to the timing of resetting the ReadS signal. Reg 11 was related to set the ReadS signal. Out\_en and col\_rst are also related to these timing sequence.

For 7 bit register 11 – 13, nearly every bit in these registers are connected with the corresponding control signal. In this way, through program different value to register 11 – 13, we can change states of these control signal to produce the right timing for sensor work. The table 3.7 listed detail information about these registers.

Register	Address	content
Reg1	0001	SR_reset
Reg4	0110	SR_set
Reg7	0100	SS_reset
Reg10	1111	SS_set
Reg11	1110	pulse register
Reg12	1010	pulse register
Reg13	1011	pulse register
Reg14	1001	row address

Table 3.6: Register Allocation

Register	Connected signal	Description
Reg11⟨0⟩	resetoff	If <i>resetoff</i> = 1, then col_rst signal for the column readout reset is not active anymore.
Reg11⟨5⟩	NSEL	If <i>NSEL</i> = 1, then current source switch on
Reg11⟨6⟩	SSH <sub>n</sub>	If <i>SSH<sub>n</sub></i> = 0, then column address gray code counter is reset to 0
Reg12⟨0⟩	SELLALL <sub>n</sub>	If <i>SELLALL<sub>n</sub></i> = 0, all rows are addressed together
Reg12⟨1⟩	SHR	
Reg12⟨2⟩	SHS	
Reg12⟨3⟩	odd_sel	If <i>field_en</i> = 1, then means odd field scan, otherwise means the even field scan
Reg12⟨6 : 4⟩	TG3G <sub>n</sub> TG2G <sub>n</sub> , and TG1G <sub>n</sub>	
Reg13⟨4 : 2⟩	TG1 <sub>n</sub> , TG2 <sub>n</sub> , and TG3 <sub>n</sub>	
Reg13⟨5⟩	ROW <sub>n</sub>	
Reg13⟨6⟩	RES <sub>n</sub>	

Table 3.7: Pulse Generation Registers



### 3.7 Sensor Overview

Figure 3.17 is the final layout of the image sensor. And the table 3.8 conclude some basic specifications of the sensor.

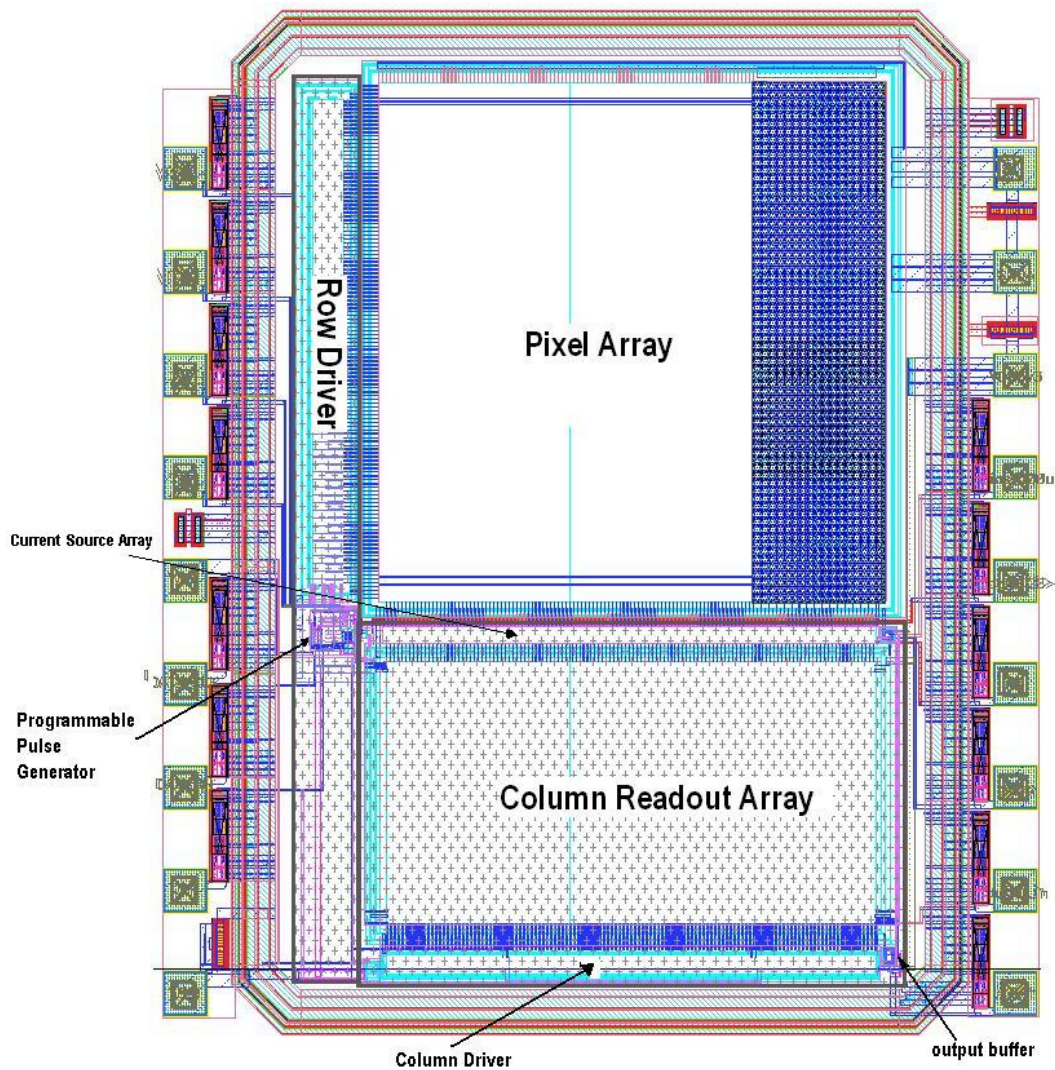


Figure 3.17: Layout of the Whole Image Sensor

Technology	TSMC 0.18um CMOS Image Sensor Mixed Signal Technology
Die size	$2.3mm \times 2.7mm$
Supply voltage	1.8V/3.3V
Pixel type	4T APS
Pixel Pitch	10um
Pixel Array	$96 \times 128$
Clock Frequency	416 kHz

Table 3.8: Sensor Overview

### 3.8 Conclusion

In this chapter, the architecture and working principle of an universal image sensor test chip with a charge domain interlacing pixel design are introduced and implemented in silicon. From section 3.2 to section 3.6, the individual blocks of the sensor both of the analog part(pixel array, current source, column readout circuit, and output buffer) and of the digital part (row and column driver arrays, programmable pulse generator) are presented respectively.

In the next chapter, the basic measurement result of the testchip and PCB level setup will be given. The basic function ability of the test chip is proved by test result.



## Chapter 4

# Initial Measurement Results

This chapter focus on the measurements of the designed sensor. The measurement set-up will firstly be described, then the most important part, the initial measurement results, will be presented, as well as the analysis and discussion of the results.

### 4.1 Measurement Setup

The setup of the measurement can be found in Fig 4.1, where the under-test image sensor is placed on the designed printed circuit board(PCB). The PCB is connected to the computer to process the digital image signal. On the oscilloscope we can also see the waveform of the sensor analog output. It can directly help us to know whether sensor is working normally. To better understand the measurement setup, the IO pins of designed chip are described in table 4.1.

The measurement PCB is mainly composed by under-test sensor, FPGA, ADC, frame grabber, quartz crystal, and power supply system. The FPGA is the central control part of the PCB. First of all, it generates the suitable pixel clock, data clock, and data-in for the image sensor. Changing the driving sequence and working mode of the sensor will be very flexible by changing the programmable input data sequence. Secondly, the FPGA supplies the

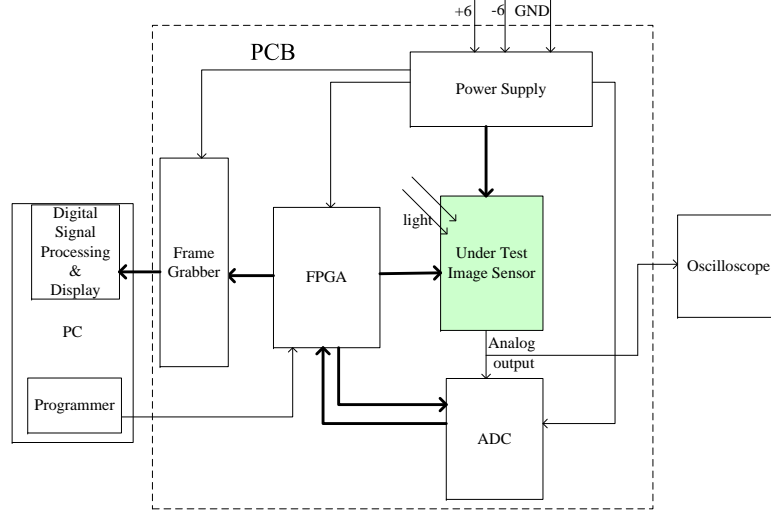


Figure 4.1: Measurement setup for the sensor

Pin name	Type	Description
DATA_CLK	Input clock	Clock for writing series data into register(10MHz)
DATA_IN	Digital input	Programmable data input of sensor
CLK	Input clock	pixel clock, in one clock period, one pixel was readout(416.6kHz)
Aout	analog output	the analog output include the reset and video signal
VDD3V3	power supply	main power for analog circuit(3.3V)
GNDA	ground	analog ground
VDDI	power supply	adjusted pixel array voltage(3.3V)
TG_L	power supply	adjusted low voltage for transfer gate (0V)
TG_H	power supply	adjusted high voltage for transfer gate(3.3V)
Vresel_H	power supply	adjusted high voltage of $V_g$ (3.3V) for pixel reset and row select transistor
Vresel_L	power supply	adjusted low voltage of $V_g$ for pixel reset transistor(0V)
VSS	ground	digital ground
VDD	power supply	main power for digital circuit (1.8V)
Test pads	test output	reserving 5 test pads for important biasing signals, middle stage output signal and so on

Table 4.1: IO pins of the designed image sensor

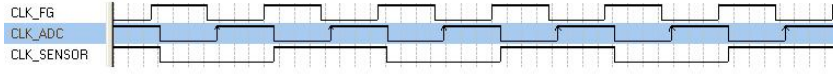


Figure 4.2: ADC supply clock

sample clock, digital input data for off-chip ADC, which can control the working status of ADC, to make the ADC sample the output analog signal of sensor and convert them to 12 bits digital number. Finally, the FPGA is also connected with the frame grabber to provide the clock and other control signals for the grabber.

In this measurement setup, we choose an 12 bit, 40MHz A/D converter to process the analog output of the sensor. To suit the common mode input voltage range and 1V p-p input range of the ADC, a resistant divider is used to adjust the sensor output signal to the half of the original signal. Luckily, there is a variable gain amplifier in the ADC, which can compensate for the lost of the signal input range and achieve 2-V full scale range. Of course, in this transition, the noise performance will also be affected.

In the figure 4.2, the timing relationship between the sensor pixel clock, and ADC sample clock is shown. In one sensor clock period, there are two ADC sample periods, which sample the reference reset level and the video signal level respectively. The allows for Correlated-Double Sampling afterwards. Clk\_FG is the clock of the frame grabber which has some delay with CLK\_ADC

## 4.2 Measurement Result

### 4.2.1 Sensor Analog Output

The sensor can output an analog signal and it clearly show light response. The integration time is 17.4ms.



Figure 4.3: Two photodiodes shared amplifier structure readout with strong light intensity( $TG1 = high$ ;  $TG2 = high$ )

1. Basic light response: to measure the image sensor, the basic thing is to test the light response of the sensor. The pixels in the fifth row are readout as example. Figure 4.3 and figure 4.4 are “two photodiodes shared-amplifier structure” output under strong light condition and low light condition in respectively. The two transfer gates  $TG1\langle 5 \rangle$ , and  $TG2\langle 5 \rangle$  which are connected to the two photodiode are opened together. Because we did not complete CDS technology fully on chip, here we can see the both the reset level and the video signal level. Cursor1 indicates the pixel reset level, and cursor2 indicates the pixel signal level.

From the figure 4.3 we can see  $V_{rst} = 2.78V$ ,  $V_{sig} = 1.16V$ . After subtraction, the real signal across these two photodiodes is  $V_{rst} - V_{sig} = 1.62V$  (nearly saturated). In figure 4.4 we can see  $V_{rst} = 2.78V$ ,  $V_{sig} = 2.64V$ . The real signal in this low light situation is  $V_{rst} - V_{sig} = 0.14V$ . From the figure above we can clearly see the light response.

2. Charge binning response for two photodiodes shared-amplifier struc-



Figure 4.4: Two photodiodes shared amplifier structure readout with low light intensity( $TG1 = high; TG2 = high$ )

ture: in chapter 2, the charge binning technology is introduced, and based on this technology, this thesis proposed two pixel structures to enlarge the signal level. Figure 3.3 in chapter 3 shows the two pixel structures we proposed. Here we will compared the pixel response of the normal one  $pixel_{Row5}$  readout with the charge binning of two photodiodes in one "two photodiode shared-amplifier structure" in figure 4.5. In the interlace scan, if TG1 and TG2 open together, then electrons accumulated in photodiode 1 and photodiode 2 will be transferred into one floating diffusion and then be readout. Here, the readout signal under a certain light level is  $V_{rst} - V_{sig} = 2.80 - 2.44 = 0.36V$ . If with the same light level, just TG1 is open, TG2 is closed, then only the electrons accumulated in photodiode1 will be readout. The readout signal is  $V_{rst} - V_{sig} = 2.80 - 2.64 = 0.16V$ . Compared these two results we can see charge binning can clearly increase the signal level. In this situation, the difference of these two is 0.2V.

### 3. Charge binning response for three photodiodes shared amplify struc-



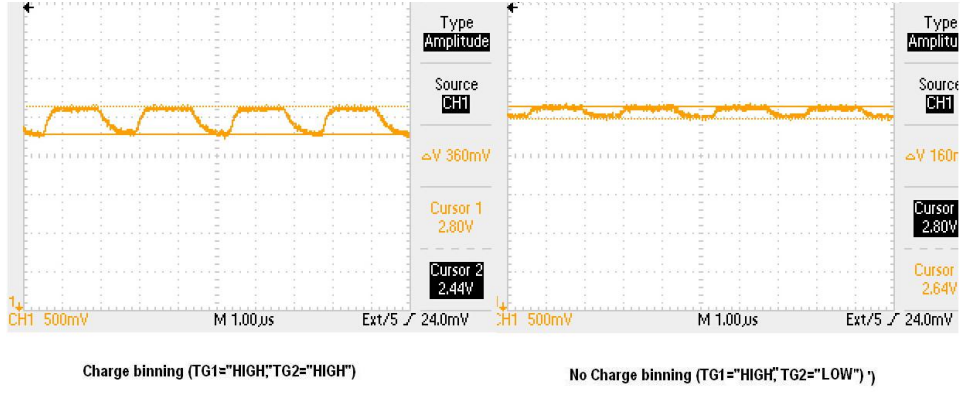


Figure 4.5: Charge binning comparison for two photodiodes shared-amplifier structure readout under the same light intensity

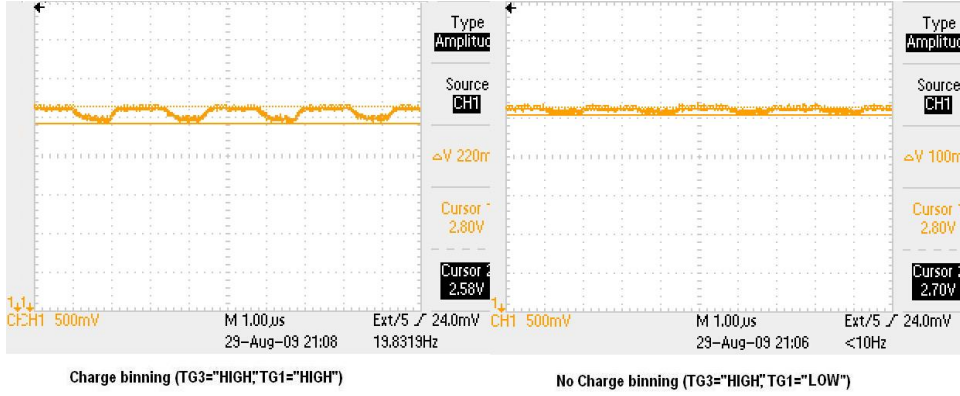


Figure 4.6: Charge binning comparison for three photodiodes shared-amplifier structure readout under same light intensity.

ture: the measurement result (Pixel in Row 66) for the other pixel design “three photodiodes shared amplify structure” shown in the figure 4.6. It also shows two waveforms. One is for the charge binning condition when both of TG3 and TG1 (figure3.3) open together, the signal be readout is  $V_{rst} - V_{sig} = 2.80 - 2.58 = 0.22V$ . The other one is with only TG3 open to readout electrons in the photodiode 2, the signal we get is  $V_{rst} - V_{sig} = 2.80 - 2.7 = 1.0.1V$ . The difference of TG1 open or not is 0.12V which is similar with the last measurement for “two photodiodes shared-amplifier structure”.

It should be clear that the light conditions for these two pixel structure measurements is different. So it can not compared these two pixel structures from data above.

### **4.2.2 image result**

In this subsection, the image result we get will be shown here. The figure 4.7 is image we get from the progressive scan. Because of the rotation of the figure, the top part is the three photodiodes shared amplifier structure. The bottom part of the image uses the two photodiodes shared amplifier structure.

The figure 4.8 is the mickeymouse image get from the interlace scan in the field integration mode. The top one is the even field scan, and the bottom one is the odd field scan.

Compared these two figures, we can see the signal level in the background of figure 4.8 is clearly has more light than figure 4.7. But in reality, these image are get from the same illumination condition. This reveals that the charge domain interlacing principle can enhance the signal level in certain degree.

## **4.3 Conclusion**

With the very first measurement results of the designed sensor, it has been shown that sensor is working and the proposed pixel structures can truly enhance the signal level to a certain degree. The detailed performance measurement and analysis will be done in the future.



Figure 4.7: Image result of progressive scan



Figure 4.8: Image result of interlace scan



## Chapter 5

# Conclusion and Future Work

### 5.1 Conclusion

CMOS image sensors suffer from several noise sources which will affect the image performance especially under low illumination. To improve the overall quality of the image, a high S/N ratio and wide dynamic range are desired. To improve the S/N ratio, a lot of work has been done to reduce many kinds of noise sources. It can be done by using correlated double sampling technology to cancel the reset noise and the transistor offset and so on. Reducing the noise also can be done by improve the technology and the device to reduce the noise sources at their origins. But improving the S/N ratio can also be achieved by enhancing the signal level under the same light condition.

Inspired by the field integration mode of the interlaced scan, we can add the signal of neighboring rows signal together and using the interlace mode to achieve a the high signal level under the same light conditions. To realize this mechanism, the easiest way is to add the pixel readout signal in voltage domain or even in the digital domain. But for an image sensor a lot of noise sources are coming from the readout course of the pixel. If the readout signal is added in the voltage domain, this will increase the noise level of the output stage which can not achieve the purpose of improving

the S/N ratio. To deal with this problem, this thesis proposes two different pixel structures based on 4T APS structure and both of them can combine the collected charges of two pixels and then readout them together.

The first pixel structure uses one pixel readout structure connected to two photodiodes, by using one floating diffusion to combine the photon-generated electrons from two pixels together and then readout this combined signal. From the photodiode standpoint, each photodiode is connected with two readout structures and two transfer gates which are active in the even field scan and odd field scan respectively. The other pixel design uses one pixel readout structure connected to three photodiodes. Both of these structures can realize the charge domain interlacing principle to enhance the signal level from the front end of the sensor.

To test these pixel designs and the working principle, a programmable universal image sensor driving circuit architecture was proposed, which can driving and readout the pixel array flexible and easily change it through different programming. This sensor can not only support progressive scan, frame integration interlace scan mode, voltage domain field integration interlace scan mode, but also can realize the charge domain interlacing principle with some special pixel designs.

The designed image sensor is implemented in TSMC 0.18 $\mu$ m process, and the first measurement result were given. Further testing results are expected after September 2009.

## 5.2 Future Work

Due to the limited time, only preliminary measurement results are included in this thesis, more measurements will be performed later in order to give further details about the performance analysis especially with respect to the noise aspects. On the other hands, better understanding the principle is important as well. More measurement need to be done to compared

the different pixel designs with respect their noise performance and other aspects. It is interesting to use the different scan modes and their analysis to look for similarities and differences between the measurement results and theoretical model.





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