Prescribed-performance tracking for high-power nonlinear dynamics with time-varying unknown control coefficients

Lv, Maolong; Chen, Zhiyong; De Schutter, Bart; Baldi, Simone

Important note
To cite this publication, please use the final published version (if applicable).
Please check the document version above.

Contents lists available at ScienceDirect

Automatica

journal homepage: www.elsevier.com/locate/automatica

Brief paper

Prescribed-performance tracking for high-power nonlinear dynamics with time-varying unknown control coefficients☆

Maolong Lv [a,b,1], Zhiyong Chen [e], Bart De Schutter [c], Simone Baldi [d,*]

[a] *Air Traffic Control and Navigation College, Air Force Engineering University, Xi'an 710051, China*
[b] *College of Aeronautics Engineering, Air Force Engineering University, Xi'an 710038, China*
[c] *Delft Center for Systems and Control, Delft University of Technology, Delft 2628CD, The Netherlands*
[d] *School of Mathematics, Southeast University, Nanjing 210096, China*
[e] *School of Electrical Engineering and Computing, The University of Newcastle, Callaghan NSW2308, Australia*

ABSTRACT

Prescribed-performance control (PPC) for high-power dynamics with time-varying unknown control coefficients requires to address two open problems: (a) given a Nussbaum function, which properties hold for the power of the Nussbaum function? (b) to avoid high gains, how to design a switching gain that increases only when the tracking error is close to violate the performance bounds? To address the first problem, we show with a counterexample and a positive example that only some Nussbaum functions are suited to handle time-varying unknown control coefficients for high-power dynamics. To address the second problem, we propose a new switching conditional inequality.

1. Introduction

Over the last decade, high-power nonlinear systems have been attracting great attention because: first, they generalize strict-feedback and pure-feedback systems by including more general odd-integer powers (Lin & Pongvuthithum, 2003; Lin & Qian, 2000; Qian & Lin, 2002) in the dynamics; second, they have been used to describe classes of practical systems such as boiler-turbine units (Chen & Chen, 2020), hydraulic dynamics (Manring & Fales, 2019), aircraft wing dynamics (Fung, 1955), or mechanical systems with cubic force–deformation relations (Lin & Pongvuthithum, 2003; Lin & Qian, 2000; Qian & Lin, 2002). The main technique for control of high-power nonlinear systems is the so-called adding-one-power-integrator technique, successfully used in stabilization (Lin & Qian, 2000; Sun & Liu, 2007) and

tracking problems (Lin & Pongvuthithum, 2003; Qian & Lin, 2002). However, handling unknown signs of constant or time-varying control coefficients (Chen & Huang, 2015; Ding, 2015; Ding & Ye, 2002; Ge, Fan, & Lee, 2004; Huang, Wang, Wen, & Zhou, 2018; Li & Liu, 2018; Liu & Huang, 2008; Liu & Tong, 2017; Ye, 2011), and guaranteeing transient and steady-state specifications (Li & Liu, 2019; Liu, Sun and Li, 0000; Liu, Sun and Zhou, 0000) still pose open problems for high-power nonlinear systems, as explained hereafter.

The term "sign of the control coefficient" (also called "control direction" in some literature) refers to the sign of the control gain function. A control law in the presence of this uncertainty may apply its control action with incorrect sign and destabilize the system (Chen, 2019; Krstic, Kanellakopoulos, & Kokotovic, 1995). These signs have been assumed to be known until Nussbaum (Nussbaum, 1983) proved stability with unknown signs using a special function (later called Nussbaum function) alternating its effects in both directions of the sign. Although alternative methods exist to tackle unknown control coefficients, such as logic-based switching (Huang & Yu, 2018), nonlinear proportional–integral control (Psillakis, 2017), and extremum seeking (Scheinker & Krstic, 2013), the Nussbaum function method is probably the most studied one. A fundamental tool to prove stability with the Nussbaum function is the so-called conditional inequality, which consists in guaranteeing the boundedness of a Lyapunov-like function when its derivative along the system trajectories is upper bounded by an appropriate expression depending on the Nussbaum function. As the

control coefficients can be constant or time-varying, three representative conditional inequalities have been proposed so far (Chen, 2019; Ge & Wang, 2003; Ye & Jiang, 1998) to handle these cases. The first conditional inequality was formulated in Ye and Jiang (1998) to handle unknown signs of constant control coefficients. The second conditional inequality in Ge and Wang (2003) (see also discussions in Psillakis (2010)) is given in integral form to handle unknown signs of time-varying control coefficients. Recently, Chen (2019) distinguished between type A and type B Nussbaum functions, where the former can handle constant control coefficients, but only the latter can handle time-varying control coefficients. Unfortunately, the capability to handle time-varying control coefficients was shown in Chen (2019) only for strict-feedback and pure-feedback systems. At the same time, combining the adding-one-power-integrator and Nussbaum methods (Li & Liu, 2019) requires to take the derivative of the virtual control laws, which gives rise to negative fractional terms not well defined when the error crosses zero. Therefore, handling high-power nonlinear systems via the Nussbaum method is an open question.

With respect to guaranteeing transient and steady-state specifications (e.g. convergence rate or steady-state error), the prescribed-performance control (PPC) technique first (Bechlioulis & Rovithakis, 2008) and low-complexity PPC later (Bechlioulis & Rovithakis, 2014) have been successfully applied to strict-feedback (Theodorakopoulos & Rovithakis, 2015; Zhang & Yang, 2017) and pure-feedback systems (Bechlioulis & Rovithakis, 2014) with known signs of the control coefficients. To handle unknown signs, a low-complexity control scheme was recently developed in Zhang and Yang (2019) for strict-feedback dynamics. Although the combination of the Nussbaum method and PPC appears promising, one major challenge is to avoid high-gain issues, due to the presence of high powers. With these problems in mind, realizing Nussbaum PPC for high-power nonlinear dynamics with unknown signs of time-varying control coefficients requires to answer two questions: *(i) is the positive odd-integer power of a type B Nussbaum function still a type B Nussbaum function? (ii) is it possible to design a different conditional inequality that may allow the Nussbaum gain to stop increasing over some time intervals?*

This paper answers these open questions as follows:

• A counterexample and a positive example are given to show that the positive odd-integer-power of a type B Nussbaum function may not be a type B Nussbaum function. Only some particular type B Nussbaum functions keep their property even when elevated to a positive odd-integer power. These latter functions can be used for handling time-varying unknown control coefficients in high-power systems.

• A new switching conditional inequality is proposed. Instead of always increasing the Nussbaum gain, its design is based on increasing the Nussbaum gain only when the tracking error is close to violate the performance bounds.

2. Problem formulation

This paper considers the high-power nonlinear systems:

$$
\begin{cases}
\dot{\chi}_i(t) = \phi_i(t, \overline{\chi}_i) + \ell_i(t, \overline{\chi}_i)\chi_{i+1}^{r_i}(t), \ i = 1, \ldots, n-1, \\
\dot{\chi}_n(t) = \phi_n(t, \overline{\chi}_n) + \ell_n(t, \overline{\chi}_n)u^{r_n}(t), \\
y(t) = \chi_1(t),
\end{cases}
\tag{1}
$$

where $\overline{\chi}_i = [\chi_1, \ldots, \chi_i]^T \in \mathbb{R}^i$, r_i, $i = 1, \ldots, n$, are known positive-odd integers, and $u \in \mathbb{R}$ is the control input. The unknown continuous nonlinear functions $\phi_i(\cdot, \cdot) : \mathbb{R}^+ \times \mathbb{R}^i \to \mathbb{R}$ (referred to as drift coefficients) and $\ell_i(\cdot, \cdot) : \mathbb{R}^+ \times \mathbb{R}^i \to \mathbb{R}$, $i = 1, \ldots, n$, (referred to as control coefficients) satisfy the following assumption.

Assumption 1 (*Zhang & Yang, 2017*)**.** There exist unknown, continuous, and positive functions $\overline{\phi}_i(\cdot) : \mathbb{R}^i \to \mathbb{R}^+$, $\underline{\ell}_i(\cdot)$, and $\overline{\ell}_i(\cdot) : \mathbb{R}^i \to \mathbb{R}^+$, $i = 1, \ldots, n$, such that for all t

$$
|\phi_i(t, \overline{\chi}_i)| \le \overline{\phi}_i(\overline{\chi}_i), \quad \underline{\ell}_i(\overline{\chi}_i) \le |\ell_i(t, \overline{\chi}_i)| \le \overline{\ell}_i(\overline{\chi}_i).
\tag{2}
$$

In line with standard Nussbaum literature (Chen, Li, Ren, & Wen, 2014; Fan, Yang, Jagannathan, & Sun, 2019; Lv, Yu, Cao, & Baldi, 2020), Assumption 1 allows the control coefficients $\ell_i(\cdot, \cdot)$ to be unknown but fixed, guaranteeing controllability of dynamics (1). Nussbaum-based definitions follow.

Definition 1 (*Chen, 2019, Definition 3.1, Nussbaum, 1983*)**.** A continuous function $\mathscr{N}(\cdot) : [0, +\infty) \to (-\infty, +\infty)$ is called a type A Nussbaum function if it satisfies

$$
\lim_{y \to +\infty} \sup \frac{\int_0^y \mathscr{N}(s)ds}{y} = +\infty, \quad \lim_{y \to +\infty} \inf \frac{\int_0^y \mathscr{N}(s)ds}{y} = -\infty.
$$

Definition 2 (*Chen, 2019, Definition 4.3*)**.** A continuous function $\mathscr{N}(\cdot) : [0, +\infty) \to (-\infty, +\infty)$ is called a type B Nussbaum function if it satisfies

$$
\lim_{y \to +\infty} \frac{\int_0^y \mathscr{N}_+(s)ds}{y} = +\infty, \quad \lim_{y \to +\infty} \sup \frac{\int_0^y \mathscr{N}_-(s)ds}{\int_0^y \mathscr{N}_+(s)ds} = +\infty,
$$

$$
\lim_{y \to +\infty} \frac{\int_0^y \mathscr{N}_-(s)ds}{y} = +\infty, \quad \lim_{y \to +\infty} \sup \frac{\int_0^y \mathscr{N}_+(s)ds}{\int_0^y \mathscr{N}_-(s)ds} = +\infty,
$$

where $\mathscr{N}_+(s) = \max\{0, \mathscr{N}(s)\}$ and $\mathscr{N}_-(s) = \max\{0, -\mathscr{N}(s)\}$ are the positive and negative truncated functions of $\mathscr{N}(s)$.

Remark 1. Note that type B Nussbaum functions are a special class of type A Nussbaum functions (Chen, 2019). It was shown in Chen (2019) that type A Nussbaum functions can handle unknown signs of constant control coefficients, but may fail to handle unknown signs of time-varying control coefficients. Accordingly, type B Nussbaum functions were proposed to tackle the time-varying scenarios.

The main problem studied in this paper is stated below.

Prescribed-performance control (PPC) problem: Consider a bounded reference signal $y_r(t)$ with bounded derivative and a performance function $\rho_1(t) = (\rho_{1,0} - \rho_{1,\infty})\exp(-\kappa_1 t) + \rho_{1,\infty}$ for positive constants $\rho_{1,0} > \rho_{1,\infty}$ and κ_1. The PPC problem aims to design a controller for the system (1) such that the closed-loop system satisfies the following two properties:

(P1) The output tracking error $e_1(t) = y(t) - y_r(t)$ evolves in the prescribed set $\Omega = \{e_1(t) \in \mathbb{R} \mid |e_1(t)| < \rho_1(t)\}$ for $t \ge 0$; and

(P2) The closed-loop signals are bounded on the entire time domain $[0, +\infty)$.

The PPC problem has been well formulated in literature, e.g., Bechlioulis and Rovithakis (2008, 2014). However, this problem remains unsolved for the class of dynamics (1) and even the stability analysis recently proposed in Chen (2019) does not apply. Solving this problem requires to address two open issues: given a Nussbaum function, which properties hold for the power of the Nussbaum function? To avoid high gains, how to design a switching gain that increases only when the tracking error is close to violate the performance bounds? These two problems are addressed by the technical results in the next section.

3. Technical results

The high-power terms in (1) require that the positive odd-integer power of a Nussbaum function, denoted by $\mathscr{N}^r(s)$, is still a

Nussbaum function. However, we show that even if $\mathcal{N}(s)$ is a type B Nussbaum function, $\mathcal{N}^r(s)$ may not result in a type B Nussbaum function. A counterexample and a positive example are given in the following two propositions, with proofs in Appendix.

Proposition 1 (*Counterexample*)**.** *Consider the function*

$$\mathcal{N}(s) = \sum_{\lambda \in \mathbb{N}^+} \mathcal{N}_\lambda(s + 2 - 2^\lambda), \tag{3}$$

where $\mathbb{N}^+$ is the set of positive integers and

$$\mathcal{N}_\lambda(s) = \begin{cases} 2^{\left(\lambda^3 + \frac{1}{3}\right)\lambda} \sin(s\pi), & \text{if } s \in [0, 1) \\ -2^{\lambda^4} \sin\left(\dfrac{s-1}{2^\lambda - 1}\pi\right), & \text{if } s \in [1, 2^\lambda) \\ 0, & \text{otherwise.} \end{cases} \tag{4}$$

Then, $\mathcal{N}(\cdot)$ is a type B Nussbaum function, but $\mathcal{N}^r(\cdot)$ with $r \geq 3$ a positive odd integer is not *a type B Nussbaum function.*

Proposition 2 (*Positive Example*)**.** *Consider the function*

$$\mathcal{N}(s) = \exp(\mu s^2) \cos\left(\frac{\pi s}{2}\right), \quad \mu > 0. \tag{5}$$

Then, $\mathcal{N}^r(\cdot)$ is a type B Nussbaum function for any positive odd integer $r \geq 1$.

Remark 2. The above propositions may lead to a new class of Nussbaum functions which are those functions where $\mathcal{N}^r(\cdot)$ satisfies Definition 2 for any positive odd integer r. Function (5) belongs to such class.

The following lemma is instrumental to constructing a Nussbaum gain that increases only when the tracking error is close to violate the performance bounds.

Lemma 1 (*Switching Conditional Inequality*)**.** *Let $\mathcal{N}(\cdot)$ be a type B Nussbaum function. Consider two continuous and piecewise differentiable functions $V(\cdot)$ and $s(\cdot)$ such that*

$$\dot{V}(t) \leq \left[\ell(t)\mathcal{N}(s(t)) + \beta\right]\dot{s}(t), \tag{6}$$

$$\dot{s}(t) \begin{cases} \geq 0, & \text{if } V(t) \geq \phi, \\ = 0, & \text{if } V(t) < \phi, \end{cases} \tag{7}$$

where ϕ and β are positive constants, $V(0) < \phi$, $s(0) = 0$, and $\ell(\cdot)$ is a time-varying unknown function satisfying $\ell(t) \in [l_1, l_2]$, $\forall t$ with either $0 > l_2 > l_1$ or $l_2 > l_1 > 0$. Then, $V(\cdot)$ and $s(\cdot)$ are bounded on the entire time domain $[0, +\infty)$.

Proof. For better comprehension, a sketch of the idea behind (7) is shown in Fig. 1. Let $0 = t_0 < t_1 \leq t_2 \leq t_3 \leq \cdots$ be the time sequence satisfying $V(t_j) = \phi$, $V(t) < \phi$, $\forall t \in (t_{2j-2}, t_{2j-1})$, and $V(t) \geq \phi$, $\forall t \in [t_{2j-1}, t_{2j}]$, for $j = 1, 2, \ldots$. According to the time sequence above, we consider the case of $t \in [t_{2m-1}, t_{2m}]$ for $m \in \mathbb{N}^+$. Integrating $\dot{V}(\cdot)$ over the time intervals $[t_0, t_1)$, $[t_1, t_2)$, $\ldots$, $[t_{2m-2}, t_{2m-1})$, $[t_{2m-1}, t]$ results in

$$V(t) \leq \sum_{j=1}^{m-1} \int_{t_{2j-1}}^{t_{2j}} \left[\ell(t)\mathcal{N}(s(t)) + \beta\right]\dot{s}(t)dt + \sum_{i=1}^{m} \int_{t_{2j-2}}^{t_{2j-1}} \dot{V}(t)dt$$

$$+ \phi + \int_{t_{2m-1}}^{t} \left[\ell(t)\mathcal{N}(s(t)) + \beta\right]\dot{s}(t)dt$$

$$\leq \phi + \sum_{j=1}^{m-1} \int_{t_{2j-1}}^{t_{2j}} \left[\ell(t)\mathcal{N}(s(t)) + \beta\right]\dot{s}(t)dt$$

$$+ \int_{t_{2m-1}}^{t} \left[\ell(t)\mathcal{N}(s(t)) + \beta\right]\dot{s}(t)dt,$$

where the integral over $t \in [t_{2j-2}, t_{2j-1})$ has been removed by observing that $V(t_{2j-1}) = V(t_{2j-2}) = \phi$. Then, it follows that

$$V(t) \leq \phi + \sum_{j=1}^{m-1} \int_{t_{2j-1}}^{t_{2j}} \left[\ell(t)\mathcal{N}(s(t)) + \beta\right]\dot{s}(t)dt$$

$$+ \underbrace{\sum_{j=1}^{m-1} \int_{t_{2j-2}}^{t_{2j-1}} \left[\ell(t)\mathcal{N}(s(t)) + \beta\right]\dot{s}(t)dt}_{\Theta(s(t))}$$

$$+ \int_{t_{2m-1}}^{t} \left[\ell(t)\mathcal{N}(s(t)) + \beta\right]\dot{s}(t)dt$$

$$\leq \phi + \int_{0}^{t} \left[\ell(t)\mathcal{N}(s(t)) + \beta\right]\dot{s}(t)dt$$

$$\leq \phi + \beta s(t) + \underbrace{l_2 \int_{0}^{s(t)} \mathcal{N}_+(\tau)d\tau - l_1 \int_{0}^{s(t)} \mathcal{N}_-(\tau)d\tau}_{\Xi(s(t))}, \tag{8}$$

by noting the facts that $\Theta(s(t)) \equiv 0$ due to $\dot{s}(t) = 0$ for $t \in [t_{2j-2}, t_{2j-1}]$, $s(0) = 0$, and $\mathcal{N}(s) = \mathcal{N}_+(s) - \mathcal{N}_-(s)$. When $s(t) = 0$, $\forall t$, the boundedness of $s(t)$ and $V(t)$ can be trivially obtained according to (8).

When $s(t) \neq 0$, it is obtained from (8) that

$$0 \leq \frac{V(t)}{s(t)} \leq \underbrace{\overbrace{\left[\frac{\Xi\left(s(t)\right)}{s(t)}\right]}^{\Delta(s(t))} + \frac{\phi}{s(t)} + \beta}_{\Upsilon(s(t))}. \tag{9}$$

In the following, we prove boundedness of $s(\cdot)$ on $[0, +\infty)$ by contradiction. If $s(\cdot)$ is unbounded, one can calculate the limit behavior of $\Delta(s)$ in (9) as $s \to +\infty$, using Definition 2. In particular, for the case $0 > l_2 > l_1$,

$$\liminf_{s \to +\infty} \Delta(s)$$

$$= \lim_{s \to +\infty} \overbrace{\frac{1}{s}\int_{0}^{s} \mathcal{N}_-(\tau)d\tau}^{\to +\infty} \overbrace{\left[-l_1 + l_2 \underbrace{\sup \frac{\int_{0}^{s} \mathcal{N}_+(\tau)d\tau}{\int_{0}^{s} \mathcal{N}_-(\tau)d\tau}}_{\to -\infty}\right]}^{\to -\infty}$$

$$= -\infty, \tag{10}$$

and similarly, for the case $l_2 > l_1 > 0$,

$$\liminf_{s \to +\infty} \Delta(s)$$

$$= \lim_{s \to +\infty} \overbrace{\frac{1}{s}\int_{0}^{s} \mathcal{N}_+(\tau)d\tau}^{\to +\infty} \overbrace{\left[l_2 - l_1 \underbrace{\sup \frac{\int_{0}^{s} \mathcal{N}_-(\tau)d\tau}{\int_{0}^{s} \mathcal{N}_+(\tau)d\tau}}_{\to -\infty}\right]}^{\to -\infty}$$

$$= -\infty. \tag{11}$$

Note that 'inf' in (10) and (11) becomes 'sup' due to $l_2 < 0$ and $l_1 > 0$, respectively. The relations above indicate that an unbounded s leads to a negative unbounded $\Delta(s)$. Independently of whether the unboundedness of $\Delta(s)$ occurs in finite time or at infinity (this depends on the behavior of $s(\cdot)$), the consequence would be that there exists a time $\bar{t} > 0$ such that

$$\Upsilon\left(s(\bar{t})\right) \leq -\varepsilon$$

for some positive ε, which contradicts (9). It concludes that $s(\cdot)$ is bounded over the entire time domain $[0, +\infty)$, so are $\Xi(s(\cdot))$ and hence $V(\cdot)$ from (8).
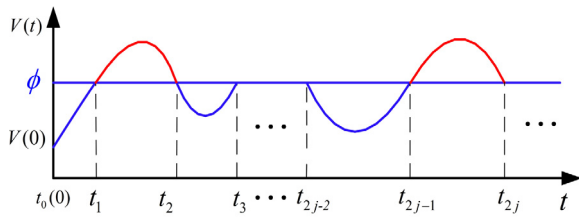
Fig. 1. Illustration of the evolution of $V(\cdot)$.

Finally, let us now consider the case of $t \in (t_{2m}, t_{2m+1})$. The boundedness of $s(\cdot)$ and $V(\cdot)$ is guaranteed by the above argument for $t = t_{2m}$ and the facts that $V(t) < \phi$ and $\dot{s}(t) = 0$ for $t \in (t_{2m}, t_{2m+1})$. ∎

Remark 3. Lemma 1 encompasses (Chen, 2019, Lemma 4.3) as special case when $\dot{s}(t) = 0$ in (7) is never active (e.g. for sufficiently small ϕ). Existing conditional inequalities (Ge & Wang, 2003, Lemma 2), (Ge et al., 2004, Lemma 2), and (Liu & Tong, 2017, Lemma 1) guarantee boundedness on a finite time interval $[0, t_\delta]$, $t_\delta < +\infty$ (cf. discussion in Psillakis (2010, Remark 1)): the proposed Lemma 1 ensures boundedness on the entire time domain $[0, +\infty)$, thanks to the properties of type B Nussbaum functions used in the proof by contradiction (cf. (10)–(11)).

4. Nussbaum gain adaptive PPC design

This section starts with the performance functions $\rho_i(t) = (\rho_{i,0} - \rho_{i,\infty}) \exp(-\kappa_i t) + \rho_{i,\infty}$ for positive constants $\rho_{i,0} > \rho_{i,\infty}$ and κ_i, $i = 1, \ldots, n$. In line with Bechlioulis and Rovithakis (2008, 2014), Theodorakopoulos and Rovithakis (2015) and Zhang and Yang (2017), the initial conditions $e_i(0)$ should satisfy the initial feasibility $|e_i(0)| < \rho_i(0)$, i.e. start inside the prescribed performance. Let $\alpha_1(t) = y_r(t)$, $\alpha_{i+1}(t)$, $i = 1, \ldots, n$, be the virtual control laws to be designed, and $u(t) = \alpha_{n+1}(t)$ be the real control law.

Next, we introduce the virtual tracking error $e_i(t) = \chi_i(t) - \alpha_i(t)$ and the error transformation

$$\mathcal{T}_i(t) = \frac{\tan\left(\frac{\pi}{2} \frac{e_i(t)}{\rho_i(t)}\right)}{\cos^2\left(\frac{\pi}{2} \frac{e_i(t)}{\rho_i(t)}\right)}, \quad i = 1, \ldots, n. \tag{12}$$

The virtual control functions are devised as follows,

$$\alpha_{i+1}(t) = \varrho_i \mathcal{N}\left(s_i(t)\right) \mathcal{T}_i(t), \quad i = 1, \ldots, n, \tag{13}$$

where $\varrho_i > 0$ is a design parameter and $\mathcal{N}^r(\cdot)$ is a type B Nussbaum function for any positive odd integer $r \geq 1$. An adaptation law for $s_i(t)$ is constructed as

$$\dot{s}_i(t) = \begin{cases} \mathcal{T}_i^{r_i+1}(t), & \text{if } |e_i(t)| \geq \delta_i \rho_i(t) \\ 0, & \text{if } |e_i(t)| < \delta_i \rho_i(t) \end{cases} \tag{14}$$

for a constant $\delta_i \in (0, 1)$. Similar to Zhang and Yang (2017, Eq. (8)), Eq. (14) increases only when the error is close to violate the performance bound: however, the stability analysis in Zhang and Yang (2017) is for strict-feedback dynamics and cannot be used here. The way we prove stability relies on the proposed Lemma 1. Before the main result, we use a lemma similar to Zhang and Yang (2017, Lemma 3), thus the proof is omitted.

Lemma 2. If $\overline{\chi}_i(\cdot)$, $\dot{\alpha}_i(\cdot)$, $s_i(\cdot)$, $\mathcal{T}_i(\cdot)$, and $e_{i+1}(\cdot)$ are bounded on a time interval $[0, t_\delta]$ with t_δ a strictly positive time instant, then $\dot{\alpha}_{i+1}(\cdot)$ is bounded on $[0, t_\delta)$ for $i = 1, \ldots, n$.

Theorem 1. Under Assumption 1 and with $\mathcal{N}^r(\cdot)$ being a type B Nussbaum function for any positive odd integer $r \geq 1$, consider the closed-loop system composed of (1), the control laws (12)–(13), and the adaptation law (14). In particular, $\mathcal{N}^r(\cdot)$ is a type B Nussbaum function for any positive odd integer $r \geq 1$. If the initial conditions $e_i(0)$ satisfy $|e_i(0)| < \rho_i(0)$, $i = 1, \ldots, n$, then the PPC problem is solved in the sense of P1 and P2.

Proof. (Time dependence of the functions e_i, α_i, $\dot{\alpha}_i$, and $\mathcal{N}(s_i)$ will be omitted whenever unambiguous). Taking the time derivative of e_i along (1), (12) and (13) yields

$$\begin{aligned} \dot{e}_i &= \dot{\chi}_i - \dot{\alpha}_i = \phi_i(t, \overline{\chi}_i) + \ell_i(t, \overline{\chi}_i)(e_{i+1} + \alpha_{i+1})^{r_i} - \dot{\alpha}_i \\ &= \phi_i(t, \overline{\chi}_i) + \ell_i(t, \overline{\chi}_i)\vartheta_i(e_{i+1}, \alpha_{i+1})e_{i+1}^{r_i} - \dot{\alpha}_i \\ &\quad + \ell_i(t, \overline{\chi}_i)\gamma_i(e_{i+1}, \alpha_{i+1})\alpha_{i+1}^{r_i} \\ &= F_i(t) + \gamma_i(e_{i+1}, \alpha_{i+1})\ell_i(t, \overline{\chi}_i)\varrho_i^{r_i} \mathcal{N}^{r_i}(s_i)\mathcal{T}_i^{r_i}(t), \end{aligned}$$

$$\dot{e}_n = F_n(t) + \ell_n(t, \overline{\chi}_n)\varrho_n^{r_n} \mathcal{N}^{r_n}(s_n)\mathcal{T}_n^{r_n}(t), \tag{15}$$

where the second equality used the separation lemma of Lv, De Schutter, Shi, and Baldi (2022) and Lv, Yu, Cao, and Baldi (0000), $|\vartheta_i(e_{i+1}, \alpha_{i+1})| \leq \bar{\vartheta}_i$ with $\bar{\vartheta}_i$ a positive constant, $\gamma_i(e_{i+1}, \alpha_{i+1}) \in [1 - \bar{\epsilon}_i, 1 + \bar{\epsilon}_i]$ with an arbitrary constant $\bar{\epsilon}_i \in (0, 1)$, $F_i(t) = \phi_i(t, \overline{\chi}_i) + \ell_i(t, \overline{\chi}_i)\vartheta_i(e_{i+1}, \alpha_{i+1})e_{i+1}^{r_i} - \dot{\alpha}_i$, $i = 1, \ldots, n - 1$, and $F_n(t) = \phi_n(t, \overline{\chi}_n) - \dot{\alpha}_n$.

In what follows, we will prove that $|e_i(t)| < \rho_i(t)$, $i = 1, \ldots, n$, holds for $t \geq 0$ using a contradiction. Suppose there exists an error e_m such that

$$|e_m(t_m)| \geq \rho_m(t_m), \quad \forall m \in \{1, \ldots, n\}. \tag{16}$$

Let $t_\delta = \min\{t_m\}$ be the time instant when (16) is violated for the first time. Then, due to continuity of e_i and the fact $|e_i(0)| < \rho_i(0)$, $i = 1, \ldots, n$, it follows that

$$|e_i(t)| < \rho_i(t), \quad \forall t \in [0, t_\delta), \tag{17}$$

and that there exists an error e_δ satisfying

$$\lim_{t \to t_\delta^-} |e_\delta(t)| = \lim_{t \to t_\delta^-} |\rho_\delta(t)|, \quad \delta \in \{1, \ldots, n\}, \tag{18}$$

where t_δ^- denotes the left limit of t_δ. To seek a contradiction, the analysis given below is conducted on a finite time interval $[0, t_\delta)$.

Step 1: Consider the Lyapunov function candidate

$$V_1(t) = \frac{1}{2} \tan^2\left(\frac{\pi}{2} \frac{e_1(t)}{\rho_1(t)}\right), \quad \forall t \in [0, t_\delta). \tag{19}$$

When $|e_1(t)| < \delta_1 \rho_1(t)$, it immediately follows that

$$V_1(t) < \frac{1}{2} \tan^2\left(\frac{\pi \delta_1}{2}\right) \triangleq \overline{\psi}_1. \tag{20}$$

From (14), we further have

$$\dot{s}_1(t) = 0, \quad \text{when } V_1(t) < \overline{\psi}_1. \tag{21}$$

When $|e_1(t)| \geq \delta_1 \rho_1(t)$, $V_1(t) \geq \overline{\psi}_1$ holds. Taking the time derivative of $V_1(t)$ along (15) yields

$$\begin{aligned} \dot{V}_1(t) &= \frac{\pi}{2} \frac{\mathcal{T}_1(t)}{\rho_1^2(t)}\left[\dot{e}_1(t)\rho_1(t) - e_1(t)\dot{\rho}_1(t)\right] \\ &= \mathcal{T}_1(t)F_{1f}(t) + g_{1f}(t)\mathcal{N}^{r_1}(s_1)\mathcal{T}_1^{r_1+1}(t), \end{aligned} \tag{22}$$

where

$$F_{1f}(t) = \frac{\pi}{2}\left(\frac{F_1(t)}{\rho_1(t)} - \frac{e_1(t)\dot{\rho}_1(t)}{\rho_1^2(t)}\right),$$

$$g_{1f}(t) = \frac{\pi}{2}\frac{1}{\rho_1(t)}\gamma_1(e_2, \alpha_2)\ell_1(t, \chi_1)\varrho_1^{r_1}.$$

According to the boundedness of y_r and its derivative, $\alpha_1(\cdot)$ and $\dot{\alpha}_1(\cdot)$ are bounded on $[0, t_\delta)$, which, together with (17), yields the boundedness of $\chi_1(\cdot)$ on $[0, t_\delta)$. By Assumption 1, the boundedness of χ_1 and $\dot{\alpha}_1$ results in that of $F_1(\cdot)$ and hence $F_{1f}(\cdot)$ on $[0, t_\delta)$. Invoking the boundedness of $\gamma_1(e_2, \alpha_2)$, $\rho_1(\cdot)$, and $\ell_1(\cdot, \chi_1)$ leads to the boundedness of $g_{1f}(\cdot)$ on $[0, t_\delta)$. Then, it follows from the Extreme Value Theorem that there exist positive constants $\bar{F}_{1f}$, $\underline{g}_{1f}$, and $\bar{g}_{1f}$ such that

$$|F_{1f}(t)| \le \bar{F}_{1f}, \ g_{1f}(t) \in [\underline{g}_{1f}, \bar{g}_{1f}], \ 0 \notin [\underline{g}_{1f}, \bar{g}_{1f}]. \tag{23}$$

Substituting $|e_1(t)| \ge \delta_1 \rho_1(t)$ into (12) gives

$$\left| \mathcal{T}_1^{r_1}(t) \right| \ge \frac{\tan^{r_1}\left(\frac{\pi}{2}\delta_1\right)}{\cos^{2r_1}\left(\frac{\pi}{2}\delta_1\right)} \ge \tan^{r_1}\left(\frac{\pi}{2}\delta_1\right). \tag{24}$$

Synthesizing (22)–(24) results in

$$\dot{V}_1(t) \le \frac{|F_{1f}(t)|}{|\mathcal{T}_1^{r_1}(t)|} \mathcal{T}_1^{r_1+1}(t) + g_{1f}(t)\mathcal{N}^{r_1}(s_1)\mathcal{T}_1^{r_1+1}(t)$$

$$\le \left[\frac{\bar{F}_{1f}}{\tan^{r_1}\left(\frac{\pi}{2}\delta_1\right)} + g_{1f}(t)\mathcal{N}^{r_1}(s_1) \right] \dot{s}_1(t). \tag{25}$$

Note from Proposition (5) that $\mathcal{N}^{r_1}(\cdot)$ is a type B Nussbaum function. So, we can apply Lemma 1 to prove that $V_1(\cdot)$ and $s_1(\cdot)$ are bounded on $[0, t_\delta)$. In view of (19), we can claim that there exists a constant $\bar{\sigma}_1 > 0$ such that $|e_1(t)| \le \rho_1(t) - \bar{\sigma}_1 < \rho_1(t)$, $\forall t \in [0, t_\delta)$ (equivalently to the boundedness of $\mathcal{T}_1(\cdot)$ on $[0, t_\delta)$). This, together with (12) and the boundedness of $\mathcal{N}(s_1)$, gives the boundedness of $\alpha_2(\cdot)$ and $\overline{\chi}_2(\cdot)$ on $[0, t_\delta)$ due to $\chi_i = e_i + \alpha_i$, $i = 1, 2$. By Lemma 2, $\dot{\alpha}_2(\cdot)$ is bounded on $[0, t_\delta)$.

Step $i(i = 2, \ldots, n)$: Boundedness of $\overline{\chi}_i(\cdot)$ and $\dot{\alpha}_i(\cdot)$ on $[0, t_\delta)$ was obtained from step $i - 1$. Consider the Lyapunov function candidate

$$V_i(t) = \frac{1}{2}\tan^2\left(\frac{\pi}{2}\frac{e_i(t)}{\rho_i(t)}\right), \quad \forall t \in [0, t_\delta). \tag{26}$$

When $|e_i(t)| < \delta_i \rho_i(t)$, it follows that

$$V_i(t) < \frac{1}{2}\tan^2\left(\frac{\pi\delta_i}{2}\right) \triangleq \overline{\psi}_i. \tag{27}$$

From (14) one has

$$\dot{s}_i(t) = 0, \quad \text{when } V_i(t) < \overline{\psi}_i. \tag{28}$$

When $|e_i(t)| \ge \delta_i \rho_i(t)$, it holds that $V_i(t) \ge \overline{\psi}_i$. Taking the time derivative of $V_i(t)$ along (14) gives

$$\dot{V}_i(t) = \frac{\pi}{2}\frac{\mathcal{T}_i(t)}{\rho_i^2(t)}\left[\dot{e}_i(t)\rho_i(t) - e_i(t)\dot{\rho}_i(t) \right]$$

$$= \mathcal{T}_i(t)F_{if}(t) + g_{if}(t)\mathcal{N}^{r_i}(s_i)\mathcal{T}_i^{r_i+1}(t), \tag{29}$$

where

$$F_{if}(t) = \frac{\pi}{2}\left(\frac{F_i(t)}{\rho_i(t)} - \frac{e_i(t)\dot{\rho}_i(t)}{\rho_i^2(t)} \right),$$

$$g_{if}(t) = \frac{\pi}{2}\frac{1}{\rho_i(t)}\gamma_i(e_{i+1}, \alpha_{i+1})\ell_i(t, \overline{\chi}_i)\varrho_i^{r_i}.$$

In light of Assumption 1 and the boundedness of $\overline{\chi}_i(\cdot)$, $\dot{\alpha}_i(\cdot)$ and $e_{i+1}(\cdot)$ on $[0, t_\delta)$, $F_i(\cdot)$ is bounded on $[0, t_\delta)$, which further ensures the boundedness of $F_{if}(\cdot)$ on $[0, t_\delta)$. Recalling Assumption 1 and the boundedness of $\gamma_i(e_{i+1}, \alpha_{i+1})$ leads to that of $g_{if}(\cdot)$ on $[0, t_\delta)$. Similar to Step 1, one can conclude there exist positive constants $\bar{F}_{if}$, $\underline{g}_{if}$, and $\bar{g}_{if}$ such that

$$|F_{if}(t)| \le \bar{F}_{if}, \ g_{if}(t) \in [\underline{g}_{if}, \bar{g}_{if}], \ 0 \notin [\underline{g}_{if}, \bar{g}_{if}]. \tag{30}$$
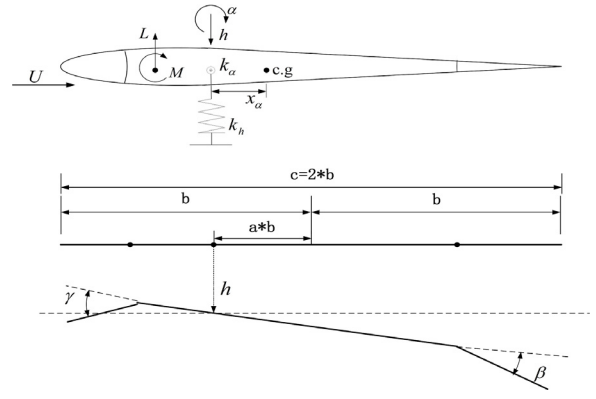

Fig. 2. Wing section with leading-edge (LE) and trailing-edge (TE) control surfaces.

Substituting $|e_i(t)| \ge \delta_i \rho_i(t)$ into (12) results in

$$\left| \mathcal{T}_i^{r_i}(t) \right| \ge \frac{\tan^{r_i}\left(\frac{\pi}{2}\delta_i\right)}{\cos^{2r_i}\left(\frac{\pi}{2}\delta_i\right)} \ge \tan^{r_i}\left(\frac{\pi}{2}\delta_i\right). \tag{31}$$

Summarizing (29)–(31) leads to

$$\dot{V}_i(t) \le \frac{|F_{if}(t)|}{|\mathcal{T}_i^{r_i}(t)|} \mathcal{T}_i^{r_i+1}(t) + g_{if}(t)\mathcal{N}^{r_i}(s_i)\mathcal{T}_i^{r_i+1}(t)$$

$$\le \left[\frac{\bar{F}_{if}}{\tan^{r_i}\left(\frac{\pi}{2}\delta_i\right)} + g_{if}(t)\mathcal{N}^{r_i}(s_i) \right] \dot{s}_i(t). \tag{32}$$

Likewise, $\mathcal{N}^{r_i}(\cdot)$ is a type B Nussbaum function, so we apply Lemma 1 to prove that $V_i(\cdot)$ and $s_i(\cdot)$ are bounded on $[0, t_\delta)$. According to (26), there exists a constant $\bar{\sigma}_i > 0$ such that $|e_i(t)| \le \rho_i(t) - \bar{\sigma}_i < \rho_i(t)$ $\forall t \in [0, t_\delta)$, which, combined with (12) and the boundedness of $\mathcal{N}(s_i)$, yields the boundedness of $\alpha_{i+1}(\cdot)$ and $\overline{\chi}_{i+1}(\cdot)$ on $[0, t_\delta)$ owing to $\chi_{i+1} = e_{i+1} + \alpha_{i+1}$. Therefore, $\dot{\alpha}_{i+1}(\cdot)$ is bounded on $[0, t_\delta)$ according to Lemma 2.

In summary, we proved that $|e_i(t)| \le \rho_i(t) - \bar{\sigma}_i < \rho_i(t)$, $i = 1, \ldots, n$, for $t \in [0, t_\delta)$. However, this contradicts the assumption in (18) and implies that t_δ should be extended to $+\infty$. As a result, $|e_i(t)| < \rho_i(t)$, $i = 1, \ldots, n$, holds for $t \in [0, +\infty)$. Given that Lemma 1 holds true on $[0, +\infty)$, the boundedness of closed-loop signals is guaranteed on $[0, +\infty)$. This completes the proof. ∎

5. Simulation verification

To validate the proposed method, a two-degree-of-freedom wing section with leading-edge (LE) and trailing-edge (TE) control surfaces as in Fig. 2 is considered. The system dynamics can be described by (Fung, 1955; Ko, Kurdila, & Strganac, 1997):

$$\begin{bmatrix} I_\alpha & m_w x_\alpha b \\ m_w x_\alpha b & m_t \end{bmatrix}\begin{bmatrix} \ddot{\alpha} \\ \ddot{h} \end{bmatrix} + \begin{bmatrix} c_h & 0 \\ 0 & c_\alpha(\dot{\alpha}) \end{bmatrix}\begin{bmatrix} \dot{\alpha} \\ \dot{h} \end{bmatrix}$$
$$+ \begin{bmatrix} k_\alpha(\alpha) & 0 \\ 0 & k_h(h) \end{bmatrix}\begin{bmatrix} \alpha \\ h \end{bmatrix} = \begin{bmatrix} M \\ -L \end{bmatrix} \tag{33}$$

where α and h denote the pitch angle and the plunge displacement, respectively; I_α is the moment of inertia; $m_w = m_t + m_l$ is the sum of wing section mass m_t and load section mass m_l; x_α is the distance between the center of mass and the elastic axis; b is the semi-chord of the wing; c_h is the plunge damping coefficient. The pitch damping $c_\alpha(\dot{\alpha})$, the pitch stiffness $k_\alpha(\alpha)$, and the plunge stiffness $k_h(h)$ are expressed as $c_\alpha(\dot{\alpha}) = \sum_{j=0}^{2} c_{\alpha j}\dot{\alpha}^j$, $k_\alpha(\alpha) = \sum_{j=0}^{2} k_{\alpha j}\alpha^j$, and $k_h(h) = \sum_{j=0}^{2} k_{hj}h^j$, where $c_{\alpha j}$, $k_{\alpha j}$, and k_{hj} are unknown non-zero constants, so they cannot be used
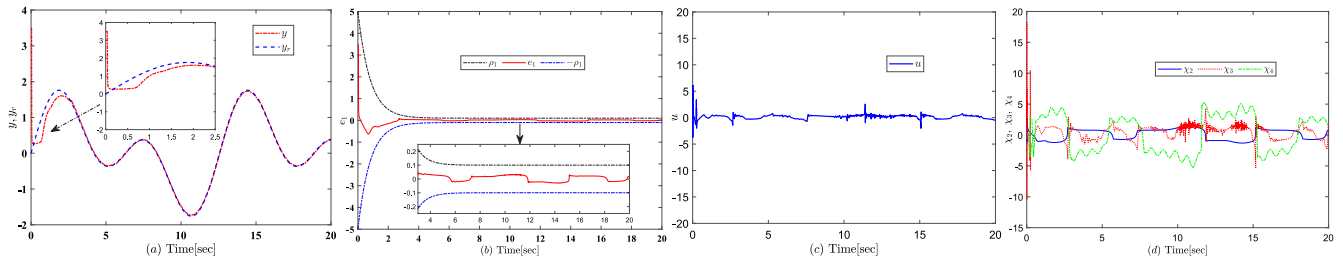
Fig. 3. (a): Evolution of y and y_r; (b): Evolution of the tracking error e_1; (c): Evolution of the control input signal u; (d): Evolution of the state variables χ_2, χ_3, and χ_4.

in control design. In (33), M and L represent the aerodynamic moment and lift expressed by

$$M = \rho U^2 b^2 s_p \left\{ \bar{c}_{l_\alpha} \left(\alpha + \frac{\dot{h}}{U} + (0.5 - a) b \frac{\dot{\alpha}}{U} \right) + \bar{c}_{l_\beta} \beta + \bar{c}_{l_\gamma} \gamma \right\}$$

$$L = \rho U^2 b s_p \left\{ c_{l_\alpha} \left(\alpha + \frac{\dot{h}}{U} + (0.5 - a) b \frac{\dot{\alpha}}{U} \right) + c_{l_\beta} \beta + c_{l_\gamma} \gamma \right\}$$

where $\bar{c}_{l_\alpha} = \left(\frac{1}{2} + a\right) c_{l_\alpha} + 2 c_{m_\alpha}$, $\bar{c}_{l_\beta} = \left(\frac{1}{2} + a\right) c_{l_\beta} + 2 c_{m_\beta}$, $\bar{c}_{l_\gamma} = \left(\frac{1}{2} + a\right) c_{l_\gamma} + 2 c_{m_\gamma}$, and ρ is the air density; U denotes the freestream velocity; c_{l_α}, c_{l_β} and c_{l_γ} are the lift derivatives; c_{m_α}, c_{m_β} and c_{m_γ} are the moment derivatives; s_p is the span; a is the nondimensional distance from midchord to the elastic axis; β and γ are the TE and LE control surface deflections, respectively. With the change of coordinates $\chi_1 = \alpha$, $\chi_2 = \dot{\alpha}$, $\chi_3 = h$, $\chi_4 = \dot{h}$, and $u = \beta + \gamma$, we can rewrite (33) as

$$\begin{cases} \dot{\chi}_1 = \chi_2, \quad \dot{\chi}_2 = \phi_2(\bar{\chi}_2) + \ell_2(\bar{\chi}_2) \chi_3^3, \\ \dot{\chi}_3 = \chi_4, \quad \dot{\chi}_4 = \phi_4(\bar{\chi}_4) + u, \end{cases} \quad (34)$$

where $\phi_2(\chi) = c_{\bar{\alpha}_1} \chi_1 + c_{\alpha_{11}} \chi_1^3 + c_{\dot{\alpha}_1} \chi_2 + c_{\dot{\alpha}_{11}} \chi_2^3 + c_{h_1} \chi_2 + c_{\beta_1} \beta + c_{\gamma_1} \gamma$, $\phi_4(\chi) = c_{\alpha_2} \chi_1 + c_{\alpha_{21}} \chi_1^3 + c_{\dot{\alpha}_2} \chi_2 + c_{\dot{\alpha}_{21}} \chi_2^3 + c_{h_{21}} \chi_3^3 + c_{h_2} \chi_4$, and $\ell_2(\bar{\chi}_2) = m_w x_\alpha b k_{h2}$ with $c_{\bar{\alpha}_1} = c_2 m_t c_{m\alpha} + c_1 m_t x_\alpha b c_{l\alpha}$, $c_{\alpha_{11}} = -m_t k_{\alpha2}$, $c_{\dot{\alpha}_1} = c_2 m_t c_{m\alpha} (0.5 - a) \frac{b}{U} - c_{\alpha0} m_t + c_1 m_t x_\alpha b c_{l\alpha} (0.5 - a) \frac{b}{U}$, $c_{\dot{\alpha}_{11}} = -m_t c_{\alpha2}$, $c_{h_1} = c_2 m_t c_{m\alpha} \frac{1}{U} + c_1 m_t x_\alpha b c_{l\alpha} \frac{1}{U} - c_h m_t x_\alpha b$, $c_{\beta_1} = c_2 m_t c_{m\beta} + c_1 m_t x_\alpha b c_{l\beta}$, $c_{\gamma_1} = c_1 m_t x_\alpha b c_{l\gamma} + c_2 m_t c_{m\gamma}$, $c_{\alpha_2} = -c_2 m_t x_\alpha b c_{m\alpha} - c_1 I_\alpha c_{l\alpha}$, $c_{\alpha_{21}} = m_t x_\alpha b k_{\alpha2}$, $c_{\dot{\alpha}_2} = -c_2 m_t x_\alpha b c_{m\alpha} (0.5 - a) \frac{b}{U} - c_1 I_\alpha c_{l\alpha} (0.5 - a) \frac{b}{U} + c_{\alpha0} m_t x_\alpha b$, $c_{\dot{\alpha}_{21}} = m_t x_\alpha b c_{\alpha2}$, $c_{h_{21}} = -k_{h2} I_\alpha$, $c_{h_2} = -c_2 m_t x_\alpha c_{m\alpha} \frac{b}{U} - c_h I_\alpha - c_1 I_\alpha c_{l\alpha} \frac{1}{U}$, $c_{\beta_2} = -c_2 m_t x_\alpha b c_{m\beta} - c_1 I_\alpha c_{l\beta}$, $c_{\gamma_2} = -c_2 m_t x_\alpha b c_{m\gamma} - c_1 I_\alpha c_{l\gamma}$, $c_1 = \rho U^2 b s_p$, and $c_2 = \rho U^2 b^2 s_p$.

Since the sign of k_{h2} is unknown, the sign of the control coefficient $\ell_2(\cdot)$ is unknown and cannot be used in the control design. Taking the same structural parameters as Ko et al. (1997) gives the values of model parameters used for simulation in Table 1. Let the reference signal be $y_r(t) = \sin(0.5t) + \sin(t)$. The initial state values are chosen as $\chi_1(0) = 3.5$, $\chi_2(0) = -1.5$, $\chi_3(0) = -2.5$ and $\chi_4(0) = -1.5$. The design parameters are chosen to be: $\varrho_1 = 1.25$, $\varrho_2 = 1.75$, $\varrho_3 = \varrho_4 = 5$, $\delta_1 = 0.75$, $\delta_2 = 0.5$, $\delta_3 = 0.35$, $\delta_4 = 0.9$, $\rho_{1,0} = \rho_{2,0} = \rho_{3,0} = \rho_{4,0} = 5$, $\rho_{1,\infty} = 0.1$, $\rho_{2,\infty} = 0.85$, $\rho_{3,\infty} = 0.5$, $\rho_{4,\infty} = 0.75$, $\kappa_1 = 1.25$, $\kappa_2 = 0.75$, $\kappa_3 = \kappa_4 = 0.5$. The parameters and initial conditions of Nussbaum functions are $\mu = 0.25$ and $s_1(0) = s_2(0) = s_3(0) = s_4(0) = 0$, respectively.

Simulation results are shown in Figs. 3 and 4, where: Fig. 3(a)–(b) show that output y tracks the reference signal y_r with bounded tracking error while the tracking error e_1 evolves within the prescribed bounds $(-\rho_1, \rho_1)$; Fig. 3(c)–(d) show the boundedness of the control signal u and state variables χ_2, χ_3, and χ_4; Fig. 4(a)–(b) show the boundedness of s_1, s_2, s_3, s_4, $\mathcal{N}(s_1)$, $\mathcal{N}(s_2)$, $\mathcal{N}(s_3)$, and $\mathcal{N}(s_4)$. To investigate the influence of the parameter δ_i, $i = 1, \ldots, 4$, on the closed-loop response, we use three different sets of values for δ_i: Case 1: $\delta_1 = 0.15$, $\delta_2 = 0.2$, $\delta_3 = 0.25$, $\delta_4 = 0.3$;

Table 1
The values of model parameters.

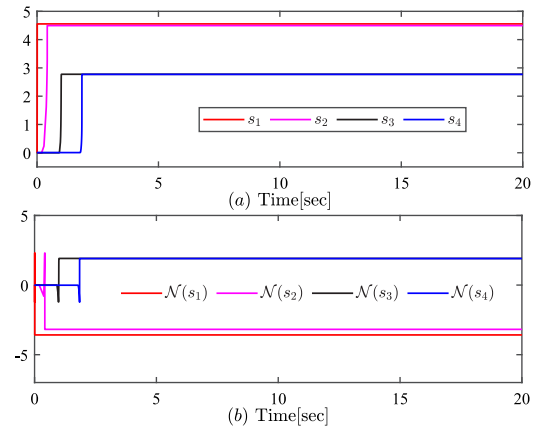| Coefficient	Value	Coefficient	Value
$c_{\bar{\alpha}_1}$	0.7835	$c_{\alpha_{11}}$	-1.5616
$c_{\dot{\alpha}_{11}}$	-7.6423	c_{h_1}	2.6583
c_{γ_1}	0.7256	c_{α_2}	-5.8731
$c_{\dot{\alpha}_2}$	-3.2567	$c_{\dot{\alpha}_{21}}$	1.2548
c_{h_2}	-8.2431	c_{α_1}	0.5717
$c_{\dot{\alpha}_1}$	4.9527	c_{β_1}	0.5394
$c_{\alpha_{21}}$	2.2495	$c_{h_{21}}$	-0.6724
c_{α_0}	-1.0395	$c_{\dot{\alpha}_2}$	6.7242
k_{h_0}	2.3985	k_{h_1}	-4.7592
k_{h_2}	3.6937	k_{α_0}	-2.0593

Fig. 4. (a): Evolution of s_1, s_2, s_3, and s_4; (b): Evolution of $\mathcal{N}(s_1)$, $\mathcal{N}(s_2)$, $\mathcal{N}(s_3)$, and $\mathcal{N}(s_4)$.

Case 2: $\delta_1 = 0.25$, $\delta_2 = 0.3$, $\delta_3 = 0.35$, $\delta_4 = 0.4$; Case 3: $\delta_1 = 0.35$, $\delta_2 = 0.45$, $\delta_3 = 0.55$, $\delta_4 = 0.6$. The trajectories of the adaptation parameters s_i are in Fig. 5, validating the boundedness of s_i for different δ_i, $i = 1, \ldots, 4$.

To show the advantages of the proposed method in handling time-varying unknown control directions, two situations are considered: the proposed method with a type A Nussbaum function $\mathcal{N}(s) = \sin(3\pi s)s^2$ and with a type B Nussbaum function $\mathcal{N}(s) = \cos\left(\frac{\pi s}{2}\right) \exp(0.25s)$. The simulation results for a type B Nussbaum function have been already shown in Fig. 4, while the simulation results for a type A Nussbaum function are in Fig. 6, from which it can be seen that type A Nussbaum function (thought for fixed control coefficients) may fail to stabilize the system if the coefficients are not fixed. Table 2 validates the advantages of our proposed method in terms of: integral absolute value (IAV) $\left[\int_0^T \sum_{i=1}^4 |\mathcal{N}_i'(t)| dt \right]$, integral time absolute value (ITAV) $\left[\int_0^T \sum_{i=1}^4 t |\mathcal{N}_i'(t)| dt \right]$, and root mean square value (RMSV)
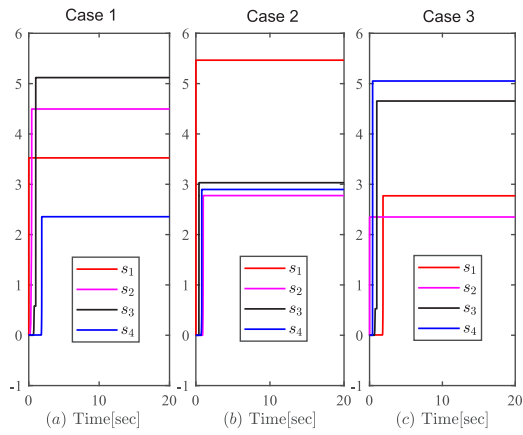
Fig. 5. Evolution of s_1, s_2, s_3, and s_4 under three cases.
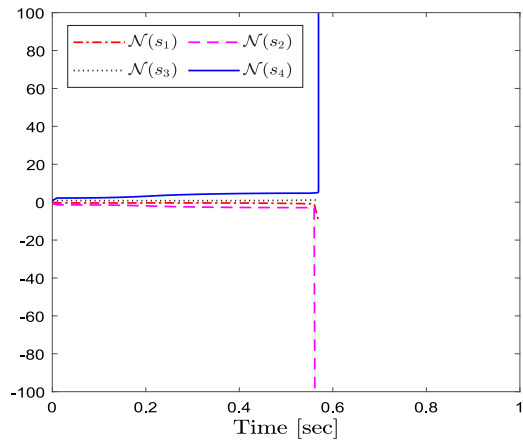

Fig. 6. Evolution of $\mathscr{N}(s_1)$, $\mathscr{N}(s_2)$, $\mathscr{N}(s_3)$, and $\mathscr{N}(s_4)$ for a type A Nussbaum function.

Table 2
Performance indices with two types of Nussbaum functions.

	Type B	Type A
IAV	**110.71**	$\rightarrow \infty$
ITAV	**1296.74**	$\rightarrow \infty$
RMSV	**4.38**	$\rightarrow \infty$

$\left[\frac{1}{T}\int_0^T \sum_{i=1}^4 \mathscr{N}'^2_i(t)dt\right]^{\frac{1}{2}}$, where $\mathscr{N}'_i = \varrho_i \mathscr{N}(s_i(\cdot))\mathfrak{I}_i(\cdot)$, $i = 1, \ldots, 4$ represents the value of controller gain.

6. Conclusions

In the context of prescribed-performance control (PPC) for high-power dynamics with time-varying unknown control coefficients, this work has shown that only some particular type B Nussbaum functions can be used for handling time-varying unknown control coefficients in high-power systems. Then, a novel switching Nussbaum conditional inequality was designed to avoid high gains, by letting the switching gain increases only when the tracking error is close to violating the performance bounds. An interesting topic deserving future investigation is PPC with time-varying unknown control coefficients and positive-odd rational powers, which contains positive-odd integer powers as a special case.

Appendix

Proof of Proposition 1. We first define some quantities as follows,

$$p_{\lambda,r} = \int_0^1 \left[2^{\left(\lambda^3+\frac{1}{3}\right)\lambda} \sin(s\pi)\right]^r ds$$
$$= 2^{r\left(\lambda^3+\frac{1}{3}\right)\lambda} \int_0^1 \sin^r(s\pi)ds = 2^{r\left(\lambda^4+\frac{1}{3}\lambda\right)}\alpha_r$$

and

$$q_{\lambda,r} = \int_1^{2^\lambda} \left[2^{\lambda^4} \sin\left(\frac{s-1}{2^\lambda-1}\pi\right)\right]^r ds$$
$$= 2^{r\lambda^4} \int_1^{2^\lambda} \sin^r\left(\frac{s-1}{2^\lambda-1}\pi\right)ds$$
$$= 2^{r\lambda^4}(2^\lambda-1)\int_0^1 \sin^r(s\pi)\,ds = 2^{r\lambda^4}(2^\lambda-1)\alpha_r$$

for $\alpha_r = \int_0^1 \sin^r(s\pi)ds$. In accordance with Definition 2, the proof is divided into three parts.

(i) For any $y \geq 0$, there exists $\lambda \in \mathbb{N}^+$ such that $y \in [2^\lambda-2, 2^{\lambda+1}-2)$. As a result, it holds that

$$\frac{1}{y}\int_0^y \mathscr{N}_-(s)ds \geq \frac{1}{2^{\lambda+1}-2}\int_0^{2^\lambda-1} \mathscr{N}_-(s)ds$$
$$= \frac{\sum_{k=1}^{\lambda-1} q_{k,1}}{2^{\lambda+1}-2} = \frac{\sum_{k=1}^{\lambda-1} 2^{k^4}(2^k-1)\alpha_1}{2^{\lambda+1}-2} \geq 2^\lambda\alpha_1$$

for $\lambda \geq 3$. The fact that $\lambda \rightarrow +\infty$ as $y \rightarrow +\infty$ implies $\lim_{y\rightarrow+\infty}\frac{1}{y}\int_0^y \mathscr{N}_-(s)ds = +\infty$.

(ii) Note the following calculation, with $y = 2^\lambda - 1$,

$$\frac{\int_0^y \mathscr{N}_+(s)ds}{\int_0^y \mathscr{N}_-(s)ds} = \frac{\sum_{k=1}^{\lambda} p_{k,1}}{\sum_{k=1}^{\lambda-1} q_{k,1}} = \frac{\sum_{k=1}^{\lambda} 2^{k^4+\frac{1}{3}k}}{\sum_{k=1}^{\lambda-1} 2^{k^4}(2^k-1)}. \quad (35)$$

It follows from the Stolz–Cesaro Theorem (Muresan, 2008, Sect. 3.17, pp. 85, Theorem 1.22) that

$$\lim_{\lambda\rightarrow+\infty} \frac{\sum_{k=1}^{\lambda} 2^{k^4+\frac{1}{3}k}}{\sum_{k=1}^{\lambda-1} 2^{k^4}(2^k-1)} = \lim_{\lambda\rightarrow+\infty} \frac{2^{\lambda^4+\frac{1}{3}\lambda}}{2^{(\lambda-1)^4+\lambda-1}} = +\infty$$

which, together with (35), implies $\lim_{y\rightarrow+\infty} \sup \frac{\int_0^y \mathscr{N}_+(s)ds}{\int_0^y \mathscr{N}_-(s)ds} = +\infty$.

The results $\lim_{y\rightarrow+\infty}\frac{1}{y}\int_0^y \mathscr{N}_+(s)ds = +\infty$ and $\lim_{y\rightarrow+\infty} \sup \frac{\int_0^y \mathscr{N}_-(s)ds}{\int_0^y \mathscr{N}_+(s)ds} = +\infty$ can be proved in a similar way and are omitted. According to Definition 2, $\mathscr{N}(\cdot)$ is a type B Nussbaum function.

(iii) For any $y \geq 0$, there exists $\lambda \in \mathbb{N}^+$ such that $y \in [2^\lambda-2, 2^{\lambda+1}-2)$. According to the definition of $\mathscr{N}^r$, we have

$$\frac{\int_0^y \mathscr{N}_-^r(s)ds}{\int_0^y \mathscr{N}_+^r(s)ds} \leq \frac{\int_0^{2^\lambda-2} \mathscr{N}_-^r(s)ds}{\int_0^{2^\lambda-2} \mathscr{N}_+^r(s)ds} \text{ or } \frac{\int_0^{2^{\lambda+1}-2} \mathscr{N}_-^r(s)ds}{\int_0^{2^{\lambda+1}-2} \mathscr{N}_+^r(s)ds}.$$

The following calculation

$$\lim_{y\rightarrow+\infty} \sup \frac{\int_0^y \mathscr{N}_-^r(s)ds}{\int_0^y \mathscr{N}_+^r(s)ds} \leq \lim_{\lambda\rightarrow+\infty} \frac{\int_0^{2^{\lambda+1}-2} \mathscr{N}_-^r(s)ds}{\int_0^{2^{\lambda+1}-2} \mathscr{N}_+^r(s)ds}$$
$$\leq \lim_{\lambda\rightarrow+\infty} \frac{\sum_{k=1}^{\lambda} q_{k,r}}{\sum_{k=1}^{\lambda-1} p_{k,r}} = \lim_{\lambda\rightarrow+\infty} \frac{\sum_{k=1}^{\lambda} 2^{rk^4}(2^k-1)}{\sum_{k=1}^{\lambda} 2^{r\left(k^4+\frac{1}{3}k\right)}}$$
$$= \lim_{\lambda\rightarrow+\infty}\left(2^{\lambda-\frac{r\lambda}{3}} - 2^{-\frac{r\lambda}{3}}\right) = \begin{cases} +\infty, & r=1; \\ 1, & r=3; \\ 0, & r>3. \end{cases}$$

shows the violation of Definition 2. Thus, one can conclude that $\mathcal{N}^r(\cdot)$ is not a type B Nussbaum function. This completes the proof. ∎

Proof of Proposition 2. According to Chen (2019), $\mathcal{N}^r(s)$ is a type B Nussbaum function for $r = 1$. So the remaining task is to show that statement still holds for $r \geq 3$. By the Darboux–Stieltjes integral property (Muresan, 2008, Sect. 6.12, pp. 257, Theorem 1.7, (h)), one has, for any $a \geq 0$, it holds that

$$\exp(r\mu a^2)\alpha_r \leq \int_a^{a+1} \exp(r\mu s^2)\left|\cos^r\left(\frac{\pi s}{2}\right)\right| ds$$

$$= \exp(r\mu \bar{s}^2)\int_a^{a+1}\left|\cos^r\left(\frac{\pi s}{2}\right)\right| ds \leq \exp(r\mu(a+1)^2)\alpha_r \quad (36)$$

for some $\bar{s} \in (a, a+1)$ and $\alpha_r = \int_0^1 \cos^r\left(\frac{\pi s}{2}\right) ds$, which is used in the remaining proof. In accordance with Definition 2, the proof is divided into two parts.

(i) For any $y \geq 0$, there exists $\lambda \in \mathbb{N}$ such that $y \in [4\lambda - 3, 4\lambda + 1)$, where $\mathbb{N}$ is the set of integers. As a result, one has

$$\frac{1}{y}\int_0^y \mathcal{N}_+^r(s) ds > \frac{1}{4\lambda + 1}\int_0^{4\lambda - 1} \mathcal{N}_+^r(s) ds$$

$$> \frac{1}{4\lambda + 1}\sum_{k=1}^{\lambda-1}\int_{4k-1}^{4k+1} \exp(r\mu s^2)\cos^r\left(\frac{\pi s}{2}\right) ds.$$

By (36), we can arrive at

$$\int_{4k-1}^{4k+1} \exp(r\mu s^2)\cos^r\left(\frac{\pi s}{2}\right) ds \geq 2\alpha_r \exp(r\mu(4k-1)^2)$$

and hence

$$\lim_{y\to+\infty} \frac{1}{y}\int_0^y \mathcal{N}_+^r(s) ds$$

$$\geq \lim_{\lambda\to+\infty} \frac{2\alpha_r \sum_{k=1}^{\lambda-1} \exp(r\mu(4k-1)^2)}{4\lambda + 1} = +\infty.$$

(ii) Note the following calculation, with $y = 4\lambda + 3$,

$$\frac{\int_0^y \mathcal{N}_-^r(s) ds}{\int_0^y \mathcal{N}_+^r(s) ds} = \frac{\int_0^{4\lambda+3} \mathcal{N}_-^r(s) ds}{\int_0^{4\lambda+3} \mathcal{N}_+^r(s) ds}$$

$$> \frac{\sum_{k=0}^{\lambda}\int_{4k+1}^{4k+3} \exp(r\mu s^2)\left|\cos^r\left(\frac{\pi s}{2}\right)\right| ds}{\sum_{k=0}^{\lambda}\int_{4k-1}^{4k+1} \exp(r\mu s^2)\cos^r\left(\frac{\pi s}{2}\right) ds}$$

$$\geq \frac{\sum_{k=0}^{\lambda}\left[\exp(r\mu(4k+1)^2) + \exp(r\mu(4k+2)^2)\right]\alpha_r}{\sum_{k=0}^{\lambda}\left[\exp(r\mu(4k)^2) + \exp(r\mu(4k+1)^2)\right]\alpha_r}.$$

It follows from Stolz–Cesaro Theorem (Muresan, 2008) that

$$\lim_{\lambda\to+\infty} \frac{\int_0^{4\lambda+3} \mathcal{N}_-^r(s) ds}{\int_0^{4\lambda+3} \mathcal{N}_+^r(s) ds} \geq \lim_{\lambda\to+\infty} \frac{\exp(r\mu(4\lambda+2)^2)}{\exp(r\mu(4\lambda+1)^2)} = +\infty,$$

which implies $\lim_{y\to+\infty}\sup \frac{\int_0^y \mathcal{N}_-^r(s) ds}{\int_0^y \mathcal{N}_+^r(s) ds} = +\infty.$

The results $\lim_{y\to+\infty} \frac{1}{y}\int_0^y \mathcal{N}_-^r(s) ds = +\infty$ and $\lim_{y\to+\infty}\sup \frac{\int_0^y \mathcal{N}_+^r(s) ds}{\int_0^y \mathcal{N}_-^r(s) ds} = +\infty$ can be proved similarly. According to Definition 2, $\mathcal{N}^r(\cdot)$ is a type B Nussbaum function. ∎

References

Bechlioulis, C. P., & Rovithakis, G. A. (2008). Robust adaptive control of feedback linearizable MIMO nonlinear systems with prescribed performance. *IEEE Transactions on Automatic Control*, 53(9), 2090–2099.

Bechlioulis, C. P., & Rovithakis, G. A. (2014). A low-complexity global approximation-free control scheme with prescribed performance for unknown pure feedback systems. *Automatica*, 50, 1217–1226.

Chen, Z. Y. (2019). Nussbaum functions in adaptive control with time varying unknown control coefficients. *Automatica*, 102, 72–79.

Chen, C., & Chen, G. (2020). A new approach to stabilization of high-order nonlinear systems with an asymmetric output constraint. *International Journal of Robust and Nonlinear Control*, 30, 756–775.

Chen, Z. Y., & Huang, J. (2015). *Stabilization and regulation of nonlinear systems, a robust and adaptive approach*. Springer.

Chen, W., Li, X., Ren, W., & Wen, C. (2014). Adaptive consensus of multi-agent systems with unknown identical control directions based on a novel nussbaum-type function. *IEEE Transactions on Automatic Control*, 59(7), 1887–1892.

Ding, Z. T. (2015). Adaptive consensus output regulation of a class of nonlinear systems with unknown high-frequency gain. *Automatica*, 51, 348–355.

Ding, Z. T., & Ye, X. D. (2002). A flat-zone modification for robust adaptive control of nonlinear output feedback systems with unknown high-frequency gains. *IEEE Transactions on Automatic Control*, 47(2), 358–363.

Fan, B., Yang, Q., Jagannathan, S., & Sun, Y. (2019). Output-constrained control of nonaffine multi-agent systems with partially unknown control directions. *IEEE Transactions on Automatic Control*, 64(9), 3936–3942.

Fung, Y. C. (1955). *An introduction to the theory of aeroelasticity*. Wiley.

Ge, S. S., Fan, H., & Lee, T. H. (2004). Adaptive neural control of nonlinear time-delay systems with unknown virtual control coefficients. *IEEE Transactions on Systems, Man and Cybernetics, Part B (Cybernetics)*, 34(1), 499–516.

Ge, S. S., & Wang, J. (2003). Robust adaptive tracking for time-varying uncertain nonlinear systems with unknown control coefficients. *IEEE Transactions on Automatic Control*, 48(8), 1463–1469.

Huang, J., Wang, W., Wen, C., & Zhou, J. (2018). Adaptive control of a class of strict-feedback time-varying nonlinear systems with unknown control coefficients. *Automatica*, 93, 98–105.

Huang, C., & Yu, C. (2018). Tuning function design for nonlinear adaptive control systems with multiple unknown control directions. *Automatica*, 89, 259–265.

Ko, J., Kurdila, A., & Strganac, T. (1997). Nonlinear control of a prototypical wing section with torsional nonlinearity. *Journal of Guidance, Control, and Dynamics*, 20(6), 1181–1189.

Krstic, M., Kanellakopoulos, I., & Kokotovic, P. (1995). *Nonlinear and adaptive control design*. New York, NY, USA: Wiley.

Li, F., & Liu, Y. (2018). Control design with prescribed performance for nonlinear systems with unknown control directions and nonparametric uncertainties. *IEEE Transactions on Automatic Control*, 63(10), 3573–3580.

Li, F., & Liu, Y. (2019). Global practical tracking with prescribed transient performance for inherently nonlinear systems with extremely severe uncertainties. *Science China. Information Sciences*, 62(2), Article 022204.

Lin, W., & Pongvuthithum, R. (2003). Adaptive output tracking of inherently nonlinear systems with nonlinear parameterization. *IEEE Transactions on Automatic Control*, 48(10), 1737–1745.

Lin, W., & Qian, C. (2000). Adding one power integrator: a tool for global stabilization of high-order lower-triangular systems. *Systems & Control Letters*, 39, 339–351.

Liu, L., & Huang, J. (2008). Global robust output regulation of lower triangular systems with unknown control direction. *Automatica*, 44, 1278–1284.

Liu, Y. H., Sun, C. Y., & Li, H. Y. (0000). Adaptive output feedback funnel control of uncertain nonlinear systems with arbitrary relative degree. IEEE Transactions on Automatic Control. http://dx.doi.org/10.1109/TAC.2020.3012027.

Liu, Y. H., Sun, C. Y., & Zhou, Q. (0000). Funnel control of uncertain high-order nonlinear systems with unknown rational powers. IEEE Transactions on Systems, Man, and Cybernetics: Systems. http://dx.doi.org/10.1109/TSMC.2019.2956672.

Liu, Y. J., & Tong, S. C. (2017). Barrier Lyapunov functions for nussbaum gain adaptive control of full state constrained nonlinear systems. *Automatica*, 76, 143–152.

Lv, M., De Schutter, B., Shi, C., & Baldi, S. (2022). Logic-based distributed switching control for agents in power-chained form with multiple unknown control directions. *Automatica*, 137, Article 110143.

Lv, M., Yu, W., Cao, J., & Baldi, S. (0000). A separation-based methodology to consensus tracking of switched high-order nonlinear multi-agent systems. IEEE Transactions on Neural Networks and Learning Systems. http://dx.doi.org/10.1109/TNNLS.2021.3070824.

Lv, M., Yu, W., Cao, J., & Baldi, S. (2020). Consensus in high-power multiagent systems with mixed unknown control directions via hybrid nussbaum-based control. *IEEE Transactions on Cybernetics*, http://dx.doi.org/10.1109/TCYB.2020.3028171.

Manring, N., & Fales, R. (2019). *Hydraulic control systems*. New York, USA: John Wiley.

Muresan, M. (2008). *A concrete approach to classical analysis*. Springer.

Nussbaum, R. D. (1983). Some remarks on a conjecture in parameter adaptive control. *Systems & Control Letters*, 3, 243–246.

Psillakis, H. (2010). Further results on the use of nussbaum gains in adaptive neural network control. *IEEE Transactions on Automatic Control*, *55*(12), 2841–2846.

Psillakis, H. (2017). Consensus in networks of agents with unknown high-frequency gain signs and switching topology. *IEEE Transactions on Automatic Control*, *62*(8), 3993–3998.

Qian, C., & Lin, W. (2002). Practical output tracking of nonlinear systems with uncontrollable unstable linearization. *IEEE Transactions on Automatic Control*, *47*(1), 21–35.

Scheinker, A., & Krstic, M. (2013). Minimum-seeking for CLFs: universal semiglobally stabilizing feedback under unknown control directions. *IEEE Transactions on Automatic Control*, *58*(5), 1107–1122.

Sun, Z. Y., & Liu, Y. G. (2007). Adaptive state-feedback stabilization for a class of high-order nonlinear uncertain systems. *Automatica*, *43*, 1772–1783.

Theodorakopoulos, A., & Rovithakis, G. A. (2015). Guaranteeing preselected tracking quality for uncertain strict-feedback systems with deadzone input nonlinearity and disturbances via low-complexity control. *Automatica*, *54*, 135–145.

Ye, X. D. (2011). Decentralized adaptive stabilization of large-scale nonlinear time-delay systems with unknown high-frequency-gain signs. *IEEE Transactions on Automatic Control*, *56*(6), 1473–1478.

Ye, X. D., & Jiang, J. (1998). Adaptive nonlinear design without a priori knowledge of control directions. *IEEE Transactions on Automatic Control*, *43*(11), 1617–1621.

Zhang, J. X., & Yang, G. H. (2017). Prescribed performance fault-tolerant control of uncertain nonlinear systems with unknown control directions. *IEEE Transactions on Automatic Control*, *62*(12), 6529–6535.

Zhang, J. X., & Yang, G. H. (2019). Low-complexity tracking control of strict-feedback systems with unknown control directions. *IEEE Transactions on Automatic Control*, *64*(12), 5175–5182.

Maolong Lv received the B.Sc. and M.Sc. from Air Force Engineering University, Xi'an, China, in 2014 and 2016, and the Ph.D. in systems and control from Delft University of Technology, The Netherlands, in 2021. He is currently with College of Air Traffic Control and Navigation, Air Force Engineering University. His research interests include adaptive learning control, reinforcement learning, distributed optimization, and intelligent decision-making with applications in multi-agent systems, unmanned autonomous system, UAVs. Dr. Lv was awarded a Descartes Excellence Fellowship from French Government in 2018, which allowed him a research visit in 2018–2019 at University of Grenoble. autonomous vehicles.

Zhiyong Chen received the B.E. in automation from University of Science and Technology of China, Hefei, in 2000, and the M.Sc. and Ph.D. in mechanical and automation engineering from The Chinese University of Hong Kong, in 2002 and 2005. In 2006, he joined The University of Newcastle, Australia, where he is currently a Professor. He was Changjiang Chair Professor with Central South University, Changsha, China. His research interests include nonlinear systems and control, biological systems, and reinforcement learning. He is/was an Associate Editor of *Automatica*, *IEEE Trans. on Cybernetics*, and *IEEE Trans. on Automatic Control*.

Bart De Schutter, received his Ph.D. (summa cum laude) in applied sciences at KU Leuven, Belgium in 1996. He is full professor and department head of Delft Center for Systems and Control at Delft University of Technology, The Netherlands. He is (co-)author of three books, *Optimal Trajectory Planning and Train Scheduling for Urban Rail Transit Systems*, *Reinforcement Learning and Dynamic Programming Using Function Approximators*, *Stability Analysis and Nonlinear Observer Design Using Takagi–Sugeno Fuzzy Models*. Prof. De Schutter was Associate Editor of *Automatica* and he is Associate Editor of *IEEE Trans. on Automatic Control*, and Senior Editor of *IEEE Trans. on Intelligent Transportation Systems*. He is *IEEE Fellow*.

Simone Baldi received the B.Sc. in electrical engineering, and the M.Sc. and Ph.D. in control engineering from University of Florence, Italy, in 2005, 2007, and 2011. He is professor at Southeast University, China. He was awarded outstanding reviewer of Applied Energy (2016) and Automatica (2017). He is subject editor of *Intern. Journal of Adaptive Control and Signal Processing*, associate editor of *IEEE Control Systems Letters* and technical editor of *IEEE/ASME Trans. on Mechatronics*. His research interests include adaptive and switched systems with applications in networked and multi-agent control.