

Quantifying inner-outer interactions in noncanonical wall-bounded flows

Li, Mogeng; Baars, Woutijn J.; Marusic, Ivan; Hutchins, Nicholas

DOI

[10.1103/PhysRevFluids.8.084602](https://doi.org/10.1103/PhysRevFluids.8.084602)

Publication date

2023

Document Version

Final published version

Published in

Physical Review Fluids

Citation (APA)

Li, M., Baars, W. J., Marusic, I., & Hutchins, N. (2023). Quantifying inner-outer interactions in noncanonical wall-bounded flows. *Physical Review Fluids*, 8(8), Article 084602.
<https://doi.org/10.1103/PhysRevFluids.8.084602>

Important note

To cite this publication, please use the final published version (if applicable).
Please check the document version above.

Copyright

Other than for strictly personal use, it is not permitted to download, forward or distribute the text or part of it, without the consent of the author(s) and/or copyright holder(s), unless the work is under an open content license such as Creative Commons.

Takedown policy

Please contact us and provide details if you believe this document breaches copyrights.
We will remove access to the work immediately and investigate your claim.

Green Open Access added to TU Delft Institutional Repository

'You share, we take care!' - Taverne project

<https://www.openaccess.nl/en/you-share-we-take-care>

Otherwise as indicated in the copyright section: the publisher is the copyright holder of this work and the author uses the Dutch legislation to make this work public.

Quantifying inner-outer interactions in noncanonical wall-bounded flows

Mogeng Li ^{1,*} Woutijn J. Baars ¹ Ivan Marusic ² and Nicholas Hutchins ^{2,†}

¹*Faculty of Aerospace Engineering, Delft University of Technology, 2629 HS Delft, The Netherlands*

²*Department of Mechanical Engineering, University of Melbourne, Victoria 3010, Australia*



(Received 27 April 2023; accepted 1 August 2023; published 21 August 2023)

We investigate the underlying physics behind the change in amplitude modulation coefficient in noncanonical wall-bounded flows in the framework of the inner-outer interaction model (IOIM) [Baars *et al.*, *Phys. Rev. Fluids* **1**, 054406 (2016)]. The IOIM captures the amplitude modulation effect, and here we focus on extending the model to noncanonical flows. An analytical relationship between the amplitude modulation coefficient and IOIM parameters is derived, which is shown to capture the increasing trend of the amplitude modulation coefficient with an increasing Reynolds number in a smooth-wall dataset. This relationship is then applied to classify and interpret the noncanonical turbulent boundary layer results reported in previous works. We further present the case study of a turbulent boundary layer after a rough-to-smooth change. Both single-probe and two-probe hotwire measurements are performed to acquire streamwise velocity time series in the recovering flow on the downstream smooth wall. An increased coherence between the large-scale motions and the small-scale envelope in the near-wall region is attributed to the stronger footprints of the overenergetic large-scale motions in the outer layer, whereas the near-wall cycle and its amplitude sensitivity to the superposed structures are similar to that of a canonical smooth-wall flow. These results indicate that the rough-wall structures above the internal layer interact with the near-wall cycle in a similar manner as the increasingly energetic structures in a high-Reynolds number smooth-wall boundary layer.

DOI: [10.1103/PhysRevFluids.8.084602](https://doi.org/10.1103/PhysRevFluids.8.084602)

I. INTRODUCTION

In turbulent boundary layers, large coherent structures are found in the logarithmic region. They carry a high level of turbulent kinetic energy and make a significant contribution to Reynolds stress production [1]. These structures can be further classified as large-scale motions (LSMs) and very-large-scale motions (VLSMs). The former are associated with the vortex packets formed by aligned hairpin vortices [2,3] and typically have a streamwise length of $\sim 3\delta$ (δ is the boundary layer thickness), while the latter may be related to the merging of multiple LSMs [2] and can reach a streamwise extent up to 20δ with spanwise meandering [4,5]. These structures are observed to leave a footprint in the near-wall region [4–6]. As the Reynolds number of a turbulent boundary layer increases, the separation between the outer-scaled motions and viscous-scaled near-wall cycle becomes more distinct, and the strength of these large-scale footprints also intensifies, resulting in the growth of the ‘inner-peak’ magnitude in the broadband streamwise turbulence intensity [5,7].

In addition to the direct superposition effect manifested as large-scale footprints, it has also been found that the near-wall small scales are modulated by the large scales in the outer layer [5,8,9]. In the near-wall region, the amplitude and frequency of small-scale fluctuations show a decrease when

*mogeng.li@tudelft.nl

†nhu@unimelb.edu.au

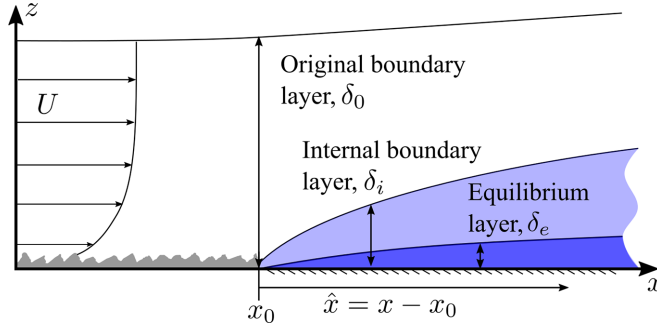


FIG. 1. Schematic of a turbulent boundary layer over a rough-to-smooth change in surface condition. The roughness transition occurs at x_0 , and $\hat{x} = x - x_0$ denotes the fetch downstream of the transition. Reproduced from Li *et al.* [38].

coexisting with large-scale low-speed regions, and vice versa in the case of large-scale high-speed regions. These observations were harnessed by the “two-scale” framework, where a local (near-wall) fine-mesh solution is coupled to the global coarse-mesh solution, to reduce computational costs at high Reynolds numbers [10,11]. In terms of the modeling efforts, quasisteady quasihomogeneous theory [12,13] provides an axiomatic description of the scale interaction in near-wall turbulence. The modulation effect was also quantified in recent works [14–18], and a predictive model, termed the inner-outer interaction model (IOIM), which outputs representative turbulence statistics in the near-wall region based on an input signal in the logarithmic region, was developed by Marusic and coworkers [19,20] and by Agostini and Leschziner [21]. The former was later revised by Baars *et al.* [22] using spectral linear stochastic estimation. The IOIM provides an opportunity to push the boundary of large-eddy simulations of wall-bounded flows to very high Reynolds numbers at affordable costs, thanks to its ability to provide representative real-time small-scale signals in the viscous-scaled near-wall region based only on large-scale outer-layer information [23–25].

Although similar amplitude modulation behaviours have been observed in turbulent boundary layers, channel, and pipe flows [26], the existence of such scale interactions is less extensively explored under noncanonical conditions. A sound understanding of how the inner- and outer-scale relationship is affected by these conditions is essential for generalising its application to a wider scope of flows. Enhanced amplitude modulation has been observed in various noncanonical flows, including boundary layers over rough walls [27–31] or permeable surfaces [32,33], and boundary layers with modified outer structures, such as energetic large-scale motions injected into the flow via freestream turbulence [34,35], upstream dynamic roughness [36] and synthetic large-scale signals generated by plasma actuators [37], to name a few. It is not yet well understood how these seemingly different flow conditions all lead to a common increase in the amplitude modulation coefficient, and we aim to bridge this gap by establishing a physics-based quantitative relationship between the amplitude modulation coefficient and IOIM parameters.

Furthermore, here we look into another scenario where the introduced large scales in the outer layer have an energy distribution across scales similar to that of a canonical boundary layer, and only the amplitude is intensified. This is achieved by a sudden rough-to-smooth surface transition occurring in the streamwise direction, as depicted in Fig. 1. Upstream of the transition, a turbulent boundary layer develops on a rough wall with equivalent sand grain roughness height k_s . Here, x is the streamwise direction, x_0 is the streamwise location of the surface transition and $\hat{x} \equiv x - x_0$ is the distance downstream of the transition. At $x = x_0$, the surface switches to a smooth wall, while the boundary layer continues to evolve and gradually adjusts to the new surface. The effect of the new surface condition is first felt in the near-wall region of the boundary layer and then gradually propagates to the interior of the flow [39]. The layer that separates the modified near-wall region from the unaffected oncoming flow farther away from the wall is generally referred to as the

internal boundary layer (IBL) with a thickness denoted by δ_i . For more details on the observation and modeling of the flow recovery, we refer to the works by Elliott [40], Antonia and Luxton [41], Hanson and Ganapathisubramani [42], Rouhi *et al.* [43], and Li *et al.* [44,45].

Turbulent boundary layers over a rough-to-smooth change in the streamwise direction offer a new perspective to further understand the physics of inner-outer interactions. When normalized by the friction velocity at the wall, LSMs and VLMS above δ_i are similar to their smooth-wall counterparts [46,47], but they are overenergized compared to the near-wall small scales. The former retain a memory of the upstream rough wall friction velocity whereas the latter scale on the much lower local smooth-wall friction velocity. How these structurally similar but more energized large-scale motions interact with the near-wall cycle will be investigated in this study.

The remainder of the paper is organized as follows: in Sec. II, we first present a summary of the definition of the amplitude modulation coefficient and the IOIM framework, as well as a quantitative relation between the two. We then review the previous studies on the amplitude modulation in noncanonical flows in Sec. III. In Sec. IV, we present a case study on the flow downstream of a rough-to-smooth change in the surface condition.

II. PHYSICAL UNDERPINNING OF AMPLITUDE MODULATION

In this section, we first briefly summarize the definition of the amplitude modulation coefficient R and the IOIM formulation, and then we provide a quantitative description of the relation between the two, supported by results computed from synthetic signals.

A. Amplitude modulation coefficient and IOIM formulation

The amplitude modulation coefficient R is a commonly reported diagnostic, largely due to the fact that it provides a straightforward quantification of the degree of amplitude modulation within a single-point time series. An example of the R profile is shown in Fig. 2(a). It is defined as the correlation between the low-pass-filtered envelope of small-scale fluctuations and the large-scale fluctuations at the same location [14]:

$$R(z^+) = \frac{\langle E_L[u_d^+(z^+, t^+)]u_s^+(z^+, t^+) \rangle}{\sqrt{\langle E_L^2[u_d^+(z^+, t^+)] \rangle} \sqrt{\langle u_s^{+2}(z^+, t^+) \rangle}}. \quad (1)$$

Here, the superscript $(\cdot)^+$ indicates inner scaling with the local friction velocity as the velocity scale, the angle brackets $\langle \cdot \rangle$ denotes time average, u represents the streamwise velocity, u_s^+ is the zero-mean large-scale superposition signal, which is usually obtained by low-pass filtering the time series with a threshold of $\lambda_x^+ = 7000$ and $u_d^+ \equiv u^+ - u_s^+$ is the detrended signal. $E_L[\cdot]$ denotes a low-pass-filtered envelope of the signal

$$E_L[u_d^+(z^+, t^+)] = \mathcal{L}[\sqrt{u_d^{+2}(z^+, t^+) + \mathcal{H}^2[u_d^+(z^+, t^+)]}], \quad (2)$$

where $\mathcal{H}[\cdot]$ is the Hilbert transform, $\sqrt{u_d^{+2}(z^+, t^+) + \mathcal{H}^2[u_d^+(z^+, t^+)]}$ is the analytic signal, and $\mathcal{L}[\cdot]$ denotes a low-pass filter.

The definition can be further generalized to a time-shifted amplitude modulation coefficient

$$R_\tau(z^+, \tau^+) = \frac{\langle E_L[u_d^+(z^+, t^+)]u_s^+(z^+, t^+ - \tau^+) \rangle}{\sqrt{\langle E_L^2[u_d^+(z^+, t^+)] \rangle} \sqrt{\langle u_s^{+2}(z^+, t^+) \rangle}}. \quad (3)$$

By definition, $R(z^+) \equiv R_\tau(z^+, 0)$ [see Fig. 2(b)]. The relative shift τ_a^+ is the lag between the superposition imprint u_s^+ and the low-pass filtered envelope $E_L[u_d^+]$ such that R_τ reaches its maximum, i.e., $R_\tau(z^+, \tau_a^+) = \max[R_\tau(z^+, \tau^+)]$, as marked by the solid circles in Fig. 2(b).

According to the IOIM [22], the statistical prediction of the fluctuating velocity u_p^+ can be constructed by considering a superposition effect of large-scale content with additively a universal

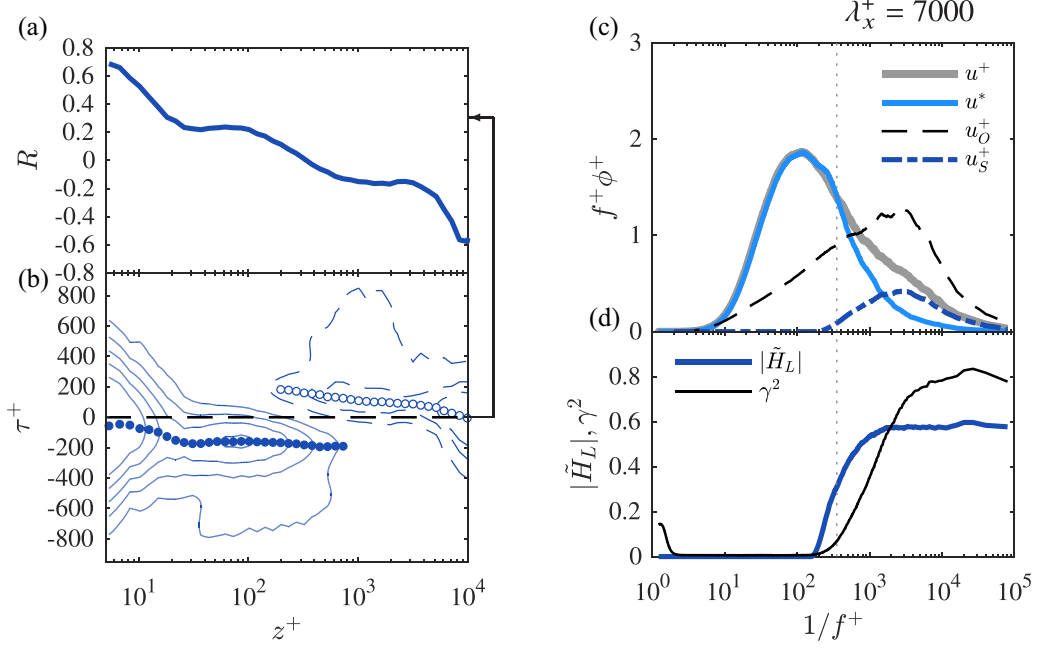


FIG. 2. (a) Amplitude modulation coefficient $R(z^+)$ [Eq. (1)] of a smooth-wall turbulent boundary layer with $\text{Re}_\tau = 1.3 \times 10^5$ [48]. (b) Isocontour of the time-shifted amplitude modulation coefficient $R_\tau(z^+, \tau^+)$ [Eq. (3)] of the same boundary layer profile. The solid contour lines are from 0.1 to 0.5 with a step of 0.1, and the dashed contour lines are from -0.3 to -0.1 with a step of 0.1. The solid and filled circles mark the τ^+ values where R_τ reaches its maximum and minimum at each wall-normal location, respectively. (c) Premultiplied energy spectra of the measured velocity u^+ , universal small scales u^* and superposition u_S^+ at $z^+ \approx 10$, and u_O^+ , the velocity measured by the outer probe at $z_O^+ = 469$. (d) The gain of the linear kernel $|\tilde{H}_L|$ and the linear coherence spectrum $\gamma^2(f^+)$ at $z^+ \approx 10$. The vertical dotted line in panels (c) and (d) marks the cutoff wavelength $\lambda_x^+ = 7000$ (with the mean velocity at the outer probe as the convective velocity) used by Mathis *et al.* [20] to separate large and small scales.

signal u^* that is subject to an amplitude modulation

$$u_p^+(z^+, t^+) = \underbrace{u^*(z^+, t^+) \{1 + \Gamma(z^+) u_S^+(z^+, t^+ - \tau_a^+)\}}_{\text{amplitude modulation}} + \underbrace{u_S^+(z^+, t^+)}_{\text{superposition}}. \quad (4)$$

Here, Γ is the amplitude sensitivity, and the large-scale imprints u_S^+ can be found from a given outer-layer large-scale signal $u_O^+(t^+)$ via

$$u_S^+(z^+, t^+) = \mathcal{F}^{-1} \{ \tilde{H}_L(z^+, f^+) \mathcal{F}[u_O^+(t^+)] \}, \quad (5)$$

where $\mathcal{F}[\cdot]$ and $\mathcal{F}^{-1}[\cdot]$ represent a Fourier transform and inverse Fourier transform, respectively, and $\tilde{H}_L(f^+)$ is the linear transfer kernel incorporating the large-scale coherence between the near-wall and outer regions.

The gain of the linear kernel $|\tilde{H}_L|$ is related to the linear coherence spectrum $\gamma^2(f^+)$ via

$$|\tilde{H}_L(f^+)| = \sqrt{\gamma^2(f^+) \frac{\langle |\mathcal{F}[u^+]|^2 \rangle}{\langle |\mathcal{F}[u_O^+]|^2 \rangle}}, \quad (6)$$

where $\gamma^2(f^+)$ is given by Bendat and Piersol [49]

$$\gamma^2(f^+) = \frac{|\mathcal{F}[u_O^+]\overline{\mathcal{F}[u^+]}|^2}{\langle |\mathcal{F}[u_O^+]|^2 \rangle \langle |\mathcal{F}[u^+]|^2 \rangle}, \quad (7)$$

with $\overline{(\cdot)}$ denoting the complex conjugate.

As shown in Figs. 2(c) and 2(d), only the large-scale energy of the outer velocity signal u_O^+ is retained in the superposition signal u_S^+ , which contributes to the large-scale end of the energy spectrum of u^+ . The small-scale end of the spectrum, however, is mainly from the universal small scale, u^* . The linear transfer kernel $|\tilde{H}_L|$ enables a smooth roll-off of the coherence from large to small scales, and the scale separation here is around the commonly used cutoff threshold of $\lambda_x^+ = 7000$.

B. Quantitative relationship between R and IOIM parameters

In this subsection, we derive a quantitative relationship of the amplitude modulation coefficient by expressing R in the framework of IOIM. Following Duvvuri and McKeon [36], we work with a modified expression of the amplitude modulation coefficient

$$R_2(z^+) = \frac{\langle E_{2L}[u_d^+(z^+, t^+)]u_S^+(z^+, t^+) \rangle}{\sqrt{\langle E_{2L}^2[u_d^+(z^+, t^+)] \rangle} \sqrt{\langle u_S^{+2}(z^+, t^+) \rangle}}, \quad (8)$$

where

$$E_{2L}[v(t^+)] = \mathcal{L}\{v^2(t^+) + \mathcal{H}^2[v(t^+)]\} \quad (9)$$

for an arbitrary time series $v(t^+)$. The modified coefficient R_2 uses the square of the analytic signal to avoid the difficulty in dealing with the square root in Eq. (2), leading to a simpler mathematical expression, and given that the amplitude modulation coefficient is a normalized measure, no significant difference is expected in the values of R and R_2 . This can be easily verified using experimental data.

By expressing the velocity signals u_d^+ and u_S^+ in a series of Fourier modes, and with some trigonometric manipulations, Duvvuri and McKeon [36] showed that

$$R_2 = \frac{2\langle u_d^{+2}u_S^+ \rangle}{\sqrt{\langle E_{2L}^2[u_d^+] \rangle} \sqrt{\langle u_S^{+2} \rangle}}. \quad (10)$$

We substitute the detrended signal expressed using the notations of IOIM (i.e., $u_d^+ = u^*[1 + \Gamma u_S^+(t^+ - \tau_a^+)]$) into Eq. (10) and noting that $\langle u^{*2}u_S^+ \rangle = 0$ because u^* is not modulated by u_S^+ by definition (the universal small-scale signal u^* is constructed by removing the modulation between u^* and u_S^+ ; see, for example, Ref. [20]). R_2 can then be expressed as

$$R_2 = \frac{4\Gamma\langle u^{*2} \rangle \langle u_S^+(t^+)u_S^+(t^+ - \tau_a^+) \rangle + 2\Gamma^2\langle u^{*2} \rangle \langle u_S^+(t^+)u_S^{+2}(t^+ - \tau_a^+) \rangle}{\sqrt{\langle \{E_{2L}[u^*] + 2\Gamma\mathcal{L}[u^{*2}u_S^+ + \mathcal{H}[u^*]\mathcal{H}[u^*u_S^+]] + \Gamma^2E_{2L}[u^{*2}u_S^+]\}^2 \rangle} \sqrt{\langle u_S^{+2} \rangle}}. \quad (11)$$

Comparing the orders of u^* , u_S^+ and Γ in the terms in the denominator of Eq. (11) and noting that both $\mathcal{L}[\cdot]$ and $\mathcal{H}[\cdot]$ are linear operators give rise to

$$E_{2L}[u^*] \sim \langle u^{*2} \rangle, \quad (12a)$$

$$\Gamma\mathcal{L}[u^{*2}u_S^+ + \mathcal{H}[u^*]\mathcal{H}[u^*u_S^+]] \sim \Gamma\langle u_S^{+2} \rangle^{1/2} \langle u^{*2} \rangle, \quad (12b)$$

$$\Gamma^2E_{2L}[u^*u_S^+] \sim \Gamma^2\langle u_S^{+2} \rangle \langle u^{*2} \rangle. \quad (12c)$$

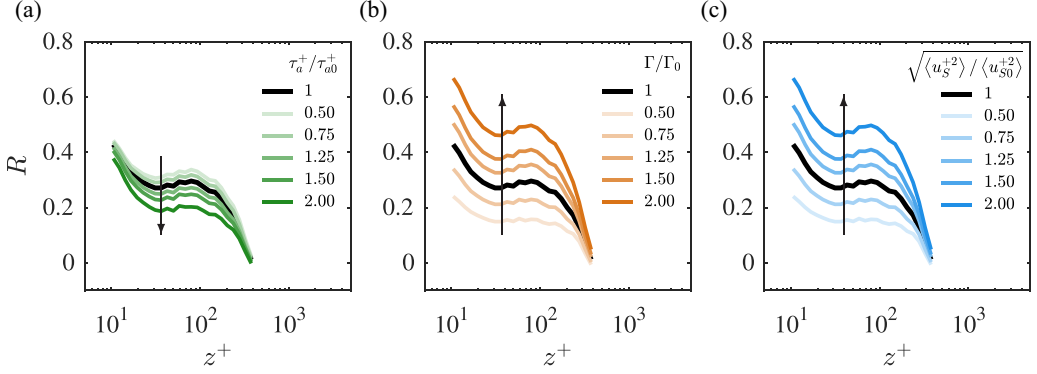


FIG. 3. Amplitude modulation coefficient R of the velocity signal constructed with various (a) τ_a^+ , (b) Γ , and (c) $\langle u_s^{+2} \rangle$ values. The baseline parameters are denoted by τ_{a0}^+ , Γ_0 , and $\langle u_{s0}^{+2} \rangle$, respectively, and they are computed from the dataset at $\text{Re}_\tau = 13\,300$ in Baars *et al.* [22]. The arrows in the panels indicate the direction of increasing the ratio between the varied parameter and the baseline.

Typically, Γ is a relatively small number ranging from $\mathcal{O}(0.01)$ to $\mathcal{O}(0.10)$ [22], and $\langle u_s^{+2} \rangle < \langle u^{*2} \rangle$ especially in the near-wall region of $z^+ \lesssim 200$ which is the current focus. Therefore, terms containing higher orders of $\Gamma \langle u_s^{+2} \rangle^{1/2}$ can be neglected, and Eq. (11) is then reduced to

$$R_2 \approx \frac{4\Gamma \langle u^{*2} \rangle \langle u_s^+(t^+) u_s^+(t^+ - \tau_a^+) \rangle}{\sqrt{E_{2L}^2[u^*]} \sqrt{\langle u_s^{+2} \rangle}}. \quad (13)$$

We identify the following three parameters that can contribute to a change in R_2 :

- (1) The relative shift τ_a^+ .
- (2) The amplitude sensitivity Γ .
- (3) The amplitude of large-scale imprints $\langle u_s^{+2} \rangle$.

Interestingly, R_2 is not affected by changes in the amplitude of universal small scales $\langle u^{*2} \rangle$. This is because both the numerator and the denominator in Eq. (11) [and Eq. (13) as well] contain the same order of $\langle u^{*2} \rangle$, which eventually cancel out. Note that changes in the energy distribution across scales in u_s^+ or u^* have more complicated consequences: for u_s^+ , it will affect the autocorrelation term $\langle u_s^+(t^+) u_s^+(t^+ - \tau_a^+) \rangle$ with a given τ_a^+ , and for u^* , it will affect how much energy remains in $E_{2L}[u^*]$ after a low-pass filter is applied. Therefore, we limit the quantitative analysis to changes in the amplitude of u_s^+ and u^* fluctuations.

In canonical smooth-wall turbulent boundary layers, the IOIM parameters (u^* , Γ , τ_a^+ , and \tilde{H}_L) are Reynolds number invariant over the range of $\text{Re}_\tau \approx 7350$ – $13\,300$ tested in the calibrations [50], and only a change in the large-scale imprint amplitude $\langle u_s^{+2} \rangle$ was observed when varying the Reynolds number. However, τ_a^+ , Γ , and $\langle u_s^{+2} \rangle$ can all be modified under noncanonical conditions, and it is important to understand how they individually contribute to the overall amplitude modulation coefficient R .

1. Effect of the relative shift τ_a^+

We can conclude from Eq. (13) that R_2 would increase with a decreasing $|\tau_a^+|$, as a result of reduced time lag, or improved alignment between modulation and superposition signals. Typically, the relative shift τ_a^+ is much smaller than the time period of u_s^+ below the center of the log region, where the predictive model is applied. Therefore, $u_s^+(t^+)$ and $u_s^+(t^+ - \tau_a^+)$ are largely in phase. The autocorrelation term $\langle u_s^+(t^+) u_s^+(t^+ - \tau_a^+) \rangle$ is positive, and increases with a decreasing $|\tau_a^+|$.

Figure 3(a) shows R [Eq. (1)] computed from the velocity signals constructed from u^* and u_s^+ with a range of different τ_a^+ values following Eq. (4). The IOIM parameters and the baseline values

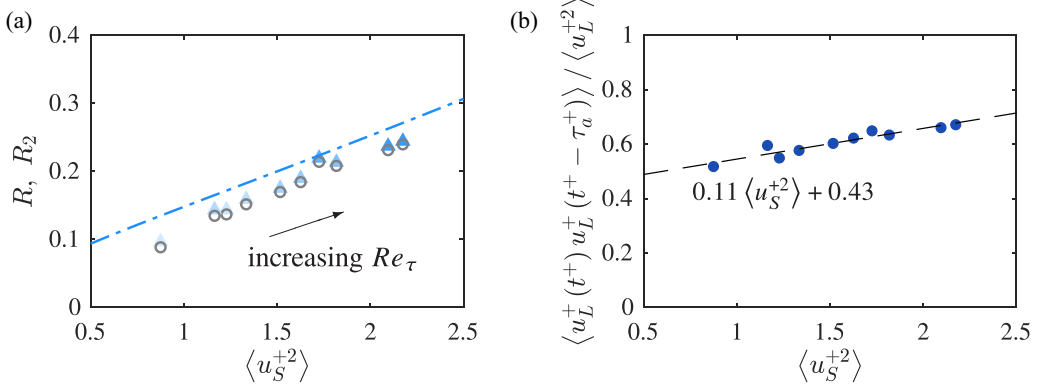


FIG. 4. (a) Amplitude modulation coefficients R (gray circles) and R_2 (blue triangles) computed from the experimental data of a canonical smooth-wall turbulent boundary layer and plotted against the corresponding superposition signal intensity $\langle u_s^{+2} \rangle$ at $z^+ = 50$. From pale to dark blue, the shade of blue triangles indicates Re_τ increasing from 2800 to 13 400. The dot-dashed blue line is Eq. (13) with the autocorrelation term $\langle u_s^+(t^+) u_s^+(t^+ - \tau_a^+) \rangle / \langle u_s^{+2} \rangle$ estimated from a fit of the experimental data. (b) Autocorrelation of u_L^+ , low-pass filtered streamwise velocity fluctuations from experimental data, at $z^+ = 50$.

of τ_{a0}^+ , Γ_0 , and $\langle u_{s0}^{+2} \rangle$ are taken from the dataset at $Re_\tau = 13\,300$ [22]. The decreasing trend of R with an increasing $|\tau_a^+|$ confirms the conclusion based on Eq. (13).

2. Effect of the amplitude sensitivity Γ

According to Eq. (13), R_2 will increase with an increasing Γ . This trend is corroborated by the increasing R computed from the signals constructed following Eq. (4) with an increasing Γ/Γ_0 [see Fig. 3(b)].

3. Effect of the superposition intensity $\langle u_s^{+2} \rangle$

Based on Eq. (13), R_2 will increase with an increasing $\langle u_s^{+2} \rangle$. In fact, a closer examination of Eqs. (13) and (11) reveals that Γ and $\langle u_s^{+2} \rangle$ can be grouped into a single variable $\Gamma \langle u_s^{+2} \rangle^{1/2}$. This is confirmed by the same trends of R with Γ and $\langle u_s^{+2} \rangle^{1/2}$ in Figs. 3(b) and 3(c), respectively. We note that the monotonic increase of R_2 with $\Gamma \langle u_s^{+2} \rangle^{1/2}$ breaks down when $\Gamma \langle u_s^{+2} \rangle^{1/2}$ becomes comparable with or larger than $\langle u^{*2} \rangle^{1/2}$ (not shown in the figure), and the full expression of Eq. (11) can introduce nonmonotonic dependence on $\Gamma \langle u_s^{+2} \rangle^{1/2}$. However, given that Γ is typically small, and $\langle u_s^{+2} \rangle$ is much smaller than $\langle u^{*2} \rangle$ in the near-wall region at the Reynolds number range investigated in the experimental dataset ($Re_\tau \lesssim 2 \times 10^4$), the nonmonotonic is less likely to occur.

To summarize, we have shown analytically that the amplitude modulation coefficient will increase with (i) a reducing $|\tau_a^+|$, (ii) an increasing Γ , and (iii) an increasing $\langle u_s^{+2} \rangle$, provided $\Gamma \langle u_s^{+2} \rangle^{1/2} \ll \langle u^{*2} \rangle^{1/2}$.

C. Verification with a smooth-wall turbulent boundary layer dataset

The analysis above is verified using an experimental smooth-wall turbulent boundary layer dataset with Re_τ ranging from 2800 to 13 400 [48]. In this series of canonical smooth-wall boundary layer profiles, both τ_a^+ and Γ are expected to remain constant, and only $\langle u_s^{+2} \rangle$ increases with an increasing Re_τ as a consequence of more energetic large-scale motions in the outer layer, providing an ideal test ground to examine the dependence of R on $\langle u_s^{+2} \rangle$. Figure 4(a) shows the amplitude modulation coefficients R and R_2 computed directly from the velocity time series. The large-scale imprint intensity $\langle u_s^{+2} \rangle$ is approximated by $\langle u^{+2} \rangle - \langle u^{*2} \rangle$, where $\langle u^{*2} \rangle$ is the intensity

of the universal small-scale signal from the calibration data of Baars *et al.* [22]. The large-scale imprint intensity $\langle u_S^{+2} \rangle$ increases with an increasing Re_τ as expected. The two coefficients R and R_2 have very similar values, and they exhibit an increasing trend with $\langle u_S^{+2} \rangle$, which is well captured by Eq. (13). The autocorrelation term $\langle u_S^+(t^+)u_S^+(t^+ - \tau_a^+) \rangle / \langle u_S^{+2} \rangle$ in Eq. (13) is smaller than 1 for a finite time shift τ_a^+ , but the exact value needs to be determined from the time series of u_S^+ . The autocorrelation term at $z^+ = 50$ can be estimated from the low-pass filtered experimental data (i.e., $\langle u_S^+(t^+)u_S^+(t^+ - \tau_a^+) \rangle / \langle u_S^{+2} \rangle \approx \langle u_L^+(t^+)u_L^+(t^+ - \tau_a^+) \rangle / \langle u_L^{+2} \rangle$ with threshold $\lambda_x^+ = 7000$ for the low-pass filter) and is observed to increase slightly from the lowest to the highest Re_τ measurements [Fig. 4(b)], because the relative phase shift $|\tau_a^+|U^+/\lambda_S^+$ reduces with increasing Re_τ , with $|\tau_a^+|$ remaining constant and λ_S^+ , the most energetic wavelengths of u_S^+ , growing with the boundary layer thickness $\delta^+ (\equiv \text{Re}_\tau)$. This increasing trend in $\langle u_L^+(t^+)u_L^+(t^+ - \tau_a^+) \rangle / \langle u_L^{+2} \rangle$ can be approximated by a linear fit of $0.11\langle u_S^{+2} \rangle + 0.43$ as shown by the black dashed line. With the autocorrelation term approximated by the linear fit, the prediction of Eq. (13) [dot-dashed blue line in Fig. 4(a)] captures the trend of data points with a small error of less than 10% of the local R_2 value, which is mainly attributed to the potential difference between $\langle u_S^+(t^+)u_S^+(t^+ - \tau_a^+) \rangle / \langle u_S^{+2} \rangle$ and $\langle u_L^+(t^+)u_L^+(t^+ - \tau_a^+) \rangle / \langle u_L^{+2} \rangle$. In summary, the increase in R and R_2 with increasing Re_τ for a canonical smooth-wall turbulent boundary layer is primarily originated from the growing $\langle u_S^{+2} \rangle$, and the slight increase in the autocorrelation term also makes a small contribution to the growth.

III. REVISITING SCALE INTERACTIONS IN PREVIOUS STUDIES

In this section, we present a summary of data from the literature and the current work, focusing on how the IOIM parameters change in various flow types and with increasing Re_τ , and discuss their commonalities and differences in the scale interaction mechanism.

The IOIM parameters reported in previous studies of various flow conditions are summarized in Table I. Notably, almost all noncanonical flows collected in the table exhibit a higher positive amplitude modulation coefficient R in the near-wall region. Further analysis of the IOIM parameters reveals that the increase in R is contributed by different mechanisms. For rough-wall flows, although the strength of $\langle u_O^{+2} \rangle$ is similar to that of a smooth-wall boundary layer, the coherence between the inner and outer layer is reduced, presumably due to the disruption of shedded vortices in the roughness sublayer. The small-scale fluctuations arise from wake vortices generated by roughness elements, the intensity of which is proportional to u_S . Therefore, the modulation sensitivity Γ in rough-wall flows is stronger than that in smooth-wall flows [28], which leads to a higher positive R . Similarly, the near-wall region of a permeable substrate is dominated by upwelling/downwelling associated with the large-scale streamwise motions [32,33], resulting in an increase in R in the near-wall region as well. Considering that for both rough and permeable substrates, the deviation from a canonical flow is introduced near to the wall, whereas the outer layer remains largely unchanged under correct scaling, these flows can be classified as the “bottom-up” category.

The common feature that links boundary layers with an increasing Re_τ , freestream turbulence, an upstream dynamic roughness element or a R -to- S change in the wall condition (Sec. IV) is that more energetic large scales are introduced in the outer layer, while the near-wall cycle (represented by the intensity of u^*) remains largely unaltered. These flows are classified as the “top-down” category in the context of large-scale modulation. The coherence between large scales in the inner and outer regions, which manifests in $|\tilde{H}_L|$, either remains the same (canonical smooth wall with increasing Re_τ), or increases (freestream turbulence, R -to- S change), and they both lead to stronger footprints $\langle u_S^{+2} \rangle$ close to the wall. The stronger $\langle u_S^{+2} \rangle$ is primarily responsible for the increased R in the “top-down” flow cases.

In summary, based on whether the near-wall cycle is modified from that of an impermeable smooth wall, various flow types collected in Table I can be further classified as “top-down” and “bottom-up” categories, which indicates whether the deviation from a canonical flow is introduced in the outer layer or near to the wall. However, we note that more complex flows, such as turbulent

TABLE I. Summary of IOIM parameters in various flow types. Quantities that cannot be inferred from the reported results are marked by “?”. Changes in the parameters are relative to a smooth-wall turbulent boundary layer at comparable Reynolds numbers. In the category of smooth-wall boundary layers with increasing Reynolds numbers, the comparison is made with regard to a lower Reynolds number. Results of the current study will be presented in details in Sec. IV.

	Flow type	Reference	$\langle u_o^{+2} \rangle$	$\langle u_s^{+2} \rangle$	$ \tilde{H}_L $	$\langle u^{*2} \rangle$	Γ	R (near wall)
top-down	R -to- S change	present study	higher	higher	higher	similar	similar	higher
	Smooth wall, increasing Re_τ	Mathis <i>et al.</i> [14,20] Baars <i>et al.</i> [22]	higher	higher	similar	similar	similar	higher
	Freestream turbulence	Dogan <i>et al.</i> [34,35]	higher	higher	higher	similar	lower	higher
	Single frequency large-scale input	Duvvuri and McKeon [36] Squire <i>et al.</i> [28] Anderson [29]	higher	higher	?	similar	?	?
bottom-up	Rough wall	Pathikonda and Christensen [53] Blackman <i>et al.</i> [31]	similar	lower	lower	dependent on roughness morphology	higher	higher
		Efstathiou and Luhar [54] Kim <i>et al.</i> [32]	similar/lower	?	?	dependent on substrate morphology	?	higher
	Permeable wall	Mathis <i>et al.</i> [51] Harun <i>et al.</i> [55] Drózdź <i>et al.</i> [56]	lower higher	lower higher	similar lower	lower/similar higher	lower lower	similar higher

boundary layers subjected to nonzero pressure gradients [51], do not fit either category in the classification because both the near-wall modulation mechanism and outer-layer large-scale motions are modified. Moreover, the work by Andreolli *et al.* [52] reaches a conclusion that is worth investigating further in the future, e.g., that when amplitude modulation is artificially blocked, large-scale superposition also ceases to exist. This may suggest that the IOIM parameters are interconnected, although in the present paper we treat them independently and focus on their contribution to the overall modulation effect.

IV. CASE STUDY: TURBULENT BOUNDARY LAYER FOLLOWING A STEP CHANGE IN SURFACE ROUGHNESS

In this section, we present the new experimental results of a turbulent boundary layer downstream of a rough-to-smooth change in the surface conditions, which is another noncanonical flow configuration in the “top-down” category. We will present the experimental conditions in Sec. IV A, and then explore the detailed modulation behaviours using both single-probe and two-probe results in Secs. IV B–IV C. The results are briefly discussed in Sec. IV D.

A. Experimental setup

Simultaneous two-probe hotwire anemometry measurements are performed in the high Reynolds number boundary layer wind tunnel (HRNBLWT) at the University of Melbourne. An upstream portion of the 27 m working section floor is covered by P24 sandpaper (SP40F, Awuko Abrasives) from the inlet to $x_0 = 7.2$ m, while the remaining length is a smooth aluminium surface. The peak-to-trough roughness height is $k_p \approx 1.2$ mm, and the equivalent sand grain roughness is $k_s \approx 2.43$ mm. A nominal zero-pressure gradient is achieved by adjusting the bleeding slots on the tunnel roof. More details of the facility can be found in Refs. [44,57].

Two-probe hotwire measurements are performed at two freestream velocities, 22.5 m s^{-1} and 31.0 m s^{-1} , and these two cases are named as *R-to-S1* and *R-to-S2*, respectively. The flow conditions of these cases correspond to the single-point dataset of cases Re10ks16 and Re14ks22 in Ref. [44], and the local friction velocity U_τ of the current cases is interpolated from the skin-friction versus \hat{x} trajectory in the same study, which was measured directly at the wall using oil-film interferometry. The procedures of the two-probe hotwire anemometry measurements are similar to that described by Mathis *et al.* [20] and Baars *et al.* [22]. The outer probe is fixed at $z_O^+ = 3.9\sqrt{\text{Re}_\tau}$, which is the geometric center of the logarithmic region where the large-scale motions are highly active. The inner probe is traversed from the wall to below the outer probe with approximately 20 logarithmically spaced points in between. Both probes are conventional single-wire hotwire probes with a Wollaston wire etched to expose the sensing element. The length-to-diameter ratio of the exposed filament is $l/d \geq 200$ [58]. For the case *R-to-S1*, both wires have a diameter of $d = 2.5 \mu\text{m}$, leading to a viscous-scaled filament length of $l_I^+, l_O^+ \approx 21$. For the case *R-to-S2*, $d = 1.5 \mu\text{m}$ wire is selected for the inner probe to maintain a similar spatial resolution with $l_I^+ \approx 19$ with an increased freestream (and friction) velocity, while the outer probe filament diameter remains $d = 2.5 \mu\text{m}$ because only the large-scale signal at this location is of the interest. Both probes are conventional single-wire hotwire probes operated by an in-house Melbourne University constant temperature anemometer (MUCTA). The hotwire sampling time T_s is more than 20 000 boundary layer turn-over time (δ_{99}/U_∞) to achieve a good convergence of the statistics. A two-probe smooth-wall dataset from Mathis *et al.* [20] and Baars *et al.* [22] is also included for comparison in this study. Parameters of the two-point measurements are summarized in Table II.

B. Single-probe results

We first present the evolution of the mean velocity and turbulence statistics downstream of the rough-to-smooth change in Fig. 5. Generally speaking, immediately after the rough-to-smooth change, the rough-wall turbulent boundary layer starts adapting to the new surface conditions first at

TABLE II. Experimental parameters of the two-point hotwire measurements, where the outer probe remains at a fixed location z_O^+ and the inner probe is traversed between $[0, z_O^+]$. l_i^+ and l_O^+ are the viscous-scaled hotwire filament length of the inner and outer probes, respectively.

Case	Color	\hat{x}/δ_0	Re_τ	$3.9\sqrt{Re_\tau}$	U_∞ (ms^{-1})	U_τ (ms^{-1})	z_O^+	δ_i^+	l_i^+	l_O^+
Smooth	black	—	7350	334	10.0	0.34	441	—	22	22
<i>R</i> -to- <i>S</i> 1	green	2.3	7200	330	22.5	0.69	331	890	21	21
<i>R</i> -to- <i>S</i> 2	magenta	2.3	9600	382	31.0	0.92	388	1180	19	31

the wall, and as the modified region enlarges, to the interior of the flow. The skin-friction coefficient experiences an undershoot before gradually increasing to the smooth-wall value. Figure 5(a) shows the inner-scaled mean velocity profiles, where the velocity scale is selected as the friction velocity U_τ measured locally with oil-film interferometry over the smooth surface. Note that in this paper, the superscript $(\cdot)^+$ indicates inner scaling with the local friction velocity as the velocity scale. Figure 5(b) shows the outer-scaled profiles, where the velocity scale is chosen as the friction velocity $U_{\tau 0}$ measured on the rough wall just upstream of the rough-to-smooth transition at $\hat{x} \rightarrow 0^-$. The inner-scaled mean velocity profiles of Fig. 5(a) collapse with the smooth-wall reference first close to the wall, while the outer-scaled profiles in Fig. 5(b) agree well with the rough-wall reference above the IBL (marked by the open circles). In the turbulence intensity profiles, a strong “outer-peak” manifests at the IBL, which is a result of the remaining energetic rough-wall structures. These

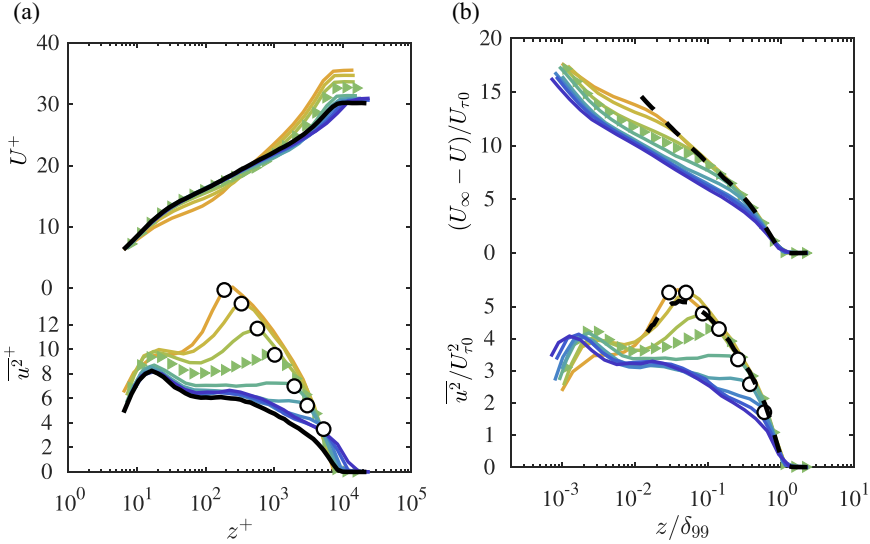


FIG. 5. Profiles of mean streamwise velocity and turbulence intensity corresponding to the flow conditions of *R*-to-*S*1. (a) is inner scaled using the local smooth-wall U_τ , while (b) is outer scaled, but using $U_{\tau 0}$, the friction velocity measured just upstream of the rough-to-smooth transition. Line colors indicate the fetch, from orange to green to blue corresponds to $\hat{x}/\delta_0 = 0.2, 0.5, 0.9, 1.9, 4.2, 7.4, 14.8, 29.2$, and 53.1 . The solid black line is a smooth-wall reference with $Re_\tau = 1.0 \times 10^4$ acquired in the same facility and normalized using the corresponding smooth-wall friction velocity [48], and dashed black line is a rough-wall reference acquired just upstream of the rough-to-smooth change and normalized by the rough-wall friction velocity. The white circles represent the edge of the IBL, determined from the variance profile [44]. The profile highlighted by triangular symbols is close to the streamwise location where the two-probe measurements in this study are performed.

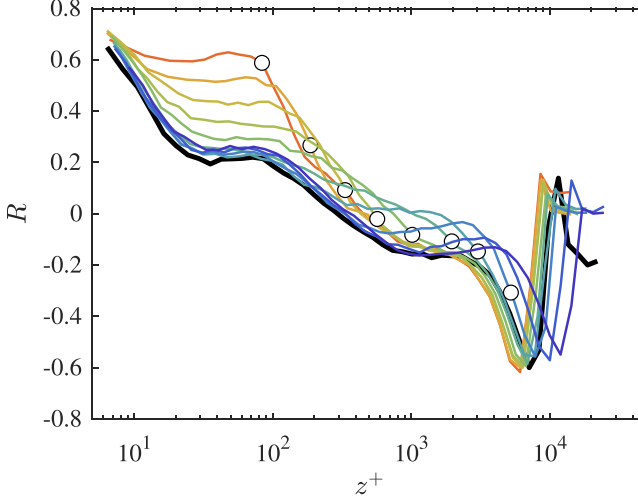


FIG. 6. Amplitude modulation coefficient R at various streamwise locations downstream of a rough-to-smooth change. Line colors indicate the fetch, from red to blue corresponds to $\hat{x}/\delta_0 = 0.08, 0.2, 0.5, 0.9, 1.9, 4.2, 7.4, 14.8, 29.2$, and 53.1 . The white circles represent the edge of the IBL. The solid black line is a smooth-wall reference with $\text{Re}_\tau = 1.0 \times 10^4$ [48].

structures leave a strong footprint in the near-wall region, as evidenced by the increased inner-peak magnitude in wall units shown in Fig. 5(a). The case R -to- $S2$ has a higher $\text{Re}_{\tau 0}$ and k_{s0}^+ compared to the case R -to- $S1$, thus, stronger large-scale motions (which scale on $U_{\tau 0}$) above the internal boundary layer are expected in the former. The amplitude modulation coefficient R [Eq. (1)] at a range of downstream locations from $\hat{x}/\delta_0 = 0.08$ to 53.1 is shown in Fig. 6. The cutoff wavelength of the large-scale filter $\mathcal{L}[\cdot]$ is computed using the local friction velocity. Only the results of R -to- $S1$ are presented here for brevity, while the R -to- $S2$ case shows similar behavior. At small \hat{x}/δ_0 , a high R is observed in the near-wall region. The coefficient R decreases with an increasing \hat{x}/δ_0 , and beyond $\hat{x}/\delta_0 > 20$, it becomes very similar to that of a smooth-wall boundary layer in the near wall region.

Isocontours of R_τ [Eq. (3)] at $\hat{x}/\delta_0 = 0.2$ (orange) and 0.9 (green) are shown in Fig. 7. In addition to the difference in the magnitude, at small fetches, the contours of positive correlations also shifts to the positive τ^+ direction. In other words, close to the rough-to-smooth change, there is a smaller time lag between the envelope of the small-scale fluctuations and large-scale motions. The optimal positive correlation achieved at the time shift τ_a^+ is shown in Fig. 7(d). Similar to the zero-time-shift R (shown in Fig. 6), the maximum R_τ values are also higher at smaller fetches, implying that the high magnitudes of R observed in Fig. 6 is more than the consequence of a smaller lag between the envelope and large-scale motions.

A comparison of τ_a^+ (time shift required for the optimum positive correlation) can be found in Fig. 8(a), where τ_a^+ becomes more negative with an increasing fetch. Figure 8(b) shows the argument of the complex cospectrum ϕ at $z^+ = 50$, premultiplied by the time period $1/f^+$, following Jacobi and McKeon [59,60] and Deshpande *et al.* [61]. The cospectrum is defined as $\phi \equiv \langle \mathcal{F}[u_s^+] \overline{\mathcal{F}[E_L[u_d^+]]} \rangle$, and it can be viewed as the spectral equivalent of the amplitude modulation coefficient R . The premultiplied argument $\tau_a^+(f^+) \equiv \arg(\phi)/(2\pi f^+)$ is essentially the time shift between u_s^+ and $E_L[u_d^+]$ in each Fourier mode, and it is reasonable that the overall time shift τ_a^+ falls in the same range as $\tau_a^+(f^+)$ at each corresponding measurement location. In addition, the increase of the time lag with increasing fetch is also apparent here, confirming the trend of τ_a^+ in Fig. 8(a). Further, the absolute time lag $|\tau_a^+(f^+)|$ is smaller at higher frequencies, meaning that the amplitude of small scales are more in-phase with the higher-frequency modes of the large scales. The increased maximum R_τ values at smaller fetches can partially be explained by the smaller scatter of $\tau_a^+(f^+)$

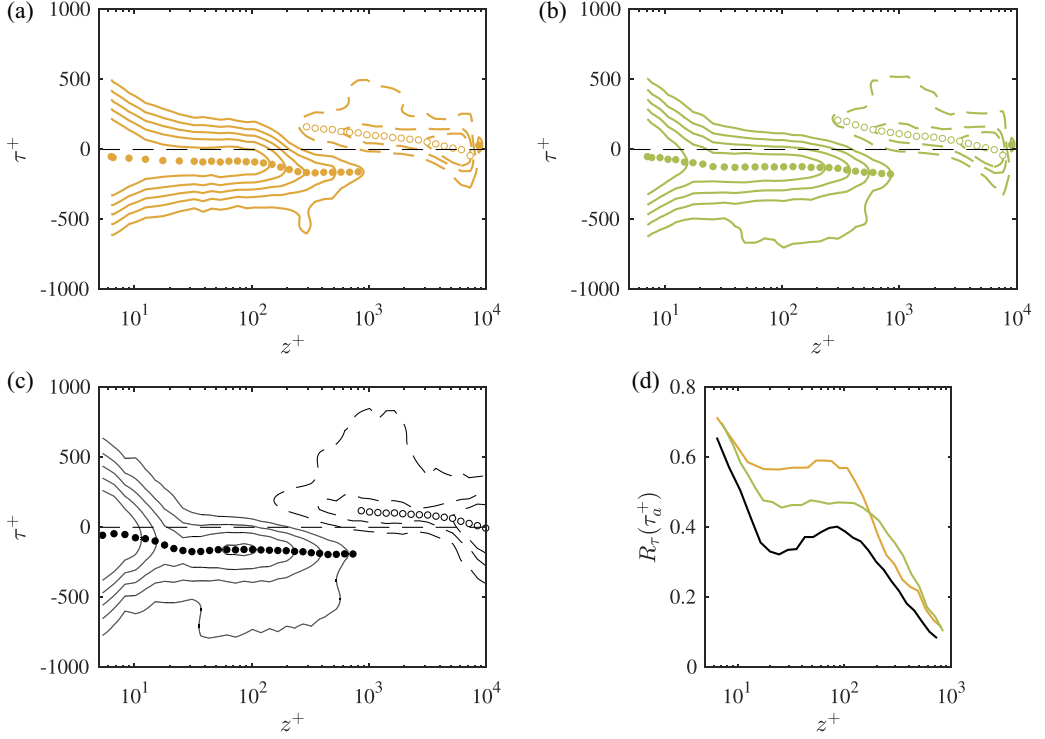


FIG. 7. (a) Isocontours of R_τ at $\hat{x}/\delta_0 = 0.2$ (a, orange) and 0.9 (b, green) and the smooth-wall reference (c, black). The solid contour lines are from 0.1 to 0.5 with a step of 0.1 , and the dashed contour lines are from -0.3 to -0.1 with a step of 0.1 . The solid and empty circles mark the τ^+ values where R_τ reaches its maximum and minimum at each wall-normal location, respectively. (d) Maximum R_τ values, which are essentially R_τ at the locations marked by solid circles in panels (a)–(c).

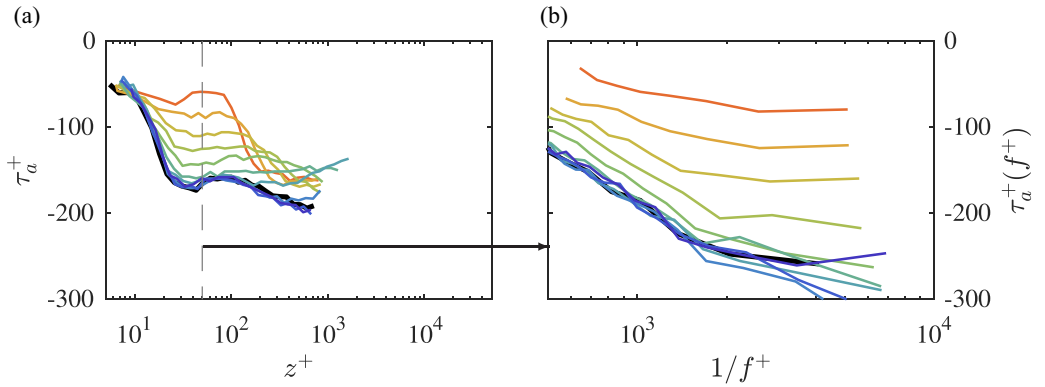


FIG. 8. (a) Time shift required for R_τ to reach its maximum. (b) Argument of the complex cospectrum of u_s^+ and $E_L[u_d^+]$ at $z^+ = 50$ (marked in panel (a) by the vertical dashed line), premultiplied by the time period $1/f^+$. Legends are the same as in Fig. 6. The solid black line is a smooth-wall reference with $\text{Re}\tau = 1.3 \times 10^4$ [48].

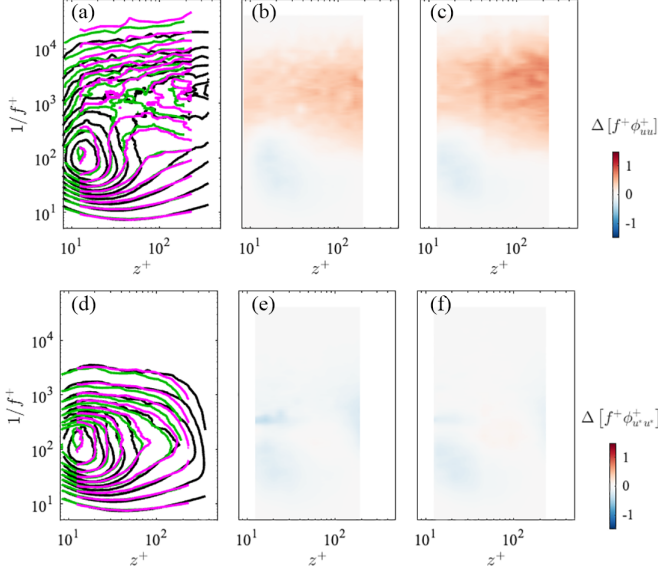


FIG. 9. Premultiplied spectra of (a) u^+ and (d) u^* . The contour levels in both plots are from 0.2 to 2 with a spacing of 0.2. Line colors black, green, and magenta represent the smooth, R -to- $S1$, and R -to- $S2$ cases, respectively. Panels (b) and (c) are the difference in $f^+\phi_{uu}^+$ between the R -to- $S1$ and R -to- $S2$ cases and the smooth-wall reference, and panels (e) and (f) are the corresponding difference in $f^+\phi_{u^*u^*}^+$.

across a range of frequencies, because a single time shift τ_a^+ can better align all Fourier modes in the u_S^+ and $E_L[u_d^+]$ signals in these cases.

The increase in R compared to the smooth-wall reference has been previously observed in rough-wall flows and attributed to the stronger correlation between the amplitude of the small-scale turbulence associated with the roughness elements and the large-scale motions [28]. Compared to the most downstream location, R in the logarithmic region is still noticeably higher at $\hat{x}/\delta_0 = 0.9$, which is equivalent to $\hat{x}/k_p \approx 110$, a fetch where we might expect a large portion of the small-scale motions directly generated from the flow interaction with the roughness elements to diminish. However, small scales may form through the shear between the surviving rough-wall structures, and exhibit a stronger amplitude modulation effect with those structures from which they originate.

In summary, based on the single-point measurements of the rough-to-smooth cases, the increase in R is contributed by both reduced $|\tau_a^+|$ and increased $\langle u_S^{+2} \rangle$, which are two out of the three factors identified in the analysis in Sec. II. Further two-probe measurements are required to quantify the effect of the modulation sensitivity Γ .

C. Two-probe results

To further understand the origin of the enhanced modulation effect observed in Sec. IV B, IOIM calibration following the procedure detailed in Baars *et al.* [22] is performed on the three cases listed in Table II. In the results below, we will be using black for the smooth-wall reference, green and magenta for the R -to- $S1$ and R -to- $S2$ cases, respectively.

Premultiplied energy spectra of the measured velocity fluctuation and the universal small-scale signal are shown in Figs. 9(a) and 9(d), respectively. Figures 9(b) and 9(c) are the difference between the rough-to-smooth and smooth-wall reference. A band with excess energy at $1/f^+ \approx 2000$ is interpreted as the large-scale footprints in the near-wall region. The universal small scale spectra of the three cases [Fig. 9(d)] are very similar, indicating a reestablishment of the near-wall cycle after the rough-to-smooth change.

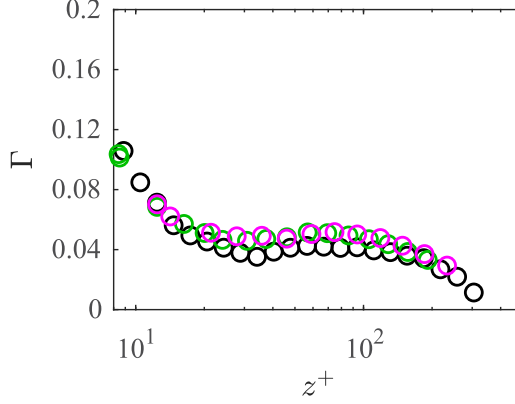


FIG. 10. Amplitude sensitivity $\Gamma(z^+)$. Line colors black, green and magenta represent the smooth, R -to- $S1$ and R -to- $S2$ cases, respectively.

The sensitivity of small scales to amplitude modulation is indicated by Γ : for a higher Γ , the universal small-scale signal u^* will be multiplied by a higher fraction of the superposition signal u_s^+ to generate the prediction. Two calibrations of a smooth-wall turbulent boundary layer at $\text{Re}_\tau \approx 7350$ and $13\,300$ result in very similar Γ [22]. For rough-to-smooth cases, as shown in Fig. 10, Γ from the three calibrations reach a good overall agreement, suggesting that the overenergized rough-wall structures in the outer layer do not seem to alter the amplitude modulation mechanism in the near-wall region.

Figure 11(a) shows $|\tilde{H}_L|$, the gain of the linear kernel [which relates the superposition u_s^+ to the outer-layer large-scale signal u_o^+ via Eq. (5)], at a wall-normal position of $z^+ = 100$. Similar trends are also seen in other wall-normal positions, and are not shown here for brevity. The magnitude of the linear transfer kernel $|\tilde{H}_L|$ is found to increase in the rough-to-smooth cases compared to the smooth-wall reference. The linear coherence spectra are shown in Fig. 11(b). In the rough-to-smooth cases, γ^2 deviates from 0 at a smaller $1/f^+$, and remains higher than that of the smooth-wall reference. A higher γ^2 indicates a stronger correlation between the velocity fluctuations obtained

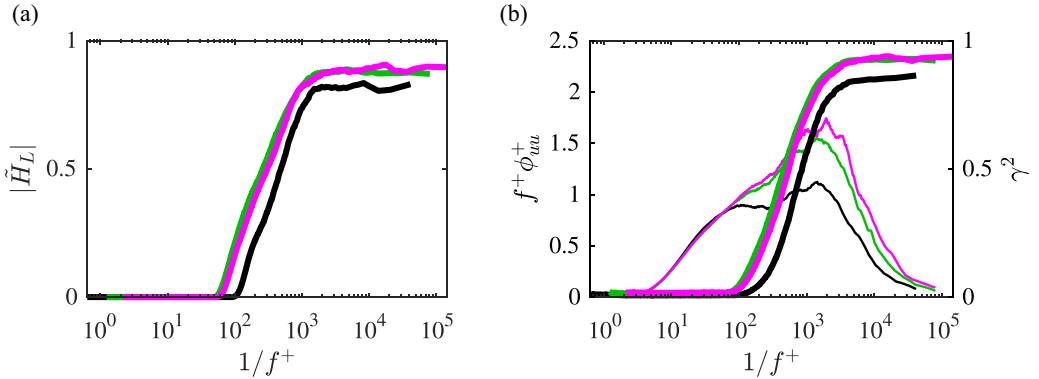


FIG. 11. (a) $|\tilde{H}_L|$, gain of the linear kernel, and (b) γ^2 , linear coherence spectra between the fixed outer and moving inner probe at $z^+ = 100$. Both quantities are filtered by a 25% bandwidth moving filter. Line colors black, green, and magenta represent the smooth, R -to- $S1$, and R -to- $S2$ cases, respectively. The premultiplied energy spectrum $f^+\phi_{uu}^+$ is also shown in panel (b) by thin lines of corresponding colors on the left vertical axis for reference.

by the inner and outer probes. These results suggest that for a given structure in the outer layer, it will leave a stronger footprint (superposition) in the near-wall region in the rough-to-smooth case as a result of the enhanced inner-outer coherence.

D. Discussion

Overall, the amplitude modulation mechanism appears to be little modified after introducing a roughness heterogeneity (at least at $\hat{x}/\delta_0 = 2.3$ as examined here). However, there is a stronger correlation between the large-scale velocity fluctuations obtained by the inner and outer probes, and the gain in the linear kernel is also higher in rough-to-smooth cases. The large-scale fluctuation $\langle u_O^{+2} \rangle$ is already stronger in the rough-to-smooth cases, and a larger fraction of it will contribute to the near-wall superposition signal through the increased gain $|\tilde{H}_L|$. In light of the analysis in Sec. II, the increase of $\langle u_S^{+2} \rangle$ is primarily responsible for the higher R value downstream of a rough-to-smooth change.

It is interesting to draw a direct comparison between the freestream turbulence [34,35] and the current rough-to-smooth cases, as both are in the “top-down” category with broadband energetic large-scale motions imposed in the outer region. The increased strength in the outer large scales makes them less susceptible to the interruptions from near-wall motions, leading to an increase in the correlation between outer- and near-wall large-scale signals, which is eventually reflected in an higher $|\tilde{H}_L|$ in both. The major difference between the two is in the coefficient Γ : the former has a lower Γ , while the value is unchanged in the latter, similar to the independence of Γ on Re_τ values observed in canonical smooth-wall boundary layers [22]. We speculate that such difference is rooted in the manner in which the outer large scales are organized, as well as the energetic wavelengths. In the freestream turbulence case, the outer structures are created by an active grid, which are inherently different from the structures organized by hairpin vortices in a developing boundary layer. The dissimilarity in the generation mechanism between large- and small-scale structures in the freestream turbulence might be the reason for the reduction in Γ . The highly energetic large scales arranged in a manner similar to that of a naturally developed boundary layer in the current configuration makes it a good mimetic of a smooth-wall turbulent boundary layer at very high Reynolds numbers.

V. CONCLUDING REMARKS

In this work, we start with examining the mechanism behind the increased amplitude modulation coefficient as reported in previous studies, utilising the framework of IOIM. An analytical relationship between the amplitude modulation coefficient R_2 and IOIM parameters is derived and verified using a smooth-wall turbulent boundary layer dataset. This framework is then applied to classify and interpret the reported amplitude modulation behaviours in previous works. We then present the case study of a turbulent boundary layer downstream of a rough-to-smooth change with both single probe and simultaneous two-probe measurements. A stronger amplitude modulation effect evidenced by higher positive R is observed. Further analysis of the two-probe data reveals that the modulation strength Γ is similar to that of a canonical smooth-wall turbulent boundary layer, and it remains the same for the two Reynolds numbers tested. The increase in R is primarily attributed to the stronger large-scale footprints $\langle u_S^{+2} \rangle$ in the near-wall region, which is contributed by both the overenergetic outer layer motions $\langle u_O^{+2} \rangle$ and stronger coherence between the inner and outer layers. These results and analyses offer a new perspective to interpret the abundant literature on the the scale interactions of noncanonical turbulent boundary layers, which can be meaningful for incorporating the IOIM in the numerical simulation of a wide range of flow conditions.

- [1] B. J. Balakumar and R. J. Adrian, Large- and very-large-scale motions in channel and boundary-layer flows, *Phil. Trans. Roy. Soc. Lond. A: Math., Phys. Eng. Sci.* **365**, 665 (2007).
- [2] K. C. Kim and R. J. Adrian, Very large-scale motion in the outer layer, *Phys. Fluids* **11**, 417 (1999).
- [3] A. J. Smits, B. J. McKeon, and I. Marusic, High-Reynolds number wall turbulence, *Annu. Rev. Fluid Mech.* **43**, 353 (2011).
- [4] N. Hutchins and I. Marusic, Evidence of very long meandering features in the logarithmic region of turbulent boundary layers, *J. Fluid Mech.* **579**, 1 (2007).
- [5] N. Hutchins and I. Marusic, Large-scale influences in near-wall turbulence, *Phil. Trans. Royal Soc.* **365**, 647 (2007).
- [6] S. Hoyas and J. Jiménez, Scaling of the velocity fluctuations in turbulent channels up to $Re_\tau = 2003$, *Phys. Fluids* **18**, 011702 (2006).
- [7] P. Vincenti, J. Klewicki, C. Morrill-Winter, C. M. White, and M. Wosnik, Streamwise velocity statistics in turbulent boundary layers that spatially develop to high Reynolds number, *Exp. Fluids* **54**, 1629 (2013).
- [8] P. R. Bandyopadhyay and A. K. M. F. Hussain, The coupling between scales in shear flows, *Phys. Fluids* **27**, 2221 (1984).
- [9] L. Agostini and M. A. Leschziner, On the influence of outer large-scale structures on near-wall turbulence in channel flow, *Phys. Fluids* **26**, 075107 (2014).
- [10] L. He, Multiscale block spectral solution for unsteady flows, *Int. J. Numer. Methods Fluids* **86**, 655 (2018).
- [11] C. Chen and L. He, Two-scale solution for tripped turbulent boundary layer, *J. Fluid Mech.* **955**, A5 (2023).
- [12] C. Zhang and S. I. Chernyshenko, Quasisteady quasihomogeneous description of the scale interactions in near-wall turbulence, *Phys. Rev. Fluids* **1**, 014401 (2016).
- [13] S. Chernyshenko, Extension of QSQH theory of scale interaction in near-wall turbulence to all velocity components, *J. Fluid Mech.* **916**, A52 (2021).
- [14] R. Mathis, N. Hutchins, and I. Marusic, Large-scale amplitude modulation of the small-scale structures in turbulent boundary layers, *J. Fluid Mech.* **628**, 311 (2009).
- [15] D. Chung and B. J. McKeon, Large-eddy simulation of large-scale structures in long channel flow, *J. Fluid Mech.* **661**, 341 (2010).
- [16] M. Guala, M. Metzger, and B. J. McKeon, Interactions within the turbulent boundary layer at high Reynolds number, *J. Fluid Mech.* **666**, 573 (2011).
- [17] B. Ganapathisubramani, N. Hutchins, J. P. Monty, D. Chung, and I. Marusic, Amplitude and frequency modulation in wall turbulence, *J. Fluid Mech.* **712**, 61 (2012).
- [18] W. J. Baars, K. M. Talluru, N. Hutchins, and I. Marusic, Wavelet analysis of wall turbulence to study large-scale modulation of small scales, *Exp. Fluids* **56**, 1 (2015).
- [19] I. Marusic, R. Mathis, and N. Hutchins, Predictive model for wall-bounded turbulent flow, *Science* **329**, 193 (2010).
- [20] R. Mathis, N. Hutchins, and I. Marusic, A predictive inner-outer model for streamwise turbulence statistics in wall-bounded flows, *J. Fluid Mech.* **681**, 537 (2011).
- [21] L. Agostini and M. Leschziner, Predicting the response of small-scale near-wall turbulence to large-scale outer motions, *Phys. Fluids* **28**, 015107 (2016).
- [22] W. J. Baars, N. Hutchins, and I. Marusic, Spectral stochastic estimation of high-Reynolds-number wall-bounded turbulence for a refined inner-outer interaction model, *Phys. Rev. Fluids* **1**, 054406 (2016).
- [23] M. Inoue, R. Mathis, I. Marusic, and D. I. Pullin, Inner-layer intensities for the flat-plate turbulent boundary layer combining a predictive wall-model with large-eddy simulations, *Phys. Fluids* **24**, 075102 (2012).
- [24] O. Cabrit, R. Mathis, V. Kulandaivelu, and I. Marusic, Towards a statistically accurate wall-model for large-eddy simulation, in *Proceedings of the 18th Australasian Fluid Mechanics Conference* (Launceston, Australia, 2012).
- [25] W. Sidebottom, O. Cabrit, I. Marusic, C. Meneveau, A. Ooi, and D. Jones, Modelling of wall shear-stress fluctuations for large-eddy simulation, in *Proceedings of the 19th Australasian Fluid Mechanics Conference* (Melbourne, Australia, 2014).

- [26] R. Mathis, J. P. Monty, N. Hutchins, and I. Marusic, Comparison of large-scale amplitude modulation in turbulent boundary layers, pipes, and channel flows, [Phys. Fluids](#) **21**, 111703 (2009).
- [27] J. P. Monty, M. S. Chong, R. Mathis, N. Hutchins, I. Marusic, and J. J. Allen, A high Reynolds number turbulent boundary layer with regular “Braille-type” roughness, in *Proceedings of the IUTAM Symposium on the Physics of Wall-bounded Turbulent Flows on Rough Walls* (Springer, Berlin, 2010), pp. 69–75.
- [28] D. T. Squire, W. J. Baars, N. Hutchins, and I. Marusic, Inner-outer interactions in rough-wall turbulence, [J. Turbul.](#) **17**, 1159 (2016).
- [29] W. Anderson, Amplitude modulation of streamwise velocity fluctuations in the roughness sublayer: Evidence from large-eddy simulations, [J. Fluid Mech.](#) **789**, 567 (2016).
- [30] S. Wu, K. T. Christensen, and C. Pantano, Modelling smooth-and transitionally rough-wall turbulent channel flow by leveraging inner-outer interactions and principal component analysis, [J. Fluid Mech.](#) **863**, 407 (2019).
- [31] K. Blackman, L. Perret, and R. Mathis, Assessment of inner-outer interactions in the urban boundary layer using a predictive model, [J. Fluid Mech.](#) **875**, 44 (2019).
- [32] T. Kim, G. Blois, J. L. Best, and K. T. Christensen, Experimental evidence of amplitude modulation in permeable-wall turbulence, [J. Fluid Mech.](#) **887**, A3 (2020).
- [33] S. M. H. Khorasani, M. Luhar, and S. Bagheri, Turbulent flows over engineered anisotropic porous substrates, [arXiv:2210.10140](#).
- [34] E. Dogan, R. E. Hanson, and B. Ganapathisubramani, Interactions of large-scale free-stream turbulence with turbulent boundary layers, [J. Fluid Mech.](#) **802**, 79 (2016).
- [35] E. Dogan, R. J. Hearst, and B. Ganapathisubramani, Modelling high Reynolds number wall–turbulence interactions in laboratory experiments using large-scale free-stream turbulence, [Phil. Trans. Roy. Soc. Lond. A: Math., Phys. Eng. Sci.](#) **375**, 20160091 (2017).
- [36] S. Duvvuri and B. J. McKeon, Triadic scale interactions in a turbulent boundary layer, [J. Fluid Mech.](#) **767**, R4 (2015).
- [37] M. Lozier, F. O. Thomas, and S. Gordeyev, Experimental studies of boundary layer dynamics via active manipulation of large-scale structures, in *Proceedings of the 12th International Symposium on Turbulence and Shear Flow Phenomena* (Osaka, Japan, 2022).
- [38] M. Li, C. M. de Silva, R. Baidya, A. Rouhi, D. Chung, I. Marusic, and N. Hutchins, Recovery of the wall-shear stress to equilibrium flow conditions after a rough-to-smooth step-change in turbulent boundary layers, [J. Fluid Mech.](#) **872**, 472 (2019).
- [39] J. R. Garratt, The internal boundary layer—A review, [Bound.-Layer Meteorol.](#) **50**, 171 (1990).
- [40] W. P. Elliott, The growth of the atmospheric internal boundary layer, [Trans. Am. Geophys. Union](#) **39**, 1048 (1958).
- [41] R. A. Antonia and R. E. Luxton, The response of a turbulent boundary layer to a step change in surface roughness. Part 2. Rough-to-smooth, [J. Fluid Mech.](#) **53**, 737 (1972).
- [42] R. E. Hanson and B. Ganapathisubramani, Development of turbulent boundary layers past a step change in wall roughness, [J. Fluid Mech.](#) **795**, 494 (2016).
- [43] A. Rouhi, D. Chung, and N. Hutchins, Direct numerical simulation of open channel flow over smooth-to-rough and rough-to-smooth step changes, [J. Fluid Mech.](#) **866**, 450 (2019).
- [44] M. Li, C. M. de Silva, D. Chung, D. I. Pullin, I. Marusic, and N. Hutchins, Experimental study of a turbulent boundary layer with a rough-to-smooth change in surface conditions at high Reynolds numbers, [J. Fluid Mech.](#) **923**, A18 (2021).
- [45] M. Li, C. M. de Silva, D. Chung, D. I. Pullin, I. Marusic, and N. Hutchins, Modelling the downstream development of a turbulent boundary layer following a step change of roughness, [J. Fluid Mech.](#) **949**, A7 (2022).
- [46] A. A. Townsend, *The Structure of Turbulent Shear Flow*, 2nd ed. (Cambridge University Press, Cambridge, UK, 1976).
- [47] D. T. Squire, C. Morrill-Winter, N. Hutchins, M. P. Schultz, J. C. Klewicki, and I. Marusic, Comparison of turbulent boundary layers over smooth and rough surfaces up to high Reynolds numbers, [J. Fluid Mech.](#) **795**, 210 (2016).

- [48] I. Marusic, K. A. Chauhan, V. Kulandaivelu, and N. Hutchins, Evolution of zero-pressure-gradient boundary layers from different tripping conditions, *J. Fluid Mech.* **783**, 379 (2015).
- [49] J. S. Bendat and A. G. Piersol, *Random Data: Analysis and Measurement Procedures* (John Wiley & Sons, New York, NY, 2011).
- [50] W. J. Baars, N. Hutchins, and I. Marusic, Reynolds number trend of hierarchies and scale interactions in turbulent boundary layers, *Phil. Trans. Roy. Soc. Lond. A: Math., Phys. Eng. Sci.* **375**, 20160077 (2017).
- [51] R. Mathis, I. Marusic, N. Hutchins, J. Monty, and Z. Harun, Inner-outer interaction predictive model for wall-bounded turbulence subjected to pressure gradient effect, in *Proceedings of the International Symposium on Turbulence and Shear Flow Phenomena (TSFP-9)*, Melbourne, Australia, 30 June–3 July (2015).
- [52] A. Andreolli, D. Gatti, R. Vinuesa, R. Örlü, and P. Schlatter, Separating large-scale superposition and modulation in turbulent channels, *J. Fluid Mech.* **958**, A37 (2023).
- [53] G. Pathikonda and K. T. Christensen, Inner-outer interactions in a turbulent boundary layer overlying complex roughness, *Phys. Rev. Fluids* **2**, 044603 (2017).
- [54] C. Efstathiou and M. Luhar, Mean turbulence statistics in boundary layers over high-porosity foams, *J. Fluid Mech.* **841**, 351 (2018).
- [55] Z. Harun, J. P. Monty, R. Mathis, and I. Marusic, Pressure gradient effects on the large-scale structure of turbulent boundary layers, *J. Fluid Mech.* **715**, 477 (2013).
- [56] A. Drózdź, P. Niegodajew, M. Romańczyk, and W. Elsner, Convection velocity in turbulent boundary layers under adverse pressure gradient, *Exp. Therm. Fluid Sci.* **145**, 110900 (2023).
- [57] V. Kulandaivelu, Evolution of zero pressure gradient turbulent boundary layers from different initial conditions, Ph.D. thesis, The University of Melbourne, 2012.
- [58] P. M. Ligrani and P. Bradshaw, Spatial resolution and measurement of turbulence in the viscous sublayer using subminiature hot-wire probes, *Exp. Fluids* **5**, 407 (1987).
- [59] I. Jacobi and B. J. McKeon, Phase relationships between large and small scales in the turbulent boundary layer, *Exp. Fluids* **54**, 1481 (2013).
- [60] I. Jacobi and B. J. McKeon, Phase-relationships between scales in the perturbed turbulent boundary layer, *J. Turbul.* **18**, 1120 (2017).
- [61] R. Deshpande, D. Chandran, A. J. Smits, and I. Marusic, On the relationship between manipulated inter-scale phase and energy-efficient turbulent drag reduction, [arXiv:2211.07176](https://arxiv.org/abs/2211.07176).