

BONDLESS INNOVATION

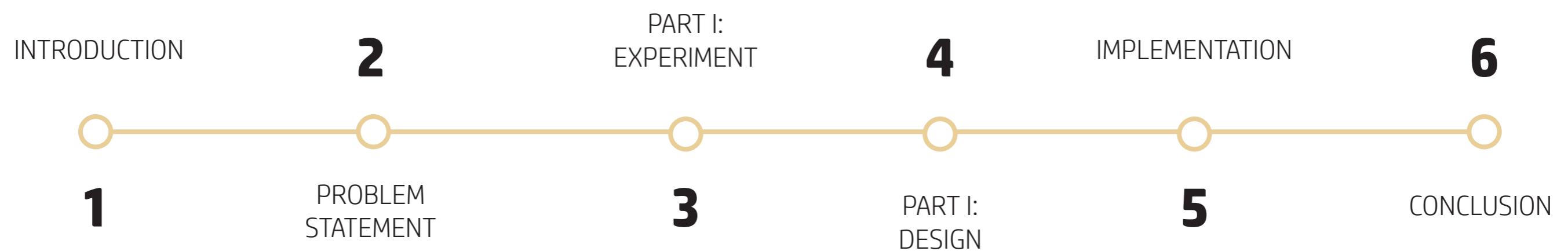
EVALUATING DIRECT ADHESION IN A CONCRETE-GLASS INTERFACE FOR FREE FORM
TRANSPARENCY.



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Dr.Ing. Marcel Bilow

“I am exploring ways to improve the **bond strength** of a **glass-concrete interface** to evaluate the **production process** for creating a new type of **hybrid facade panel**”



Todays skyline all-glass buildings



Climate crisis

Experts call for ban on glass skyscrapers to save energy in climate crisis

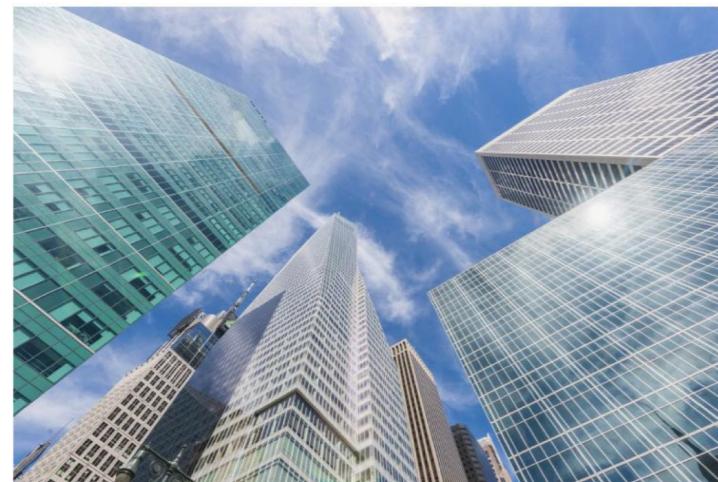
Sustainability for All.

News • Treehugger Voices

Can an All-Glass Office Building Really Be Considered Green?

By [Lloyd Alter](#)

Updated May 27, 2020



Commentary

Commentary: Buildings with fully glazed façades heat up too fast, are an environmental "failure"

Modern building façades are allowing more heat in and out of buildings, requiring a higher usage of artificial cooling and heating, says an architecture researcher.



The New York Times



[Climate Change](#) | [Climate F.A.Q.](#) | [Rising Home Insurance](#)

Glass skyscrapers: a great environmental folly that could have been avoided

Published: May 14, 2019 2.46pm CEST



How Can Buildings Beat the Heat in a Desert City? Blend Ancient and Modern.

More architects in the United Arab Emirates, the host of this year's U.N. climate summit, are moving past glass skyscrapers and focusing on sustainability.



Share full article



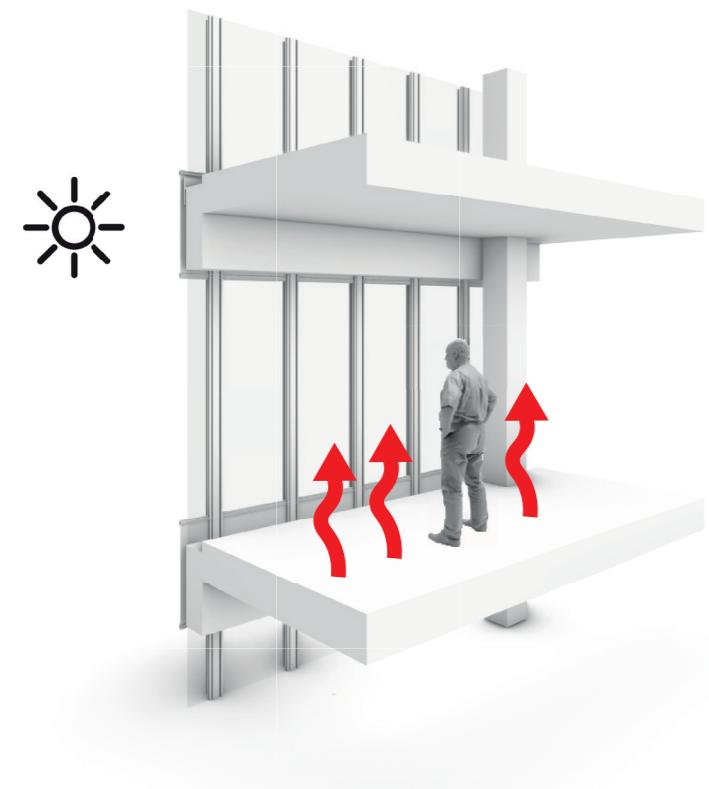
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Read in app

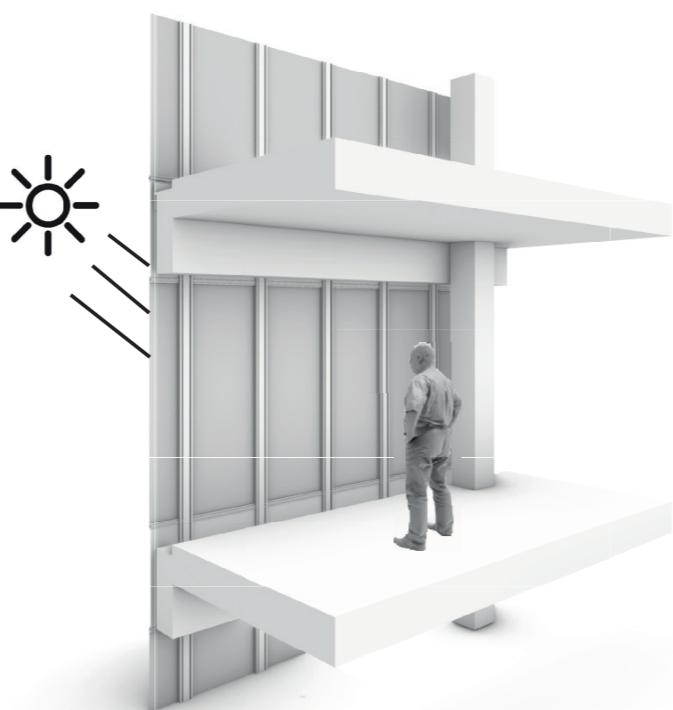


FULL GLAZED FACADE

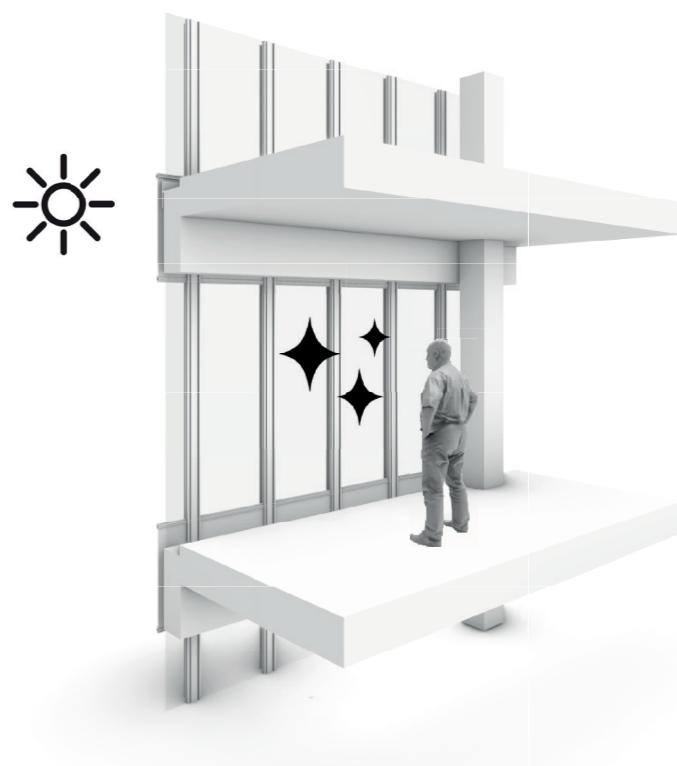
Limitations



HEAT GAIN



VIEW BLOCKAGE



GLARE

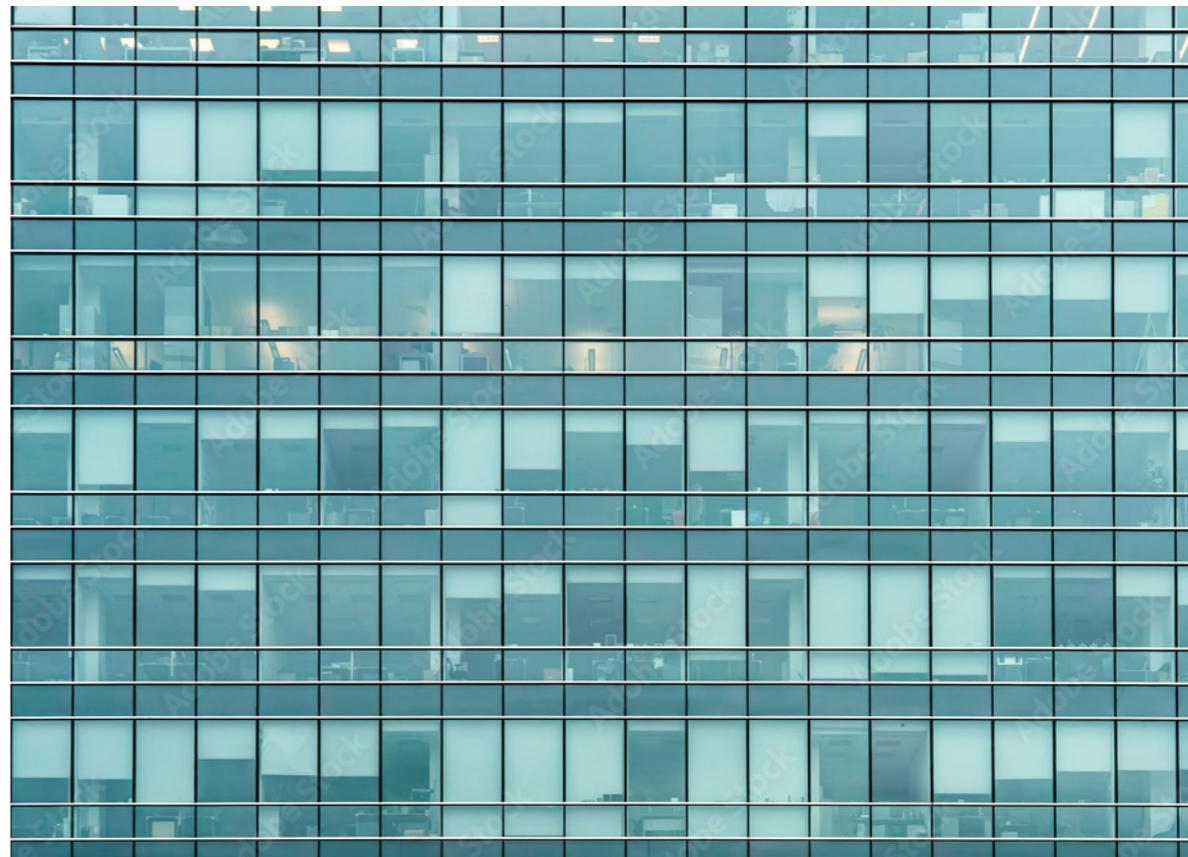
MONOTOMY

No design freedom



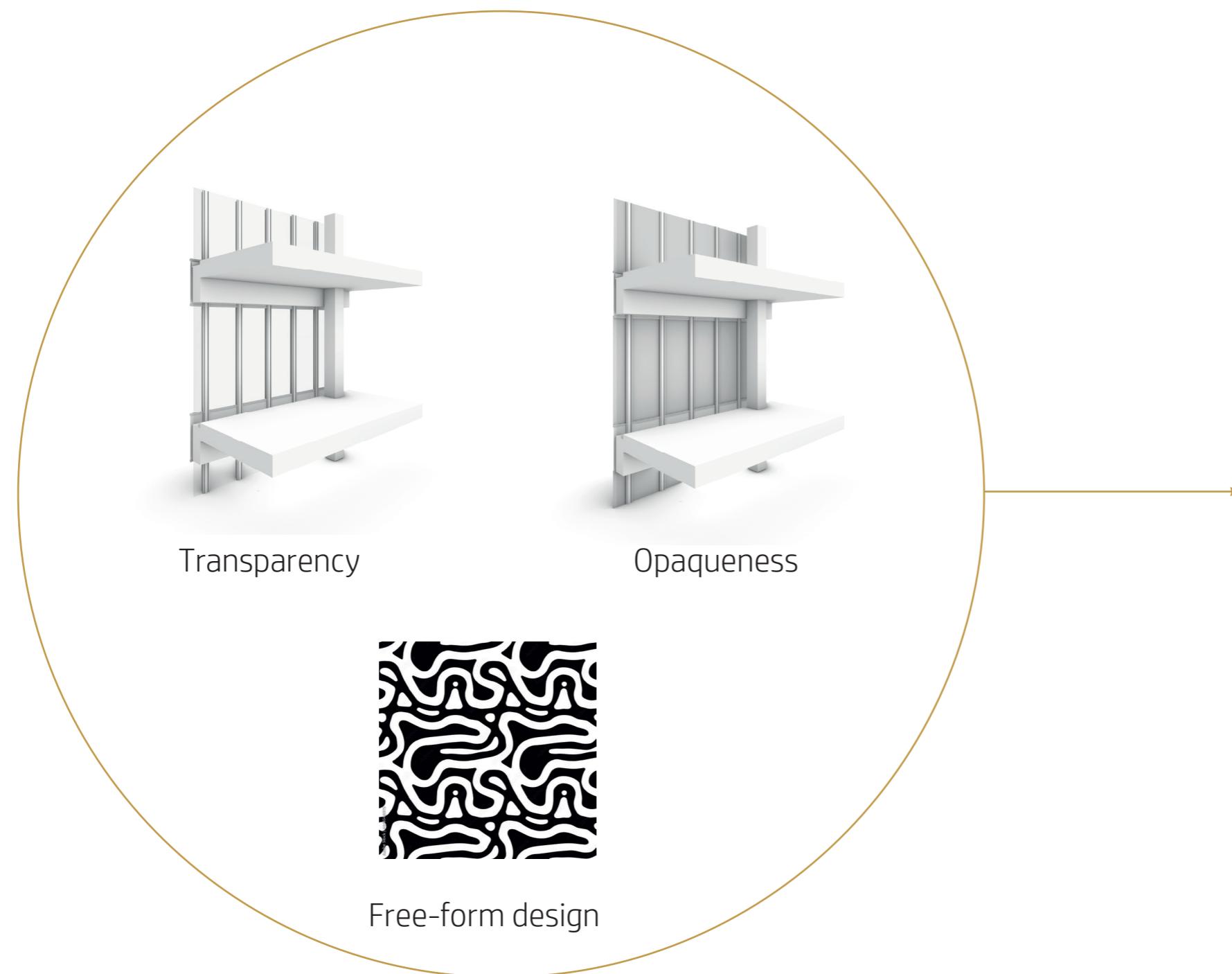
NO DESIGN FREEDOM

monotony full glazed facades

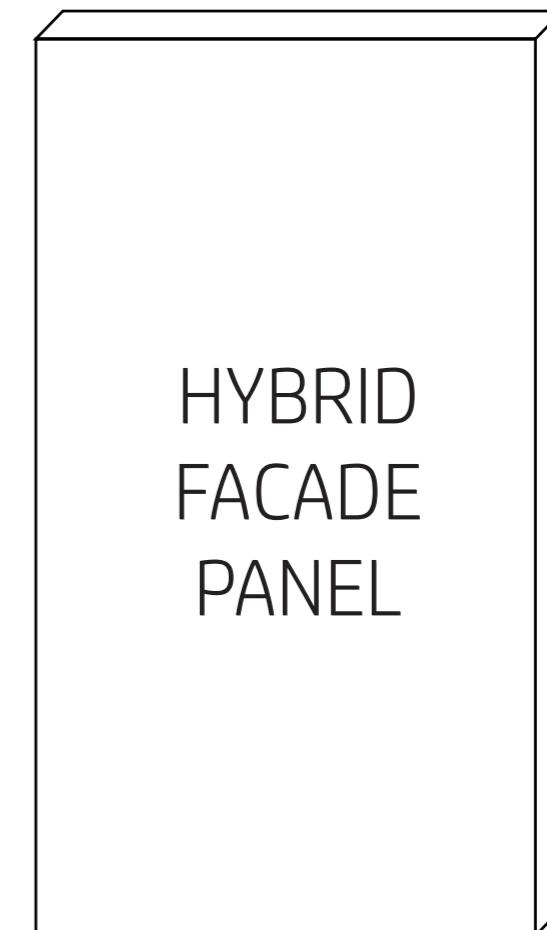


DESIGN IDEOLOGY

Hybrid facade panel



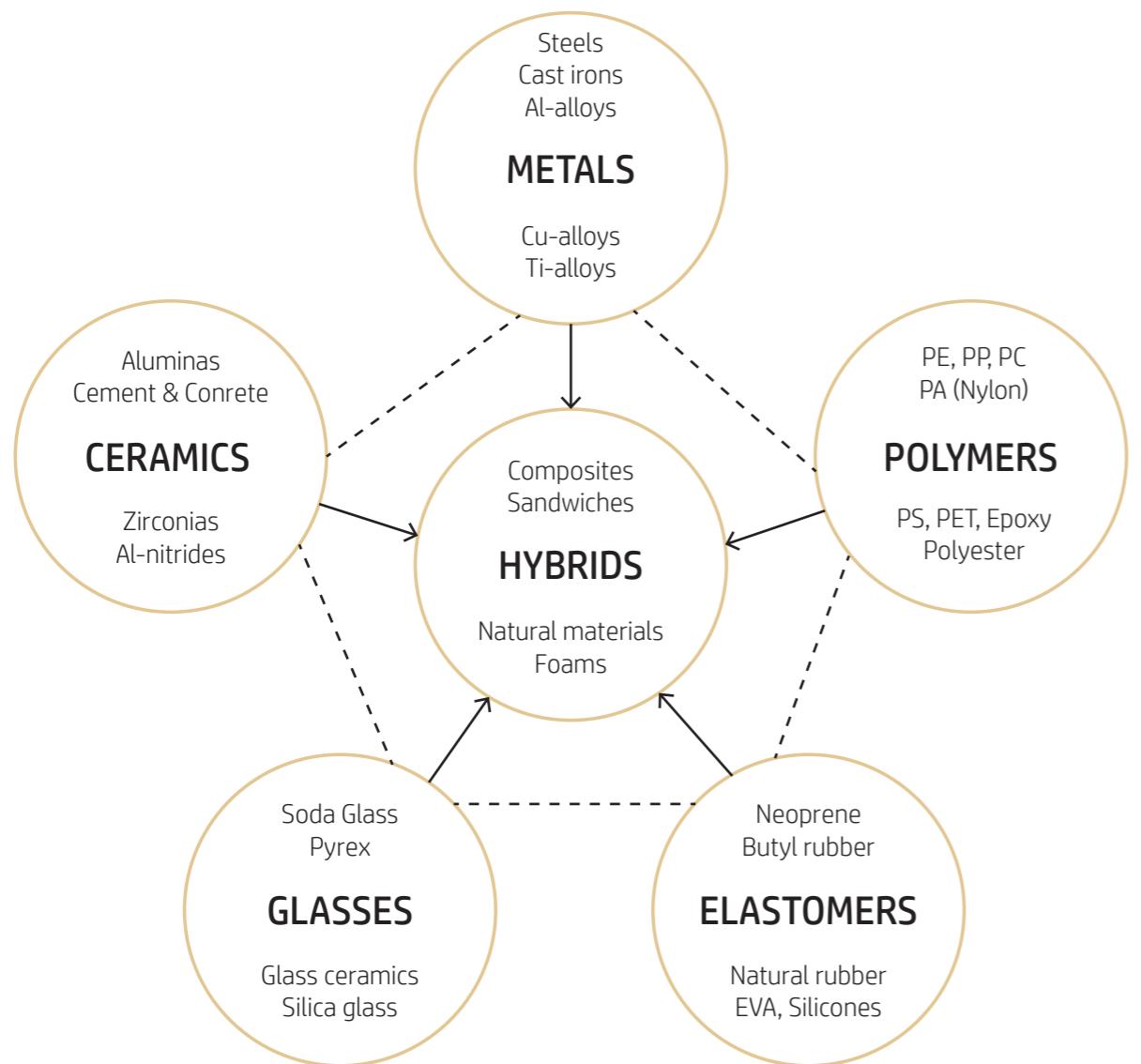
New Design
Language



HYBRID
FACADE
PANEL

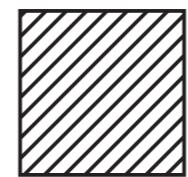
HYBRID MATERIAL

Selection

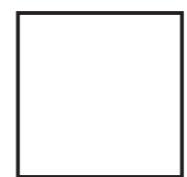


HYBRID :

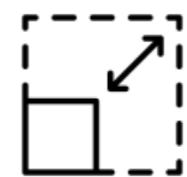
Material A



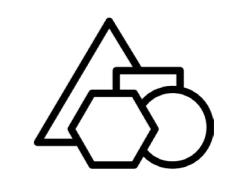
Material B



Scale

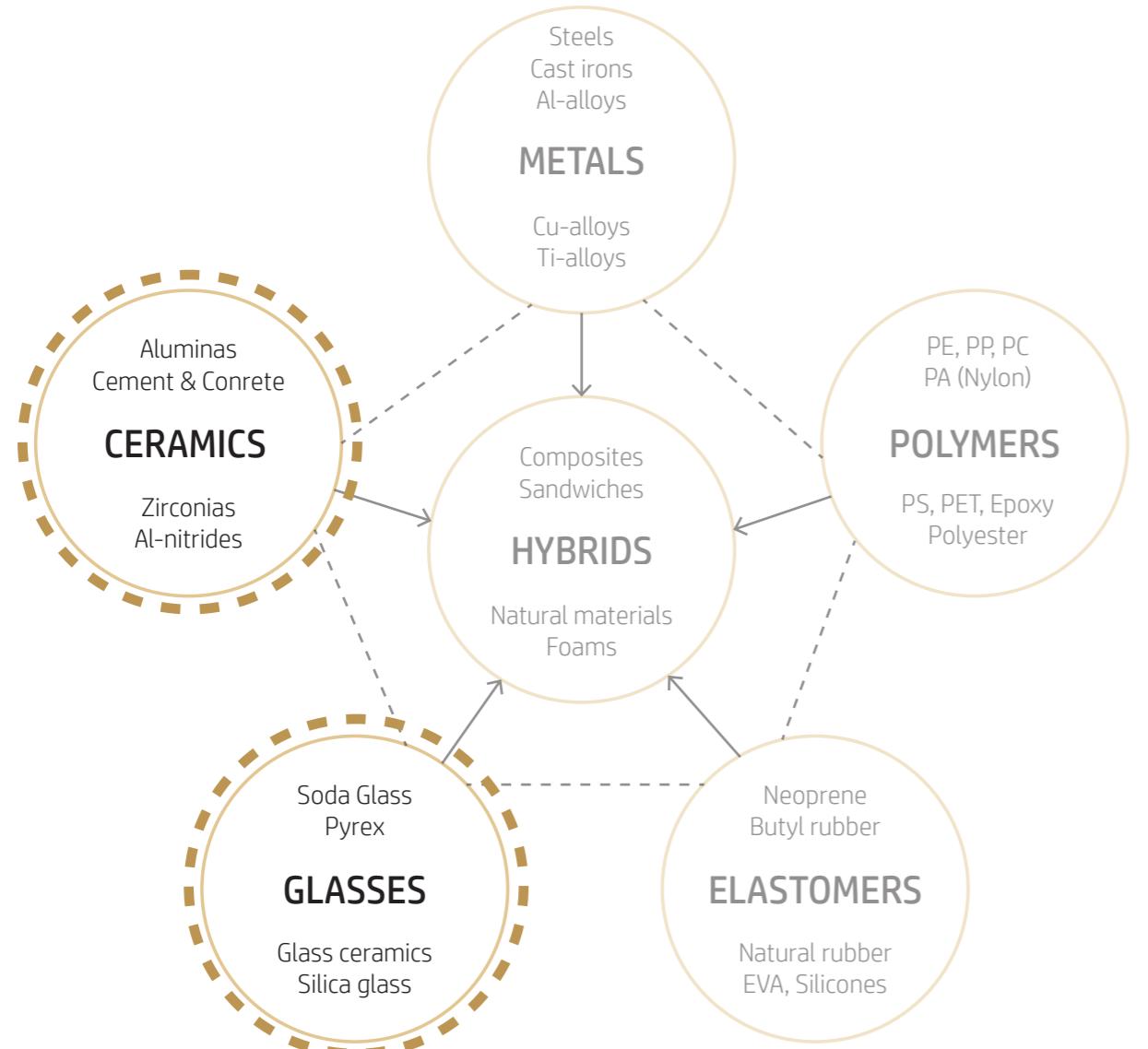


Geometry



HYBRID MATERIAL

Conclusion



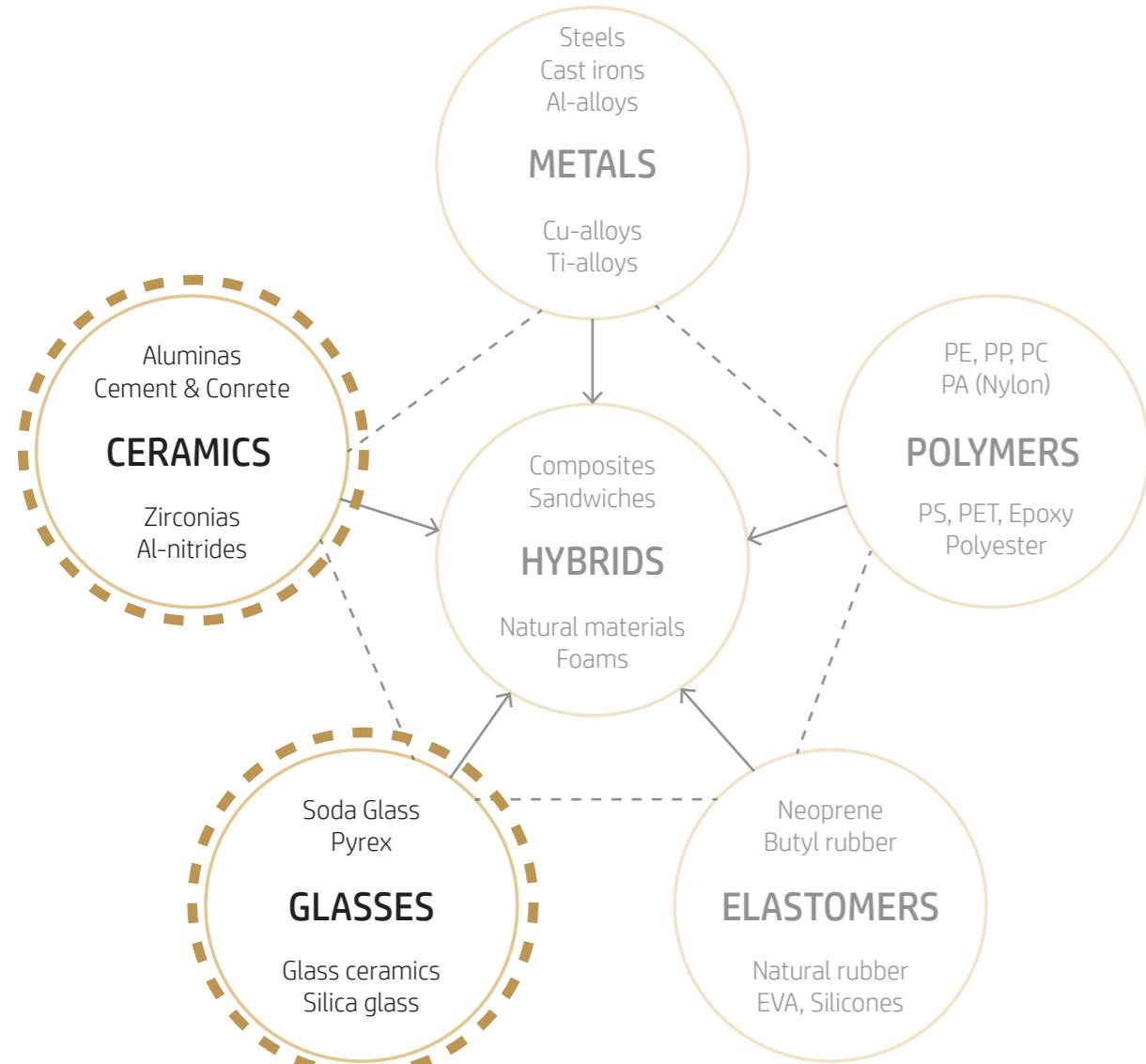
CONCRETE

+

GLASS

HYBRID MATERIAL

Conclusion



CONCRETE

Shapeability

Durable

Low costs

Most used building material

Structurability

GLASS

Optical transparency

Durable

Recyclable

Structurability

Aesthetic

Closely aligned thermal expansion

Concrete and glass ≠ sustainable

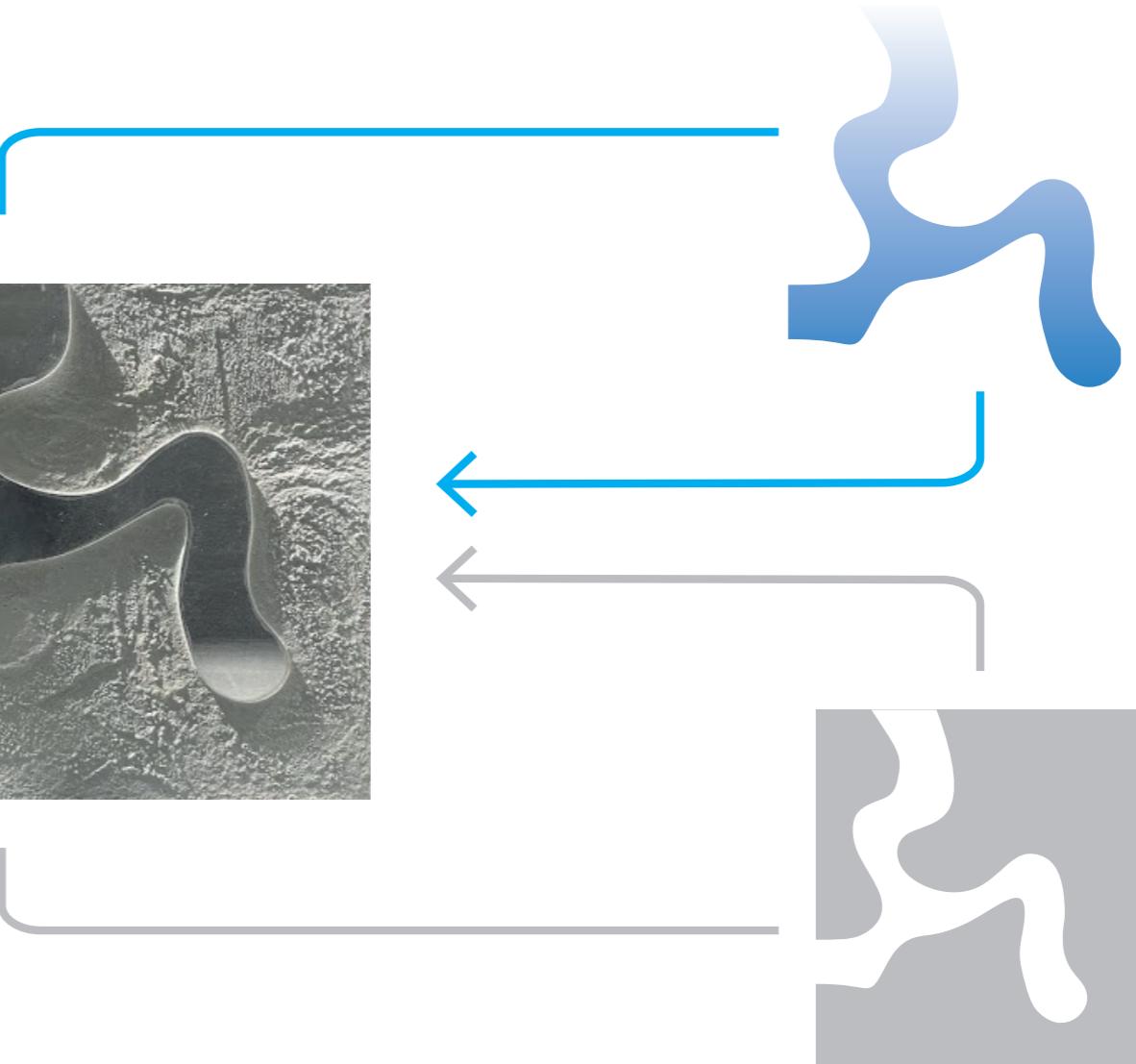
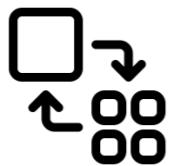
Concrete and glass = more sustainable

DESIGN FOR DISASSEMBLY

Weak Interface

DESIGN FOR DISASSEMBLY

Transforming the weak interface between concrete and glass into something useful can enhance the panel's disassembly potential.

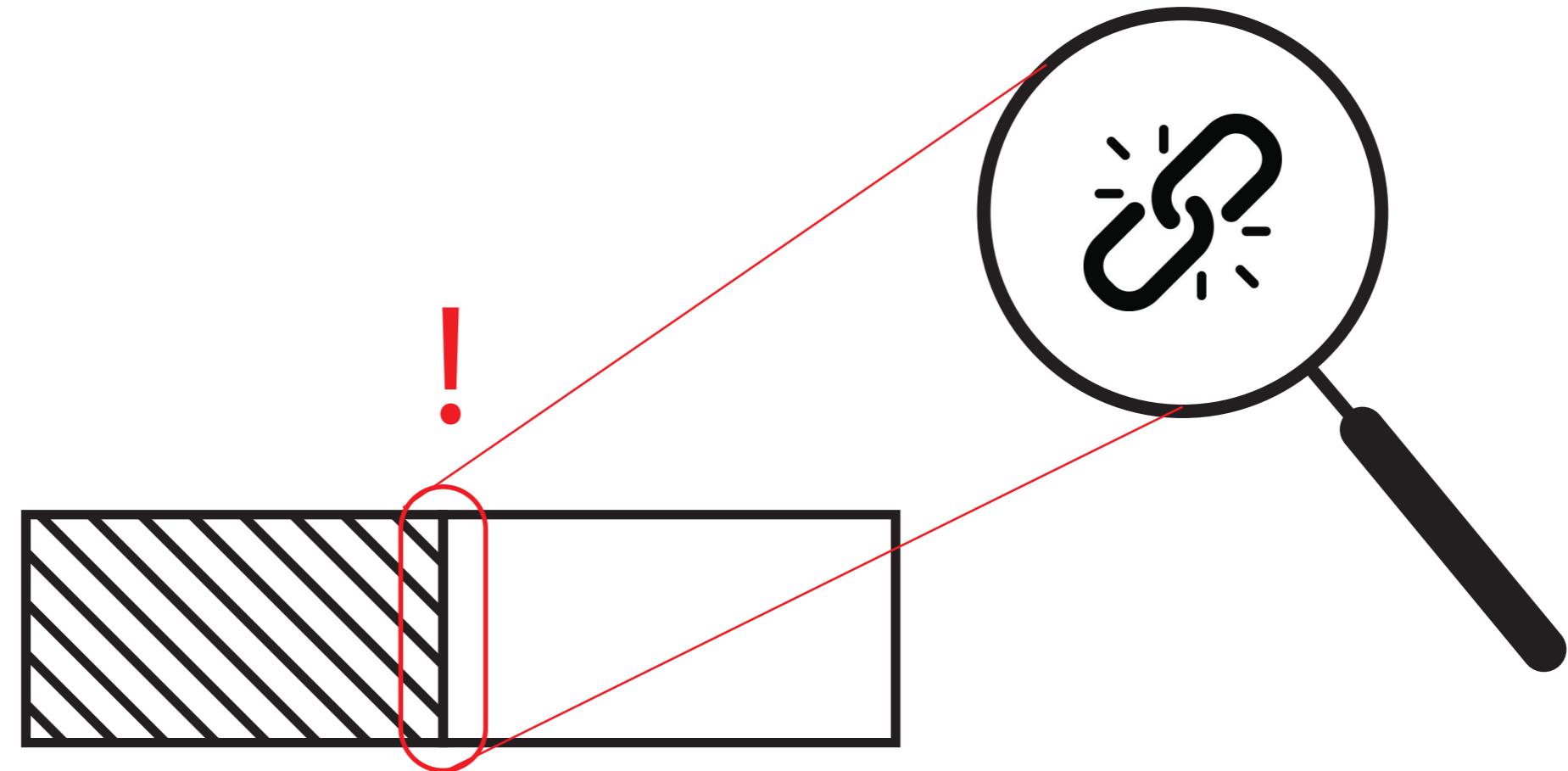


MAIN RESEARCH QUESTION

To what extend can **design considerations** ensure the structural integrity of a **hybrid interface** incorporating direct adhesion between **concrete** and **glass** for creating a hybrid facade panel?

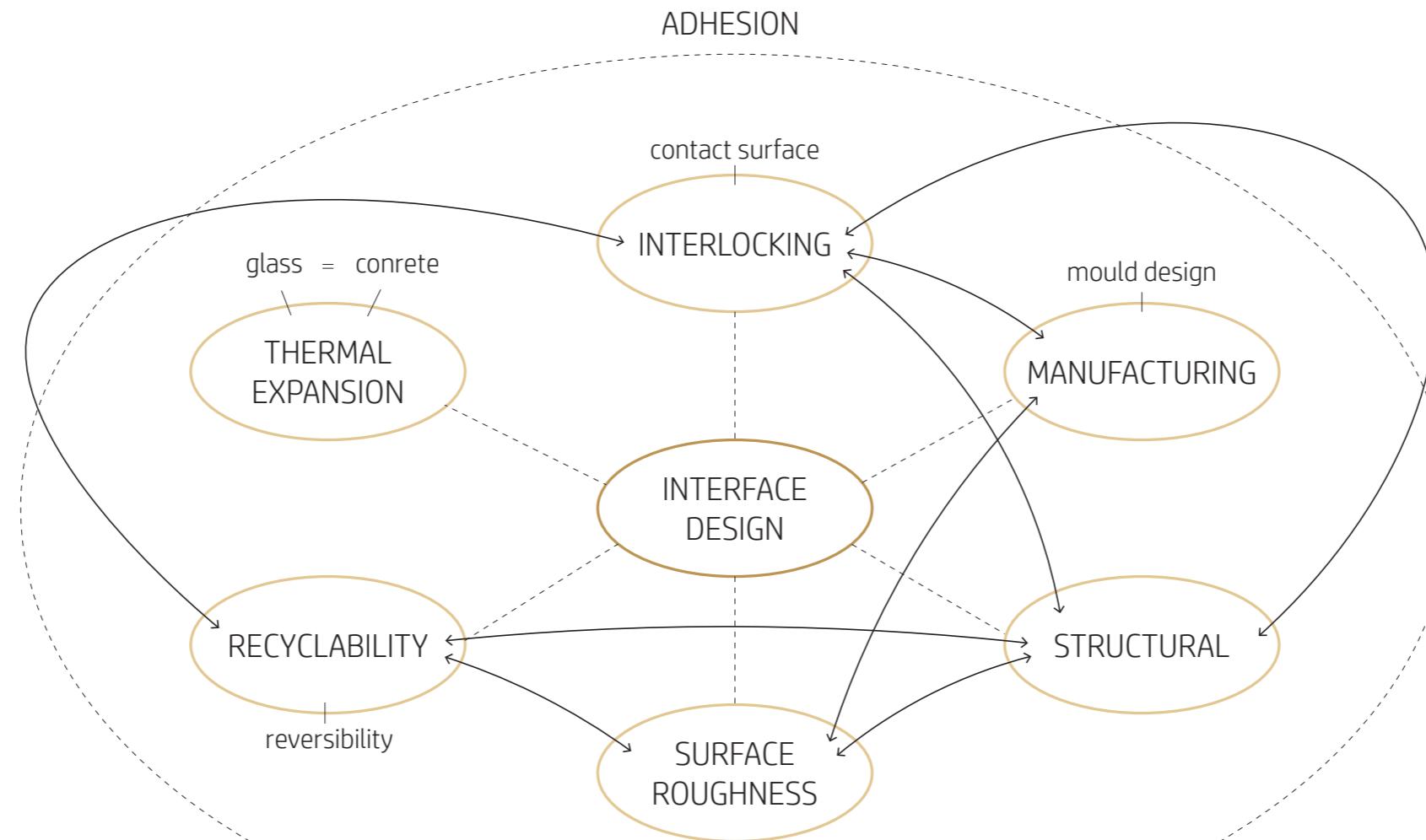
PART I:

EXPERIMENTAL PART



DESIGN CRITERIA

Interface design



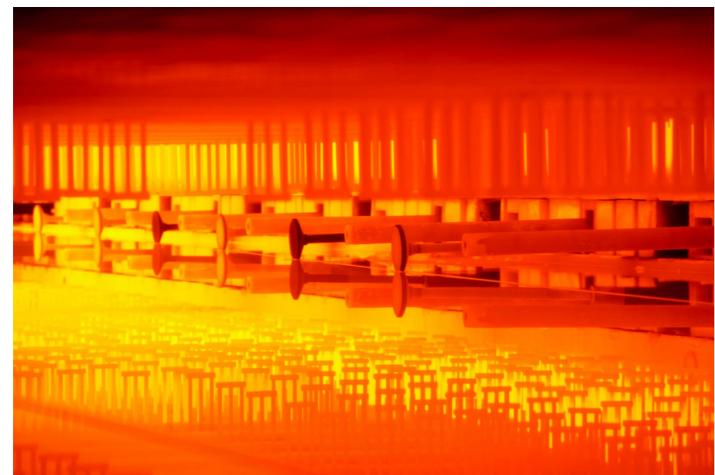
MANUFACTURING

GLASS MANUFACTURING

Options

GLASS FABRICATION METHODS

FLOAT GLASS



CAST GLASS



3D PRINTED GLASS



- Precise manufacturing
- high quality
- cost-effective
- + Limited design freedom
- + Waste generation
- + lamination (hard to recycle)

- Labor intensive
- Time consuming
- Post-processing mould making
- + Fully recyclable
- + Design freedom
- + Few manufacturing waste

- Layered transparency
- Laboratory scale
- Size limitations
- + No mould & postprocessing
- + Design freedom
- + Zero waste & recyclable

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mould making

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INTERLOCKING FORM

DESIGN OPTIONS

Interlocking form

BOW

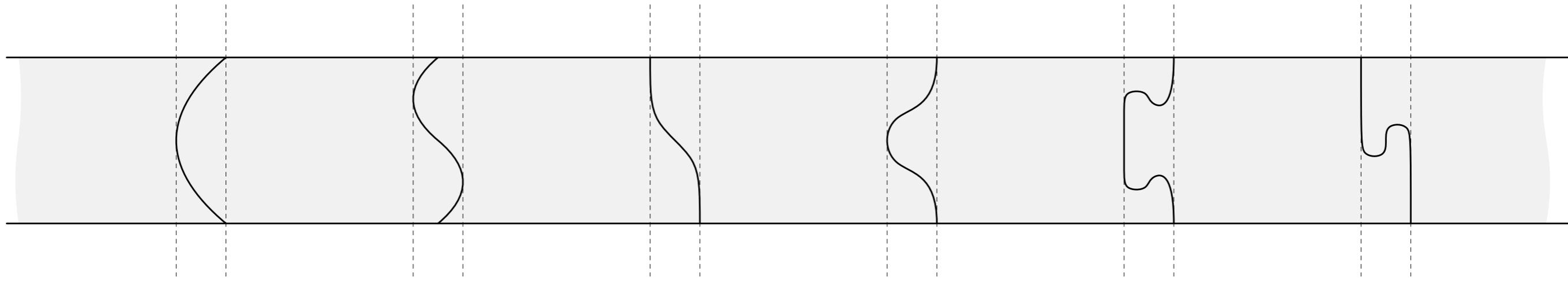
SNAKE

SHIFT

BELLY

SHROOM

GRIP



1

2

3

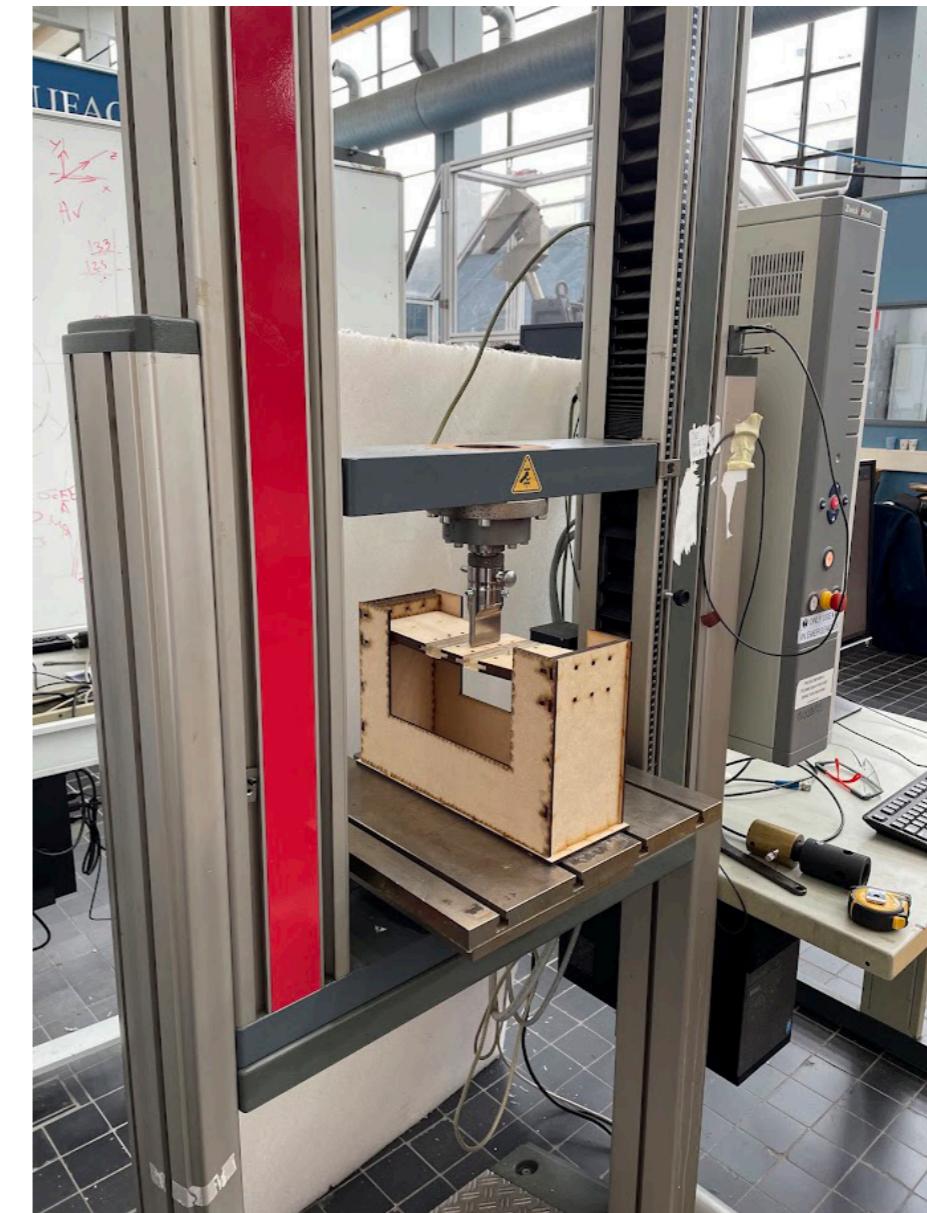
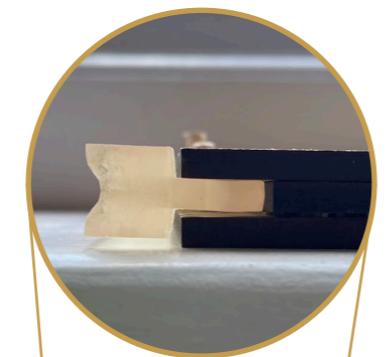
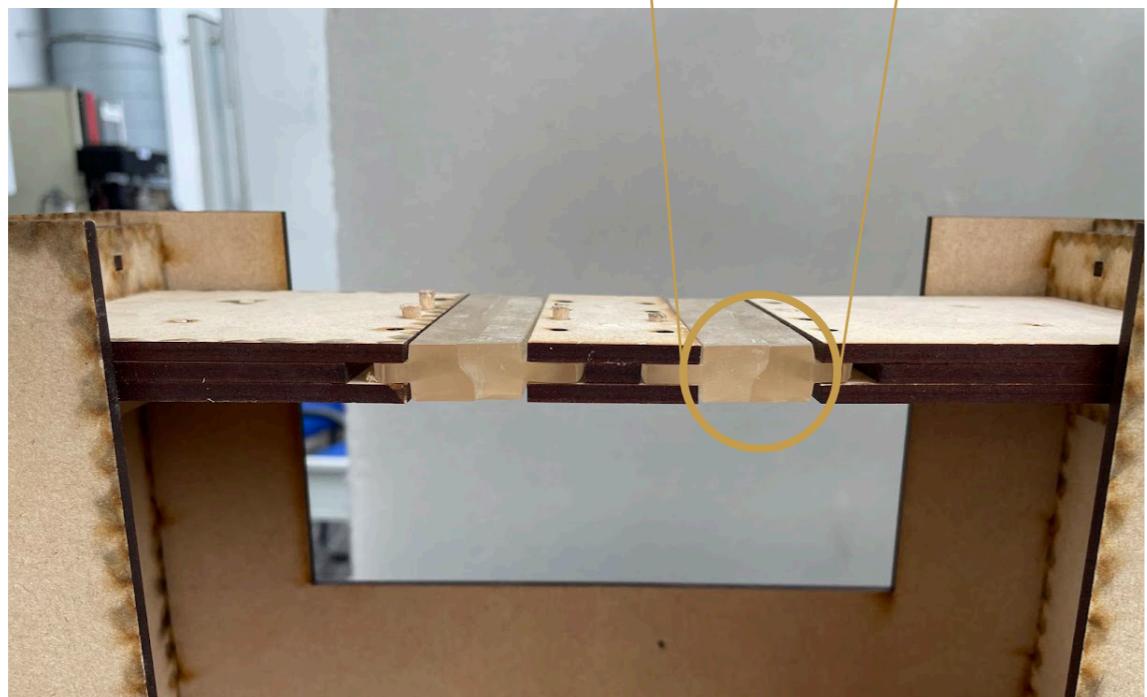
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5

6

EXPERIMENTAL SET-UP

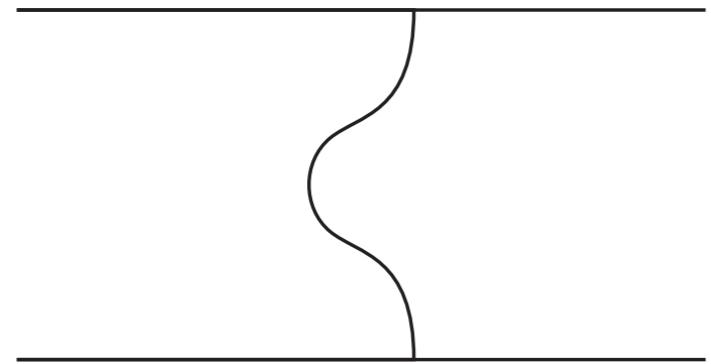
Interlocking form



CONCLUSION

Interlocking form

BELLY SHAPE

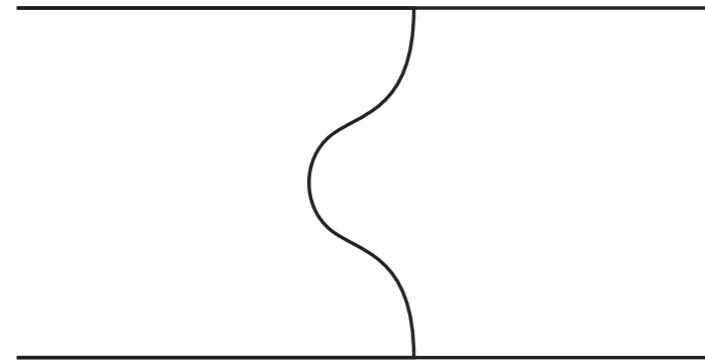


- Symmetry in the design
- Interlocking constraint
- Structural integrity
- Contact surface
- Glass manufacturing limitations

CONCLUSION

Interlocking form

BELLY SHAPE



- Symmetry in the design
- Interlocking constraint
- Structural integrity
- Contact surface
- Glass manufacturing limitations

7 - 16 - 7
D = 6
R = 3

7 - 16 - 7
D = 4.5
R = 3

7 - 16 - 7
D = 3
R = 3

10 - 10 - 10
D = 6
R = 3

10 - 10 - 10
D = 4.5
R = 3

10 - 10 - 10
D = 3
R = 3

7 - 16 - 7
D = 6
R = 6

7 - 16 - 7
D = 4.5
R = 6

7 - 16 - 7
D = 3
R = 6

10 - 10 - 10
D = 6
R = 6

10 - 10 - 10
D = 4.5
R = 6

10 - 10 - 10
D = 3
R = 6

7 - 16 - 7
D = 6
R = 12

7 - 16 - 7
D = 4.5
R = 12

7 - 16 - 7
D = 3
R = 12

10 - 10 - 10
D = 6
R = 12

10 - 10 - 10
D = 4.5
R = 12

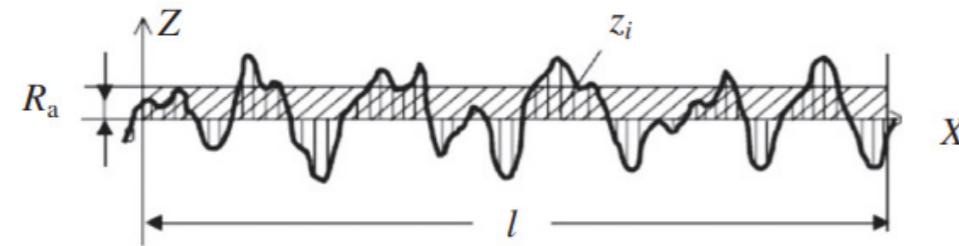
10 - 10 - 10
D = 3
R = 12



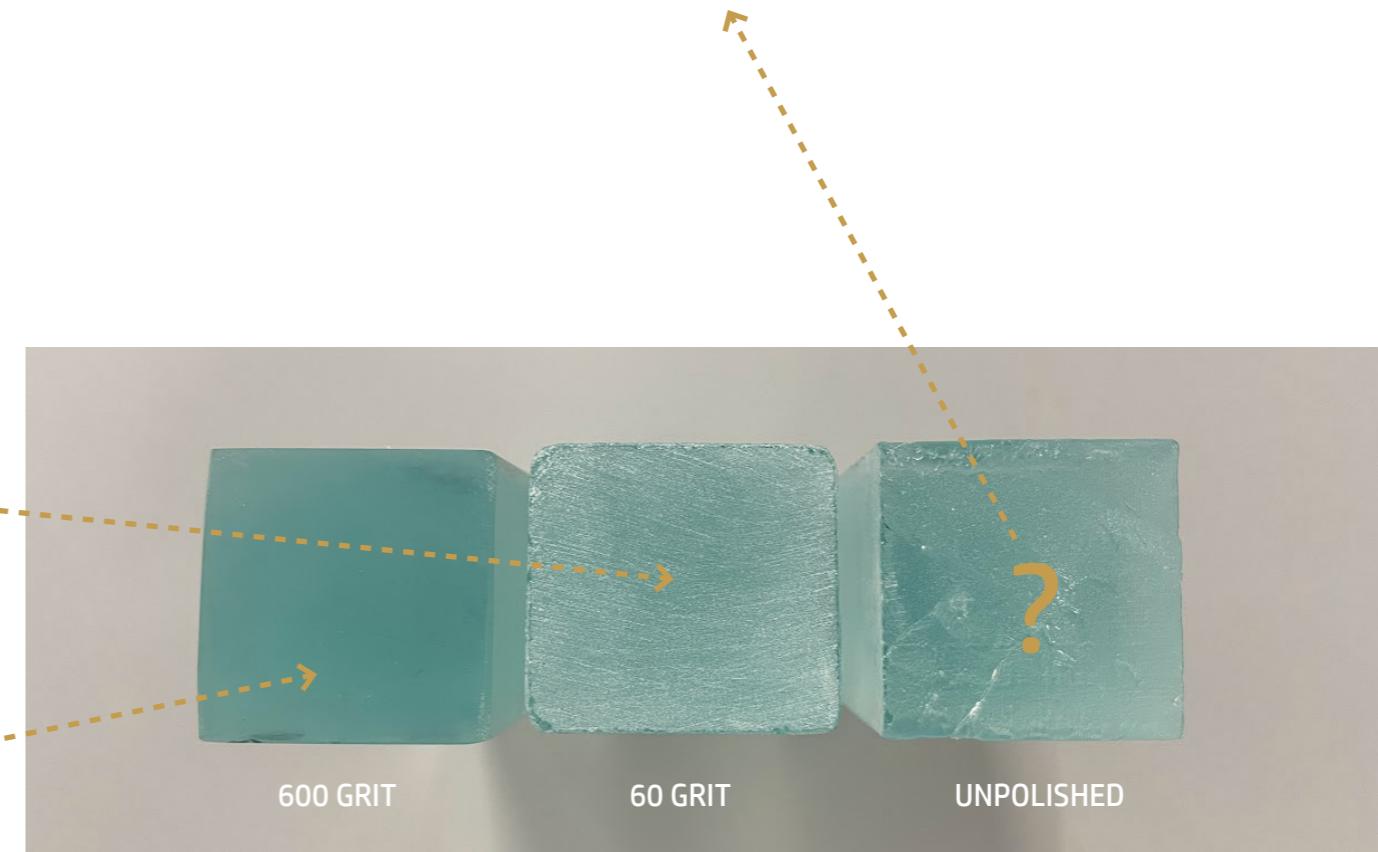
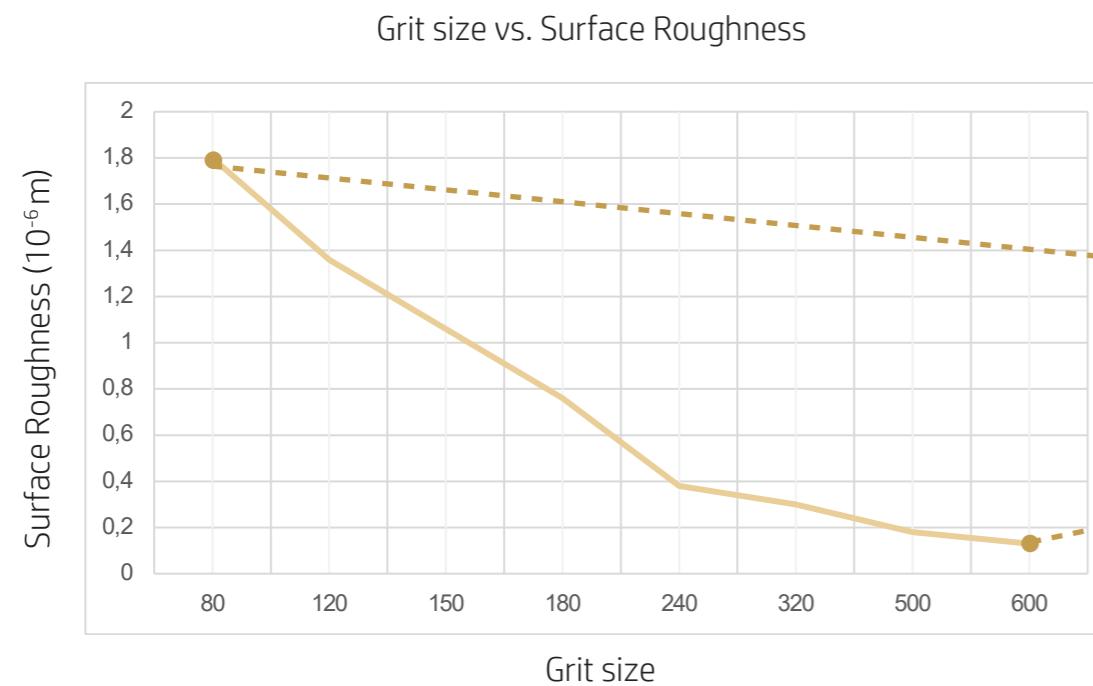
SURFACE ROUGHNESS

SURFACE ROUGHNESS

Overview

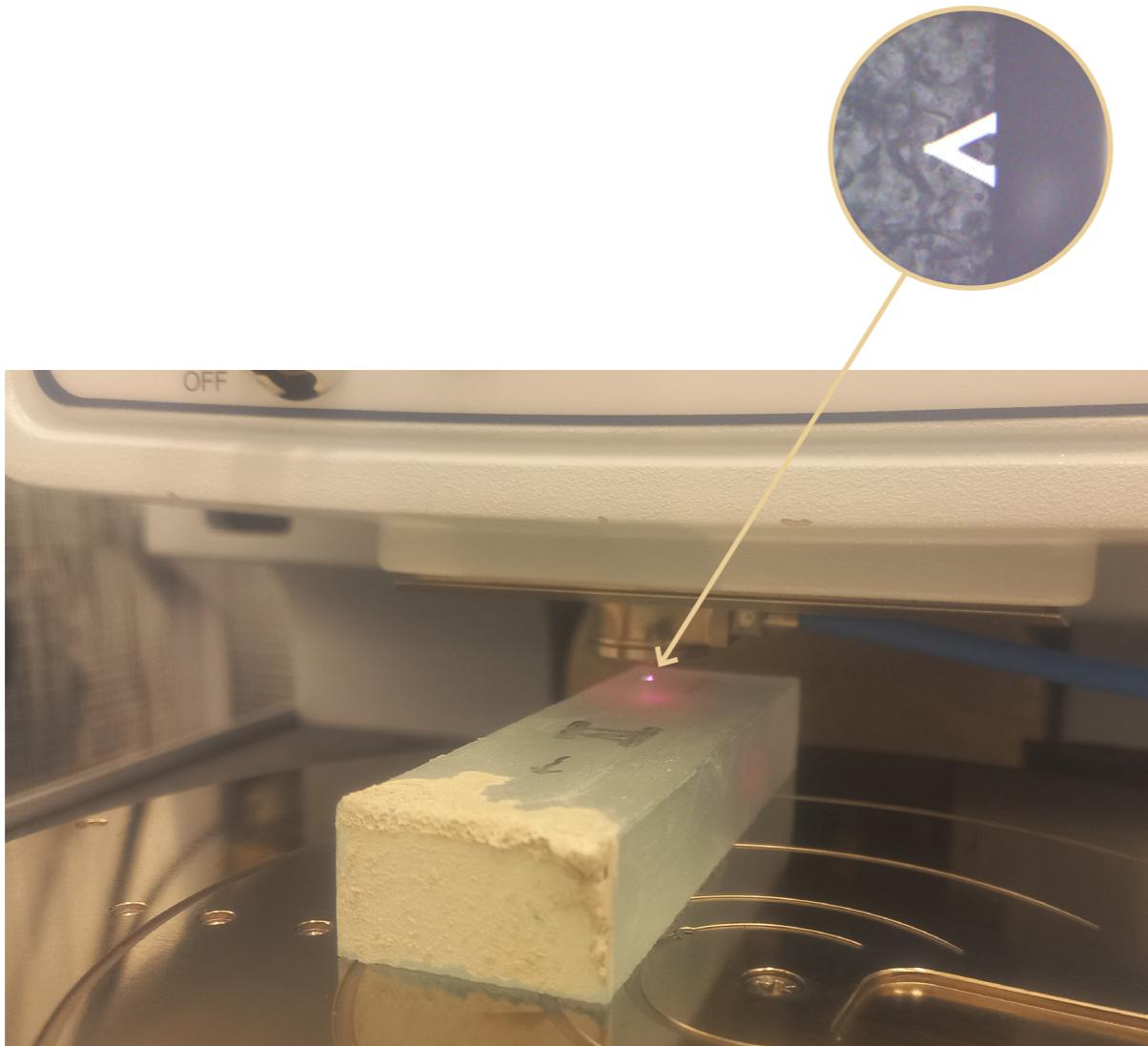


Does the **unpolished** surface and impurity from **mould particles** of a cast glass element increase the **adhesion strength** of a hybrid interface?



MICROSCOPE

Set-up



Atomic Force Microscop (AFM)

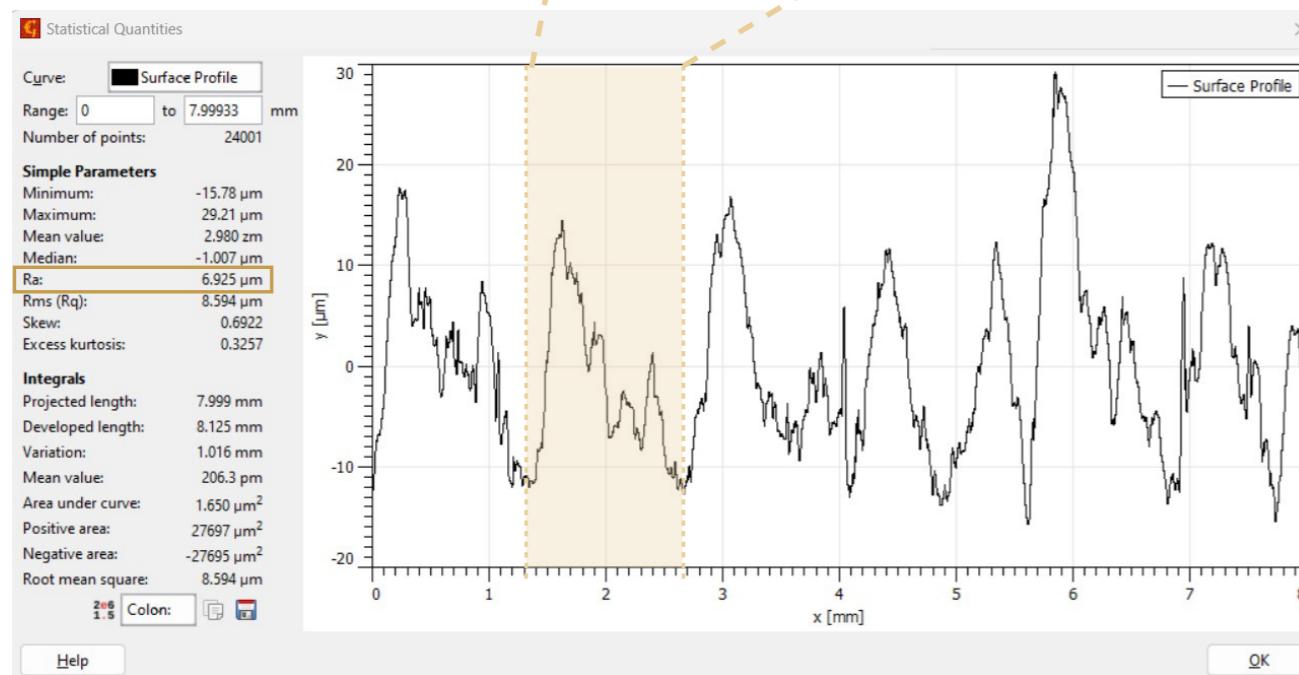
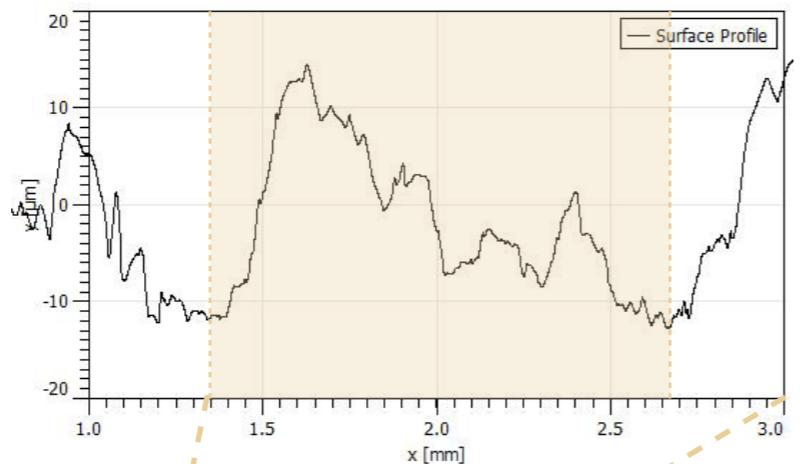


Surface unpolished cast glass.

PROFILOMETER

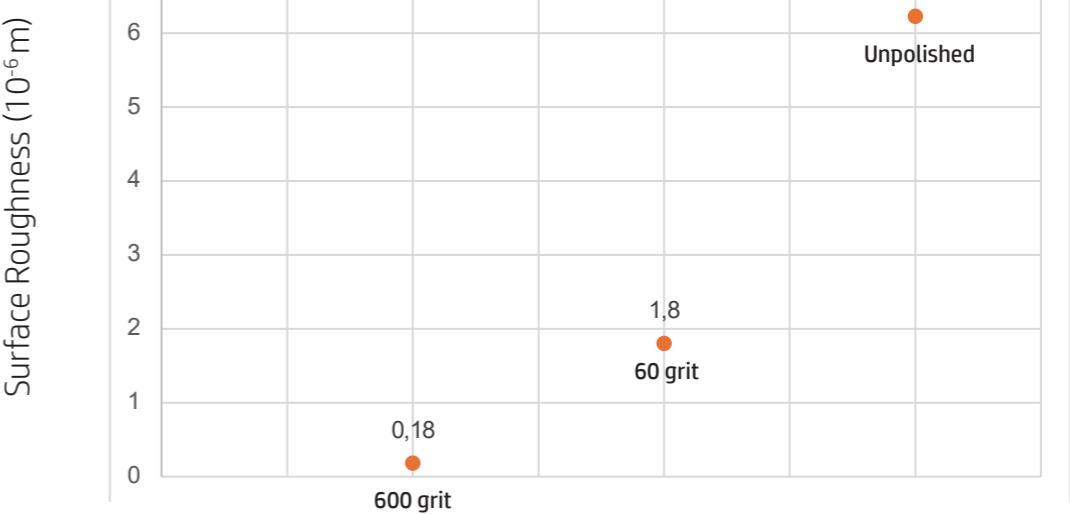
Surface Roughness

Peak average $R_a = 5.656 \mu\text{m}$



Average surface roughness
 $R_a = 6.225 \mu\text{m}$

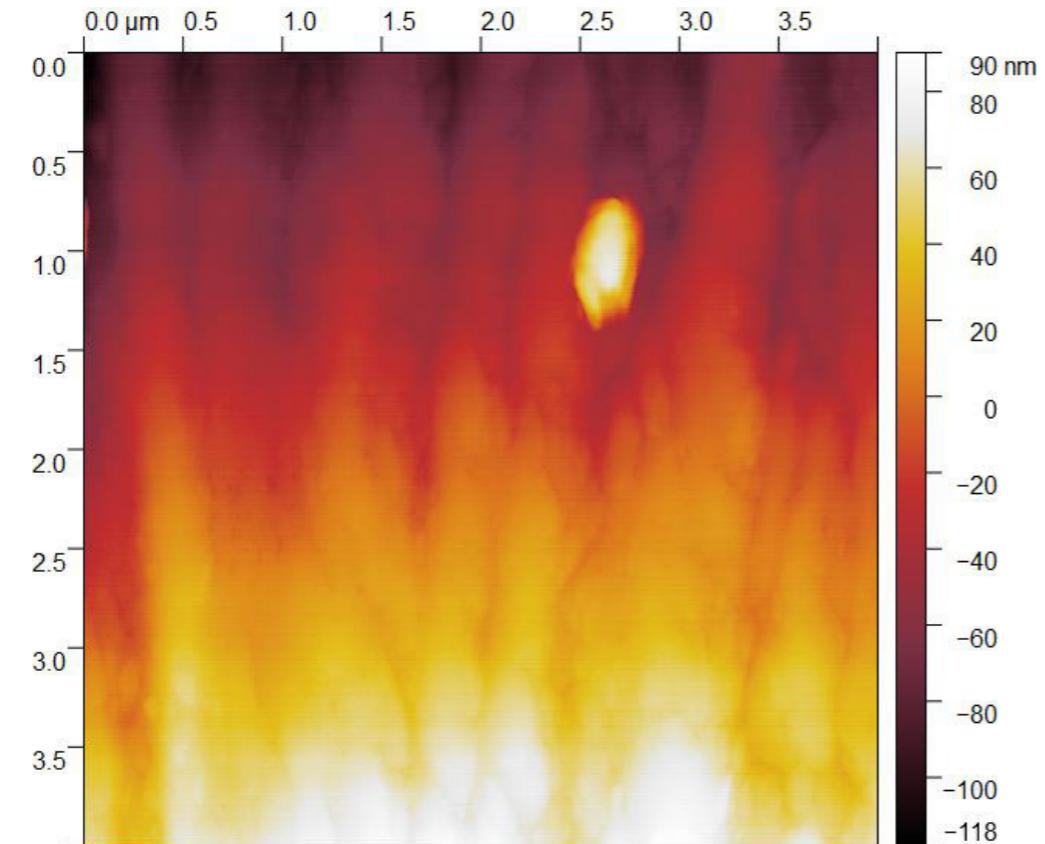
Surface Roughness of glass profiles



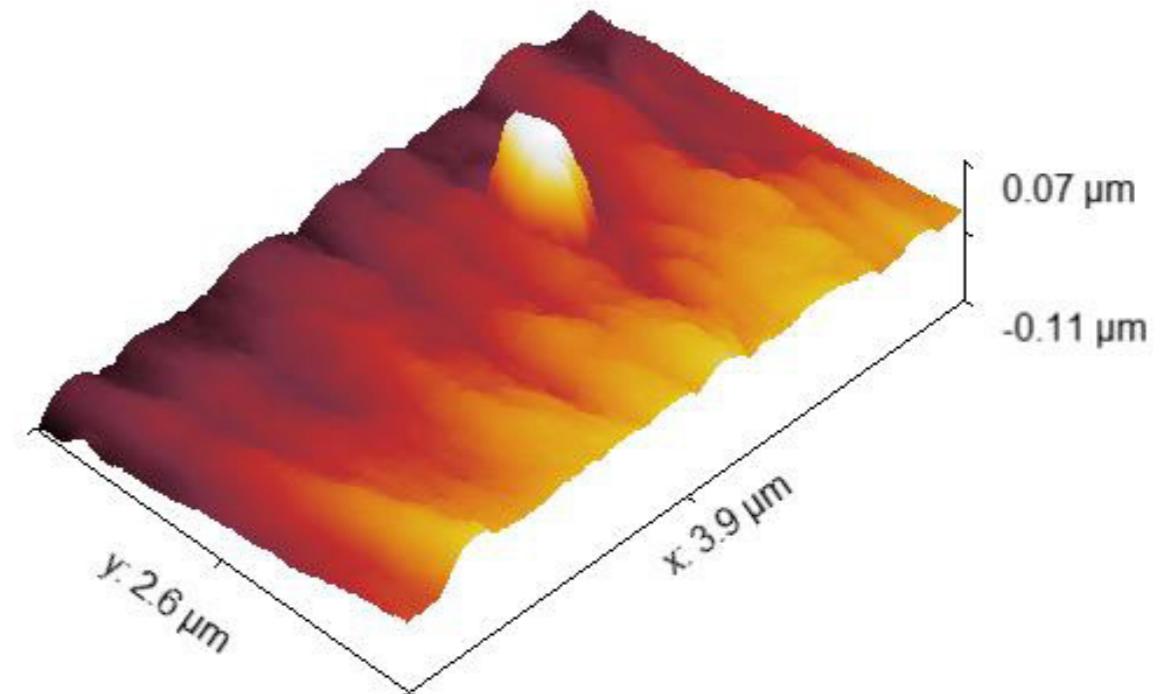
AFM RESULTS

Mould particle

Mould particles have a size of an **0,2 x 0,1 μm**



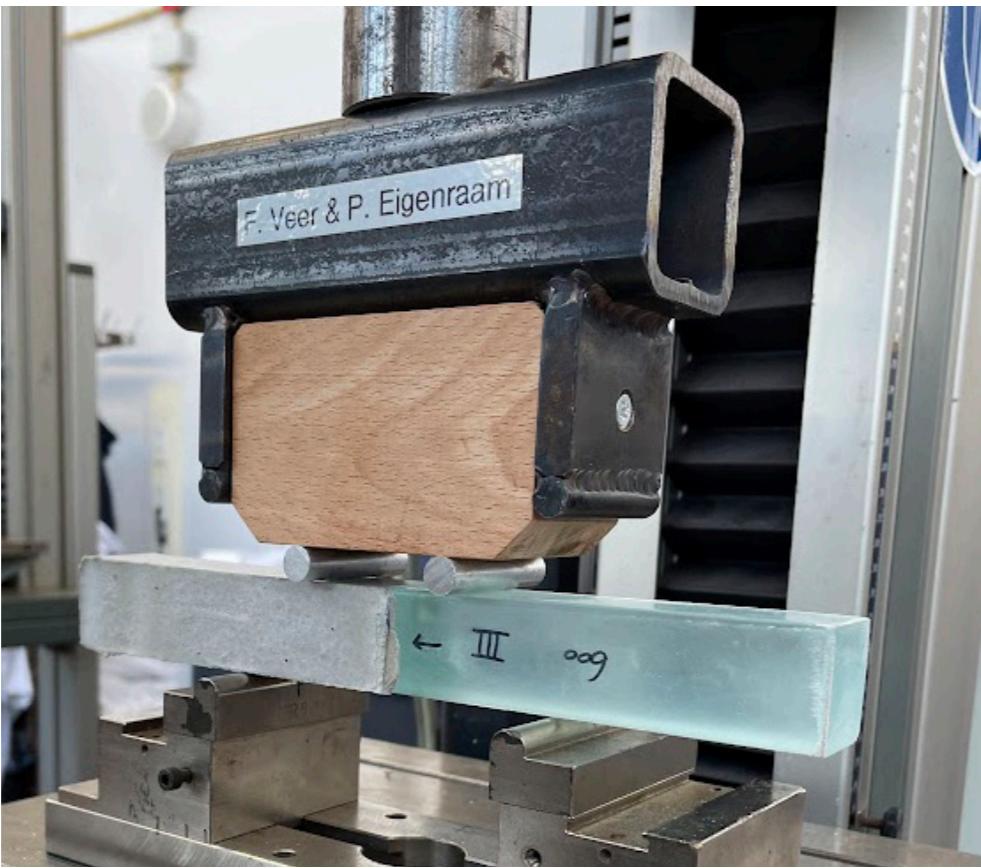
Roughness profile measured on $3.5 \times 3.5 \mu\text{m}$ surface



3D visualisation of the measured surface profile with a mould particle.

TIME FOR TESTING

4-POINT BENDING



DIRECT SHEAR TEST



4 POINT BENDING

Test

4-POINT BENDING TEST 1

SPECIMEN 240 x 30 x 30 mm



DIFFERENT SURFACE ROUGHNESSES



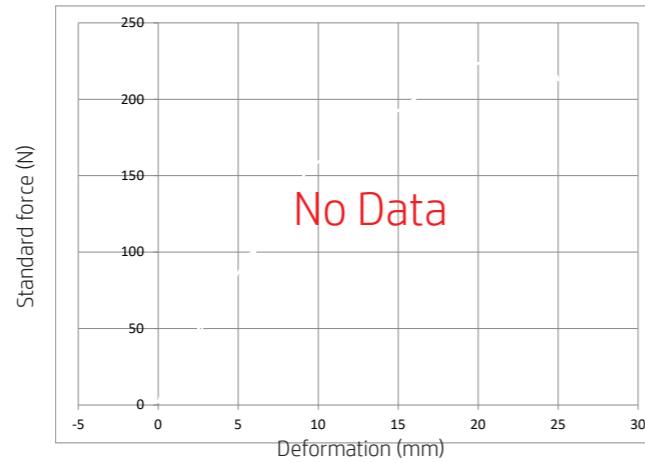
POUR RESULTS

Failure

Pouring #1



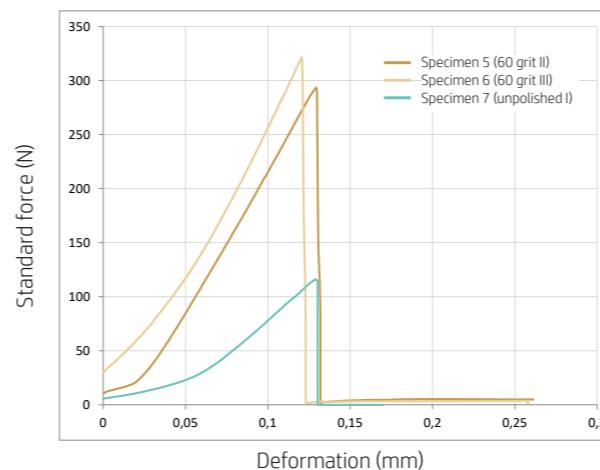
4-point bending results (Pour 1)



Pouring #2



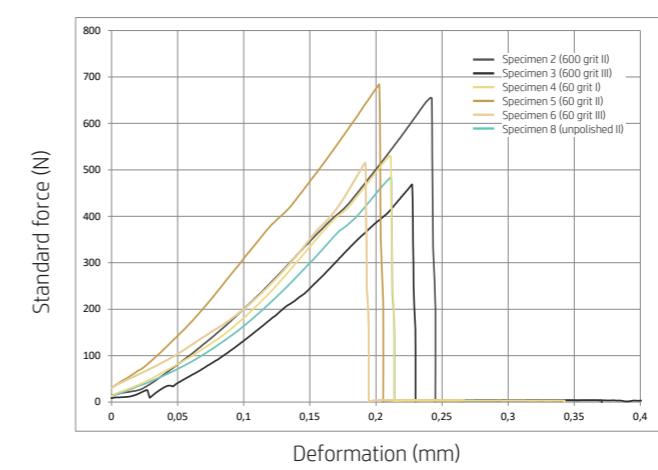
4-point bending results (Pour 2)



Pouring #3

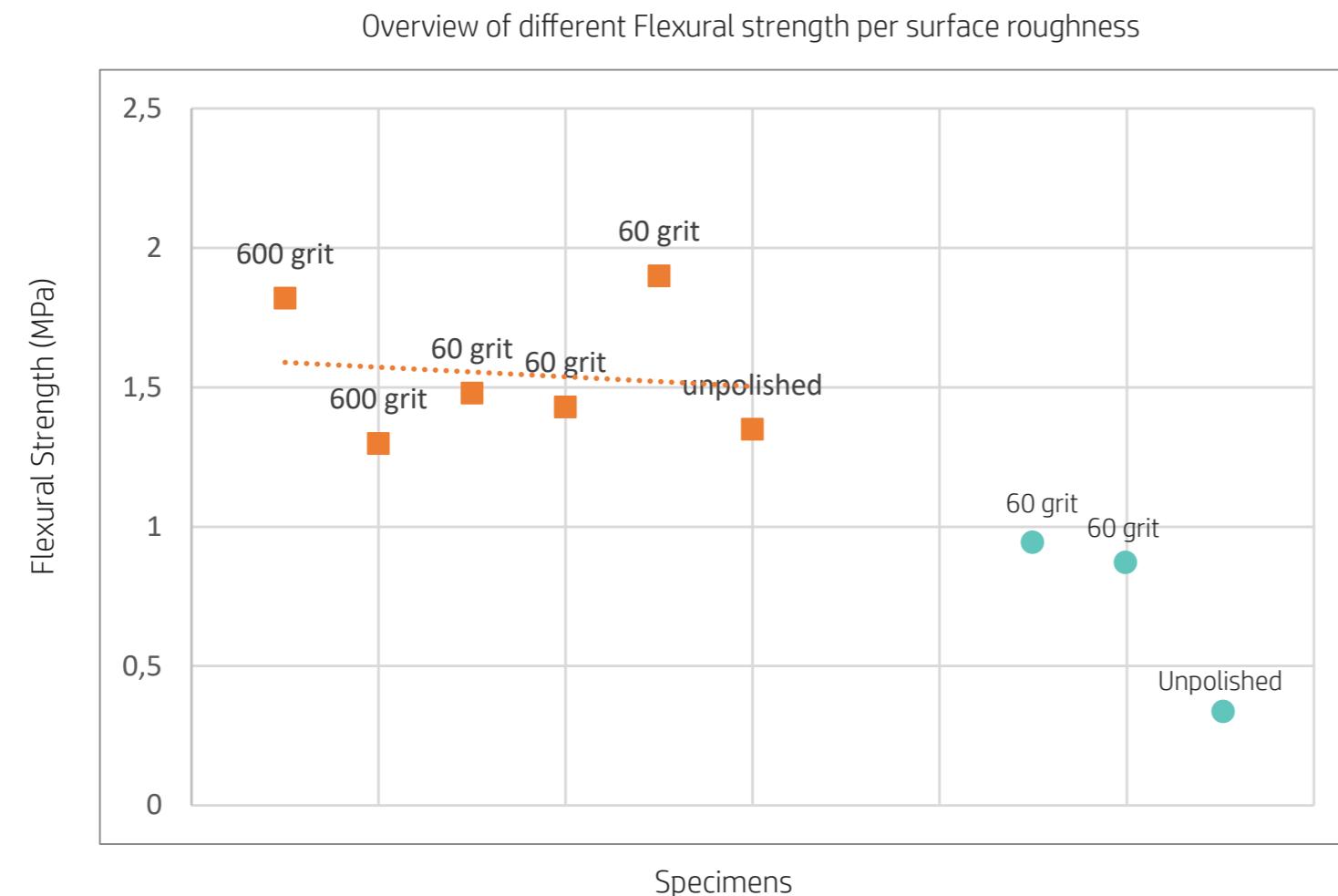


4-point bending results (Pour 3)



OVERVIEW TEST 1

Bending

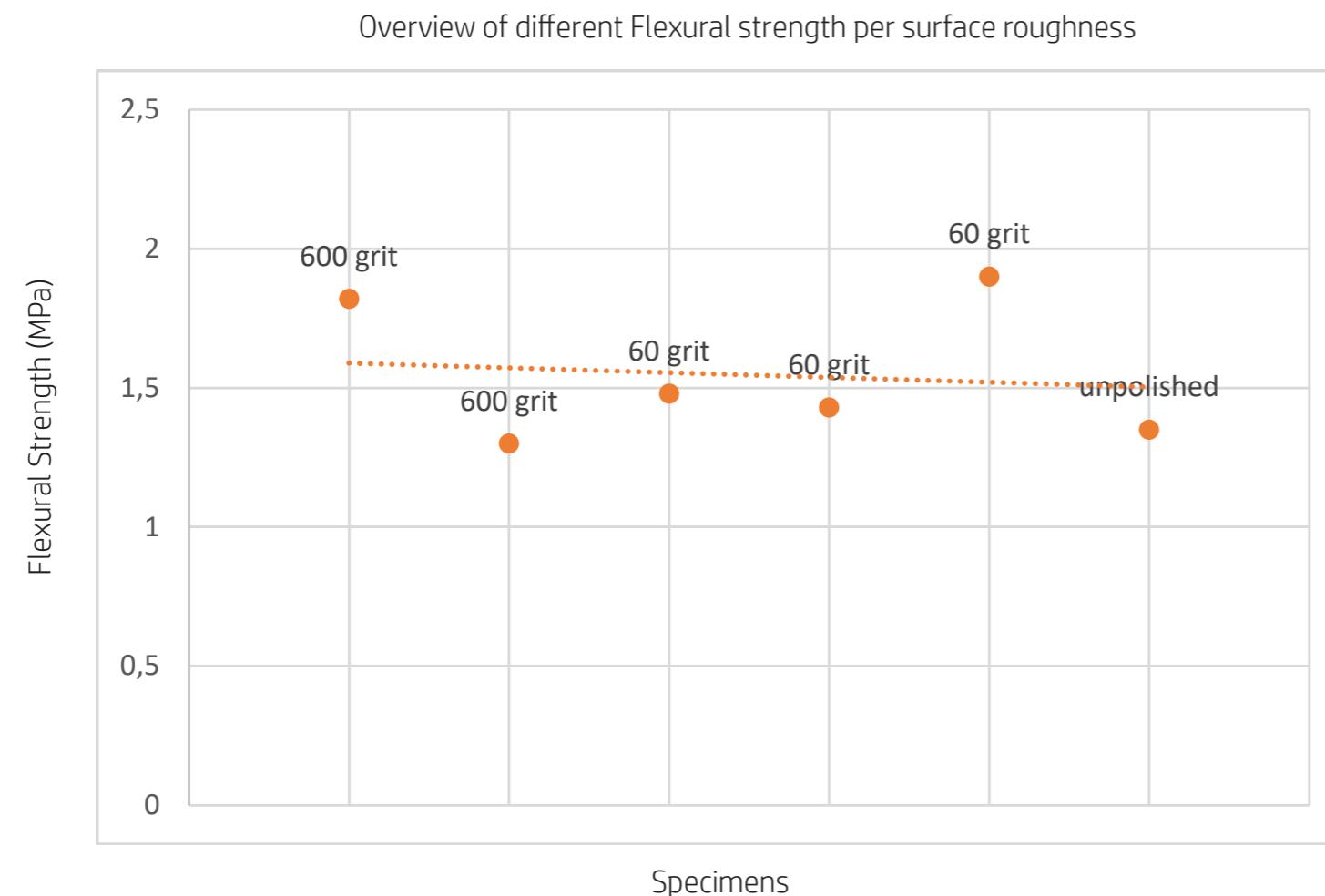


CONCLUSION

- A **well mixed concrete** mixture significantly improves the bond adhesion and strength

OVERVIEW TEST 1

Bending



CONCLUSION

- A **well mixed concrete** mixture significantly improves the bond adhesion and strength
- **Constant flexural strength** despite the different surface roughness
- All specimens had a clear break: **Brittle behaviour**
- Surface roughness influenced the **interface adhesion**
- Unpolished surface does **not improve** the interface adhesion and strength

4-POINT BENDING TEST 2

SPECIMEN 240 x 30 x 30 mm



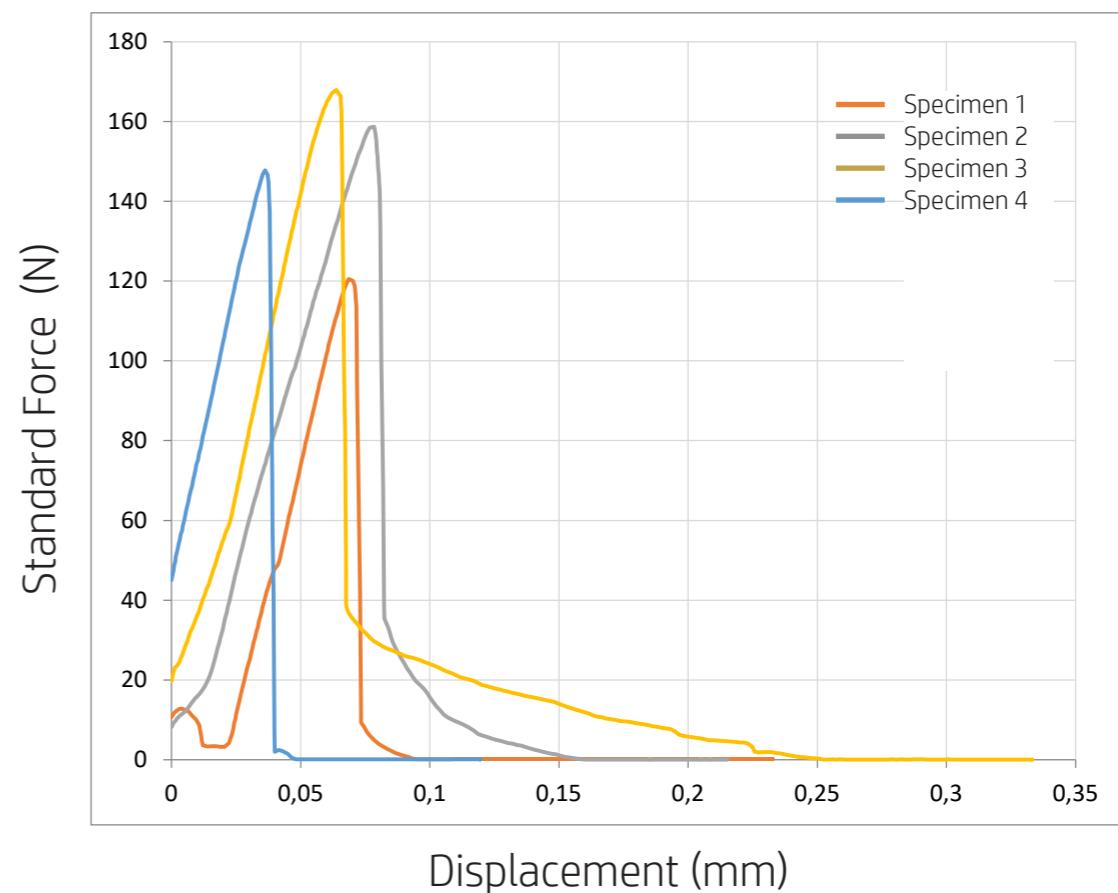
INTERLOCKING FORM



4-POINT BENDING TEST 2



Four point bending test

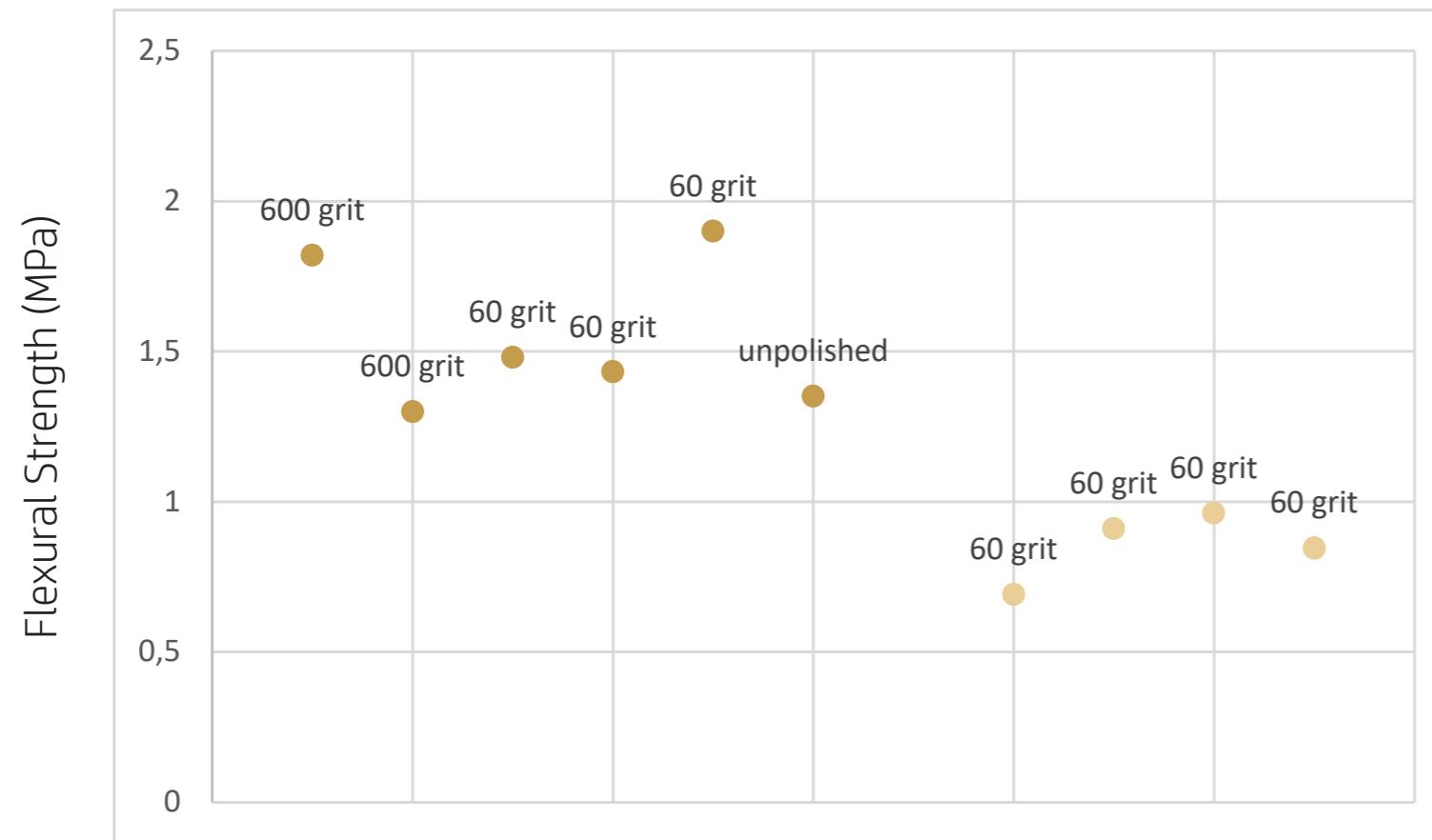


CONCLUSION

Bending stress



Bending stress overview of two 4 point bending tests



CONCLUSION:

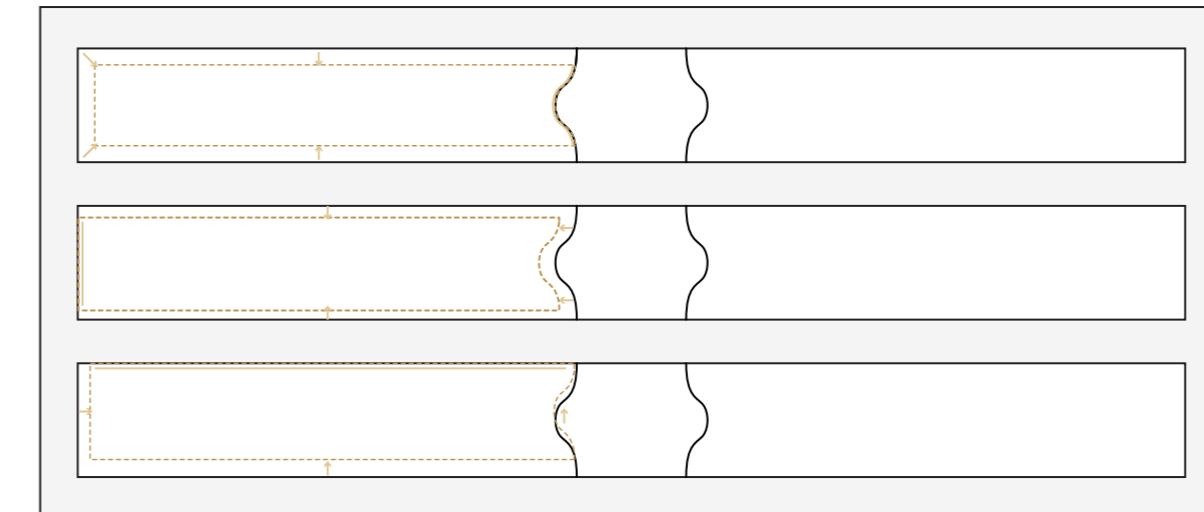
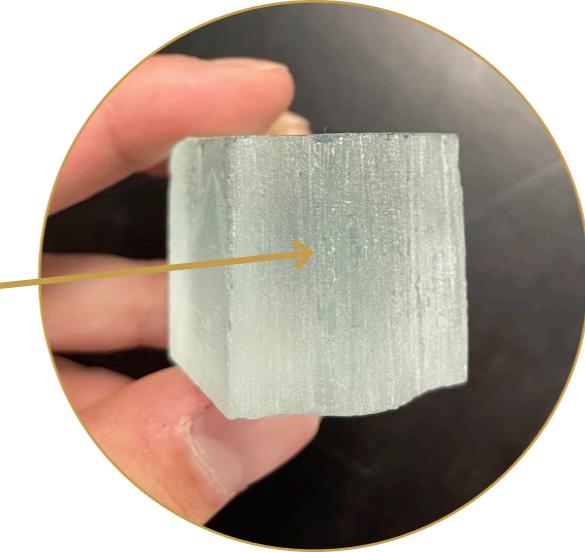
- Test 2 showed a lower bending stress capacity primarily due to the presence of **two interfaces**.
- The bending stress capacity remains **insufficient** for implementing a full-scale facade panel
- all specimens exhibited non-brittle failure, indicating that the interlocking form contributed **energy absorption in the interface**

#2 DIRECT SHEAR TEST



SHRINKAGE STRESS

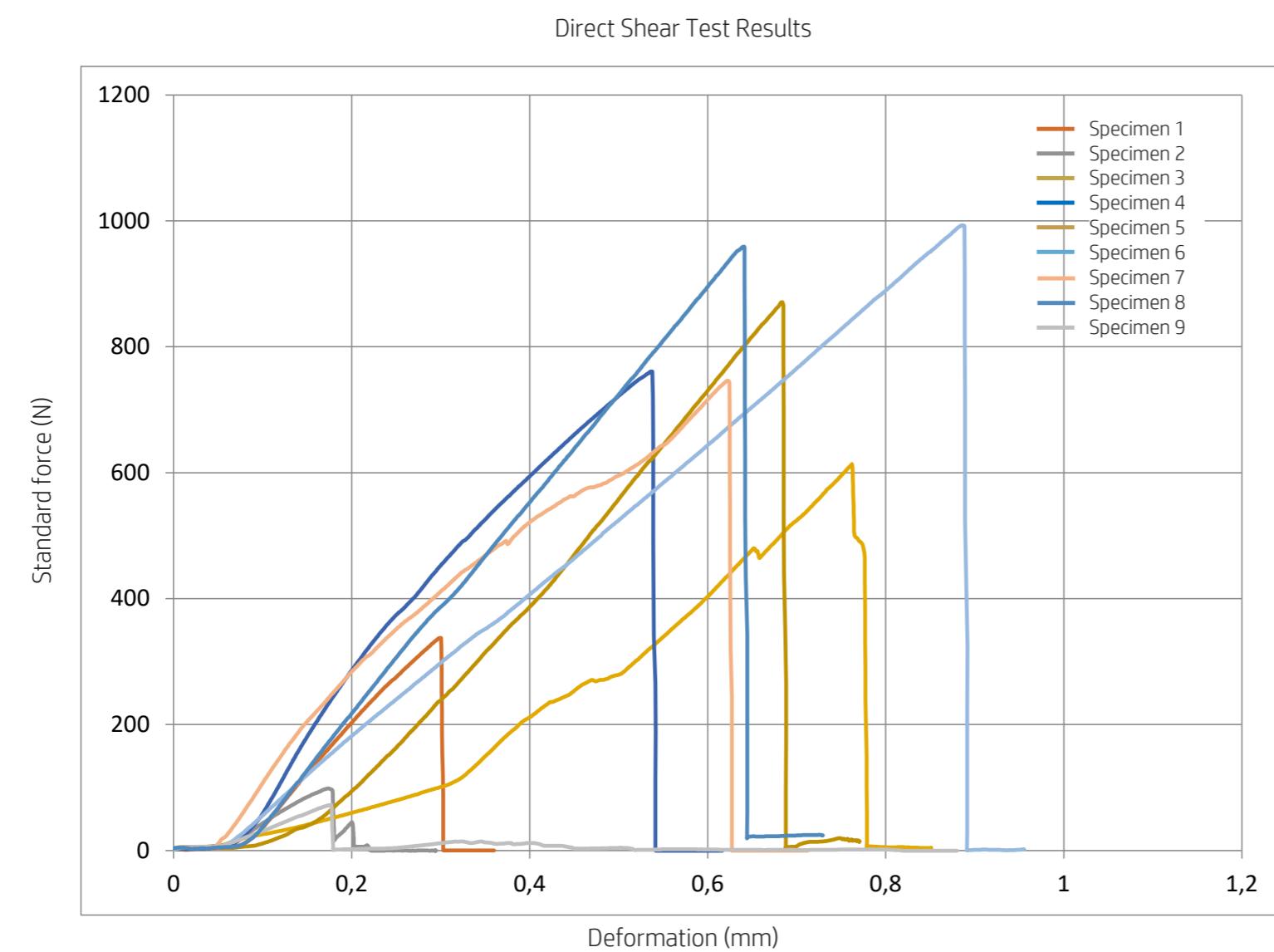
Concrete curing



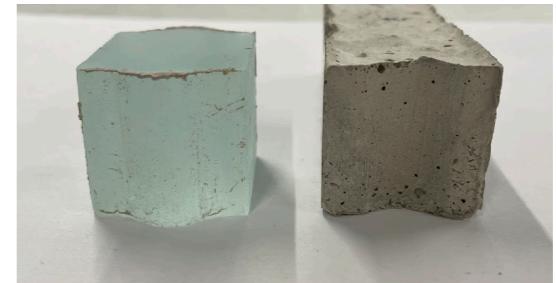
$$\sigma_{\text{shrinkage}} \text{ (MPa)} > \sigma_{\text{adhesion}} \text{ (MPa)}$$

FAILURE MODE

Shear



(1)



Interfacial failure

(2)



Interfacial failure + Concrete failure

(3)

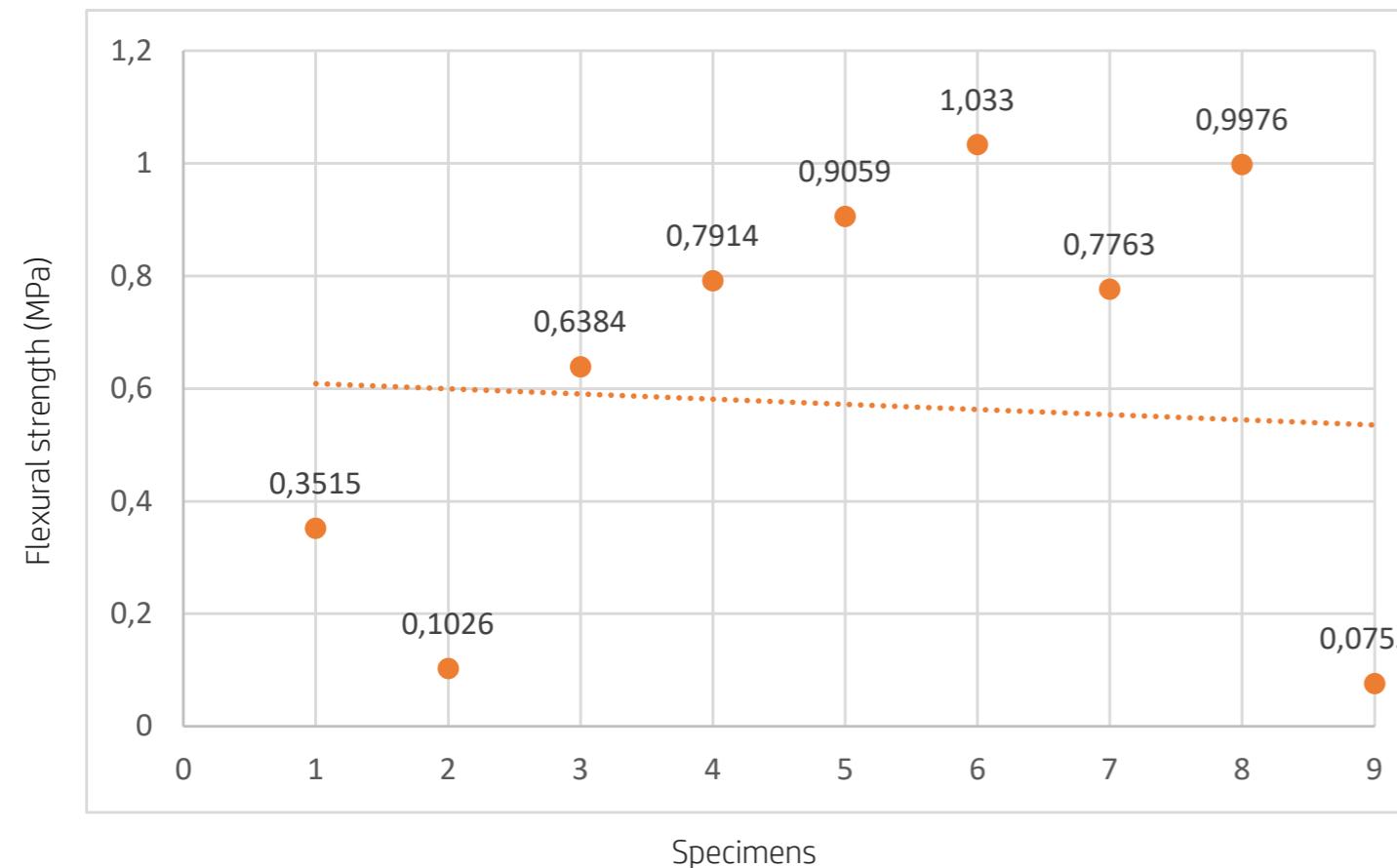


Serrated interfacial failure

CONCLUSION TEST 1

Shear

Overview Shear stress capacity of th the direct shear test results



CONCLUSIONS

- Concrete **shrinkage** causes stresses and adhesion failure that pull the glass on one side.
- The occurrence of a serrated failure suggests a significant degree of interaction between the concrete and glass
- formation of physical anchorages at the interface due the interlockiong form.
- serrated failure mode of the interface indicates a failure in the concrete

SHEAR TEST

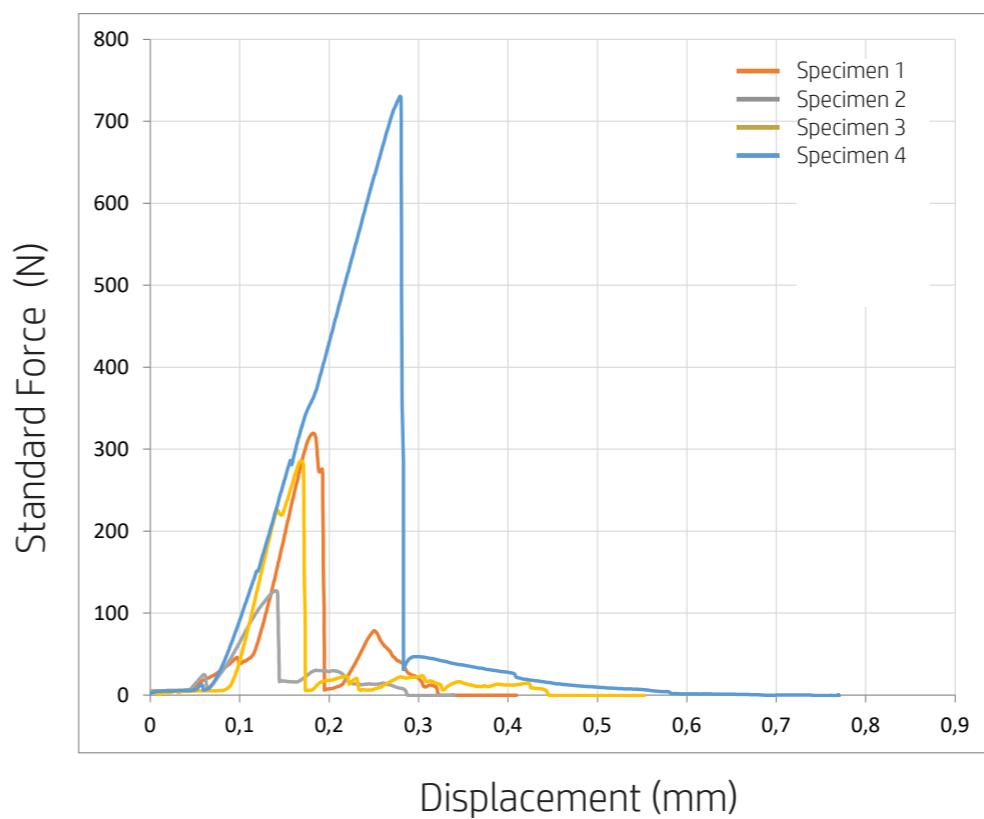
Test 2



DIRECT SHEAR TEST #2



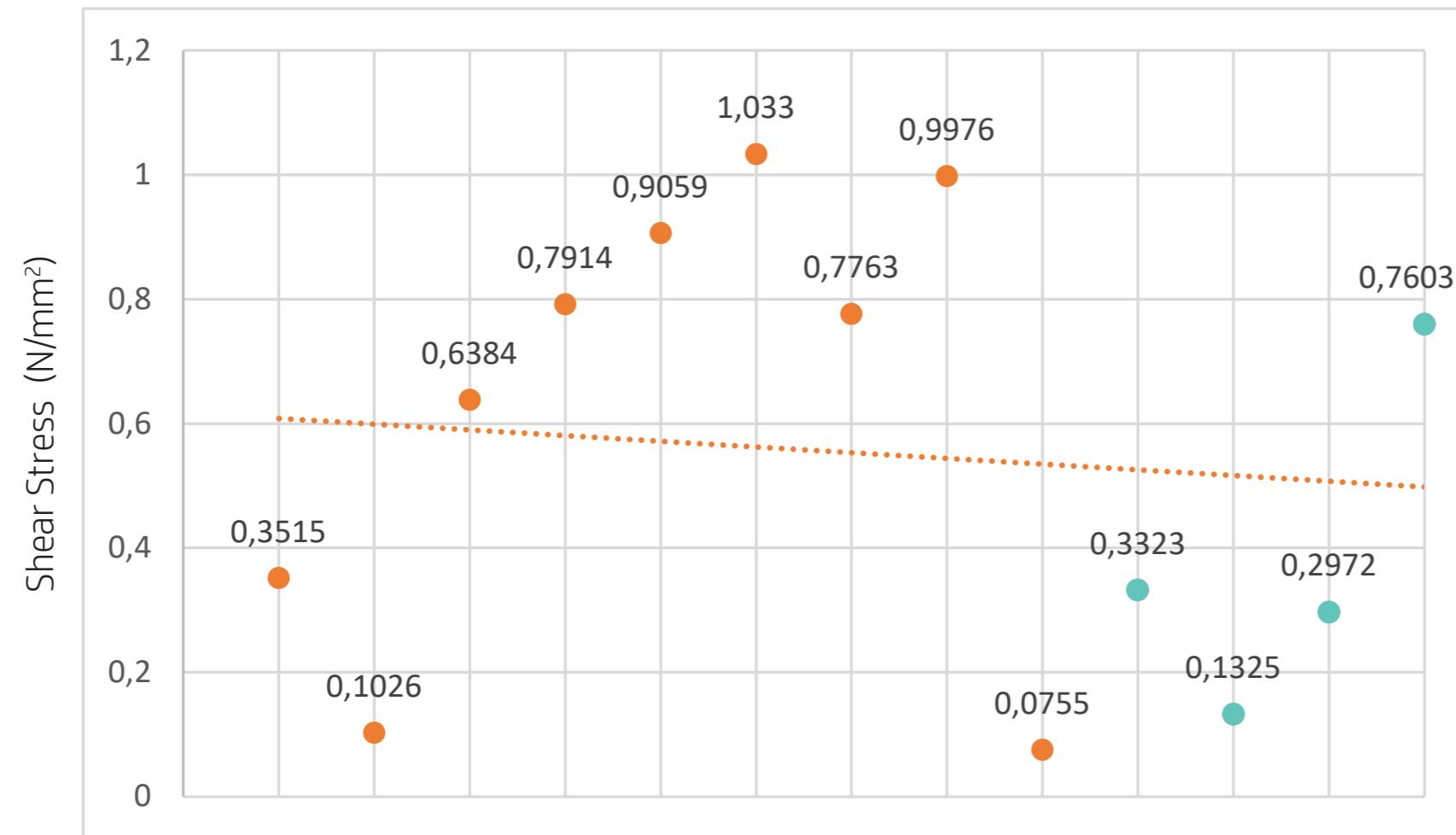
Direct shear test



SHEAR STRESS TEST

Overview

Direct shear test comparisson



60 grit polished in one direction

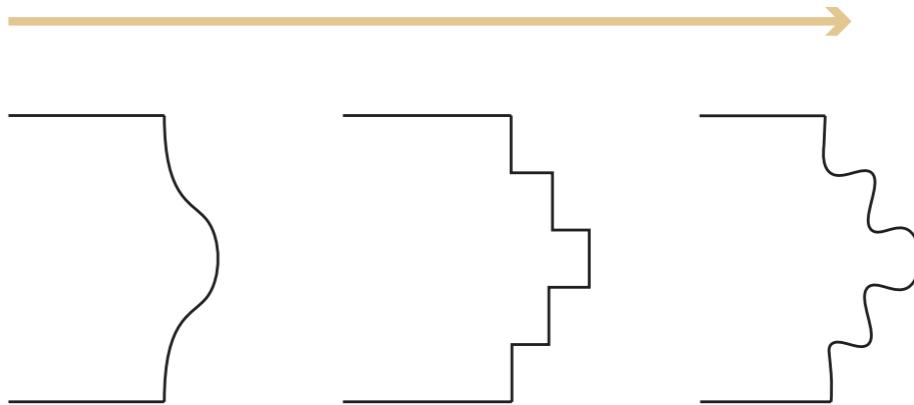


Diagonal cut with a dremmel

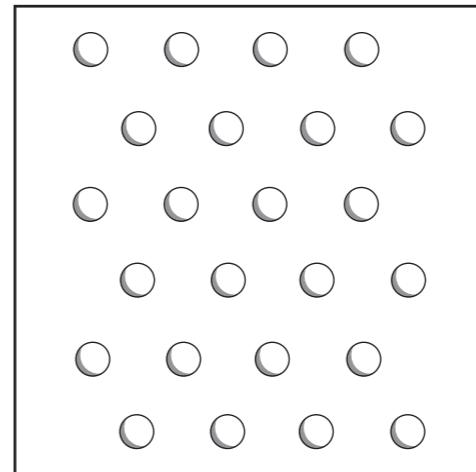
RECOMMENDATIONS

Design

- MORE EXTREME INTERLOCKING FORMS
- SURFACE ROUGHNESS INCORPORATED IN MOULD DESIGN
- NOT MICRO-SCALE BUT MACRO-SCALE ROUGHNESS
- IMPROVED CONCRETE MIXTURE (GRC OR UHPC)
- DIFFERENT SODA_LIME GLASS COM-
POISTIONS (ART GLASS)



More interlocking form

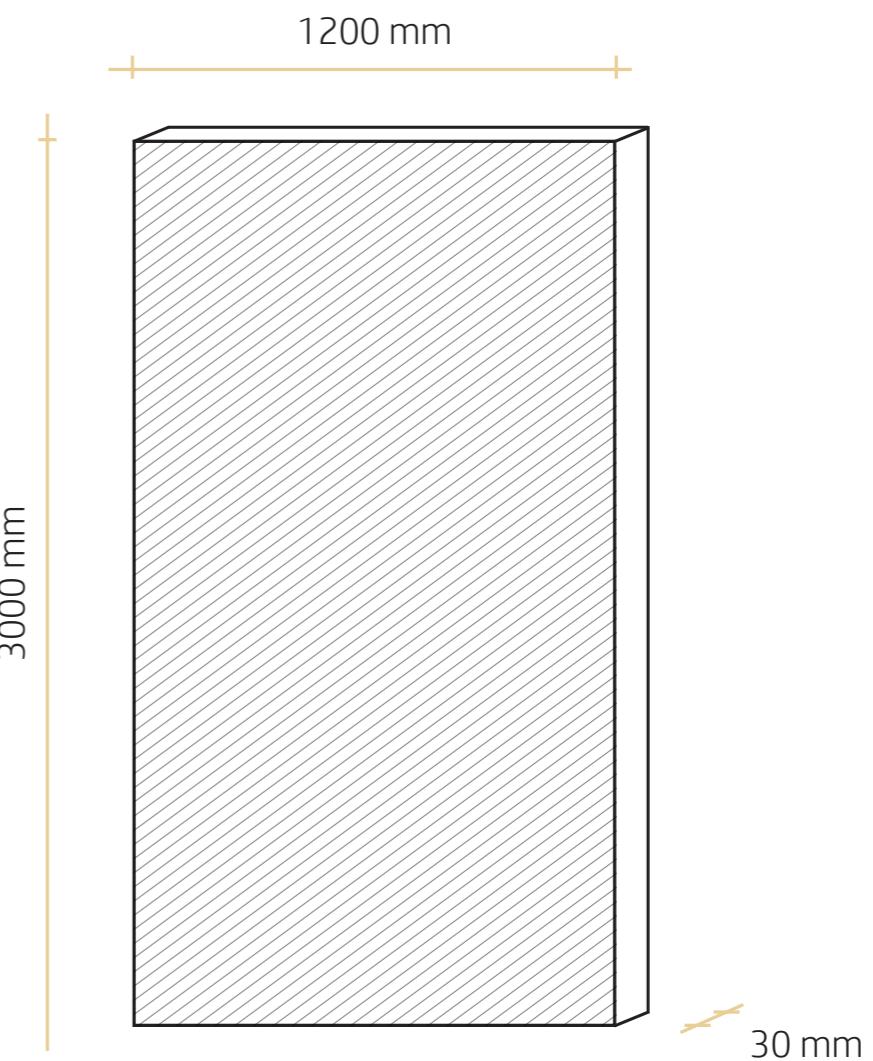
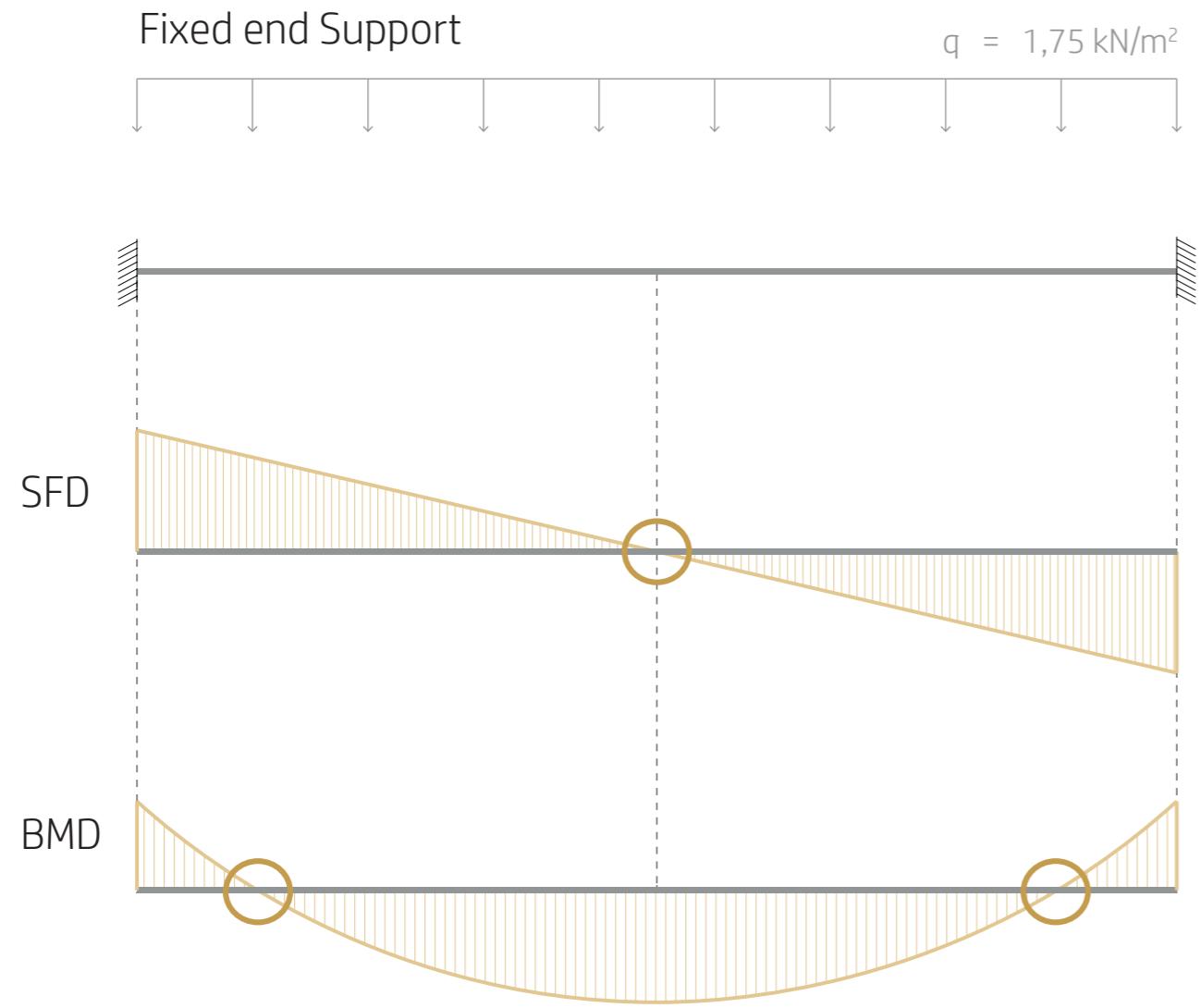


Dimpled surface as macro-roughness

What if put a hybrid interface in a facade panel?

HYBRID PANEL

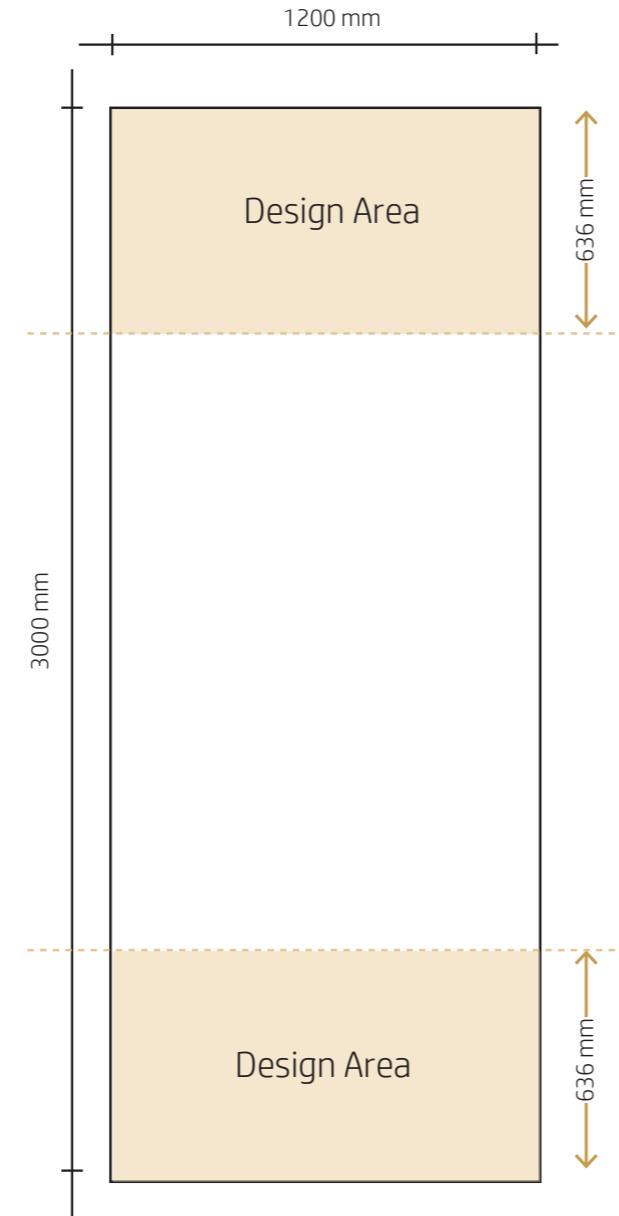
Support system



DESIGN AREA

Bending

BENDING



Limited Design Freedom

FORMULA FINDING DESIGN BENDING AREA:

$$M_x = \frac{w}{12} (6Lx - L^2 - 6x^2)$$

Where ' M_x ' is calculated with

$$\sigma = \frac{M*y}{I}$$

$$\sigma = 1,603 \text{ N/mm}^2$$

$$y = 15 \text{ mm}$$

$$I = 2700000 \text{ mm}^4$$

$$288540 = \frac{1750}{12} (6*3000x - 3000^2 - 6x^2)$$

We find 'x' as design area limit

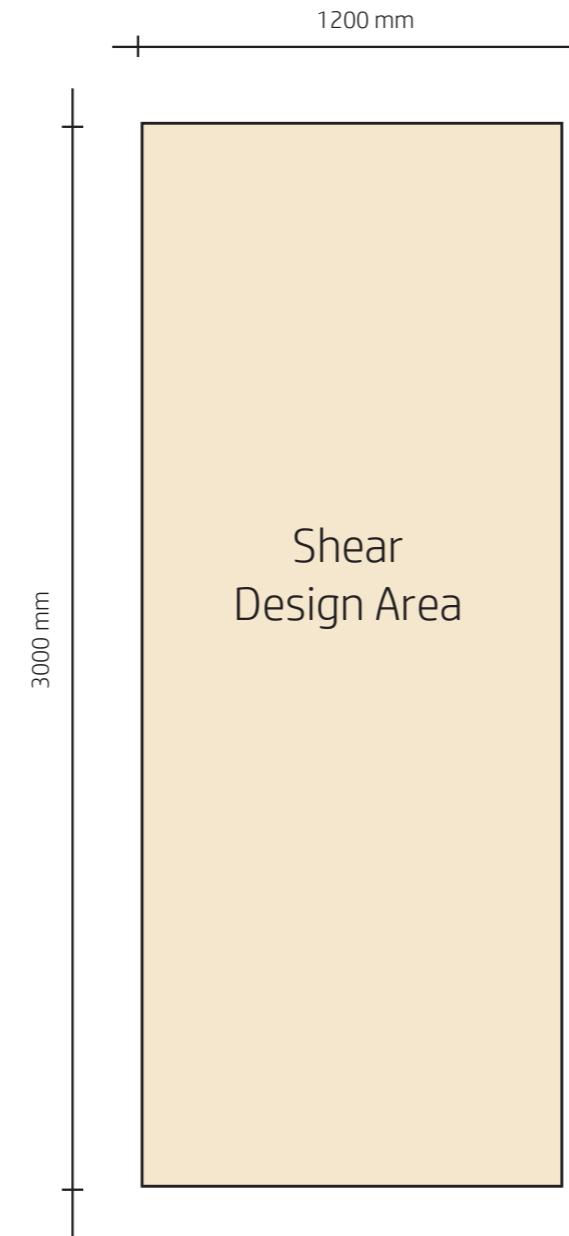
$$x = 635,95 \text{ mm and}$$

$$x = 2364,05 \text{ mm}$$

DESIGN AREA

Shear

SHEAR



Full Design Freedom

FORMULA FINDING DESIGN SHEAR STRESS CAPACITY:

$$\tau = \frac{V}{A}$$

V = maximum load

A = shear load area

$$\begin{aligned}\tau &= \frac{2625 \text{ N}}{38448,12 \text{ mm}^2} \\ &= 0.0683 \text{ N/mm}^2\end{aligned}$$

$$T_{\text{interface}} = 0,567 \text{ N/mm}^2 > T_{\text{panel}} = 0,0683 \text{ N/mm}^2$$

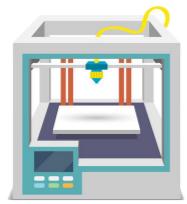
PART II:

DESIGN PART

MANUFACTURING

Steps

MANUFACTURING CONSIST OF 3 PARTS:



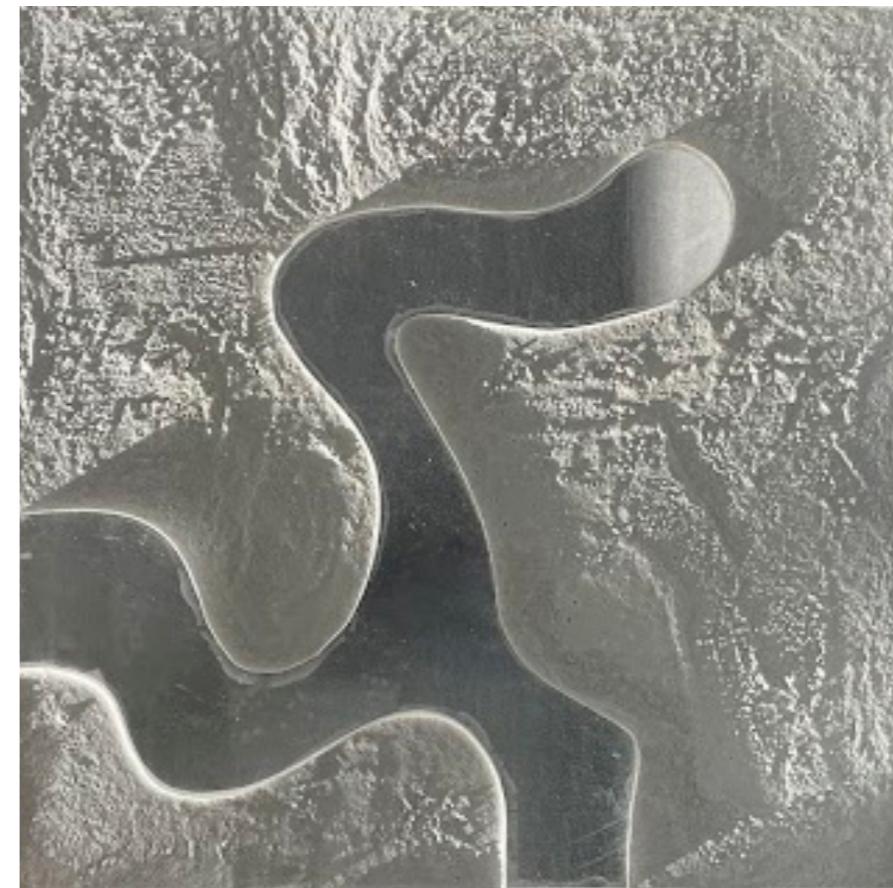
I Mould manufacturing



II Glass manufacturing

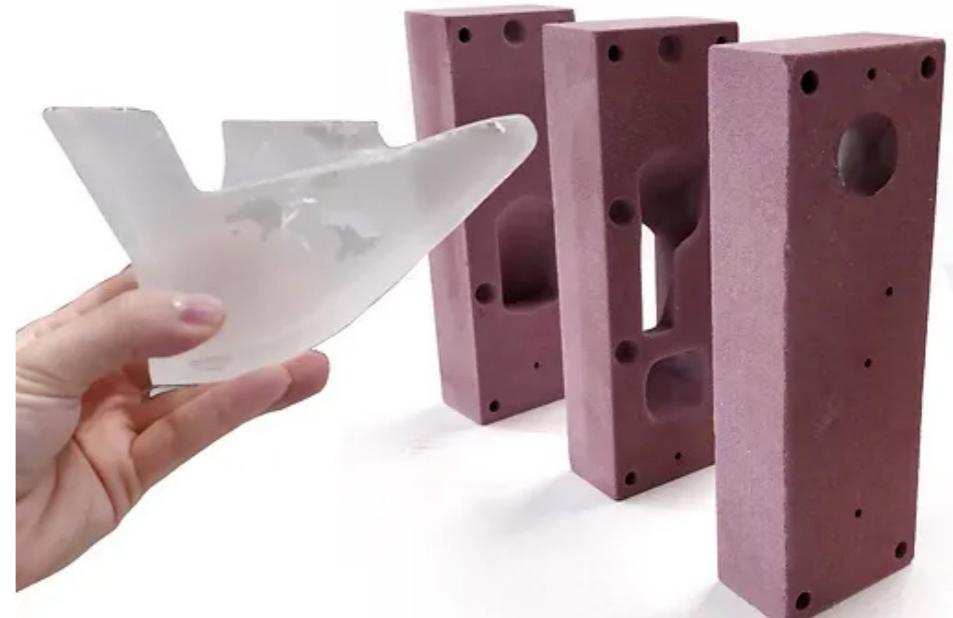
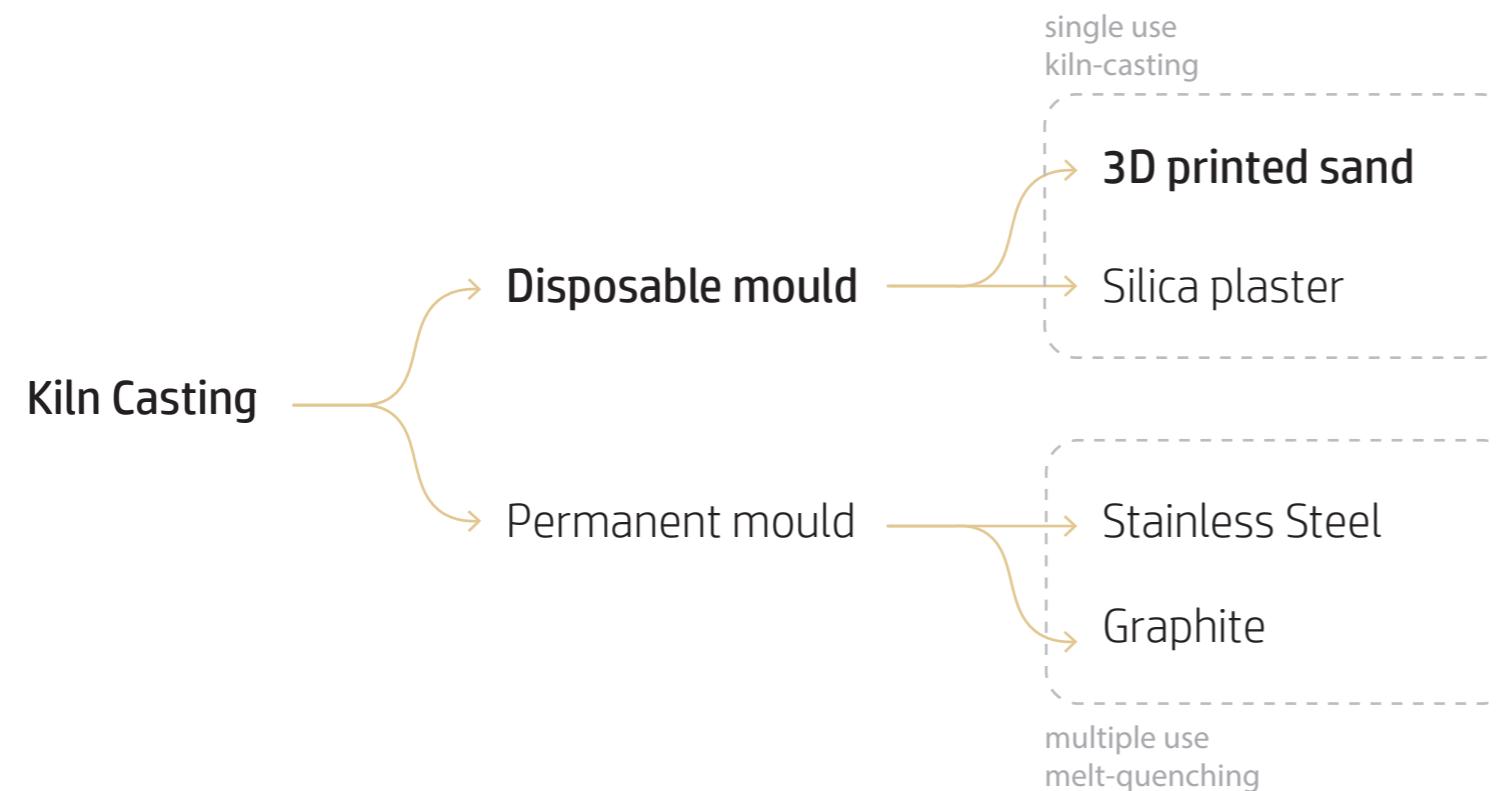


III Concrete manufacturing



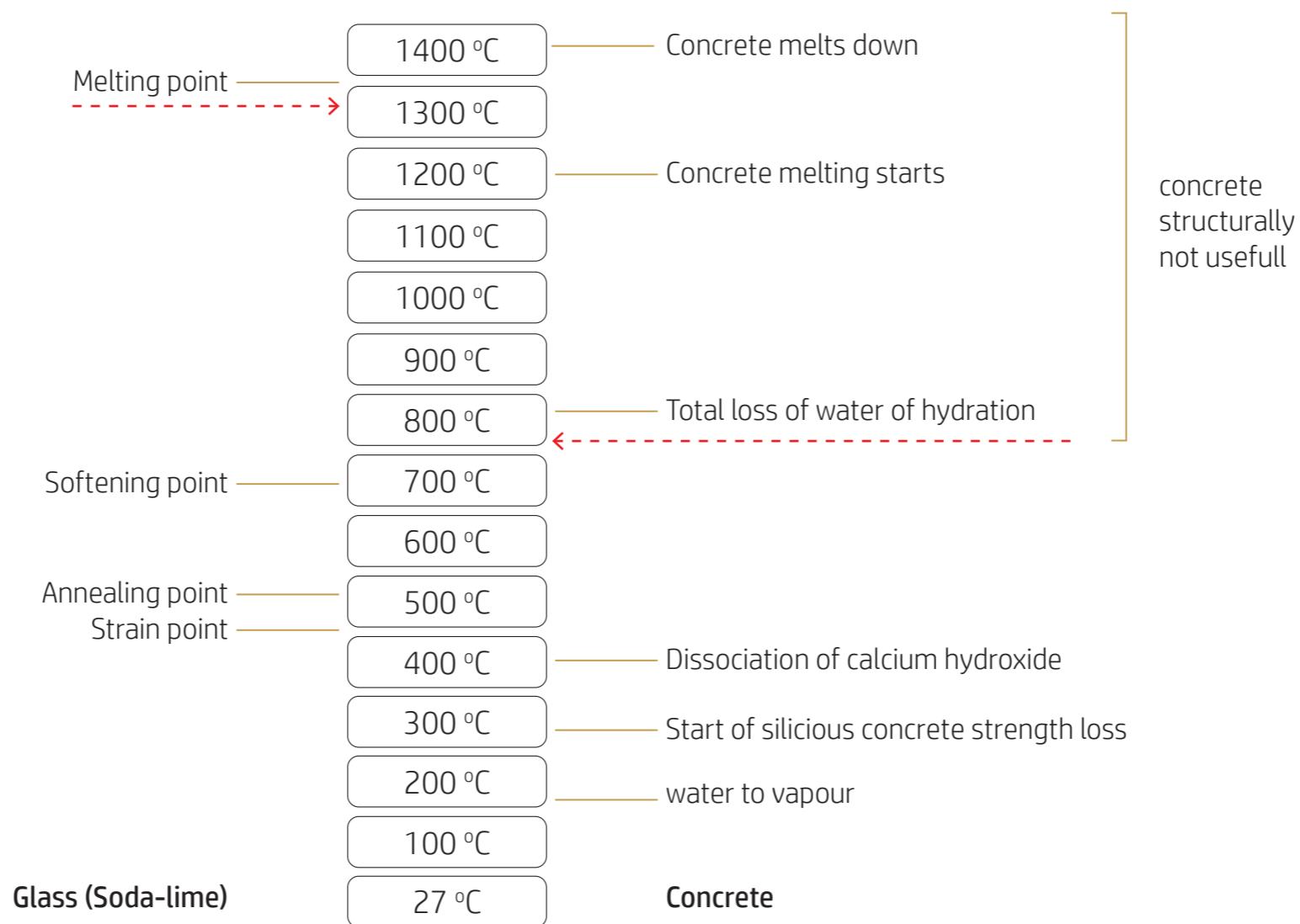
MANUFACTURING

Mould



- Biggest printable scale
- Industrialised process
- Recyclable potential

First cast glass → secondly pour concrete



DESIGNED FOR DISASSEMBLY



IMPLEMENTATION

Seagram

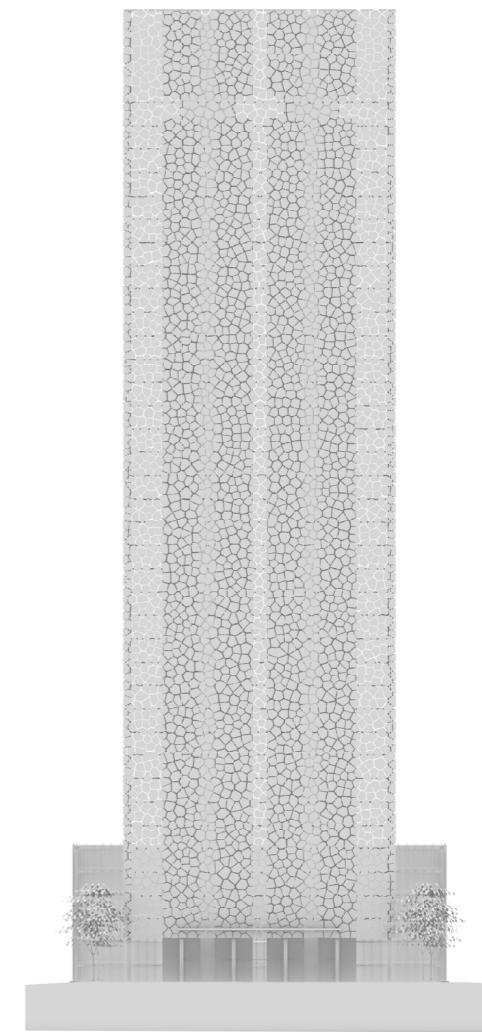
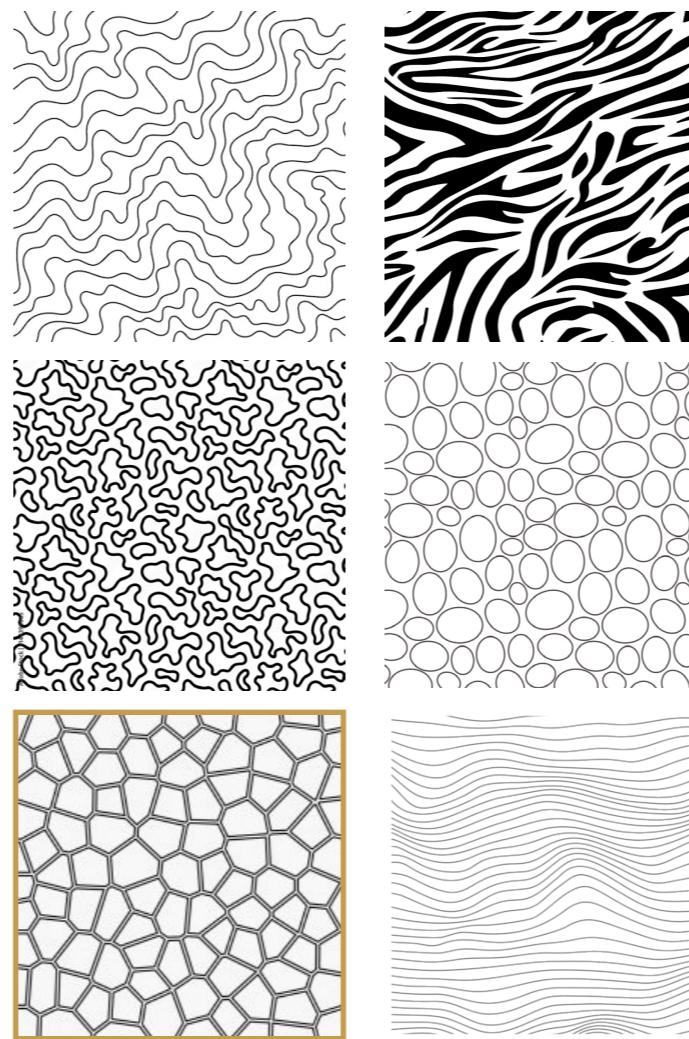
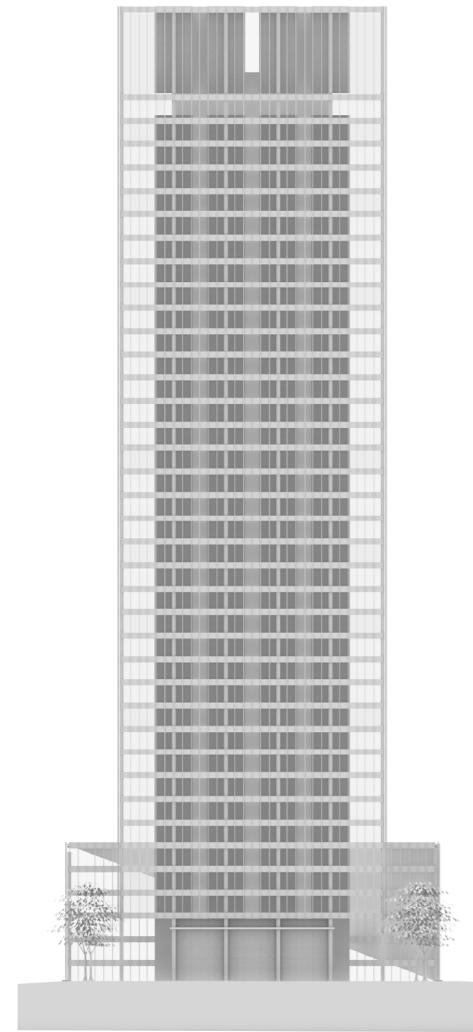


SEAGRAM OFFICE BUILDING - NEW YORK

- Single glazed
- Shading only open or closed
- Overheating in summer
- Monotone Facade

FREE-FORM DESIGN

Facade



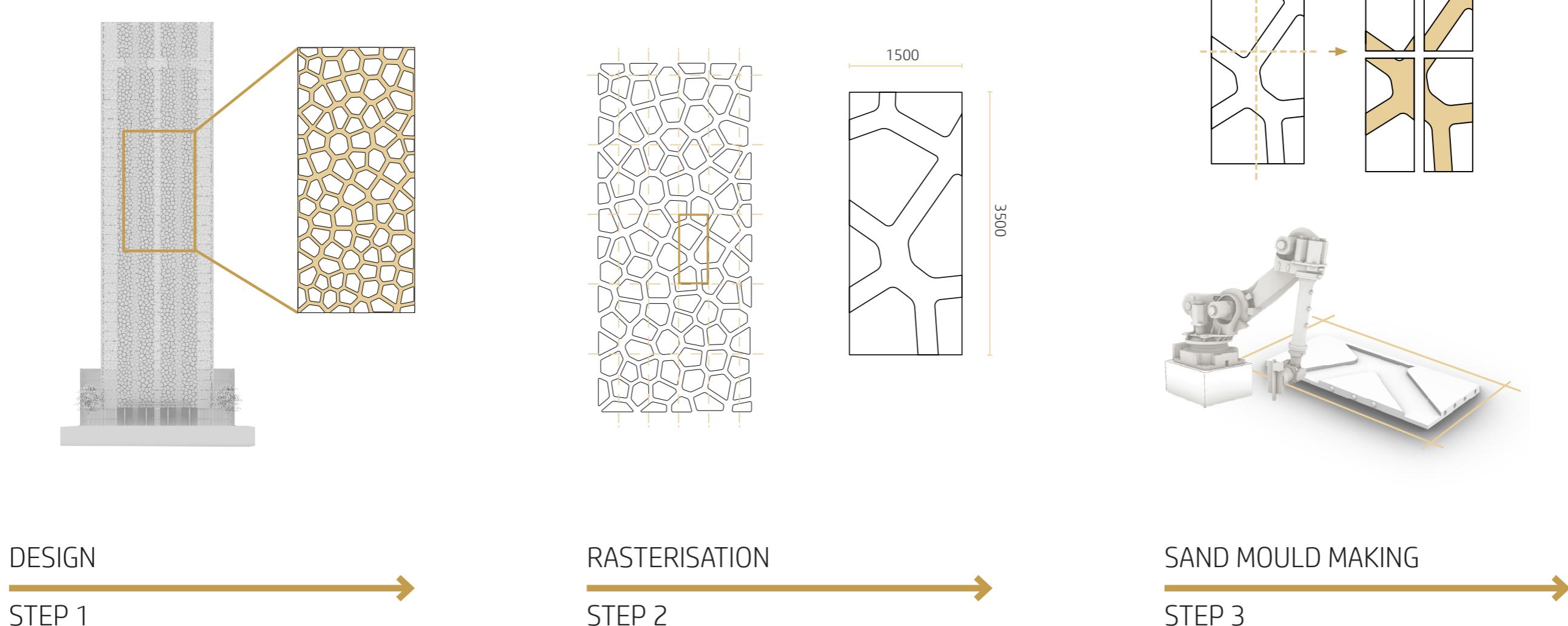
Current situation

Make free-form design

Design option

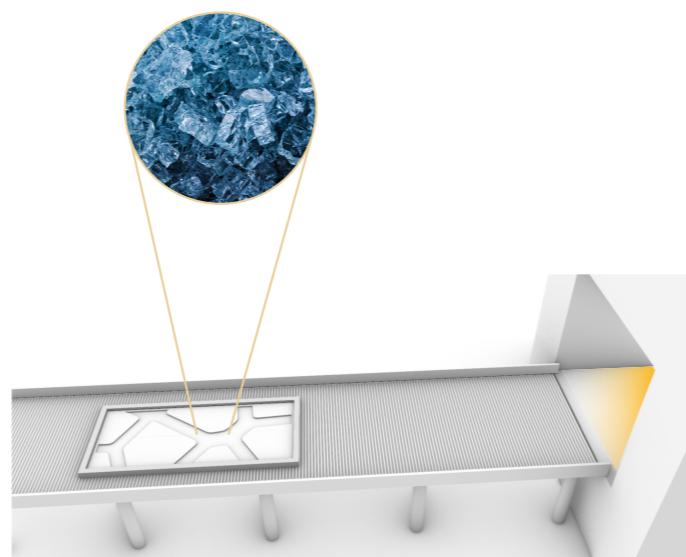
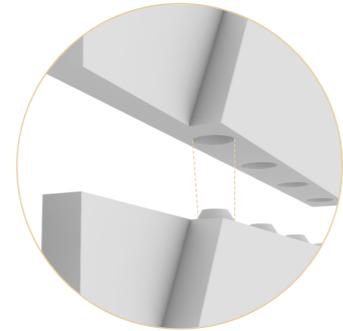
PRODUCTION STEPS

Panel



PRODUCTION STEPS

Panel

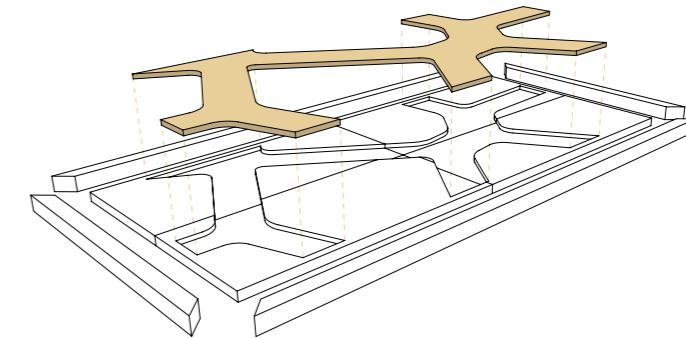


ASSEMBLY SAND MOULD

STEP 4

CULLET PLACING + FIRING

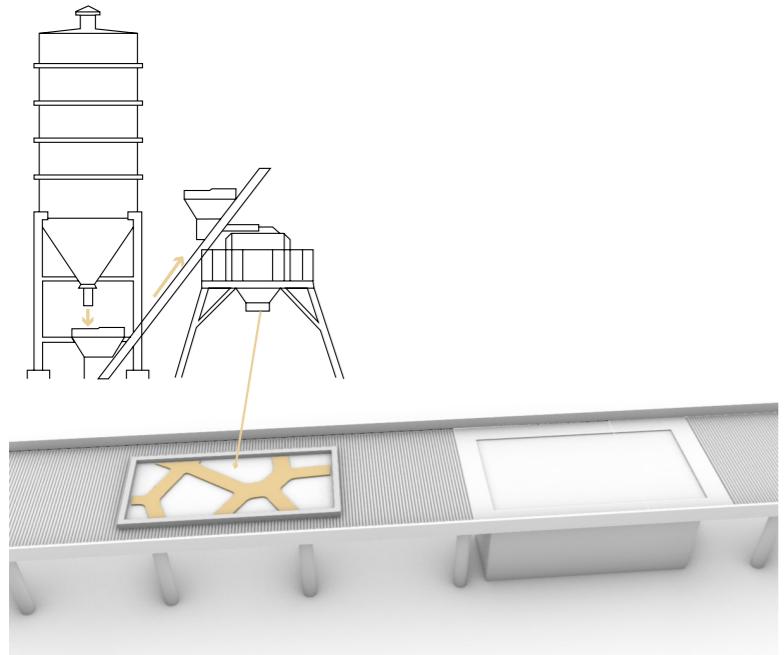
STEP 5



ANNEALING + COOLING DOWN

STEP 6

PRODUCTION STEPS



POURING CONCRETE + COMPACTING

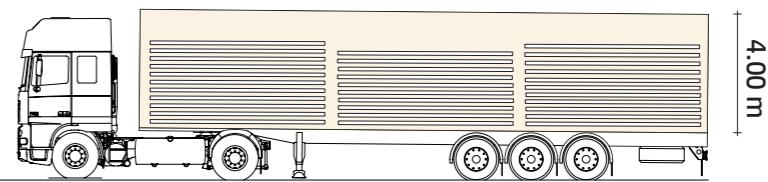
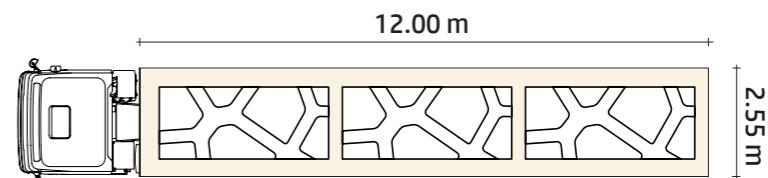
STEP 7

FINISHING

STEP 8

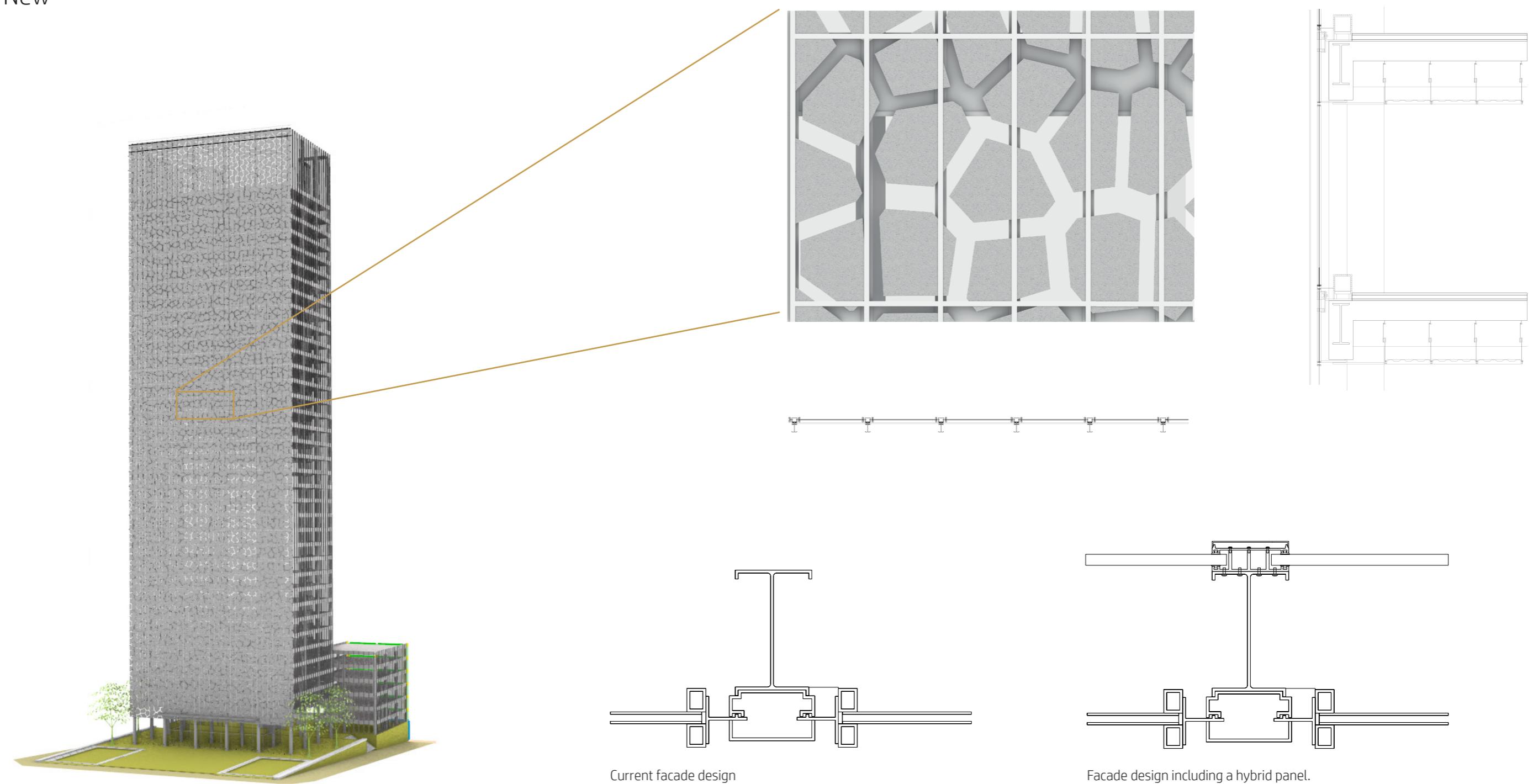
TRANSPORTATION

STEP 9



FACADE DETAIL

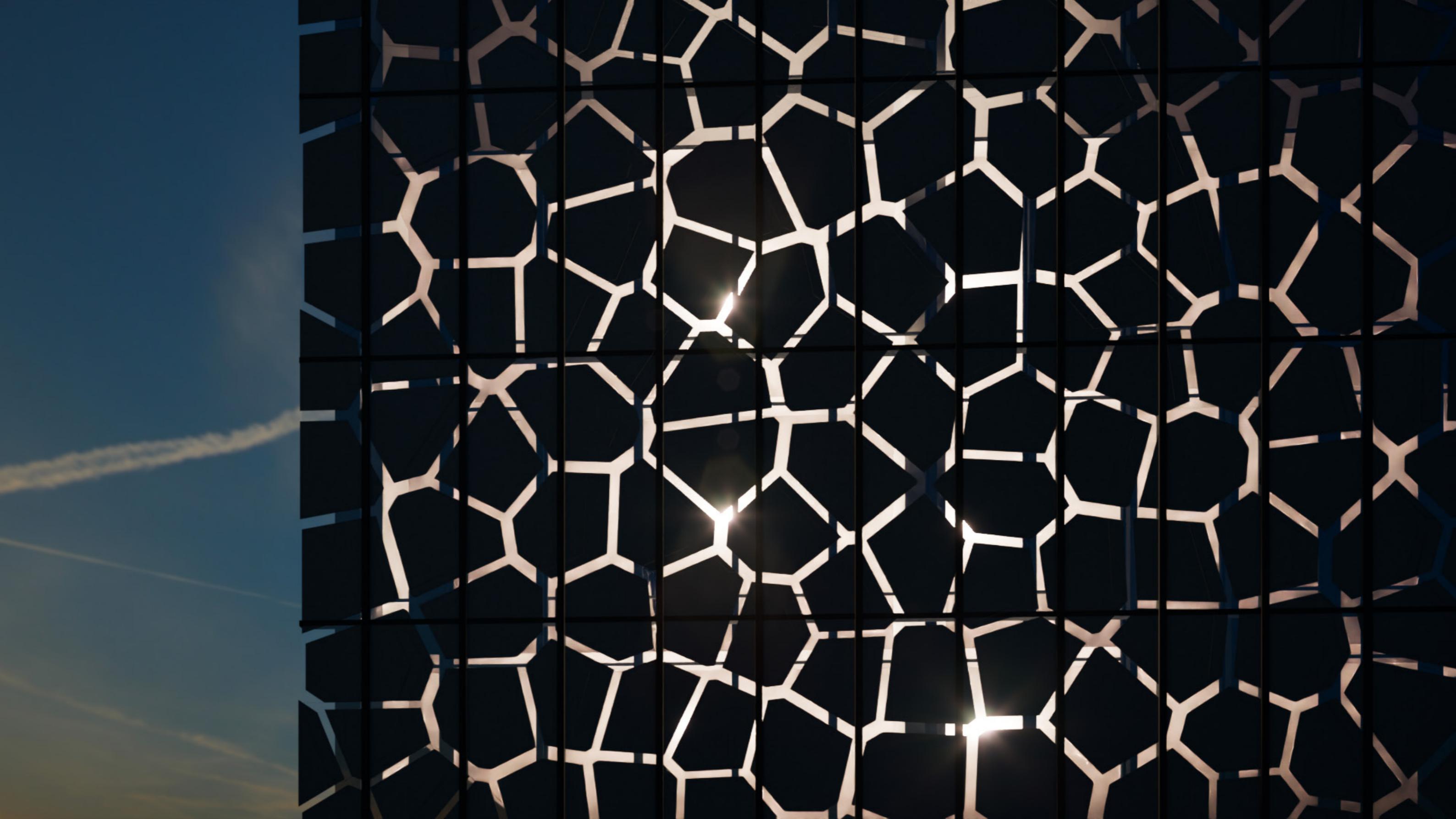
Old vs New











CONCLUSIONS

CONCLUSIONS INTERFACE:

- Shear stress capacity is feasible
- Bending stress capacity is insufficient.
- Adhesion percentage is inadequate.
- Concrete quality requires enhancement.
- Interlocking form ensures structural integrity.
- Surface roughness should be applied at the macro scale



CONCLUSIONS MANUFACTURING:

- High potential for industrialization.
- Using two materials and design for disassembly enhances recyclability potential.
- Offers a new design language
- Architectural flexibility

THANK YOU!



APPENDIX

RELEVANCE

Concrete-glass Interface

Societal Value



Innovative Construction Materials



Architectural flexibility

Scientific Value



Material Science Advancements



Interdisciplinary Knowledge

Sustainable Value



Resource Efficiency



Recyclability

CONCRETE

Mixtures



Concrete mixture (per L):

CEM I 52.5 R	450 gr
Norman Sand	1350 gr
Water	225 gr



(1)



(3)

Concrete mixture (per L):

CEM III 52.5 R	450 gr
Norman Sand	1350 gr
Water	225 gr
Glenium 51 (Plasticizer)	1 gr



(2)



(4)

Concrete mixture (per L):

CEM III/A 52.5 N	450 gr
Norman Sand	1350 gr
Water	225 gr

Concrete mixture (per L):

CEM III/A 52.5 N	450 gr
Norman Sand	1350 gr
Water	225 gr
Glenium 51 (Plasticizer)	1 gr

CONCRETE MIXTURE

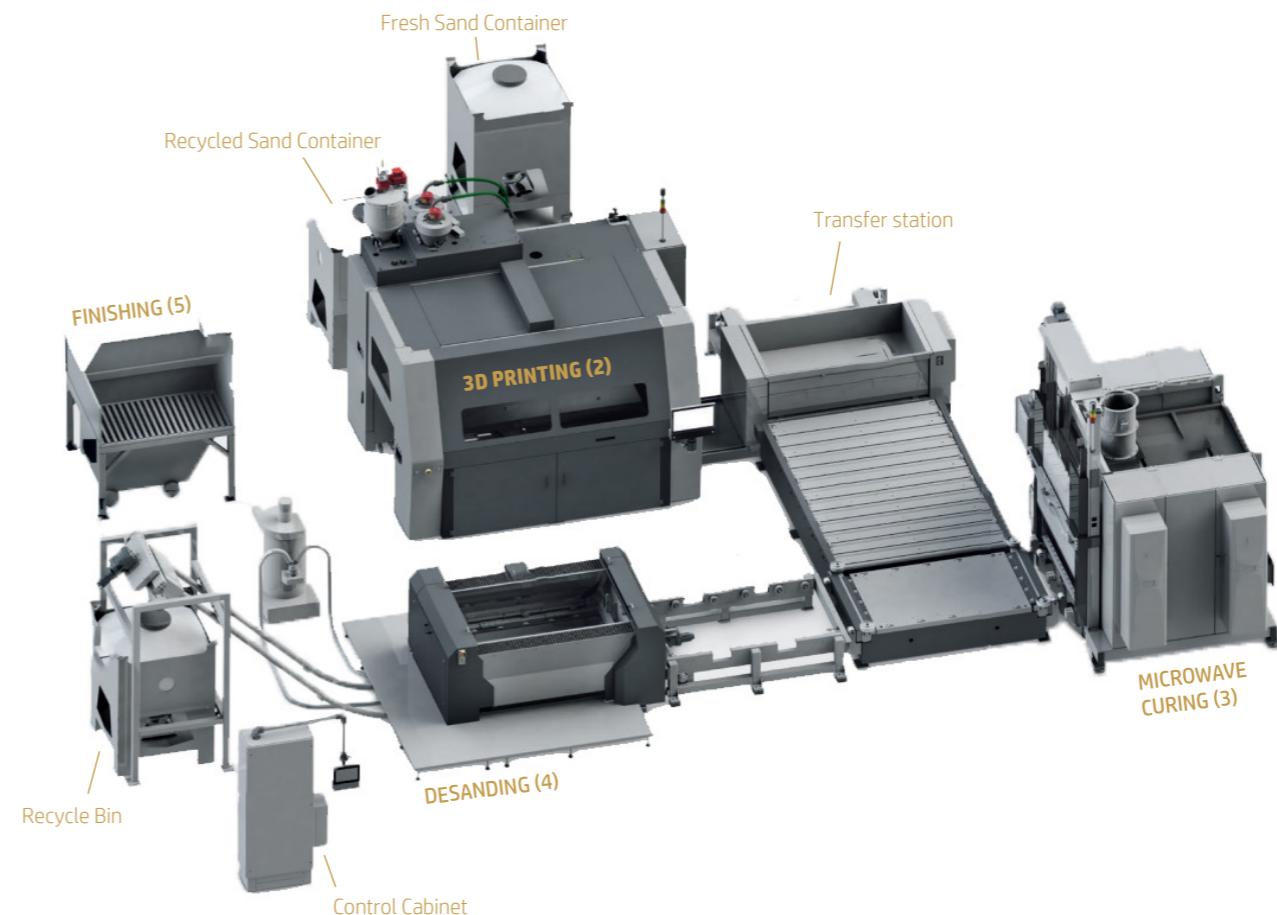
Result



1 2 3 4

CEM III + Plasticizer

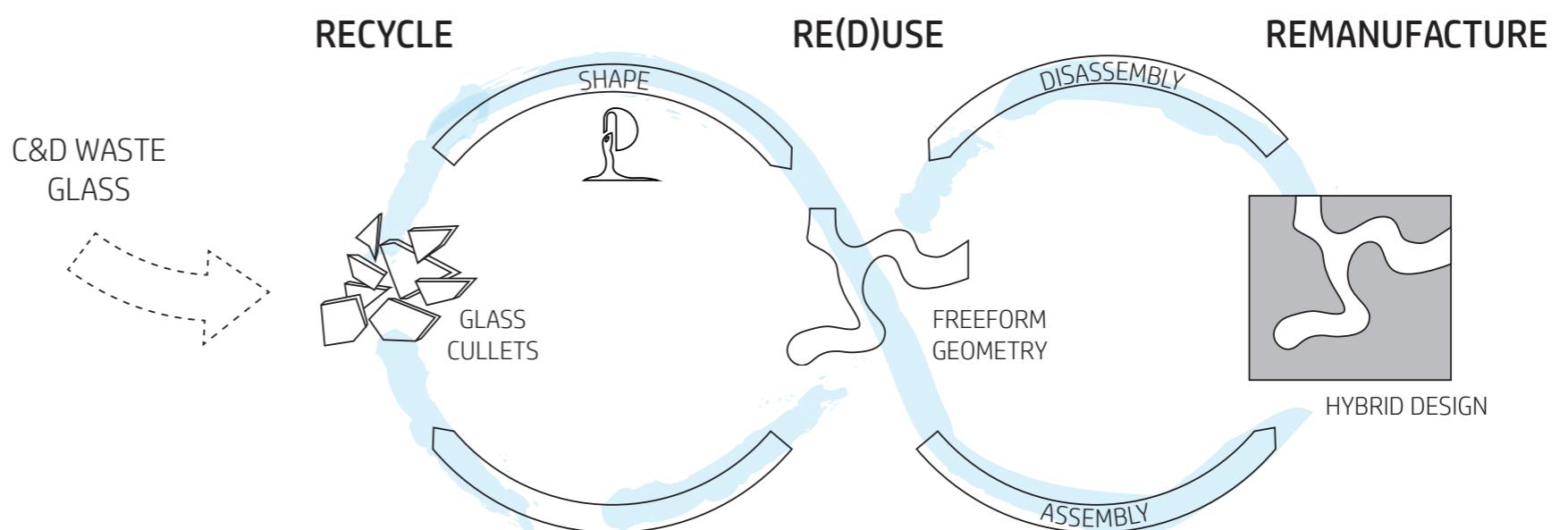
- Use an outer **frame** to constrain the interlocking sand mould pieces
- Application of **coatings** for high surface quality (Arkopal B 5).
- A minimum thickness of **3 to 4 mm** in any section of the mould, with an added thickness of 15 mm around the periphery of the geometry
- Maximum print size is **2200 x 1200 mm**
- **Recycle** sand when desanding and after firing.



MANUFACTURING

Glass

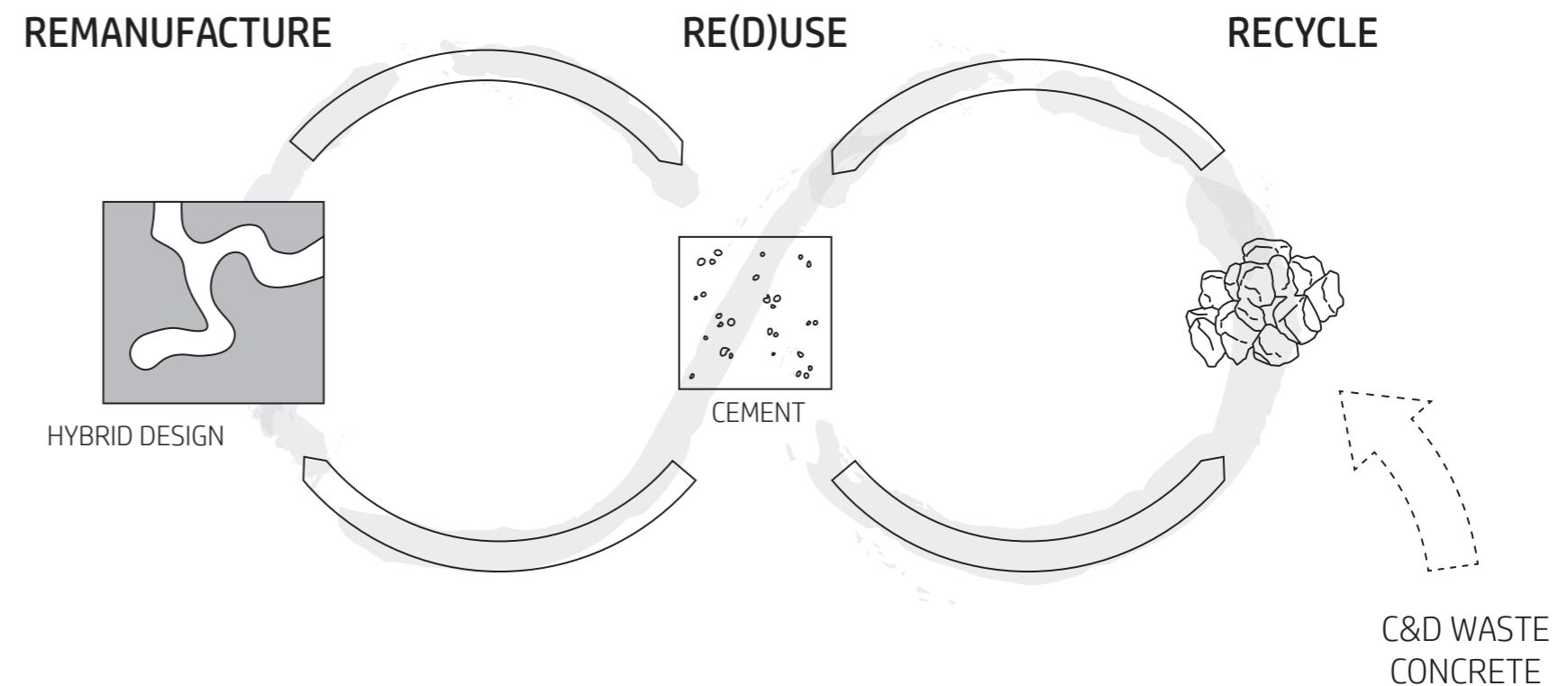
- The interface is always the weakest point; therefore, less strong glass can be used.
- There is **sustainability potential** by using recycled glass cullets.
- By avoiding additives, the glass retains its purity, making it **100% recyclable**.
- The largest kiln glass oven can accommodate a maximum size of **3500 x 1500 mm** with a thickness range of 15-40 mm.
- Use **soda-lime glass** compositions due to their favorable thermal expansion matching



MANUFACTURING

Concrete

- hybrid mixture of Glass Fiber Reinforced Concrete (**GRC**) and Ultra-High Performance Concrete (**UHPC**).
- Add supplementary cementitious materials (SCMs) to mitigate the risk of Alkali-Silica Reaction (**ASR**).
- Prefab concrete panel are already one of the most industrialised facade panels.
- concrete component can be **filtered, crushed, and recycled** to supply cement for new concrete mixtures.
- Homogeneous composition in terms of **no contaminants** in Recycled Concrete Aggregate (RCA).

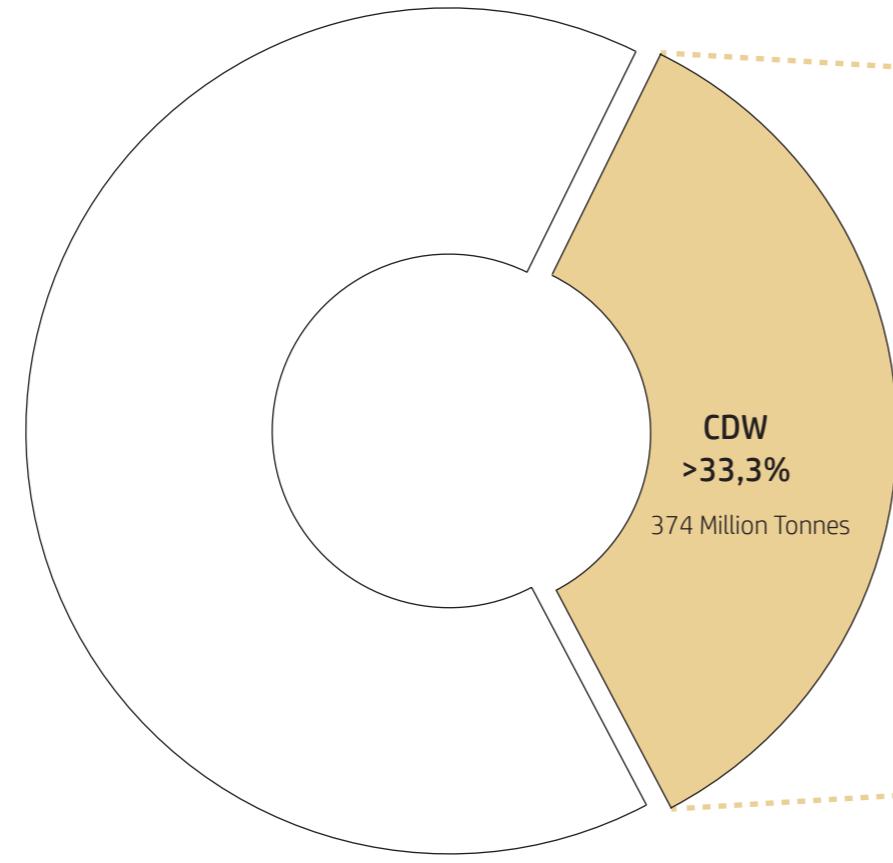


importancy factor criteria value	Structural				Physical				Chemical				Sustainable				Efficiency			
	1 Density kg/m3	2 tensile N/mm2	1 yield N/mm2	2 Compressive N/mm2	1 thermal (U) W/mC	4 expansion Ustrain / C	1 Heat capacity J/kg.C	2 Combustibility	1 Weather resistar	1 UV-resistance	3 Embodied energy MJ/kg	3 Recyclable potential	3 Durability	4 Manufacturing waste (I - V)	4 Costs EUR/kg	4 Shapeability	1 Accesible	4 Aesthetics*		
Minerals & Stone (stone)	2300	2 - 25	2 - 25	55 - 255	5,4 - 6	3,7 - 6,3	840 - 920	excellent	excellent	excellent	0,952 - 11,6	no	excellent	V	0,323 - 5,3	fair	good	-		
Fired Clays (brick)	2000	6,9 - 14	6,9 - 14	69 - 140	0,4 - 0,8	8 - 11	750 - 850	excellent	excellent	excellent	3 - 3,3	no	excellent	II	0,53 - 1,41	poor	good	-		
Cement & Concrete (concrete)	2400	1,1 - 1,3	1 - 1,2	13 - 30	1,65 - 2,6	8 - 12	835 - 1050	excellent	excellent	excellent	0,776 - 0,856	yes / no	excellent	I	0,03 - 0,05	excellent	fair	-		
Polymer Composite (FRP)	1850	207 - 304	207 - 304	207 - 257	0,42 - 0,51	8,64 - 33	1020 - 1120	good	excellent	fair	95,7 - 106	no	fair	II	28,8 - 31,6	excellent	excellent	-		
Thermoplastics (tpPVC)	1360	38 - 46	37,6 - 45,5	37 - 44,3	0,147 - 0,209	65 - 81	1000 - 1100	poor	excellent	fair	60,9 - 67,2	yes	good	II	1,5 - 1,64	excellent	excellent	-		
Natural Materials (wood)	550	2,27 - 6,13	1,26 - 3,58		0,218 - 0,382	2 - 11	1660 - 1710	fair	fair	good	11 - 115	no	fair	IV	1,47 - 2,28	fair	fair	-		
Alloys (non-ferrous) (aluminium)	2700	288 - 571	241 - 520	245 - 521	135 - 185	22,7 - 24,6	879 - 999	excellent	excellent	excellent	187 - 206	yes	excellent	III	3,03 - 3,2	fair	excellent	-		
Metals (ferrous) (stainless steel)	7700	515 - 1300	257 - 1140	252 - 1200	14 - 24,9	10,8 - 16,5	450 - 510	excellent	excellent	excellent	69,1 - 76,2	yes	excellent	III	2,4 - 2,57	fair	good	-		

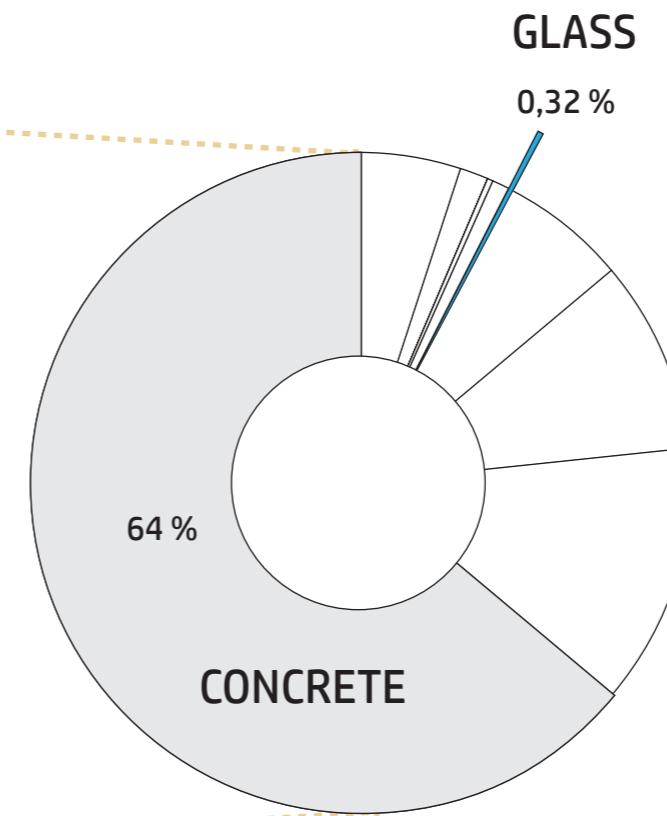
importancy factor criteria value	Structural				Physical				Chemical				Sustainable				Efficiency			
	1 Density kg/m3	2 tensile N/mm2	1 yield N/mm2	2 Compressive N/mm2	1 thermal (U) W/mC	4 expansion Ustrain / C	1 Heat capacity J/kg.C	2 Combustibility	1 Weather resistar	1 UV-resistance	3 Embodied energy MJ/kg	3 Recyclable potential	3 Durability	4 Manufacturing waste (I - V)	4 Costs EUR/kg	4 Shapeability	1 Accesible	4 Aesthetics*		
Glass	2450	40	N/A	310 -342	0,7 - 1,3	9,2 - 9,5	850 - 950	good	excellent	excellent	8,24 - 9,11	yes	excellent	good	1,2 - 1,41	good	good	excellent		
Polycarbonate	1200	62 -72	59 -69	69 - 86	0,19 - 0,22	120 - 125	1150 - 1250	fair	good	fair	101 - 111	yes	excellent	good	3,8 - 4,30	good	excellent	fair		
Acrylic	1170 - 1200	54 - 72	54 - 72	72 - 124	0,167 - 0,251	90 - 162	1400 - 1520	fair	good	excellent	107 - 118	no	good	good	1,59 - 2,22	excellent	good	excellent		
ETFE	1700	42 - 47	34 - 37	46,6 - 51,4	0,137	106	1200 - 1250	good	excellent	good	250	yes	excellent	excellent	17 - 23	good	excellent	fair		
Epoxy	1100 - 1400	45 - 89,6	36 - 71,7	103 - 172	0,181 - 0,196	81 - 117	1180 - 1240	poor	good	fair	115 - 127	no	excellent	good	2,7 - 4,76	excellent	fair	excellent		

GLASS TYPE	SODA LIME GLASS	BOROSILICATE GLASS	LEAD SILICATE GLASS	ALUMINOSILICATE GLASS	FUSED-SILICA GLASS	96% SILICA GLASS
	<p>73% SiO₂, 17% Na₂O, 5% CaO, 4% MgO, 1% Al₂O₃</p>	<p>80% SiO₂, 13% B₂O₃, 4% Na₂O, 2.3% Al₂O₃, 0.1% K₂O</p>	<p>63% SiO₂, 21% PbO, 7.6% Na₂O, 6% K₂O, 0.3% CaO, 0.2% MgO, 0.2% B₂O₃, 0.6% Al₂O₃</p>	<p>57% SiO₂, 20.5% Al₂O₃, 12% MgO, 1% Na₂O, 5.5% CaO</p>	<p>99.5% SiO₂</p>	<p>96% SiO₂, 3% B₂O₃</p>
OBSERVATIONS	Durable. Least expensive type of glass. Poor thermal resistance. Poor resistance to strong alkalis (e.g. wet cement)	Good thermal shock and chemical resistance. More expensive than sodalime and lead glass.	Second least expensive type of glass. Softer glass compared to other types. Easy to cold-work. Poor thermal properties. Good electrical insulating properties.	Very good thermal shock and chemical resistance. High manufacturing cost.	Highest thermal shock and chemical resistance. Comparatively high melting point. Difficult to work with. High production cost.	Very good thermal shock and chemical resistance. Meticulous manufacturing process and high production cost.
APPLICATIONS	<ul style="list-style-type: none"> Window panes Bottles Façade glass 	<ul style="list-style-type: none"> Laboratory glassware Household ovenware Lightbulbs Telescope mirrors 	<ul style="list-style-type: none"> Artistic ware Neon-sign tubes TV screens (CRT) Absorption of X-rays (when PbO % is high) 	<ul style="list-style-type: none"> Mobile phone screens Fiber glass High temperature thermometers Combustion tubes 	<ul style="list-style-type: none"> Outer windows on space vehicles Telescope mirrors 	<ul style="list-style-type: none"> Furnace sight glasses Outer windows on space vehicles
M.P [°C]	1350-1400 [°C]	1450-1550 [°C]	1200-1300 [°C]	1500-1600 [°C]	>>2000 [°C]	>>2000 [°C]
S.P [°C]	730 [°C]	780 [°C]	626 [°C]	915 [°C]	1667 [°C]	1500 [°C]
A.P [°C]	548 [°C]	525 [°C]	435 [°C]	715 [°C]	1140 [°C]	910 [°C]
ST. P [°C]	505 [°C]	480 [°C]	395 [°C]	670 [°C]	1070 [°C]	820 [°C]
D.E. [kg/m³]	2460 [kg/m ³]	2230 [kg/m ³]	2850 [kg/m ³]	2530 [kg/m ³]	2200 [kg/m ³]	2180 [kg/m ³]
C.E. [10^-6/°C]	8.5 [10^-6/°C]	3.4 [10^-6/°C]	9.1 [10^-6/°C]	4.2 [10^-6/°C]	0.55 [10^-6/°C]	0.8 [10^-6/°C]
Y.M [GPa]	69 [GPa]	63 [GPa]	62 [GPa]	87 [GPa]	69 [GPa]	67 [GPa]

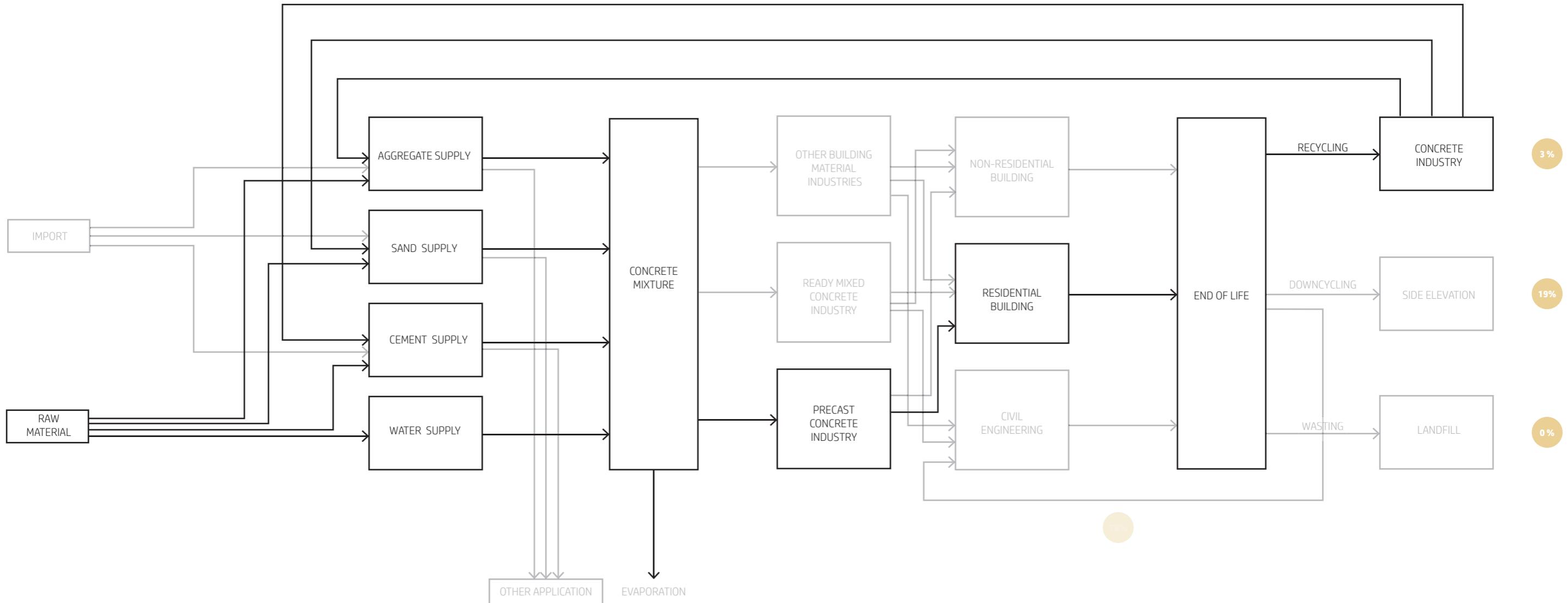
MIXTURES	NORMAL STRENGTH CONCRETE	HIGH STRENGTH CONCRETE	GLASSFIBRE REINFORCED CONCRETE	SELF-CONSOLIDATING CONCRETE	ULTRA-HIGH PERFORMANCE CONCRETE	LIGHTWEIGHT CONCRETE
PROPERTIES	Cost effective. Easy production. Raw materials widely available. Versatility in use. Lower strength. Limited durability. Cracking potential.	Increased compressive strength, but lower ductility. Better durability but more brittle than NSC. Costs economically viable.	High strength-to-weight ratio. Good durability and resistance to environmental factors. Enhanced tensile strength. Brittle. Color, texture and shape versatility. Cost-effective.	High fluidity concrete without vibration. Resistance to segregation. Easy filling, Easy passage. High deformation ability. Significant shrinkage deformation.	High flowing ability. High early and final strength. Superior durability. Expensive.	Low weight. Improved thermal properties. Lower strength properties than normal weight concrete. Less stiff. More possibilities for creep and shrinkage.
C.S. DE. C.	+	++	+++	+++	++++	+++
C.E. F.S. T.S.	2400 [kg/m³]	>3000 [kg/m³]	1800-2000 [kg/m³]	2400 [kg/m³]	2520 [kg/m³]	<2200 [kg/m³]
C.S. D. E.	20-40 [MPa]	>60 [MPa]	>40 [MPa]	34 [MPa]	>150 [MPa]	17 [MPa]
C.S. D. E.	2-5 [MPa]	4-7 [MPa]	11 [MPa]	4 [MPa]	>20 [MPa]	2 [MPa]
C.S. D. E.	3-5 [MPa]	5-10 [MPa]	15 [MPa]	15 [MPa]	45 [MPa]	2 [MPa]
C.S. D. E.	5.5 - 8.5 [10^-6/C]	5.5 - 8.5 [10^-6/C]	5-8 [10^-6/C]	5.5 - 8.5 [10^-6/C]	4 - 7 [10^-6/C]	5 - 8 [10^-6/C]

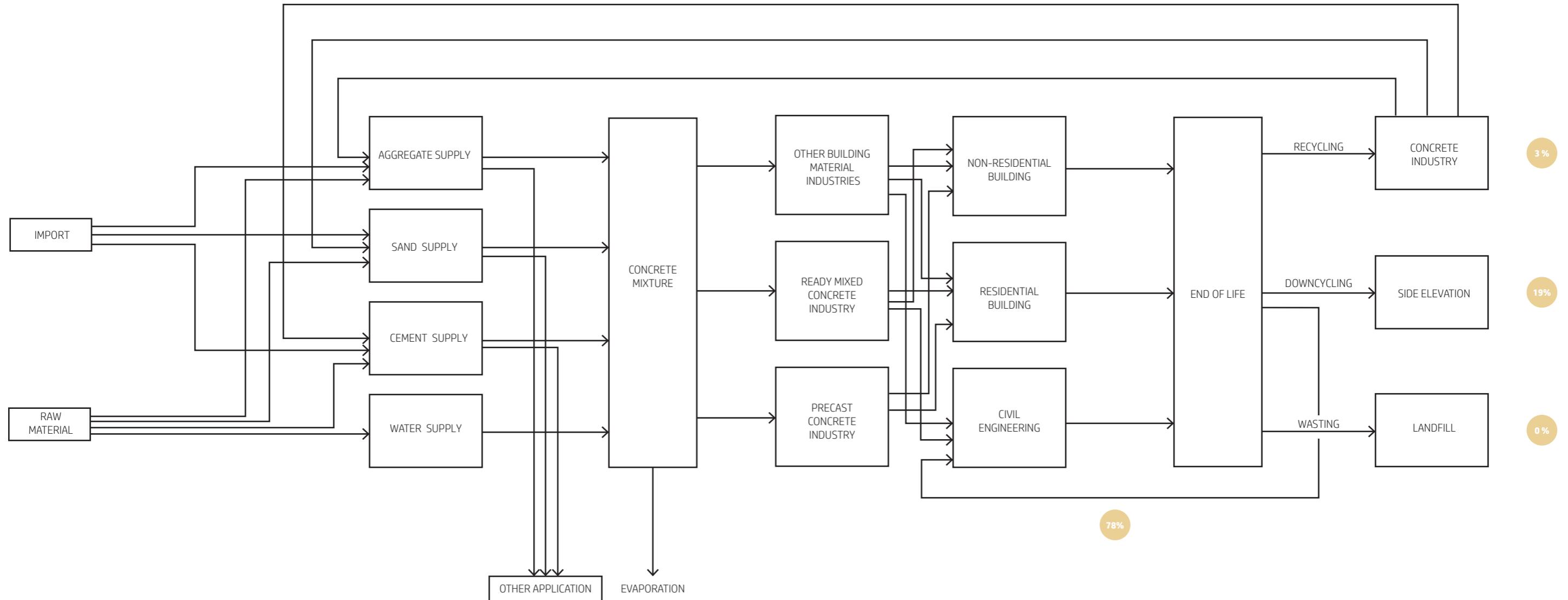


WASTE GENERATION EU



CDW WASTE



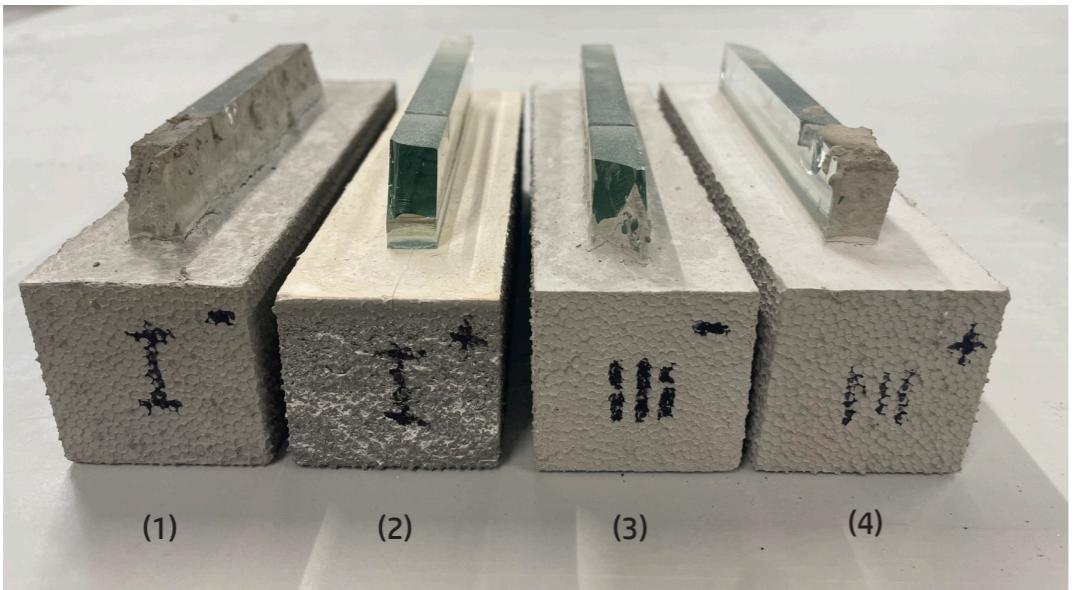


3 %

19 %

0 %

78%



ONLY TWO MATERIALS

- No Screws
- No Bolts
- No Drilling

