

### 1. Motivation & Purpose

This study aims at modeling the evolution of meanders by coupling the Bank Erosion and Retreat Model (BERM, by Chen and Duan, 2006) with a nonlinear flow model (by Blanckaert and de Vriend, 2010).

#### 1.1 Linear flow method

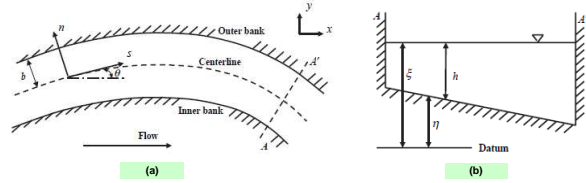


Fig. Definition of variables and coordinate system: (a) plain view; (b) channel cross-section

$$\frac{u-U}{U} = Nbk\theta_0[-\alpha \cos(ks) + \beta \sin(ks)]$$

By Johannesson & Parker (1989)

$$\alpha = \frac{kHC_f(A+A_s+F^2+1)}{H^2k^2+4C_f^2}$$

Assume:  $\theta = \theta_0 \cos(ks)$

$$\beta = \frac{2C_f^2(A+A_s+F^2-1)-H^2k^2}{H^2k^2+4C_f^2}$$

Assume:  $db/ds=0; r \gg b; \lambda \gg b$

#### 1.2 Bank Erosion & Retreat Model (BERM)

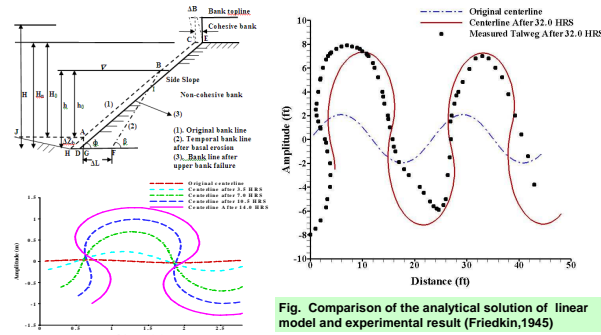


Fig. Comparison of the analytical solution of linear model and experimental result (Friedkin, 1945)

#### 1.3 Nonlinear flow method

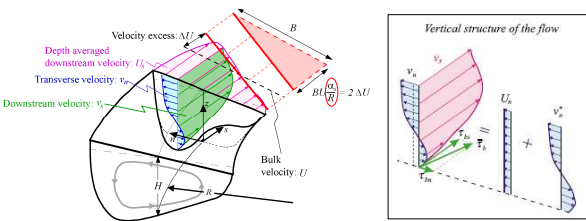


Fig. Schematization of flow structure in a bend; definition of reference system and notations used in the non-linear flow model (adapted from Blanckaert & de Vriend 2010)

## Toward nonlinear modeling of meander evolution

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### 2. Theory – physical process which redistribute flow in curved channels

$$\lambda_{\text{cos}/R} \frac{\partial}{\partial s} \left( \frac{\alpha_s}{R} \right) + \frac{\alpha_s}{R} = F_{\text{cos}/R}$$

By Blanckaert & de Vriend (2010)

$$\lambda_{\text{cos}/R} = \frac{1}{2} \frac{H}{\psi C_f} \left\{ 1 - \frac{1}{12} \frac{\alpha_s + 1}{R} \frac{B^2}{R} \right\}$$

(Extra terms compared to linear model by Johannesson and Parker (1989))

$$F_{\text{cos}/R} = \frac{1}{2} \frac{S_n Fr^2 + A - 1}{R} - \frac{1}{2} \frac{H}{\psi C_f} \frac{\partial}{\partial s} \left( \frac{1}{R} \right) \left( 1 - \frac{B^2}{6R^2} \right) + \frac{4\chi}{\psi C_f} \frac{H^2}{B^2} \frac{\partial}{\partial s} \left( \frac{v_s v_n}{HU^2} \right) \left[ 1 + \frac{1}{12} \frac{(S_n Fr^2 + A + 3) B^2}{R^2} \right] + \frac{1}{24} \frac{H}{\psi C_f} \frac{B^2}{R^2} \frac{\partial}{\partial s} \left( \frac{S_n Fr^2 + A}{R} \right)$$

Transverse water surface and bed slope

Changes in curvature

Streamwise momentum redistribution by secondary flow

Cross-flow due to changes in transverse water surface and bed slope

### 3. Verification of linear & nonlinear flow models

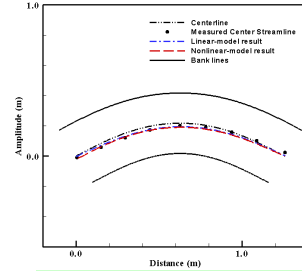


Fig. Compare results of two methods with measurement (Silva, 1995,  $\theta_0 = 30^\circ$ )

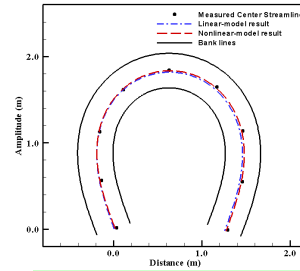


Fig. Compare results of two methods with measurement (Silva, 1995,  $\theta_0 = 110^\circ$ )

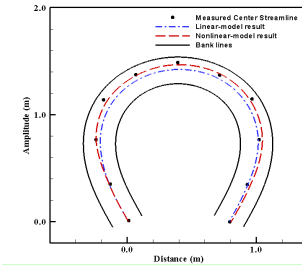


Fig. Compare results of two methods with measurement (Whitening & Dietrich, 1993,  $\theta_0 = 115^\circ$ )

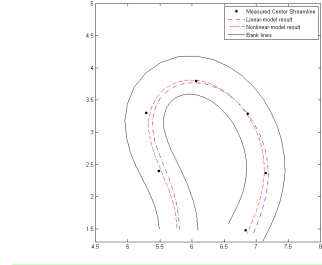


Fig. Compare results of two methods with measurement (Kinoshita flume, Abad and Garcia, 2009) (adapted from Ottevanger et al., 2012)

### 4. Flowchart for meander evolution model

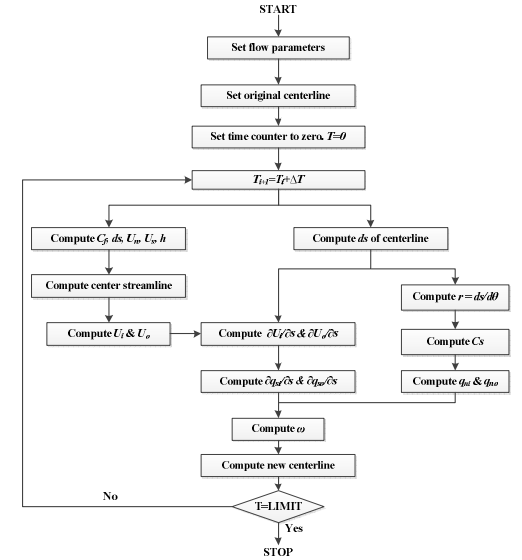


Fig. Flowchart of the calculation process

### 5. Conclusions

- ✓ The results of linear & nonlinear flow models are similar in mildly curved channels with a flat bed.
- ✓ Linear models overestimate streamwise momentum redistribution by secondary flow in strongly curved channels.
- ✓ The nonlinear flow model gives a better result in high-sinuosity channels with transverse bed slope.
- ✓ A better meander evolution model is expected and being built by coupling the Bank Erosion and Retreat Model (BERM, by Chen and Duan, 2006) with a nonlinear flow model (by Blanckaert and de Vriend, 2010).

### 6. References

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