

# The use of thin glass in heritage window glazing; testing different design concepts

Karin Backer 4552962



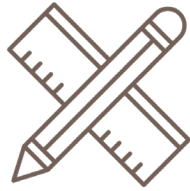
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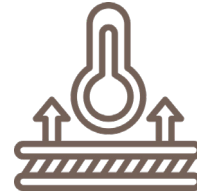
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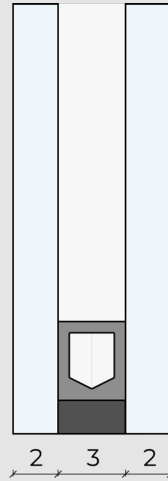


# Current situation

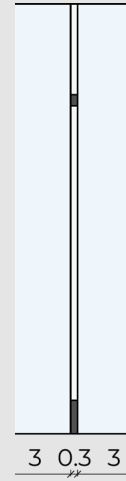
# Heritage windows



Single glazing with coating  
U-value =  $3.8 \text{ W/m}^2\text{K}$   
€80/m<sup>2</sup>



Thin insulating glass  
U-value =  $3.6 \text{ W/m}^2\text{K}$   
€220-250/m<sup>2</sup>



Vacuum glass  
U-value =  $0.5 \text{ W/m}^2\text{K}$   
€300/m<sup>2</sup>





# Research questions

# Research question

“What **alternative solutions** arise when **thin glass** is used to design an **insulating glass panel** that replaces single glazing in heritage buildings?”

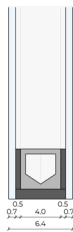
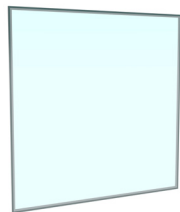
# Design criteria

- Thickness is **less than 12 mm**, preferably between 4-8 mm
- U-value **lower than 3.8 W/m²K**
- Suit NEN on glass for windows; **w = 1 kPa**
- Outside layer of thin glass
- Cavity like in between layer
- Translucent, preferably transparency
- Does not age in color or transparency
- No cracks due to thermal expansion

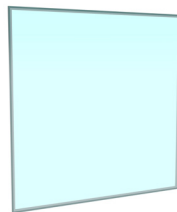


# Design proposals

1



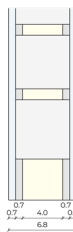
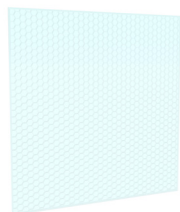
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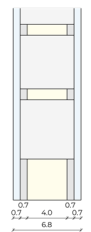
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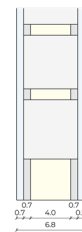
4a



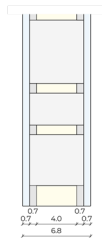
4b



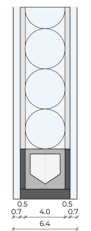
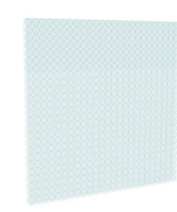
4c



5



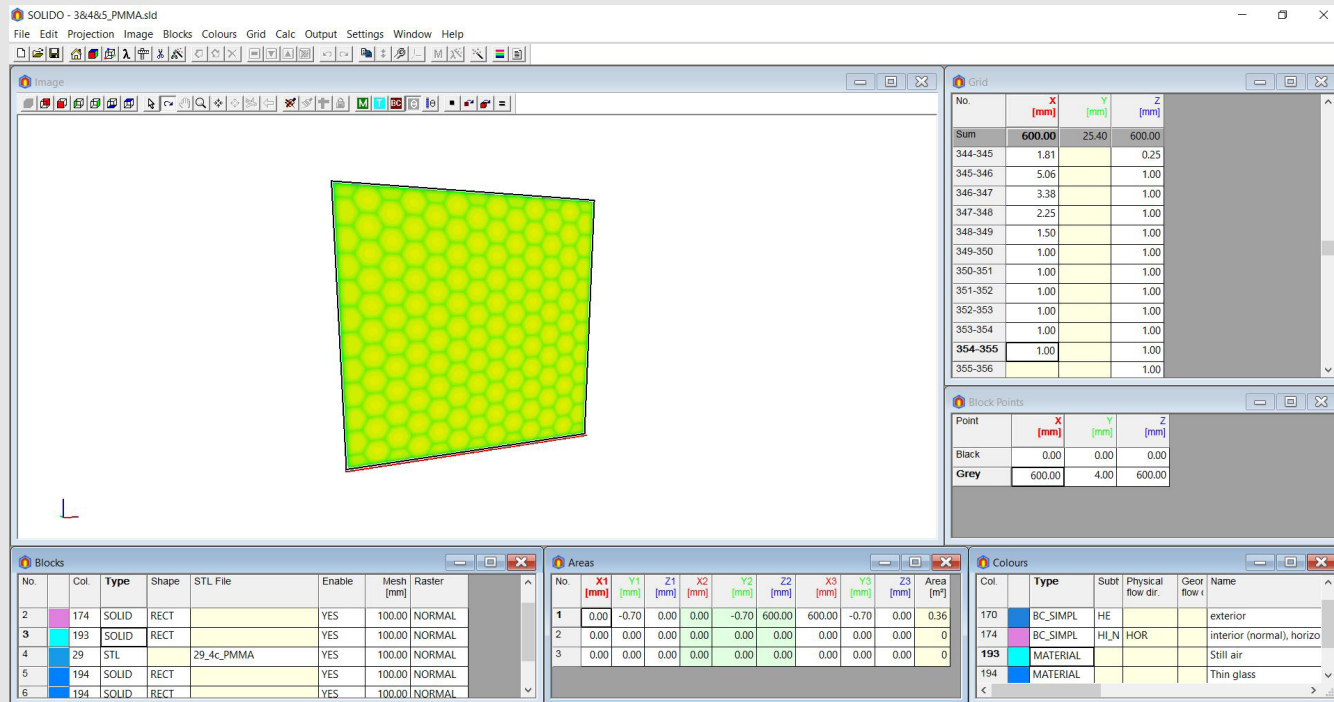
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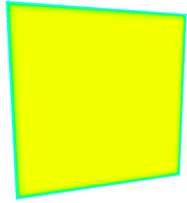


# Computer analysis

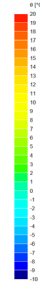
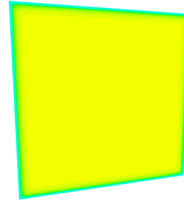
# SOLIDO



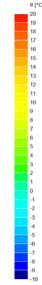
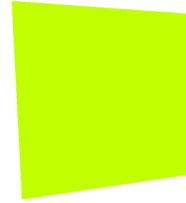
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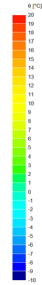
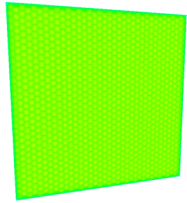
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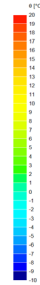
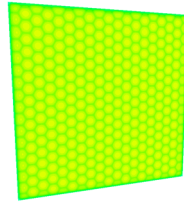
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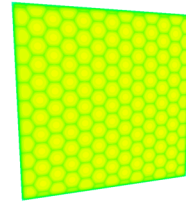
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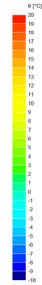
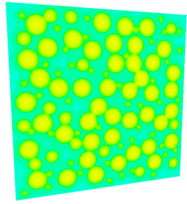
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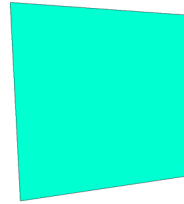
4c



5



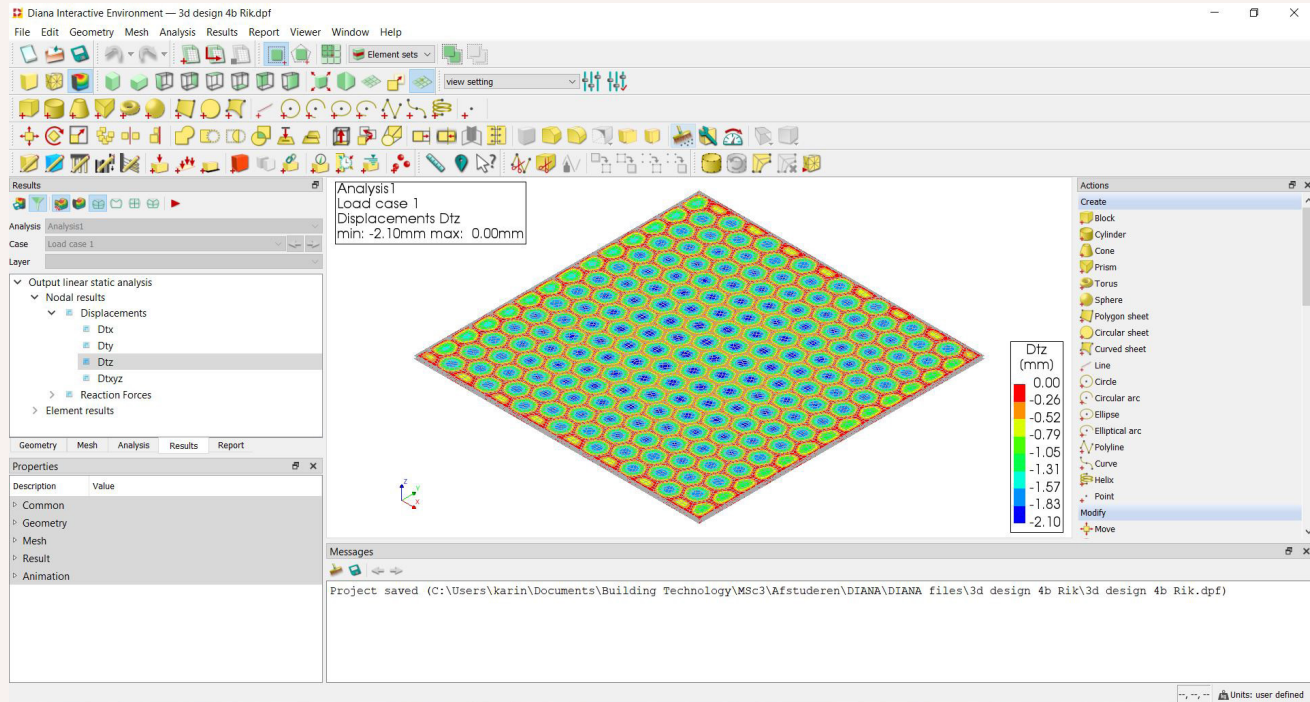
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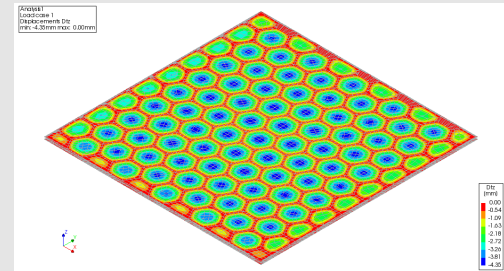
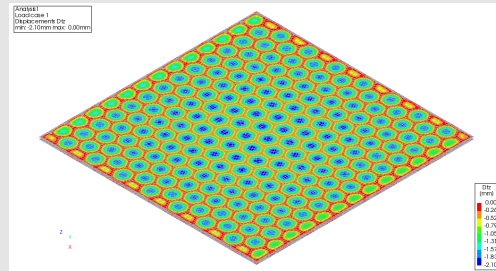
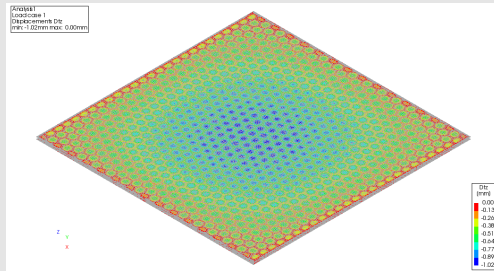
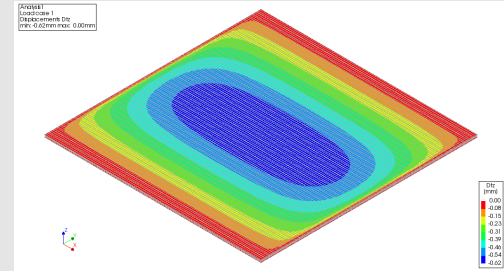
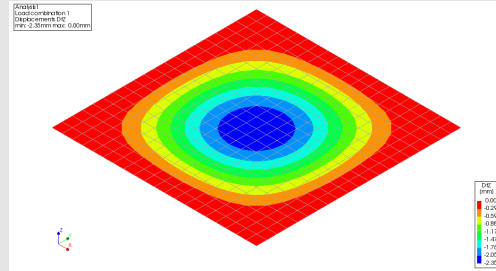
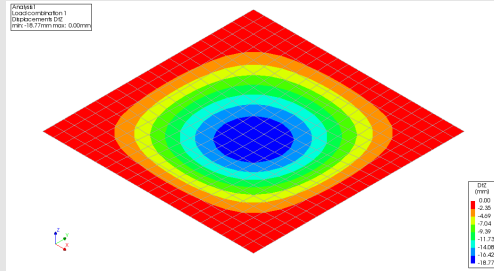


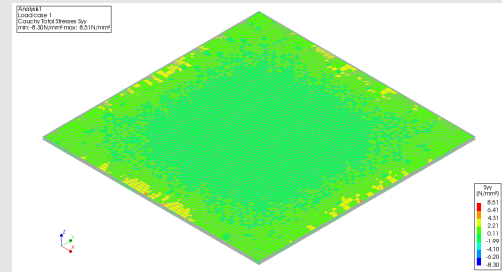
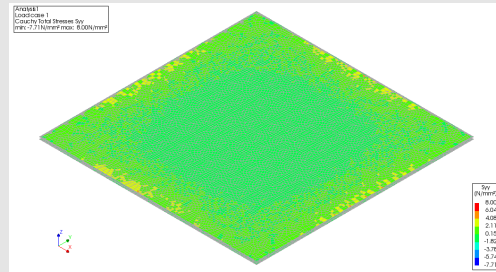
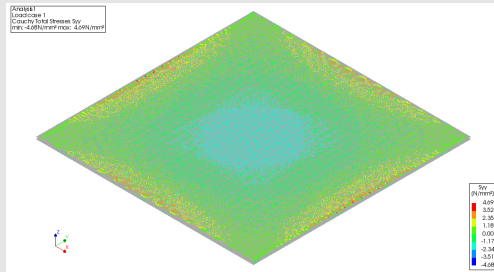
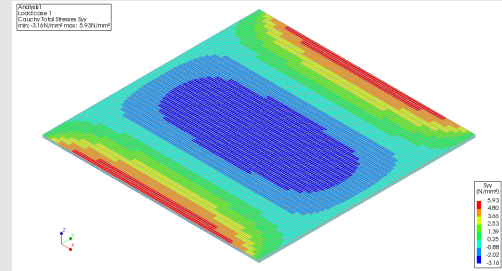
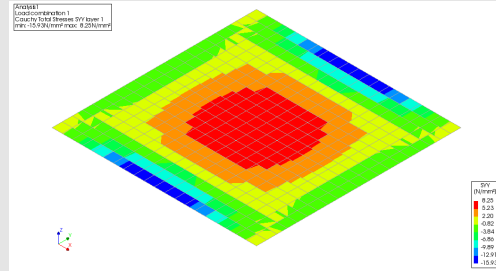
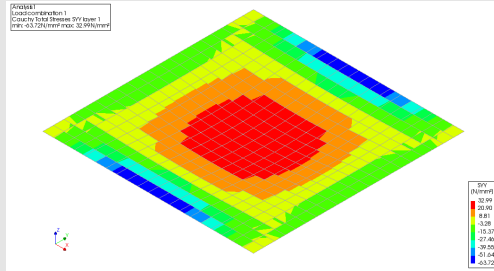


#	% still air	Q	A	U-value	>3,8
1	97%	23,87	0.25	3,18	:)
2	97%	24,02	0.25	3,20	:)
3	93%	26,00	0.25	3,47	:)
4a	76%	29,72	0.25	3,96	:(
4b	86%	26,97	0.25	3,60	:)
4c	89%	26,03	0.25	3,47	:)
5	44%	32,95	0.25	4,39	:(
6	48%	1,57	0.01	5,22	:(

# DIANA software





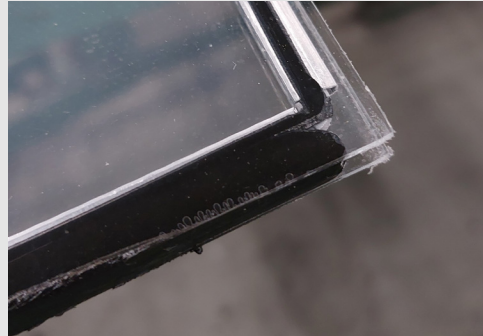
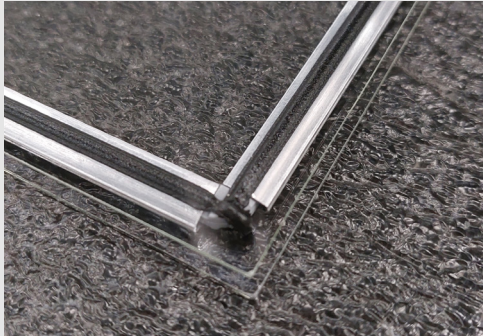


#	Deflection	Max. deflection	Check deflection	Stress	Max. stress	Check stress
1	18,77	10,88	:(	63,72	15	:(
2	2,35	10,88	:)	15,93	15	:(
3	0,62	10,88	:)	5,93	15	:)
4a	1,02	10,88	:)	4,69	15	:)
4b	2,10	10,88	:)	8,00	15	:)
4c	4,35	10,88	:)	8,51	15	:)

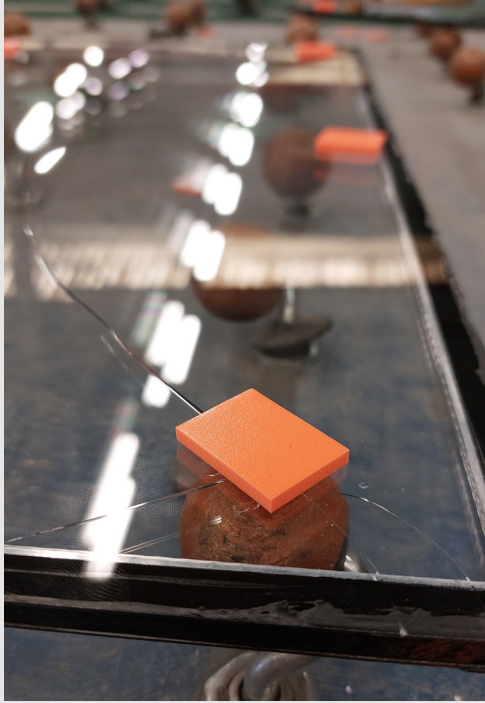


# Making prototypes

# Design 1 & 2

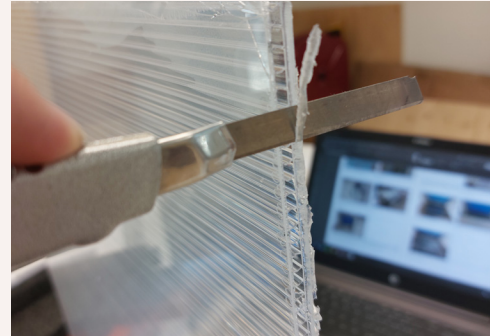
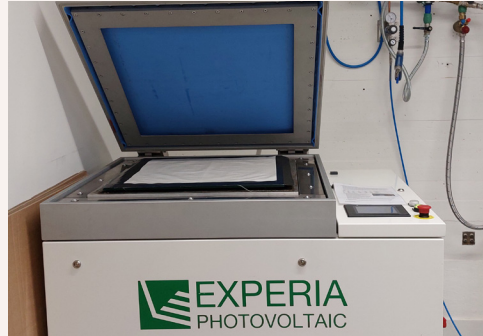
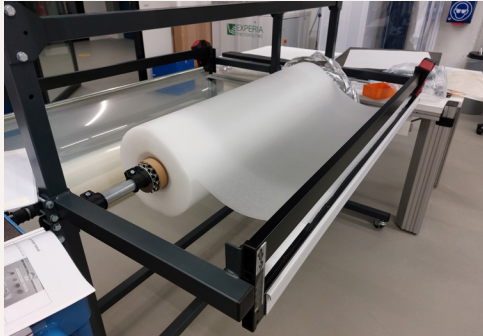






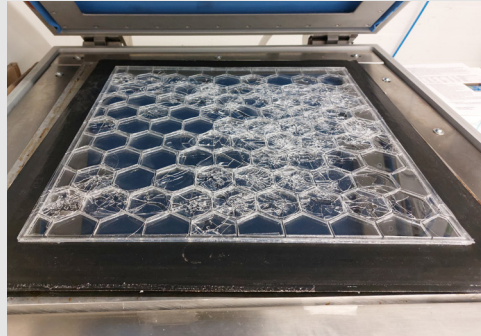
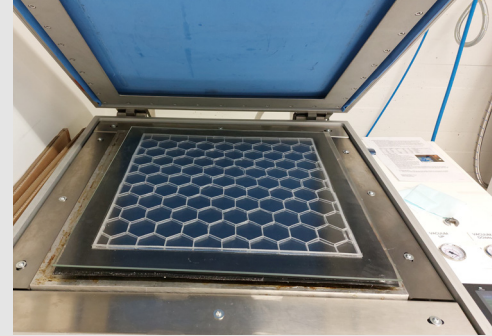
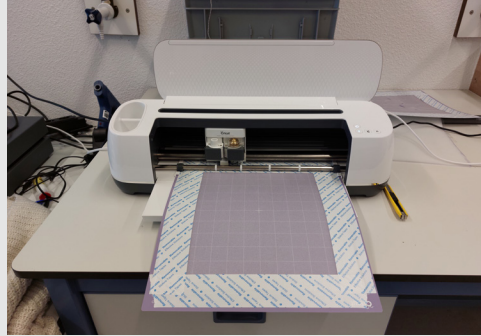
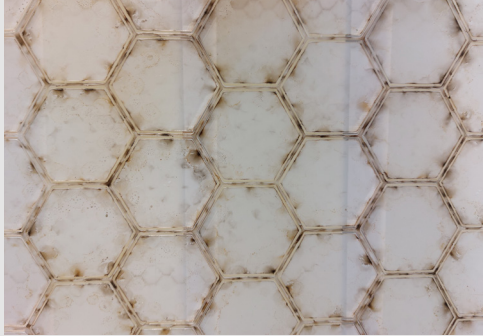


# Design 3

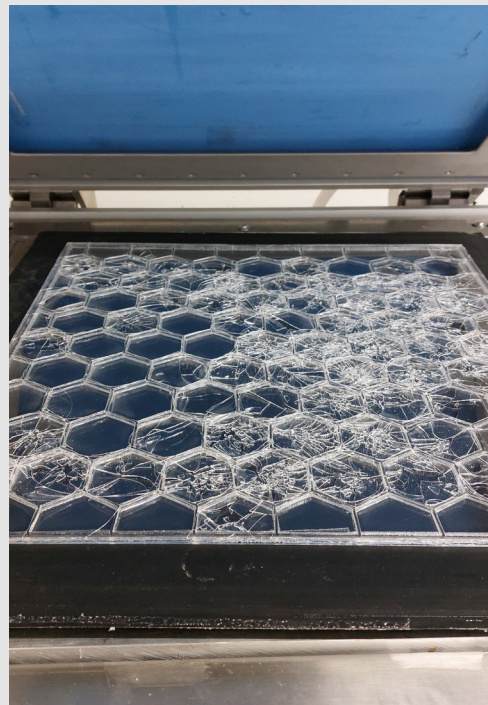




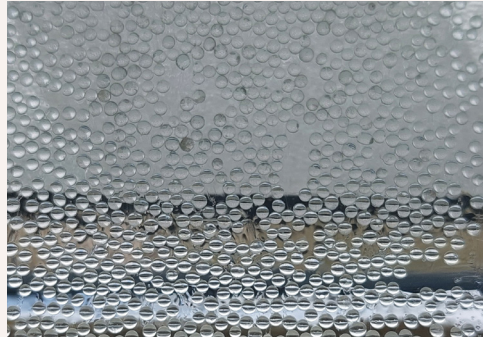
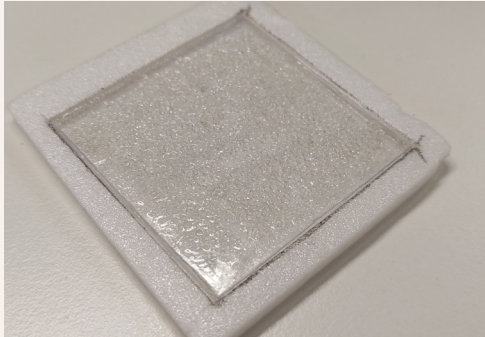
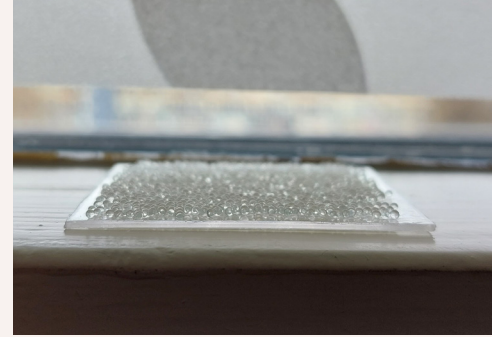
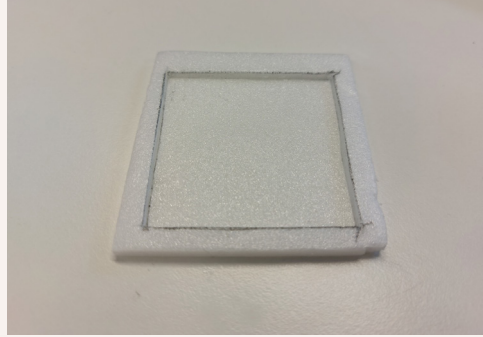
# Design 4



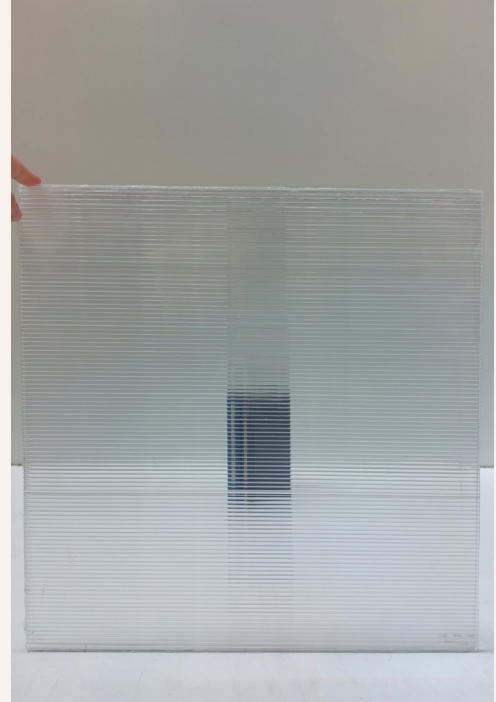




# Design 6



# Final prototypes





# Test setup

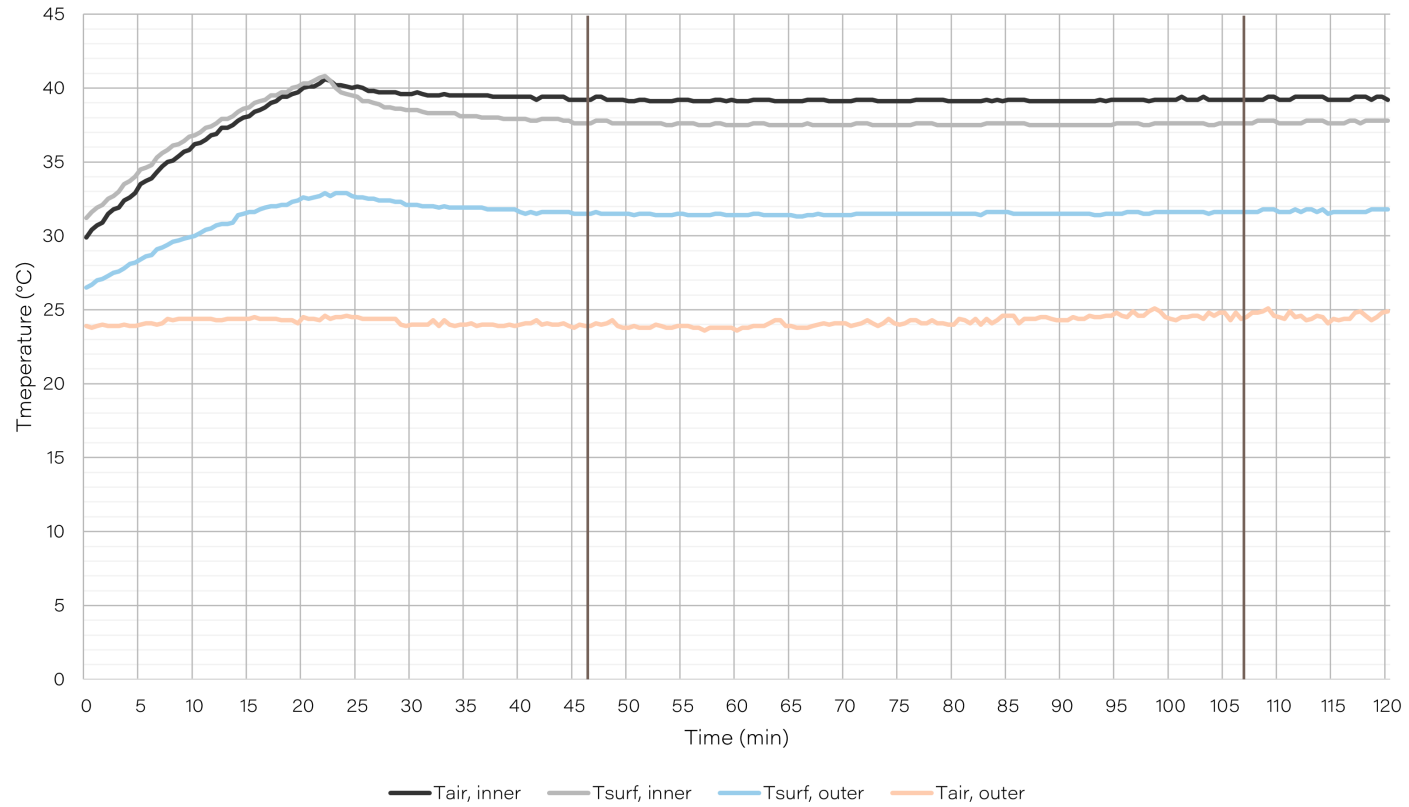


# Unguarded hot box

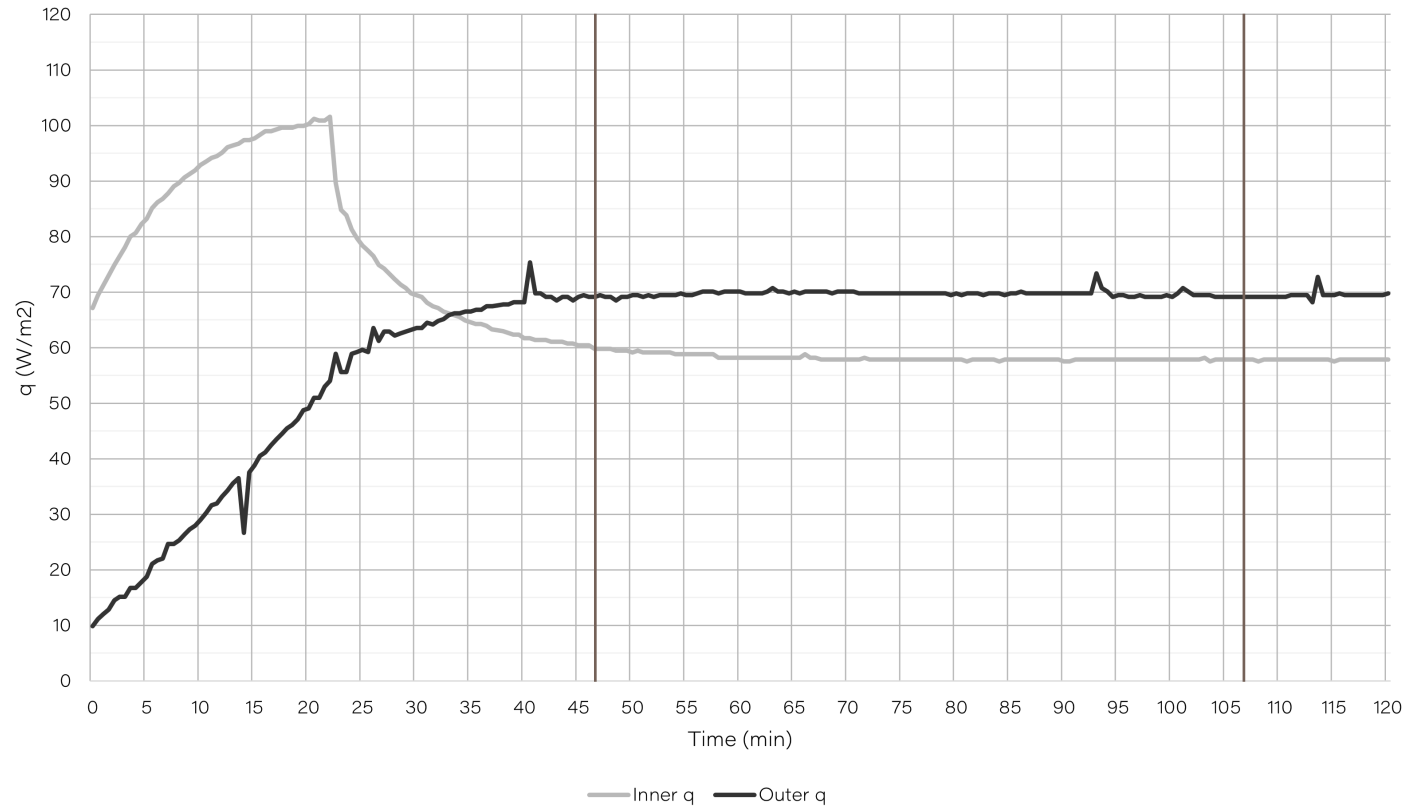




Design 2



## Design 2



$$R_c = \frac{(T_{\text{inner surf}} - T_{\text{outer surf}})}{q}$$

$$R_{\text{total}} = R_{\text{si}} + R_c + R_{\text{se}}$$

$$U_{\text{total}} = \frac{1}{R_{\text{total}}}$$

Time laps:

47 minutes to 107 minutes

Average temperature difference:

37.6 °C - 31.5 °C = 6.1 °C

Inside heat flux:

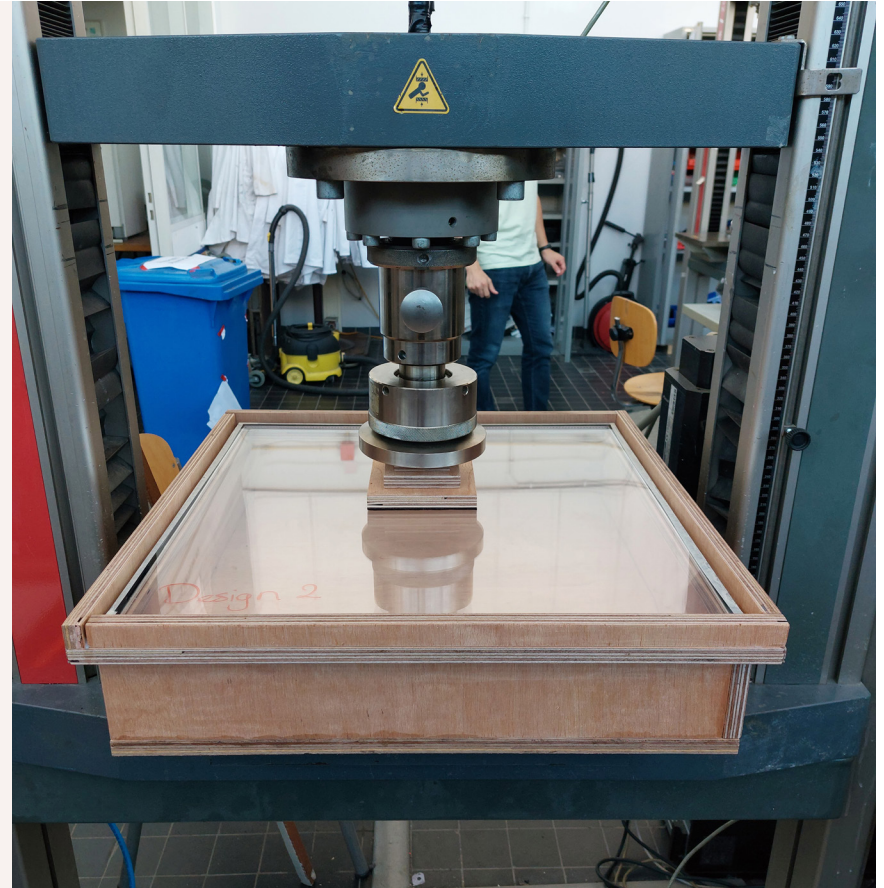
58.12 W/m<sup>2</sup>

Outside heat flux:

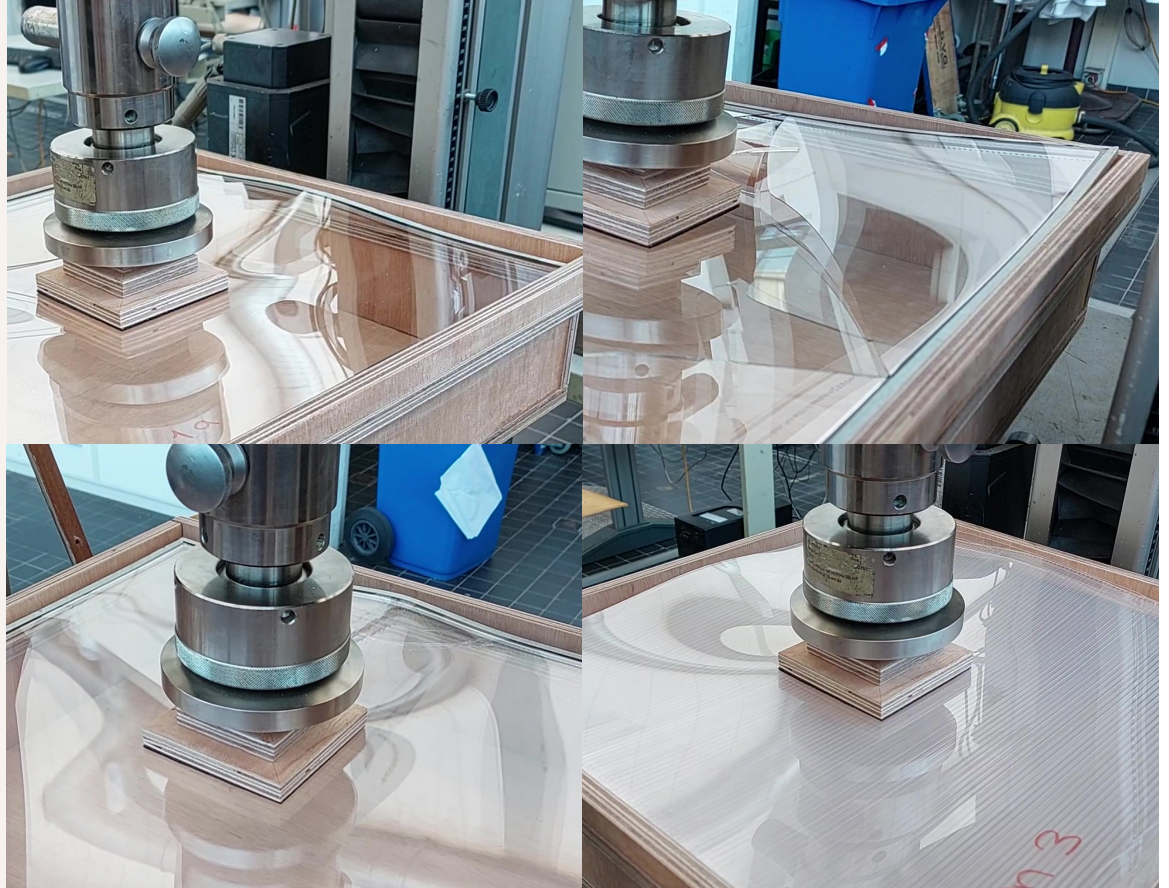
69.71 W/m<sup>2</sup>

#	Delta T	Inner q-value	Inner U-value	Outer q-value	Outer U-value	Delta U-value	SOLIDO
1	4,9	78,57	4,30	91,63	4,47	4,39	3,18
2	6,1	58,14	3,64	69,71	3,88	3,76	3,20
3	6,4	57,50	3,55	66,20	3,75	3,65	3,47
4a	9,4	84,96	3,56	85,88	3,58	3,57	3,96

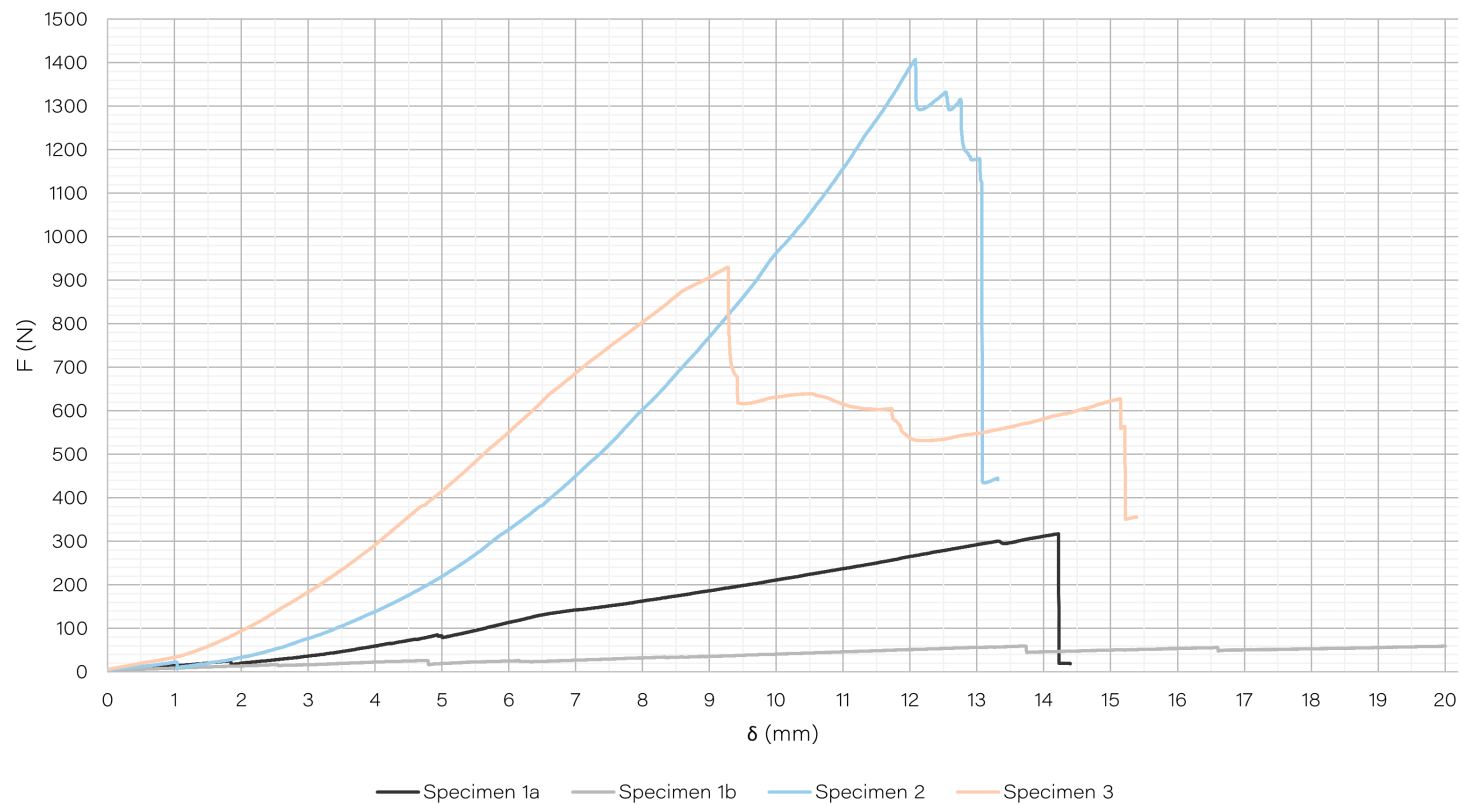
# Load on plate

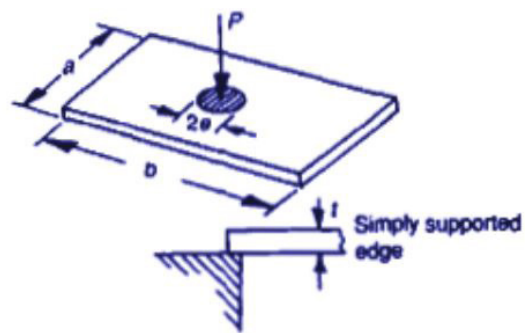


# Second order effect



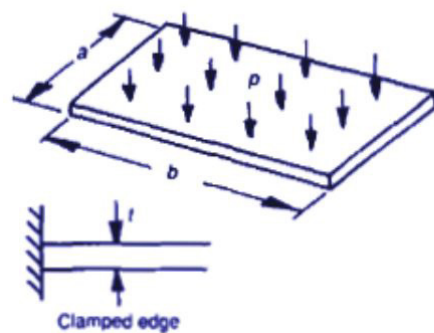
Results of bending test design 1





Stress equation at center

$$\sigma_m = \frac{1.5P}{\pi t^2} \left[ (1 + \nu) \ln \frac{2b}{\pi e} + 1 - k_2 \right]$$



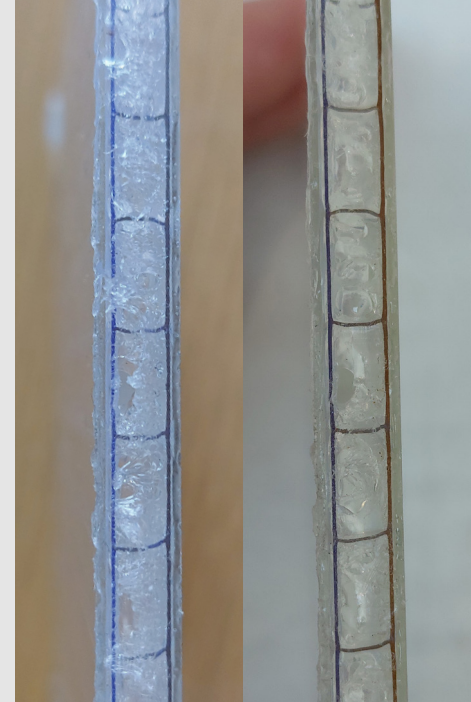
Stress equation

$$\sigma_m = \frac{pa^2}{2t^2 [0.623(a/b)^6 + 1]} \quad (\text{at middle of edge } b)$$



	$F_{\max}$ (N)	$w_{\max}$ (N/m <sup>2</sup> )	<1
Specimen 1a	318	4800	4,8
Specimen 1b	60	908	0,9
Specimen 2	1407	21276	21,3
Specimen 3	931	14071	14,1

# Ageing test

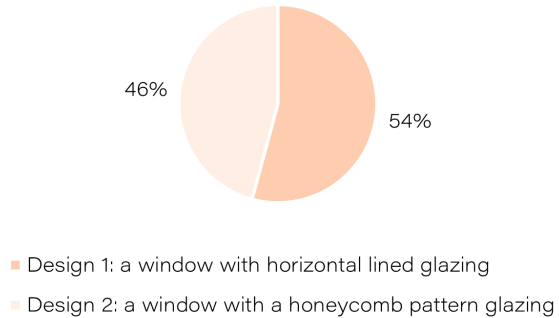


# Survey

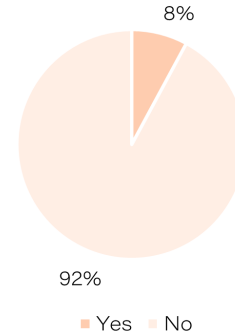




What is your personal preference?



Now knowing their U-value, did you change your preference?

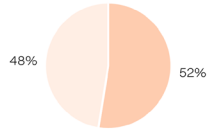


U-value

Single glazing:	5.8 W/m <sup>2</sup> *K
Horizontal lines:	3.4 W/m <sup>2</sup> *K
Honeycomb pattern:	3.6 W/m <sup>2</sup> *K

## General functions

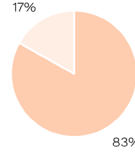
A housing building; the **living** room window



- Design 1: a window with horizontal lined glazing
- Design 2: a window with a honeycomb pattern glazing

## More private functions

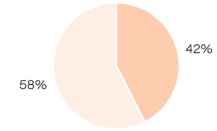
A housing building; the **bathroom** window



- Design 1: a window with horizontal lined glazing
- Design 2: a window with a honeycomb pattern glazing

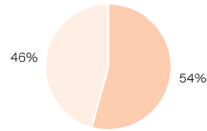
## More public functions

A **library** window



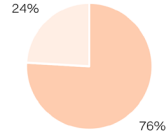
- Design 1: a window with horizontal lined glazing
- Design 2: a window with a honeycomb pattern glazing

An **office** window



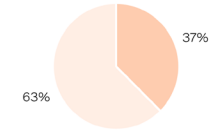
- Design 1: a window with horizontal lined glazing
- Design 2: a window with a honeycomb pattern glazing

An office building; the **toilet** window



- Design 1: a window with horizontal lined glazing
- Design 2: a window with a honeycomb pattern glazing

A **shop** window

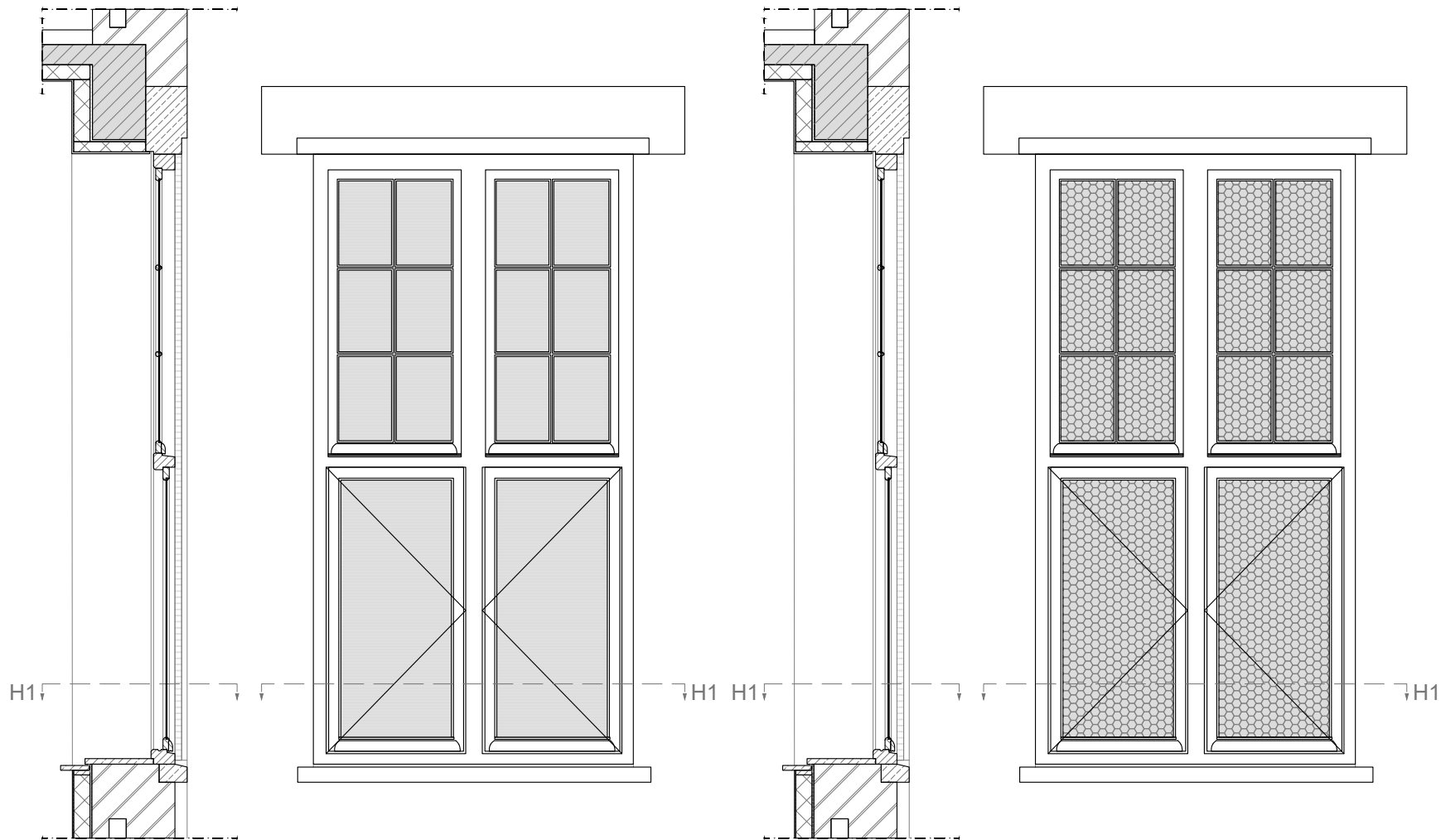


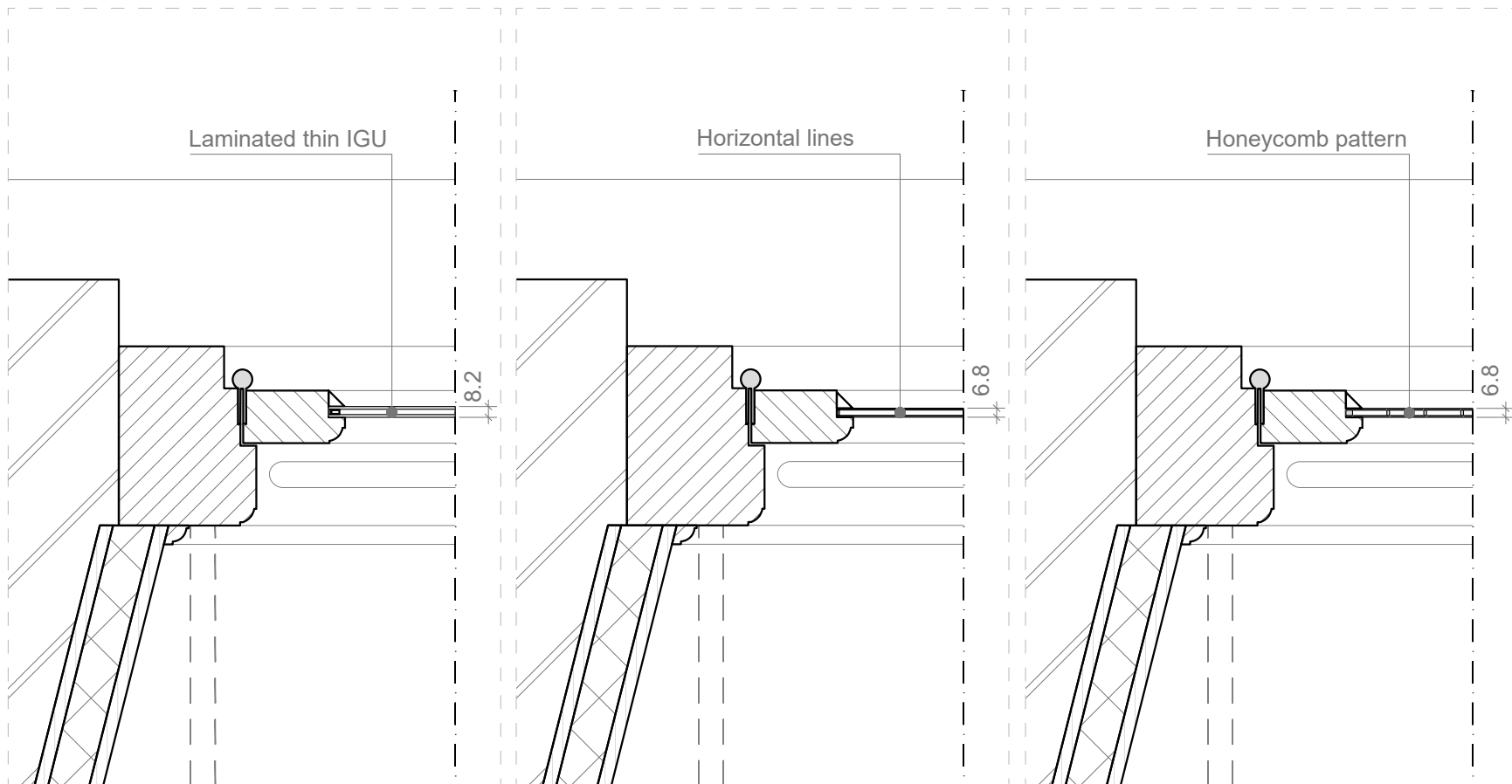
- Design 1: a window with horizontal lined glazing
- Design 2: a window with a honeycomb pattern glazing



# Conclusions







# Conclusion

	Thermal performance	Structural performance	Aesthetics	Makeability	Ageing	Total	
Design 1	★★★	★★	★★★★★	★★★★	★★★★★	3,8	★
Design 2	★★★★	★★★★★	★★★★	★★★★	★★★★	4,2	★
Design 3	★★★★★	★★★★	★★★	★★★★★	★★	3,8	★
Design 4	★★★★	★★★★	★★★	★★	★★★★	3,4	★
Design 5	★★	★★★★	★★★	★★	★★★★	3,0	★
Design 6	★	★★★	★	★★	★★★	2,0	★

# Recommendations

- Research the use of **chemically strengthened glass** for better structural performance.
- Experiment with **different lamination layers** for the highest transparency and strength (SG).
- The most optimal design for proposal 4 can be research.
- Try prototyping design 4 with structural tape or UV glue.
- Test the design also on **transport** forces or point loads.

Thank you!



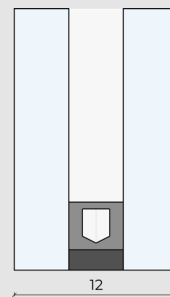
## Design objective

“Design a **thin glass panel** that could replace single glazing in heritage buildings, **aiming for similar U-values** as solutions for non-heritage buildings.”

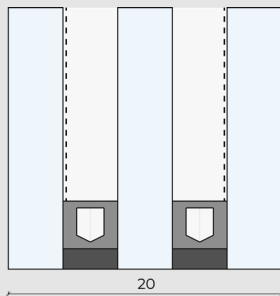
# Regular windows



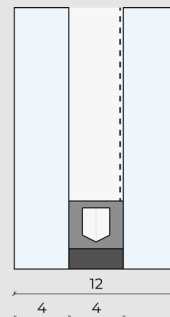
Single glazing  
U-value =  $5.8 \text{ W/m}^2\text{K}$   
€50/m<sup>2</sup>



Double glazing  
U-value =  $2.8 \text{ W/m}^2\text{K}$   
€80/m<sup>2</sup>



Triple glazing  
U-value =  $0.8 \text{ W/m}^2\text{K}$   
€120-150/m<sup>2</sup>

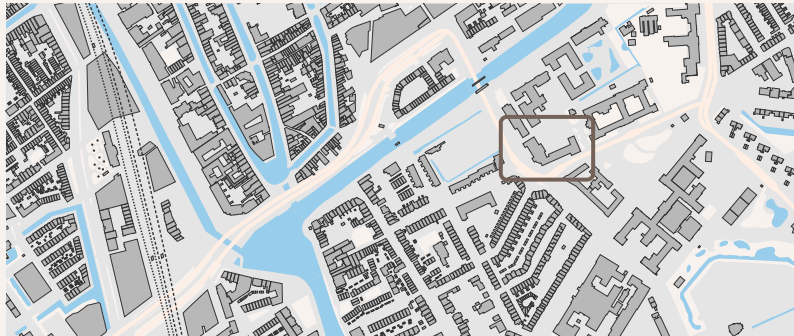


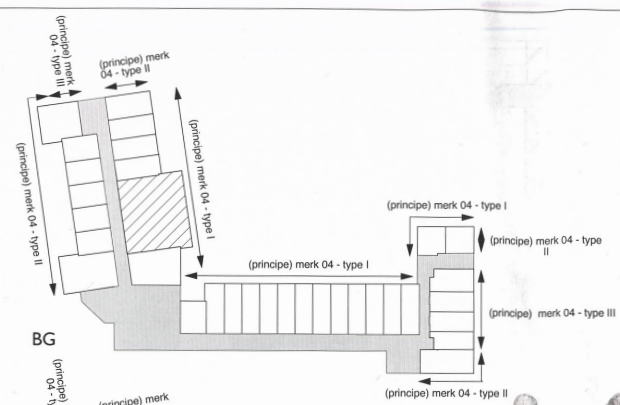
Low E coating  
U-value =  $1.6 \text{ W/m}^2\text{K}$   
€90/m<sup>2</sup>



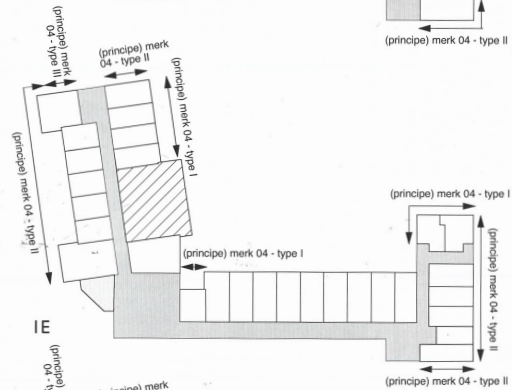
# Case study

- Mijnbouwplein 11
- Built in 1930
- G. van Drecht
- Former faculty of Applied Physics
- DUWO

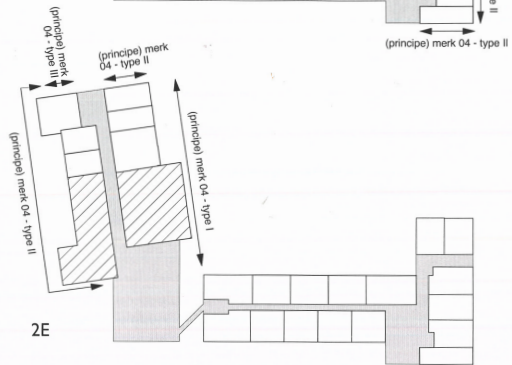




BG



IE



2E

## DETAILVERWIJZINGEN

Woningen BG 1e 2e 3e

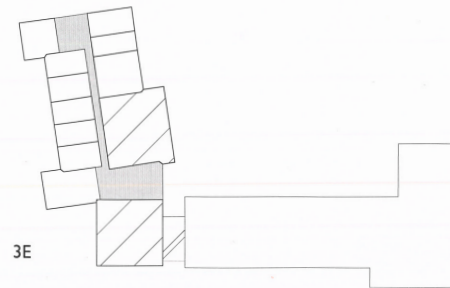
Bedrijfsruimtes

Algemene verkeersruimte (gang, trap, hal)

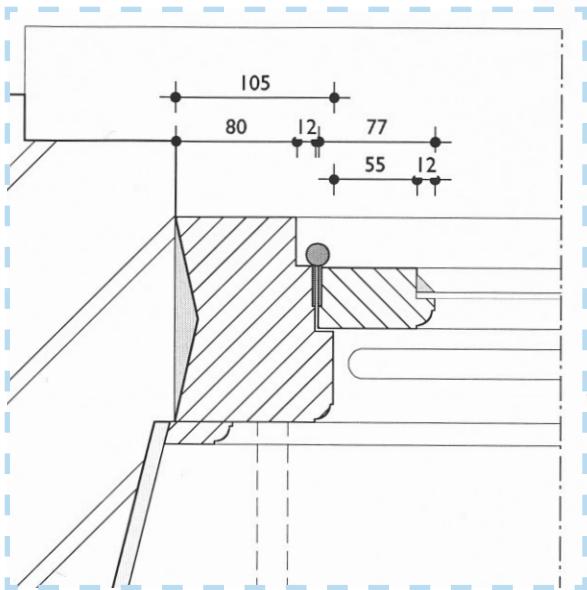
Algemene gebruiksruimte (wasruimte)

Restruimtes

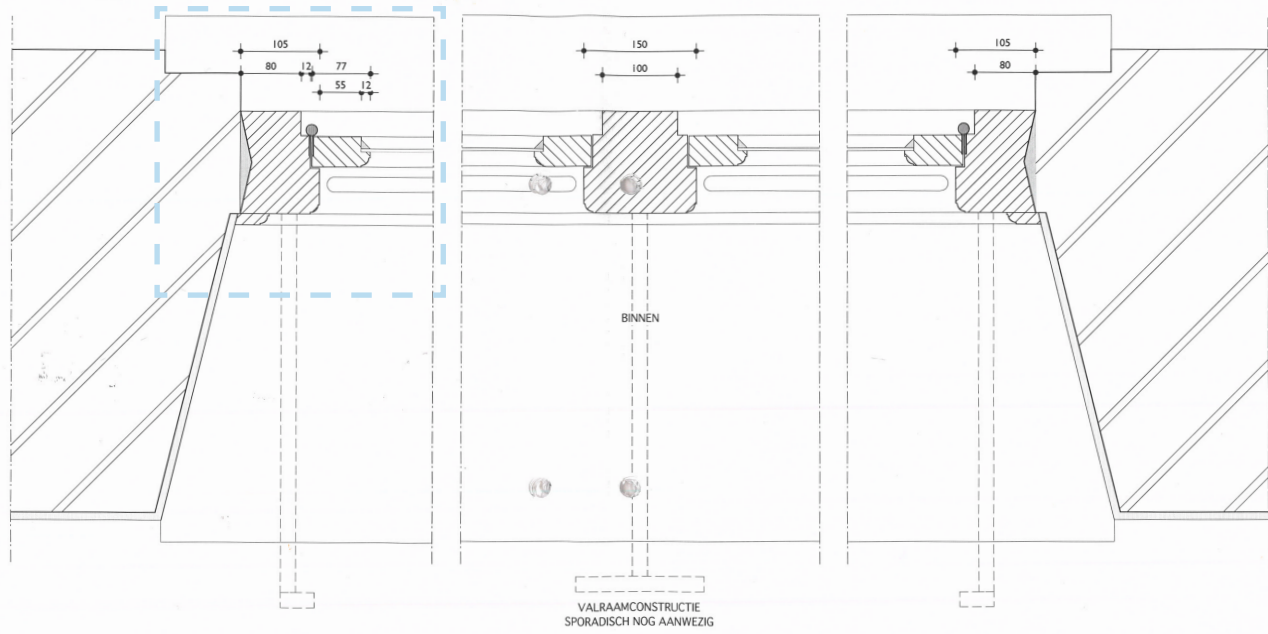
Alle kozijnen in betreffend gevelvlak worden gelijkwaardig opgelost i.o.m. architect

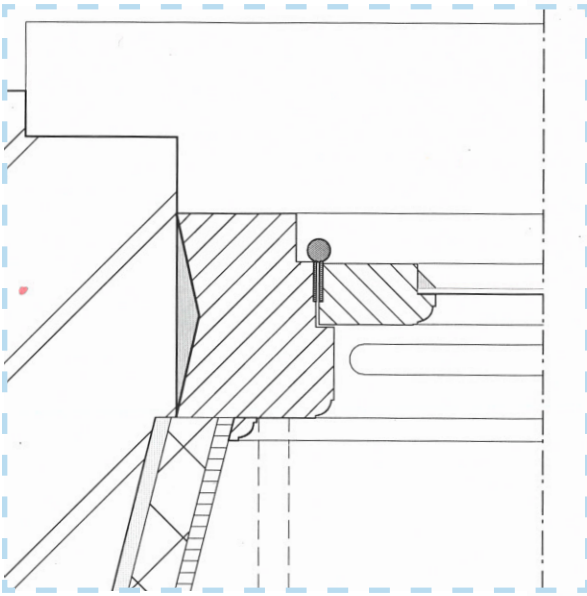


3E

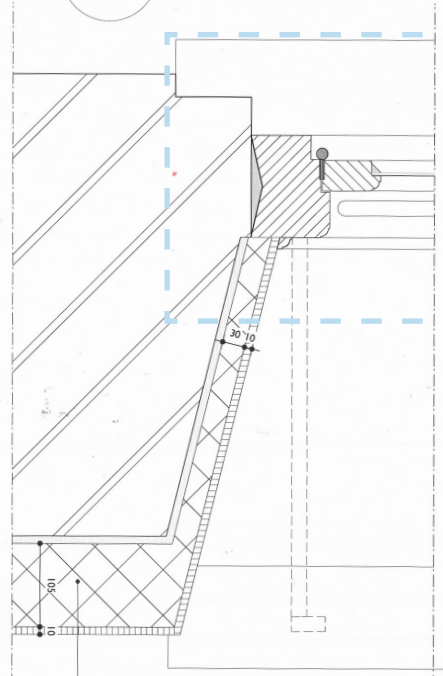


H1

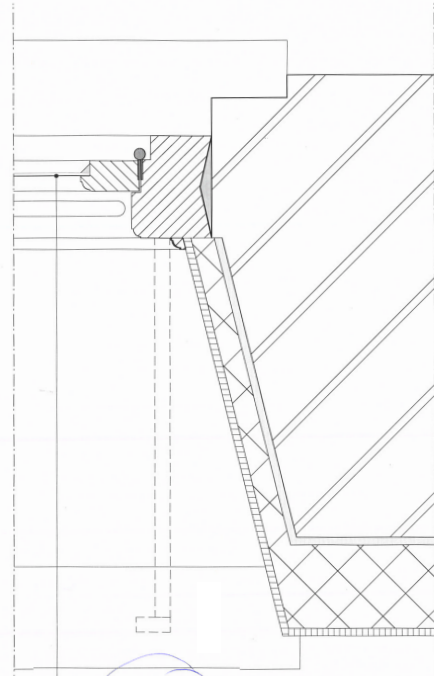
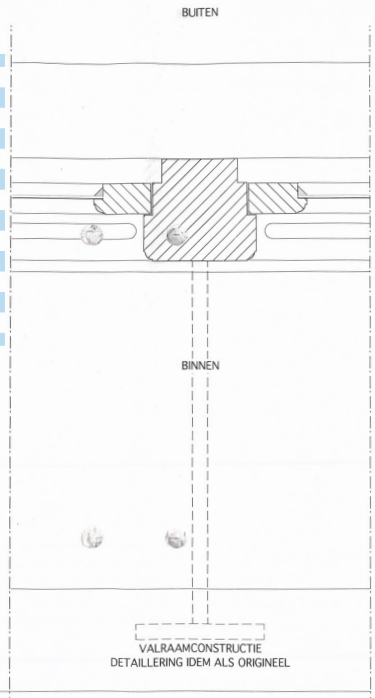




H1

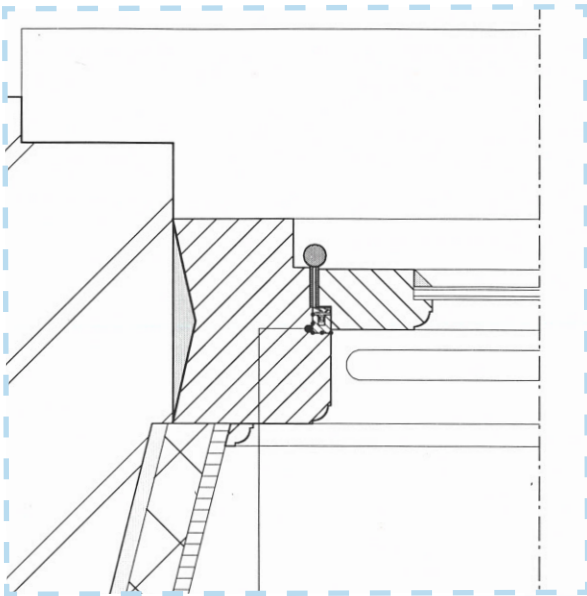


Voorzetwand:  
-isolatie 105mm.  
-dampremmende laag  
-gipsvezelplaat 10mm.

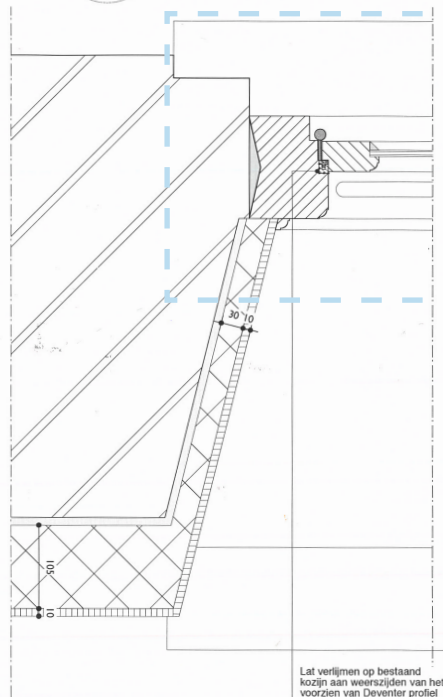


bestaand glas vervangen  
door 4mm. Ruysdaelglas

Handwritten note: *Hand*  
+0.9 → afkond gegeven  
op alwin, mits gety



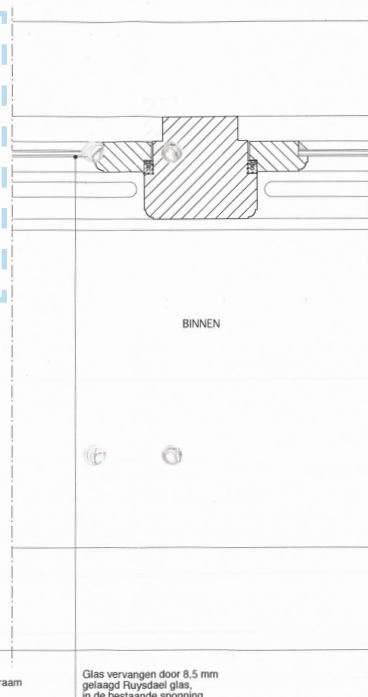
H1



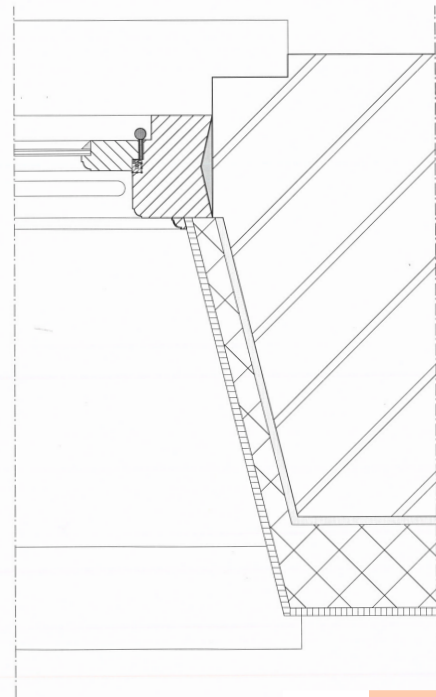
Lat verlijmen op bestaand kozijn aan weerszijden van het raam voorzien van Deventer profiel S 6577; indrukking 3 mm geluidwering: 35 db(A)

Sparing frezen in bestaand raamhout tbv het creëren van een aanslag

BUITEN



BINNEN



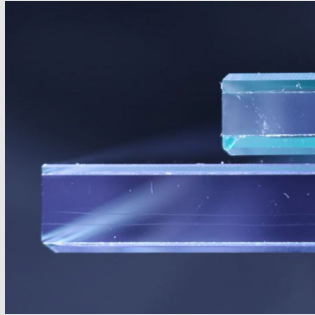
Glas vervangen door 8,5 mm gelaagd Ruysdael glas, in de bestaande sponning, afwerken met kit. Geluidwering 32 db(A)



# Literature study



# Current studies



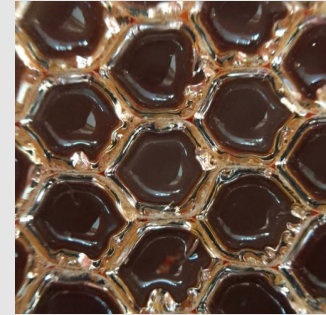
Hanig (2021)

- Cast PMMA
- Design possibility inside acrylic
- Bad thermal performance
- Focus on interior



Saleh (2020)

- Composite with 3D printed PET
- Detailed testing methods
- Thermal performance not tested

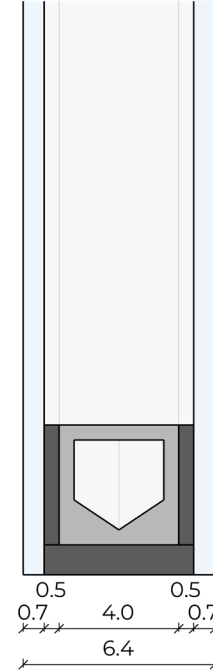
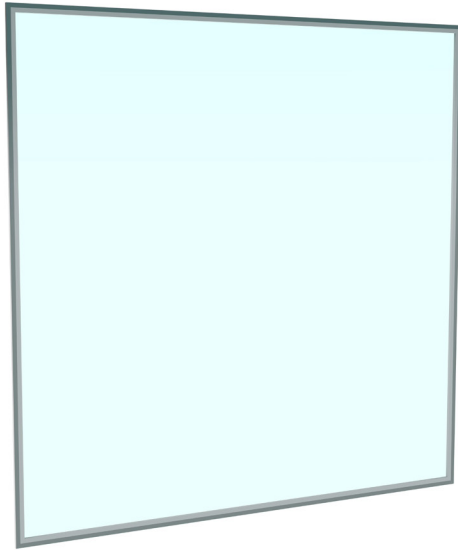


Van der Weijde (2017)

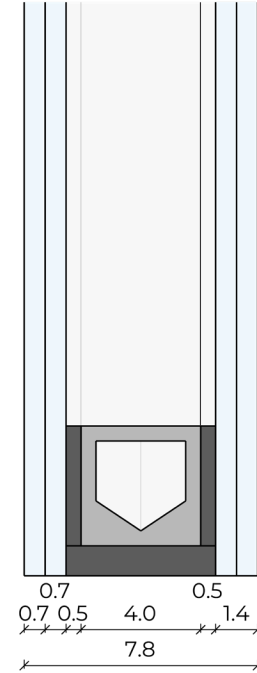
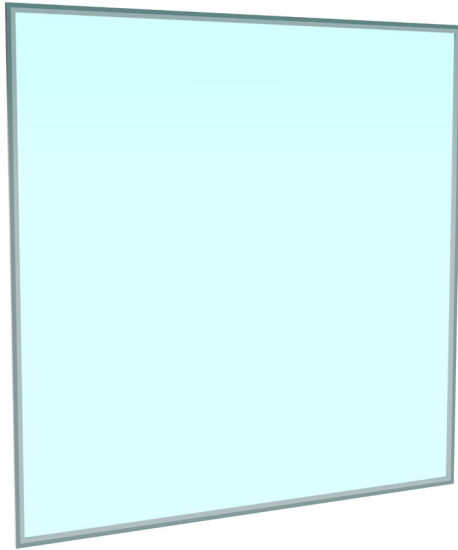
- Composite with amirid paper
- Translucent
- Different lamination techniques
- U-value of 1.4 W/m<sup>2</sup>K



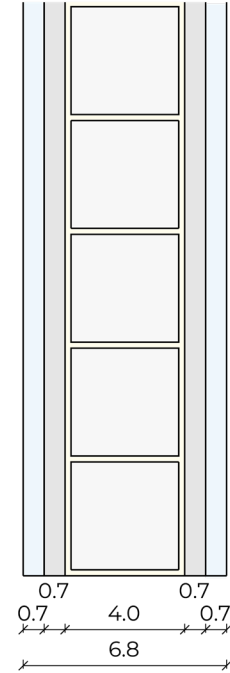
# Design proposal 1



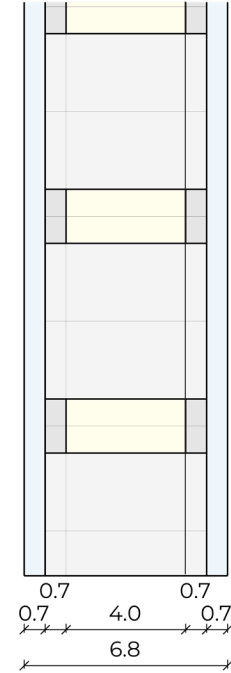
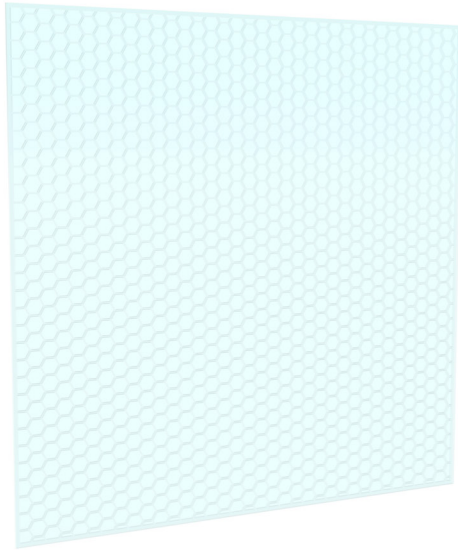
# Design proposal 2

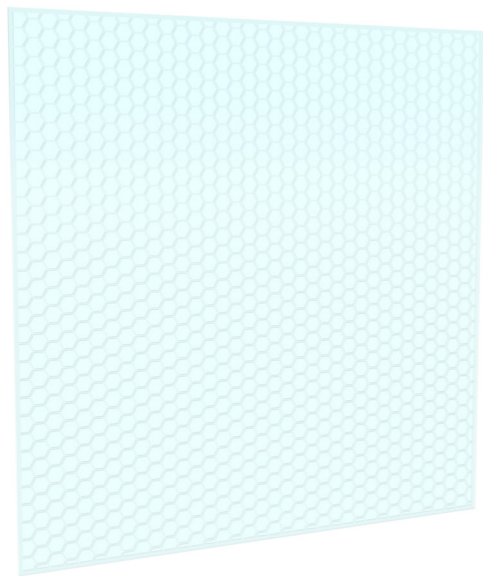
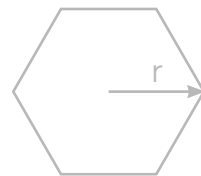


# Design proposal 3

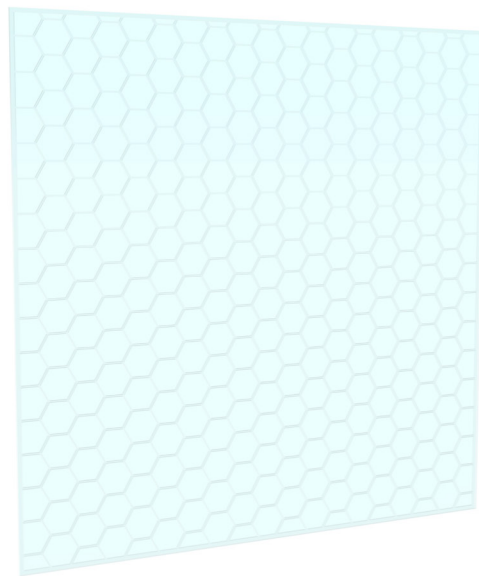


# Design proposal 4





$r = 10 \text{ mm}$

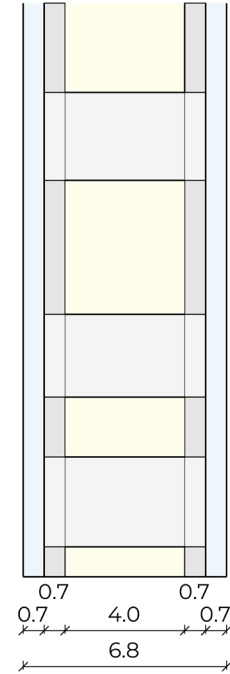
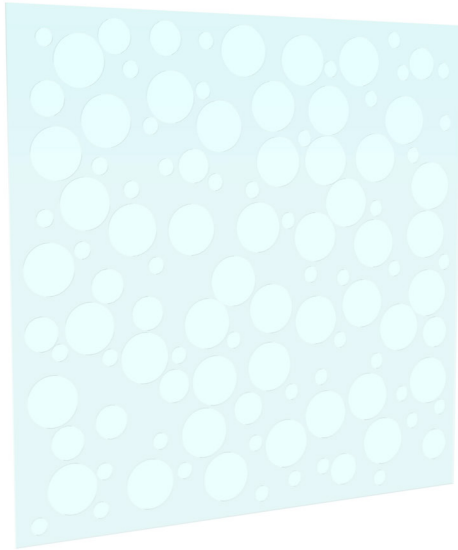


$r = 20 \text{ mm}$

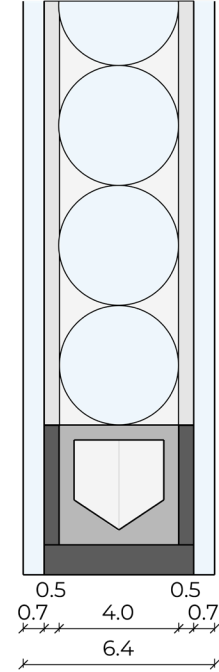
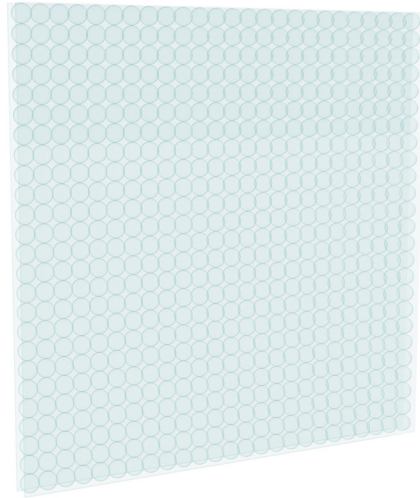


$r = 30 \text{ mm}$

# Design proposal 5

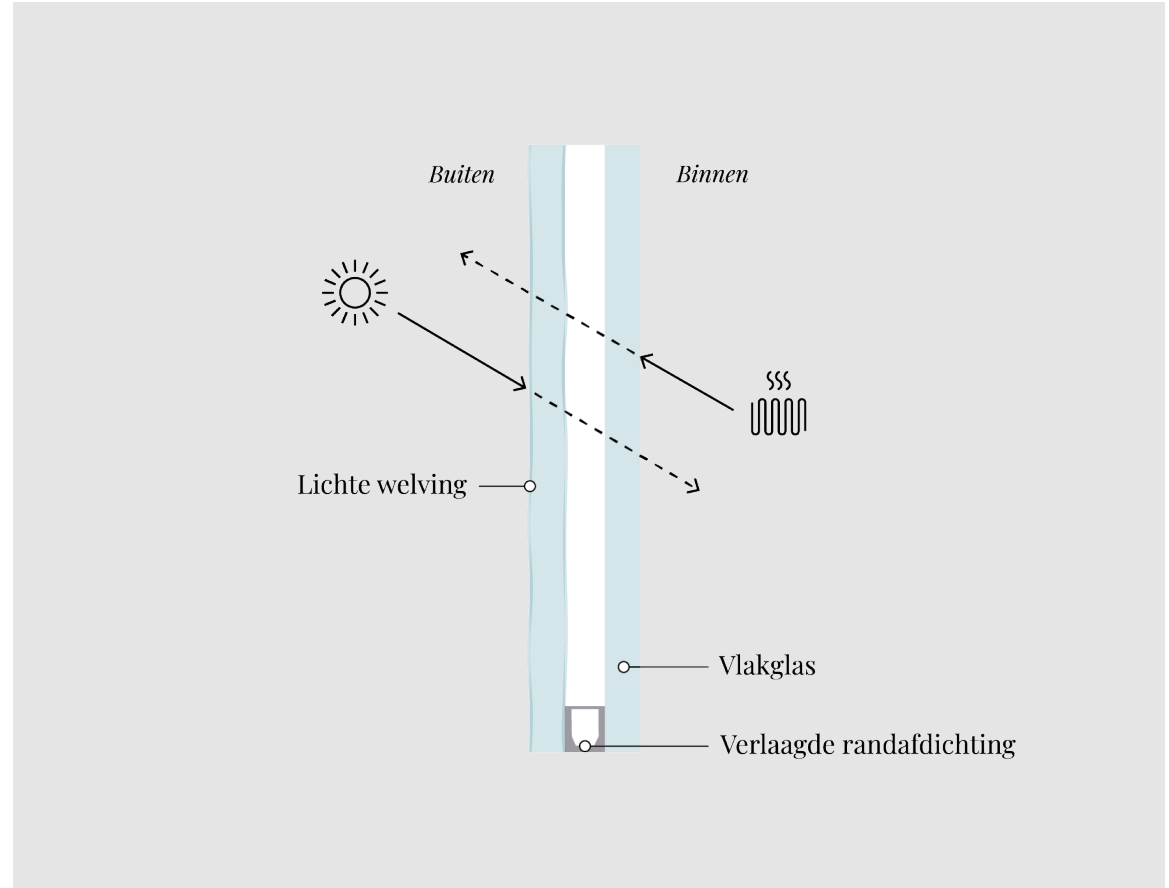


# Design proposal 6



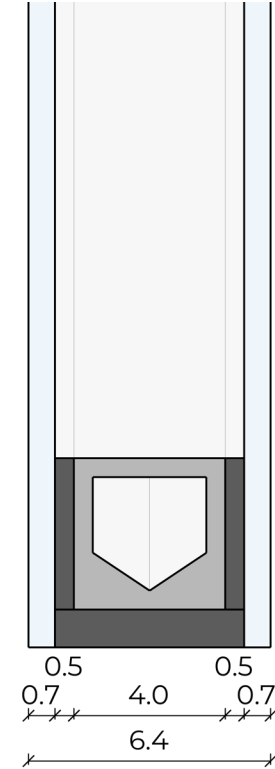


# Inspiration



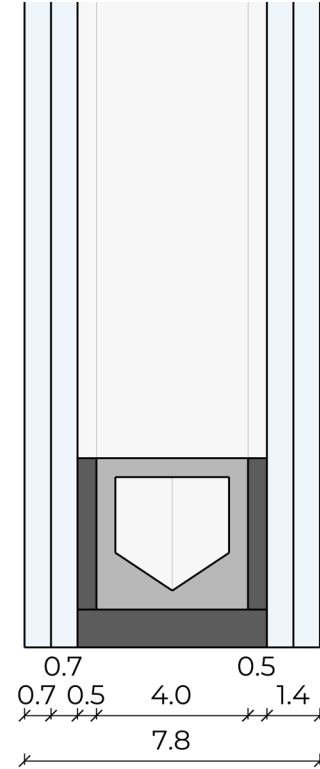
# Design proposal 1

- Use current technique
- 3 mm spacer and silicone sealant
- Panel stiffness
- U-value =  $3.37 \text{ W/m}^2\text{K}$
- Total thickness = 4.5 mm

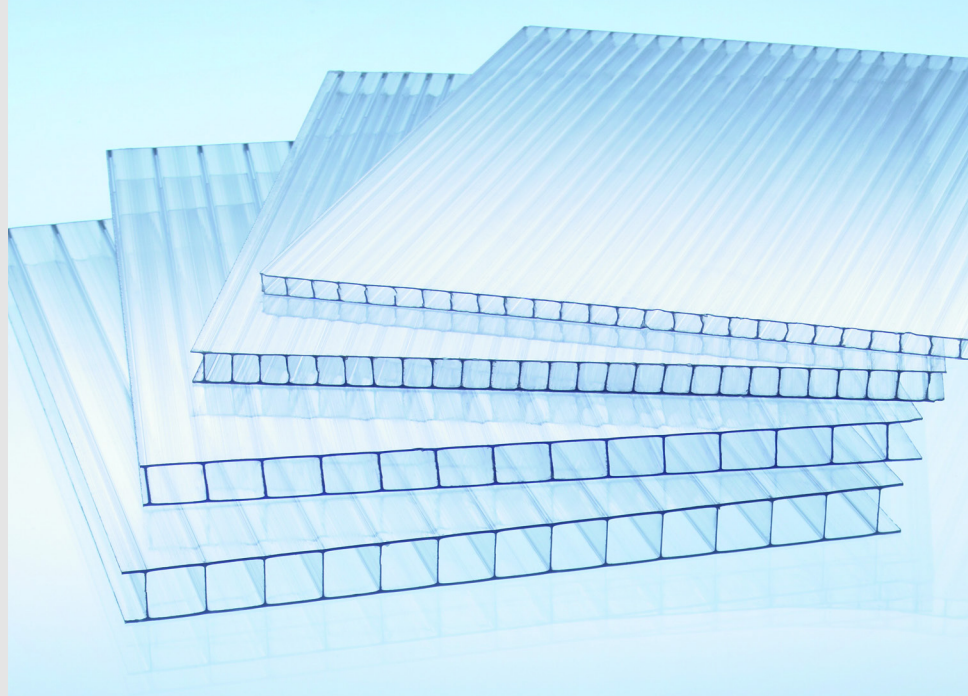


# Design proposal 2

- Use current technique
- Laminated thin glass
- 3mm spacer and silicone sealant
- Panel stiffness
- U-value =  $3.37 \text{ W/m}^2\text{K}$
- Total thickness = 6 mm

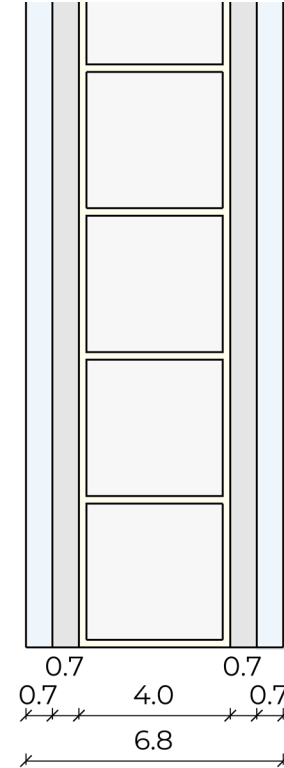


# Inspiration

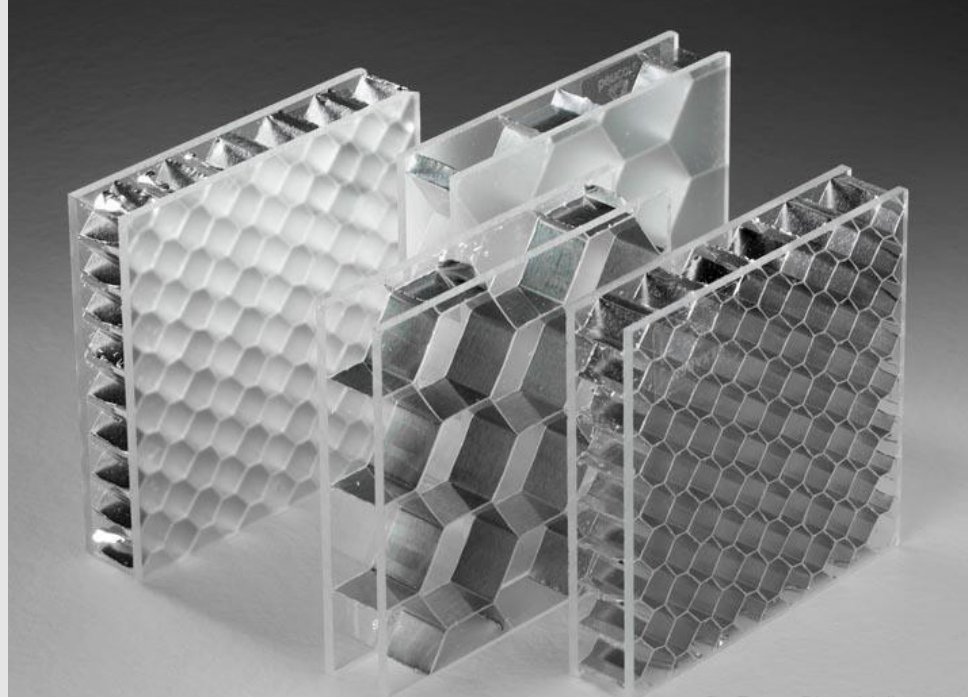


# Design proposal 3

- Use existing material
- Laminate with PVB or ionomer interlayer
- Melting temperatures
  - PVB 138°C
  - PC 147°C
  - PMMA 160°C
- Silicone seal needed?
- U-value = 2.37 W/m<sup>2</sup>K
- Total thickness = 5.5 mm

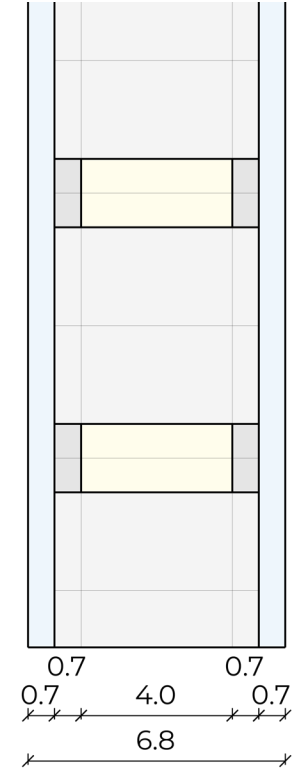


# Inspiration

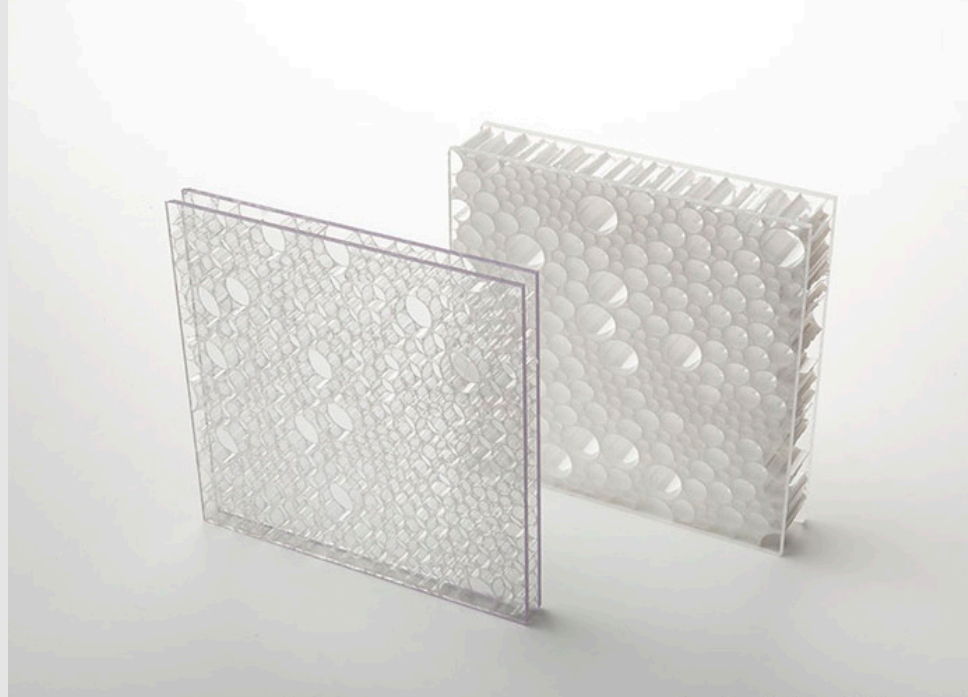


# Design proposal 4

- Lasercut PMMA sheet with hexagons
- Laminate with PVB or ionomer interlayer
- Laminate without air bubbles
- U-value = ?  $\text{W/m}^2\text{K}$
- Total thickness = 3.5 mm



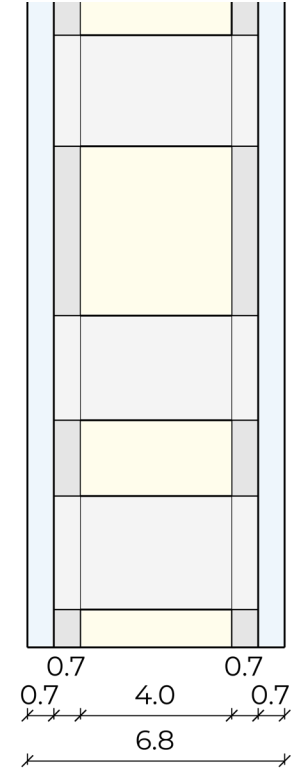
# Inspiration





# Design proposal 5

- Lasercut PMMA sheet with 'random' shapes
- Laminate with PVB or ionomer interlayer
- Laminate without air bubbles
- U-value = ?  $\text{W/m}^2\text{K}$
- Total thickness = 3.5 mm

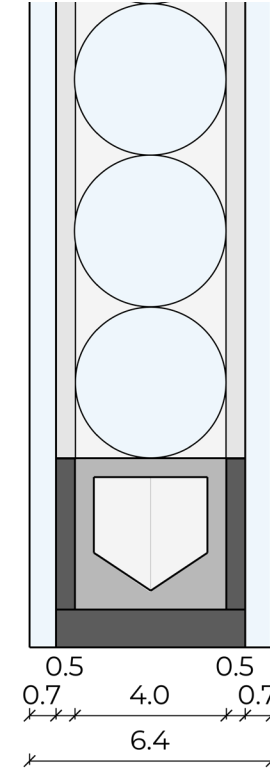


# Inspiration

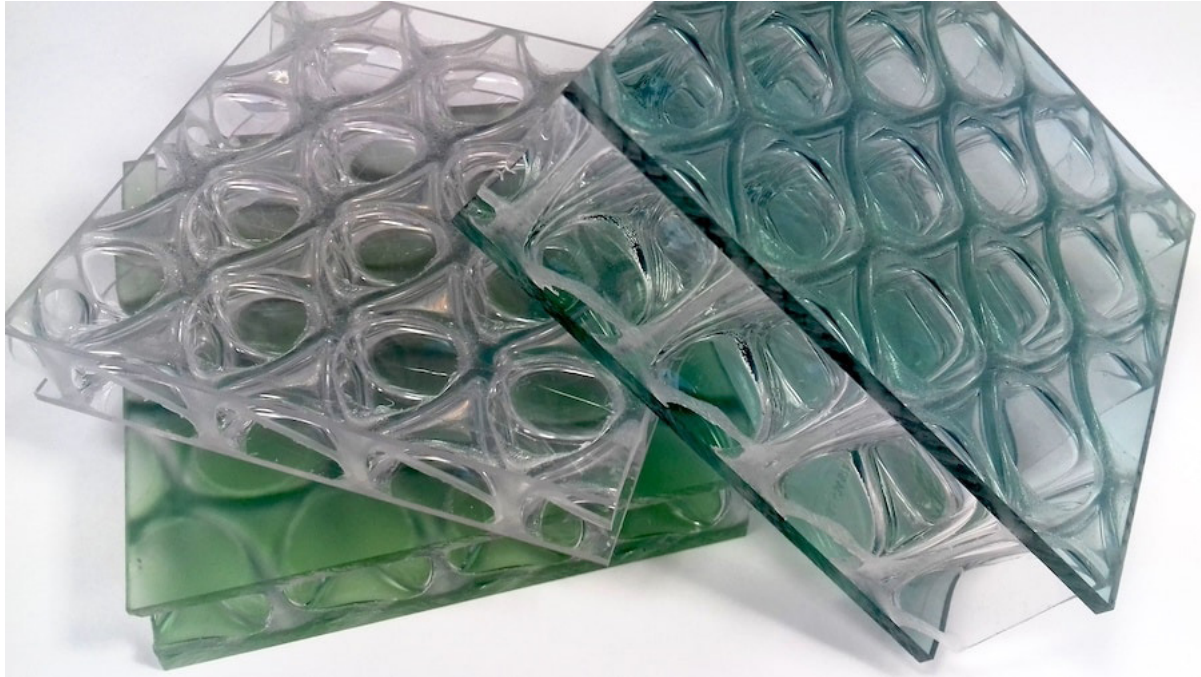


# Design proposal 6

- Use existing material
- Glue balls to one sheet
- Add second glass sheet
- Seal air inside
- U-value = ?  $\text{W/m}^2\text{K}$
- Total thickness = 4.5 mm

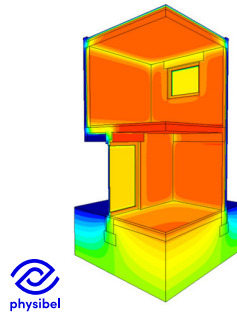








# Simulations

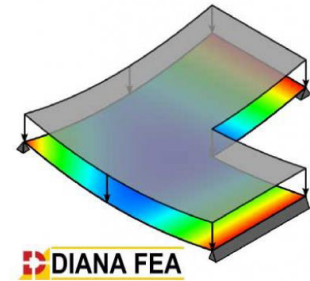


## TRISCO

- Testing thermal performance
- Gives heat flow

$$R_{\text{TRISO}} = \frac{Q}{A \cdot \Delta T}$$

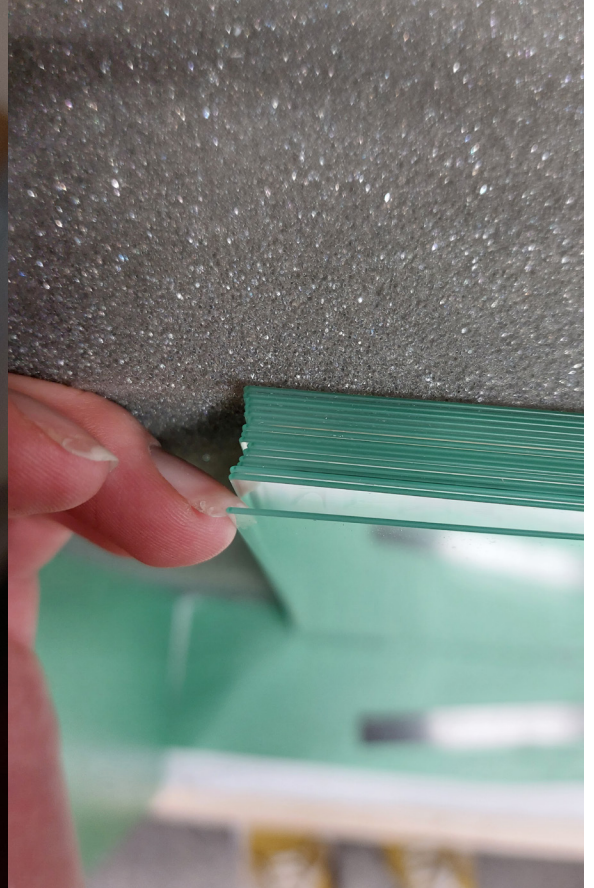
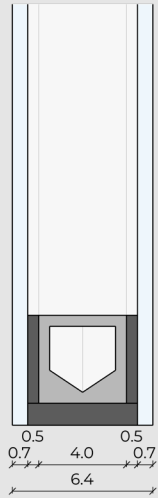
$$U_{\text{TRISCO}} = \frac{1}{R_{\text{TRISCO}}}$$



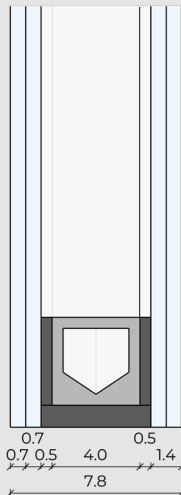
## DIANA FEA

- Testing structural performance
- Input NEN
- Gives stresses and deflection

# Design 1



# Design 2



4. Creating/modifying the process recipe
- Select item 3 from the main menu (Programs). The first step (prestart) of the recipe is displayed. These are the initial conditions (pressure and temperature) that need to be met before the program proceeds to the next step, which starts the actual lamination cycle. Tap in a field to modify its value.
  - Tap (Next), program step 2 is displayed (see fig. 5). For this and all consecutive steps, the parameters pressure (top) and bottom compartment (bottom) and the temperature of the bottom plate can be set. Time is the duration of the step, for a change in temperature account at least 1 minute per 8 °C increase. Press (End) means the pin and down (module in manufacturing tests on the heater). Press (I) means the module is lifted.
  - A recipe can consist of 15 steps maximum. When a value in the time field of 9999 seconds is set, that step is treated as the last step in the sequence (see fig. 6).
  - Below you can find the standard recipe for glass/glass and modules, optimized for Photocap 233ACF Vire.

Step	Time (s)	P <sub>top</sub> (mbar)	P <sub>bot</sub> (mbar)	T <sub>set</sub> (°C)	Pin	Remarks
1	1000	1000	1000	80	Up	Process continues when T is reached
2	120	0	0	80	Up	Evacuating
3	100	0	0	140	Up	Heating up
4	60	100	0	140	Down	Compressing
5	100	100	0	140	Down	Curing
6	30	0	1000	145	Down	Venting
7	30	0	1000	145	Up	Release
8	9999	1000	1000	60	Up	End of recipe

5. Running a lamination cycle
- Select item 6 from the main menu (Automatic).
  - Tap on the (Automatic) field.
  - Place the parts of the module in the making on the pins, control over the bottom plate. Use Teflon sheets to prevent sticking of the molten EVA to the heater or silicone cover (in the lid of the laminator).
  - Tap (Prestart). The prestart lights start flashing and will start burning continuously when the set temperature has been reached.
  - Close the lid of the laminator and keep it firmly closed. The program then automatically moves to the second step, and the execution of the lamination cycle starts. Progress can be monitored on the touch screen. If desired, the program can be forced to move to the next step by tapping (Next), or the recipe can be aborted by tapping on (Manual).
  - Sometimes a short buzzing sound can be heard when progressing to a next step. This can be ignored.
  - At the end of the lamination cycle also a buzzing sound can be heard. Open the lid of the laminator, and let the module and system cool down until the temperature has dropped sufficiently (40°C). You can now take out your module.



Fig. 7: Prestart step 1

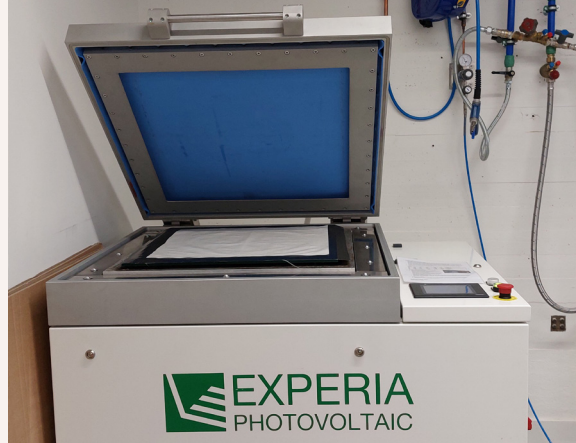
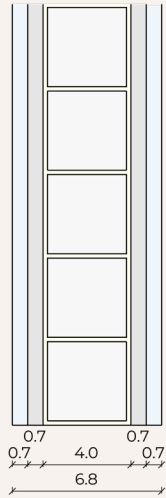
6. Finalising your work:
- Switch off the mains on the right side of the machine and close the compressed air connection
  - Make sure the heater plate, silicone sheet and Teflon sheets are clean (remove EVA residue)

Questions? Problems? Contact:  
 Maxjon Tjorne: 86278  
 Stefan Heiman: 87626



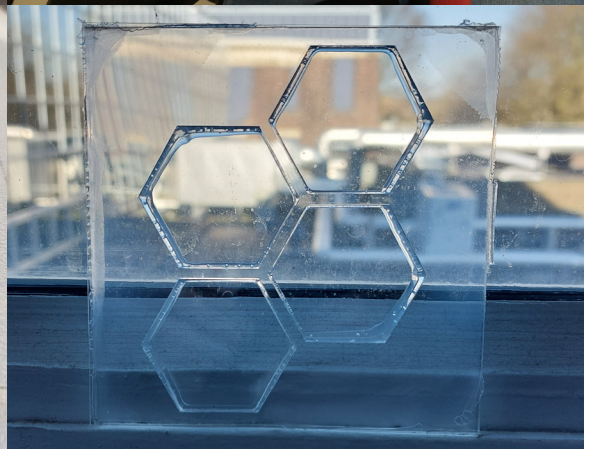
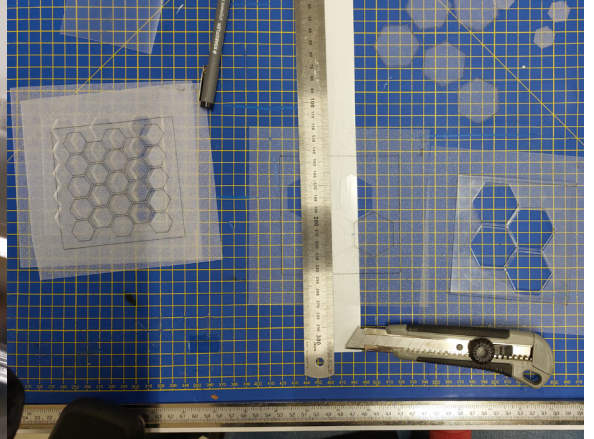
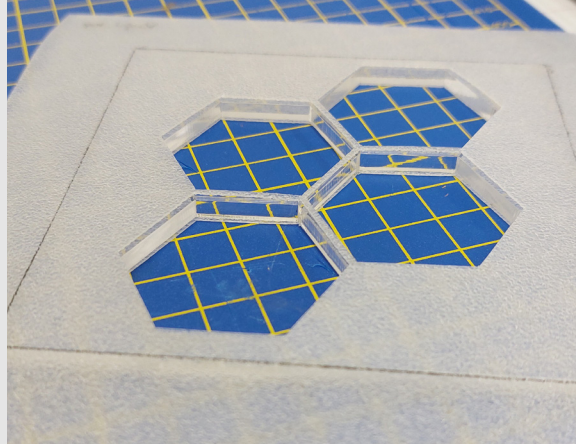
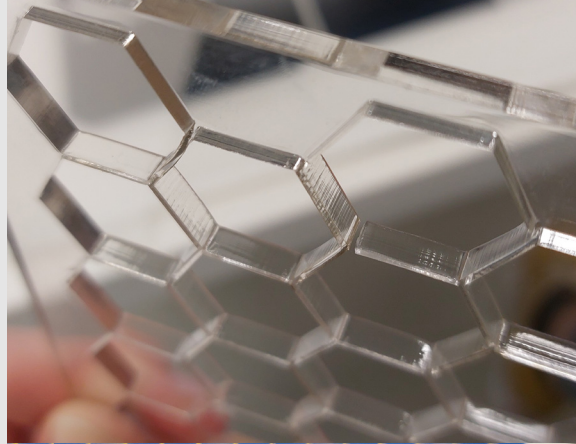
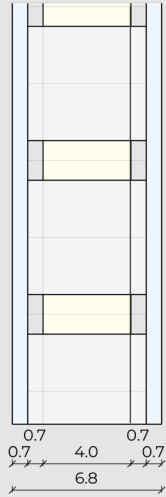


# Design 3





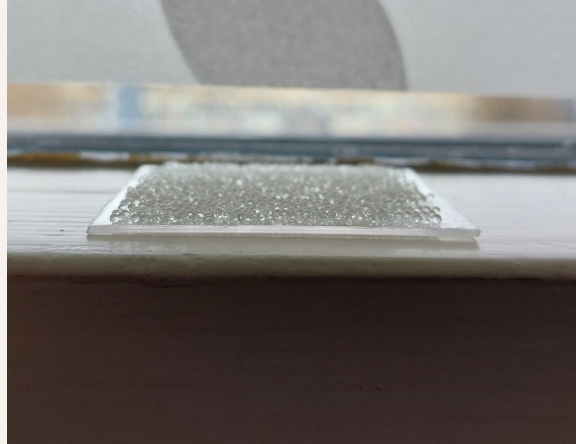
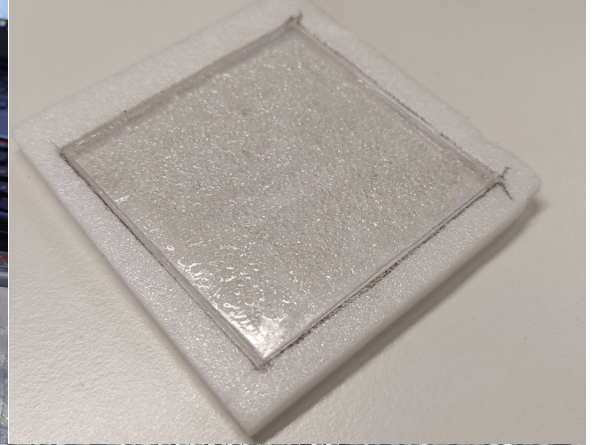
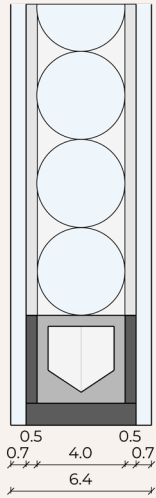
# Design 4a & 4b





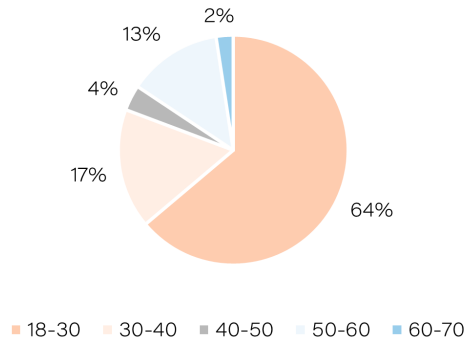


# Design 6

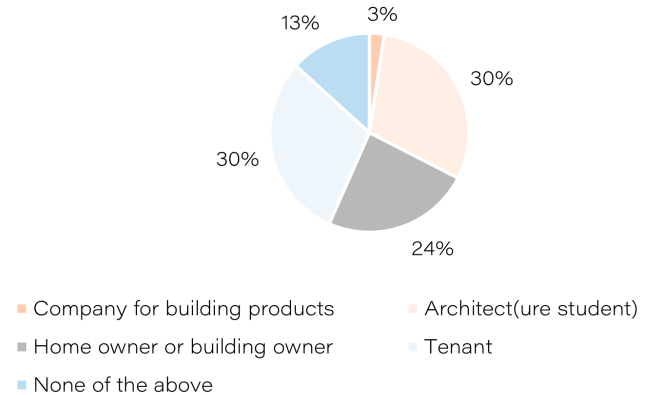


# Survey

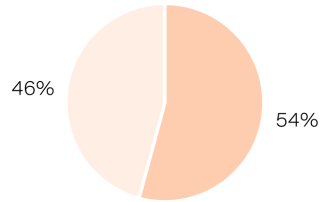
What is your age?



Which description fits you best?

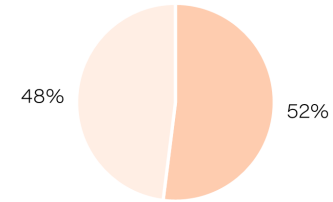


What is your personal preference?



- Design 1: a window with horizontal lined glazing
- Design 2: a window with a honeycomb pattern glazing

Architects: What is your personal preference?



- Design 1: a window with horizontal lined glazing
- Design 2: a window with a honeycomb pattern glazing

# Hand calculations



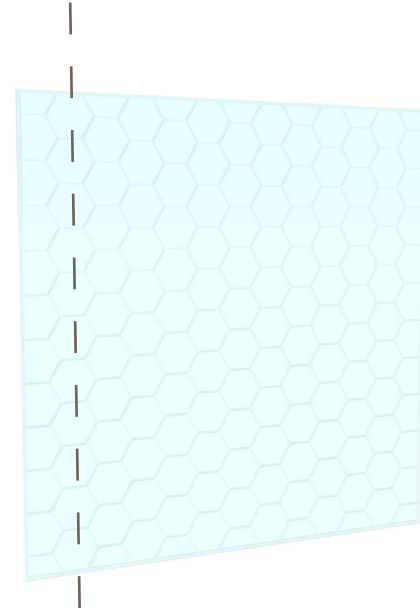
$$\text{Width}_{\text{glass,new}} = \text{Width}_{\text{glass}} * (E_{\text{glass}}/E_{\text{PMMA}})$$

$$I_{\text{total}} = \sum I + \sum (A * y^2)$$

$$\delta_{\text{max}} = \frac{1}{384} * \frac{ql^4}{EI}$$

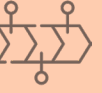
$$M_{\text{max}} = \frac{1}{12} * ql^2$$

$$\sigma_{\text{max}} = \frac{M * y}{I}$$



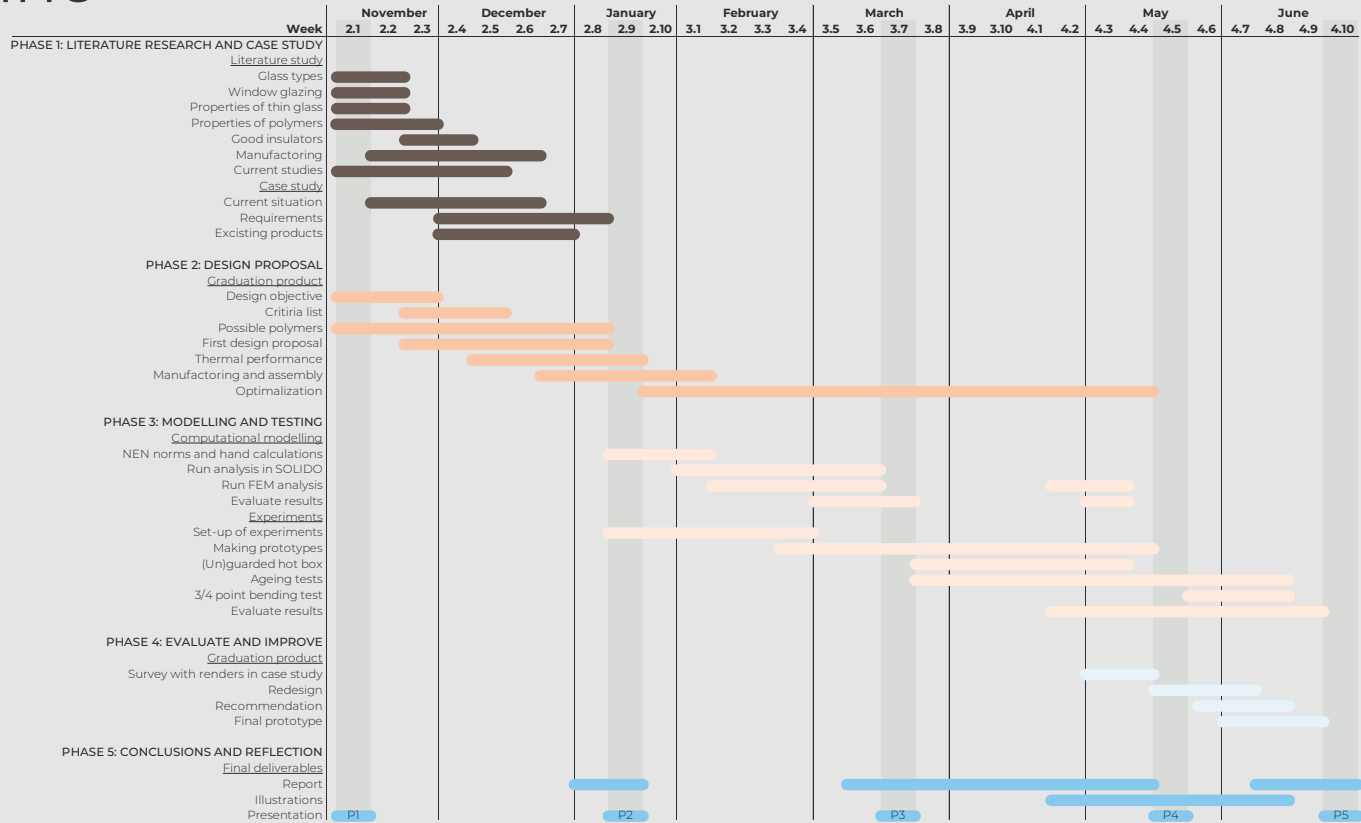


#	Material	Deflection	Allowed deflection	Check deflection	Max stress	Allowed stress	Check stress
1	Glass	40,673	10,88	: (	127,55	15	: (
2	Glass	5,084	10,88	: )	31,89	15	: (
3	Glass	0,29748	10,88	: )	7,20	15	: )
	PC				0,17	70	: )
4a	Glass	0,29753	10,88	: )	7,21	15	: )
	PMMA				0,22	70	: )
4b	Glass	0,29793	10,88	: )	7,21	15	: )
	PMMA				0,22	70	: )
4c	Glass	0,29806	10,88	: )	7,20	15	: )
	PMMA				0,22	70	: )



# Planning

# Timeline



# To do list

- Test on wind load
- Take UV samples out
- Make final results, conclusions and recommendations part
- Make 2D details of window (1:20 and 1:5)
- Decide where to place which window in case study

## Problem statement

“To **reduce the heating energy** in heritage buildings, **modern solutions** that replace the single glazing **are not as good** as solutions for non-heritage buildings.”

# Flowchart

