### Floor slab optimization

Reducing the environmental impact of concrete construction through fabrication-aware, structurally optimized floor slabs

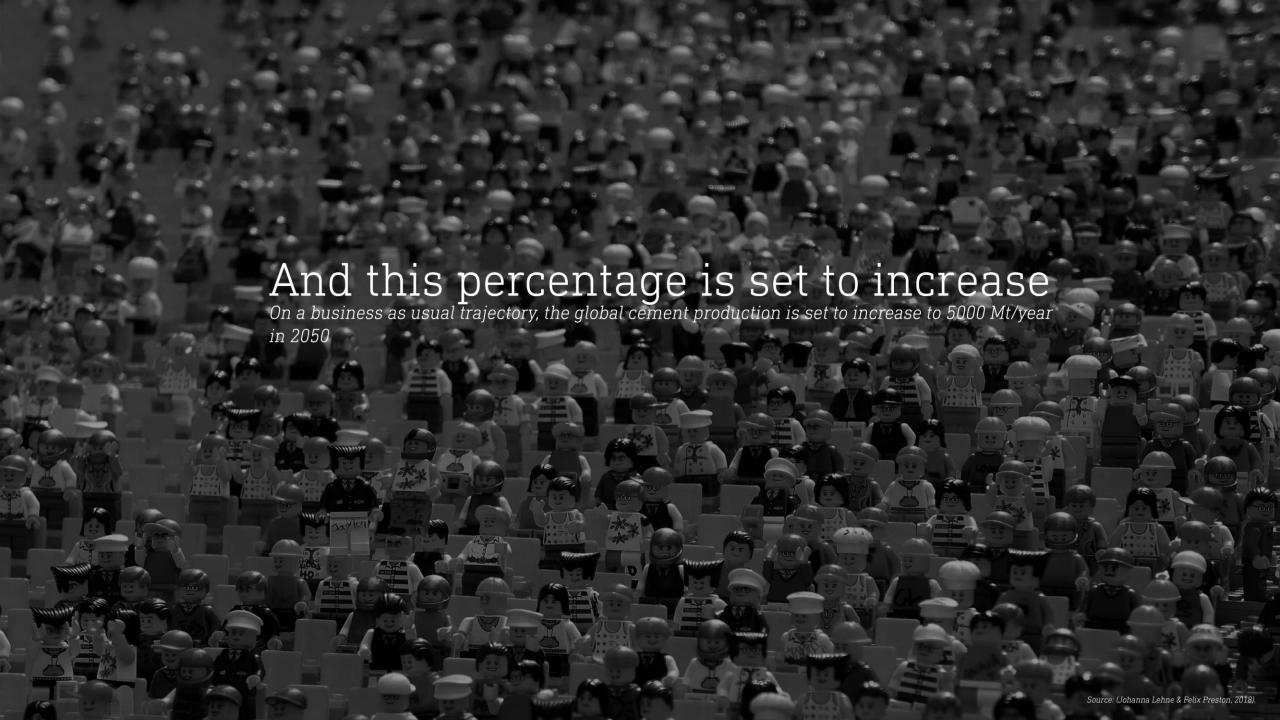
4385896 Kees Leemeijer

Building Technology Master of Science at the Delft University of Technology,

Supervisor: Dr. S. (Serdar) Asut, Dr.ir. H.R. (Roel) Schipper Graduation committee: G. Coumans









Floor slab optimization
Reducing the environmental impact of concrete construction through fabrication-aware, structurally optimized floor slabs









#### Research methodology



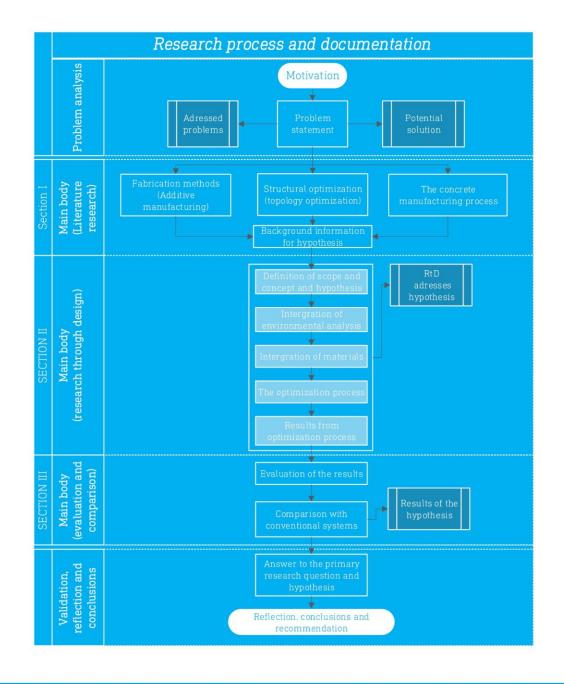








11



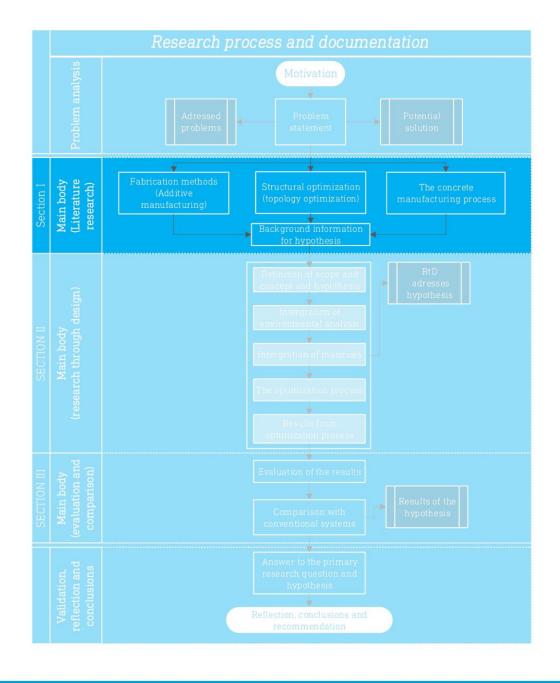








#### Fabrication methods



SECTION III EVALUATION

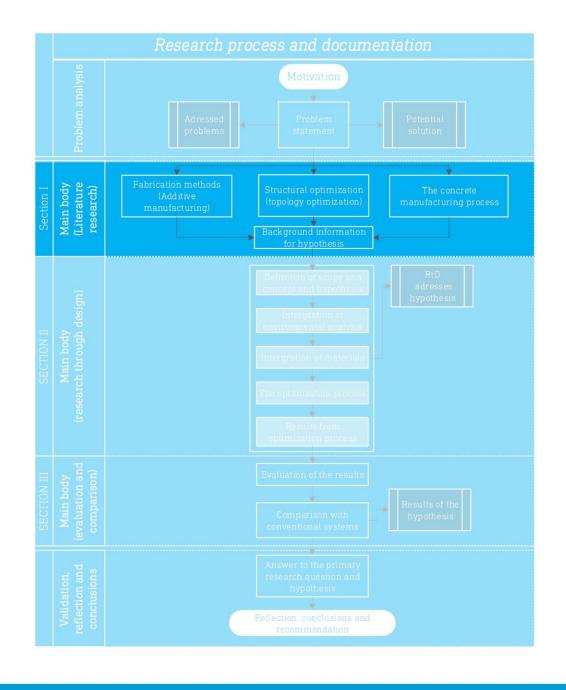






#### Fabrication methods

Structural optimization



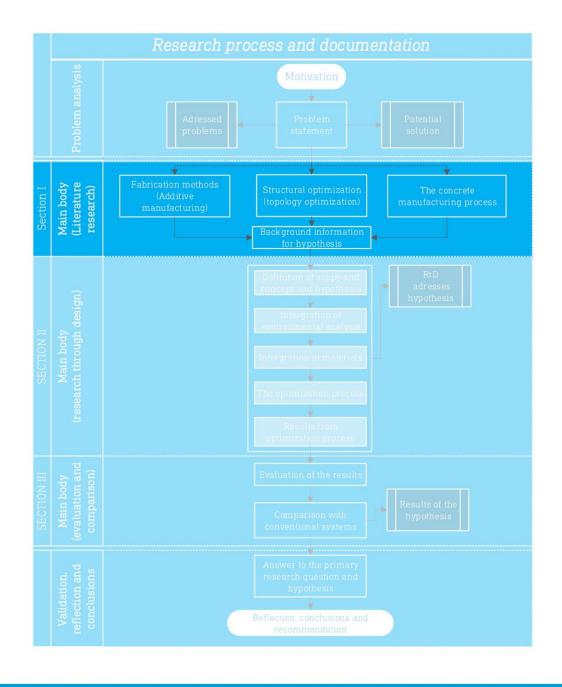




Fabrication methods

Structural optimization

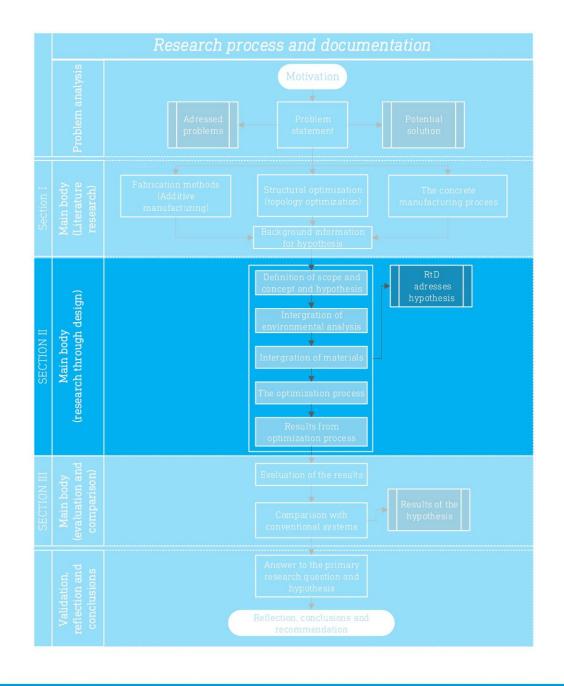
Concrete manufacturing







### Hypothesis driven design





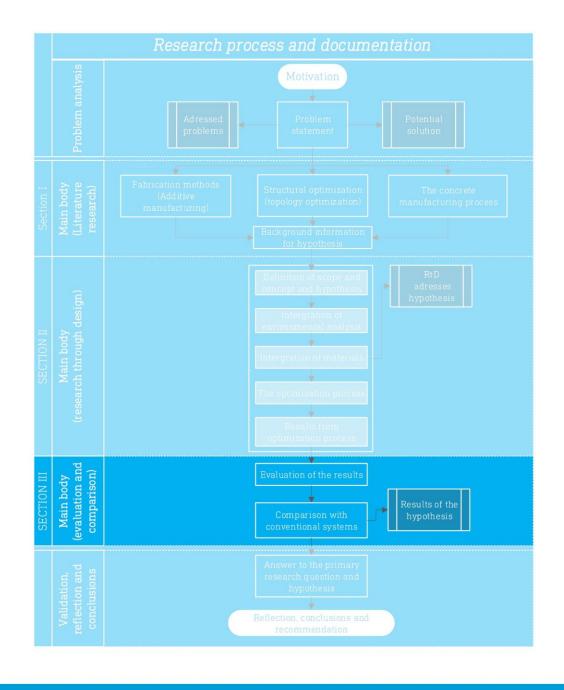






### Hypothesis driven design

Evaluated with a Life Cycle Assessment









### THE BODY OF THE RESEARCH

"Although reinforced concrete has been used for over a hundred years and with increasing interest during the last decades, few of its properties and potentialities have been fully exploited so far. Apart from the unconquerable inertia of our own minds, which do not seem to be able to adapt freely any new ideas, the main cause of this delay is a trivial technicality: The need to prepare wooden frames." – Nervi, 1956

"Although reinforced concrete has been used for over a hundred years and with increasing interest during the last decades, few of its properties and potentialities have been fully exploited so far. Apart from the unconquerable inertia of our own minds, which do not seem to be able to adapt freely any new ideas, the main cause of this delay is a trivial technicality: The need to prepare wooden frames." – Nervi, 1956

### Main research question

In what manner can we use additive manufacturing and structural optimization in the building sector to address the environmental impact of concrete construction?

### Why structural optimization and AM

Structural optimization provides a powerful method for generating the optimized models, while AM enables a cost-effective fabrication of geometrically complex shapes (J. Wu, Aage, N., Lefebvre, S., & Wang, C., 2017).

### SECTION I RESEARCH AS A BASIS FOR DESIGN

Fabrication methods (AM)

Structural optimization (S0)

Concrete manufacturing (CM)

#### Focus on the hypothesis

Reducing the environmental impact of concrete construction through fabrication-aware, structurally optimized floor slabs

SECTION III EVALUATION









### Fabrication methods (AM)

#### Process, material requirements Sustainability of the material









# Fabrication methods (AM) Sustainability of the material

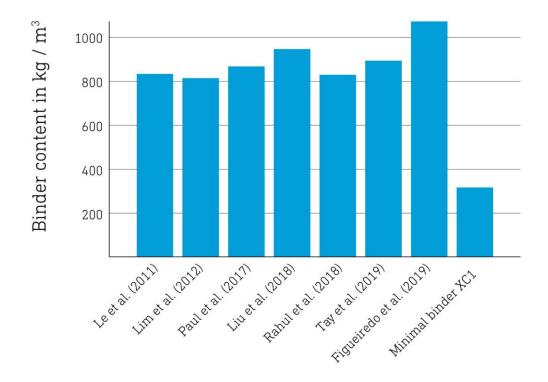
# 85% of the emissions is related to the binder in prefabricated concrete





# Fabrication methods (AM) Sustainability of the material

Process-related material requirements: 3DCP





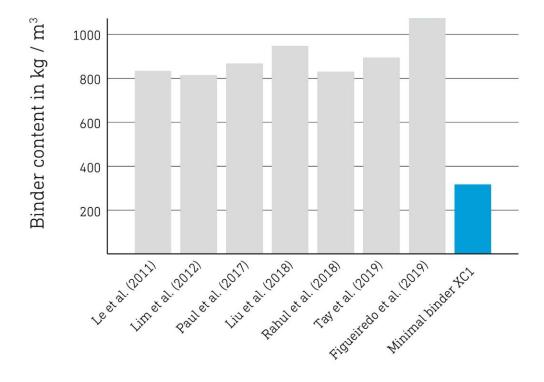


section II design



# Fabrication methods (AM) Sustainability of the material

Process-related material requirements: 3DCP



SECTION III EVALUATION







### Fabrication methods (AM) Robustness and brittle behaviour

# Difficulty of reinforcement Robustness and brittle behaviour









### Fabrication methods (AM) Robustness and brittle behaviour

# Difficulty of reinforcement Robustness and brittle behaviour







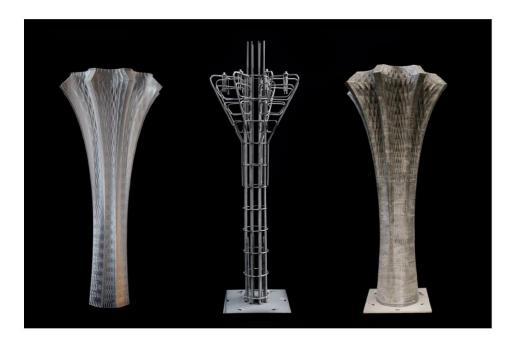




Source: (Menna et al., 2020)

### Fabrication methods (AM) Robustness and brittle behaviour

# Difficulty of reinforcement Robustness and brittle behaviour











Source: (Menna et al., 2020)

# Fabrication methods (AM) Conventional casting

Process, material requirements
Sustainability of the material

Difficulty of reinforcement
Robustness and brittle behaviour









Additive manufacturing is unlikely to adress the environmental impact of concrete construction









Process-related material requirements











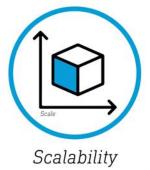
material requirements





material requirements











material requirements











### Structural optimization (S0)

Methods of structural optimization

Form finding of compression only structures

Black-box approach to concurrent optimization processes





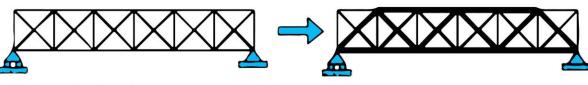












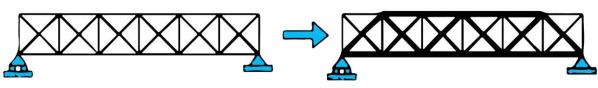
Size optimization

section II design

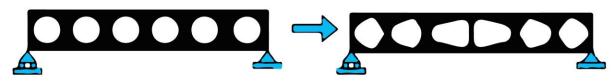








Size optimization



Shape optimization

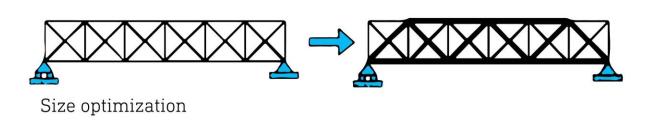


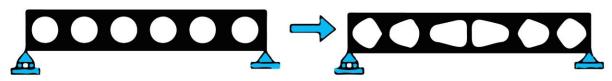




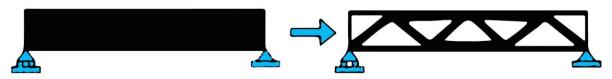


Source: (Gebisa & Lemu, 2017)





Shape optimization



Topology optimization









Material properties
Concrete is strong in compression

floorslab properties
Distributed Q-load



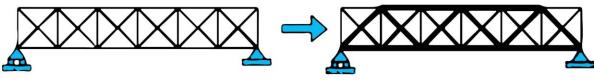


SECTION II DESIGN

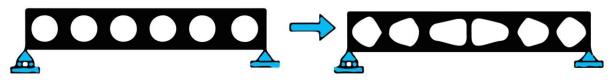
SECTION III EVALUATION



# Structural optimization for a compression dominant floor slab



Size optimization



Shape optimization

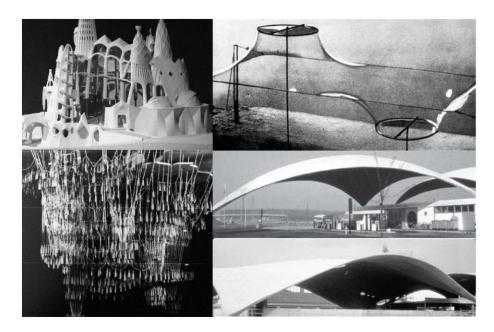
SECTION II DESIGN







# Form finding of structures for a compression dominant floor slab





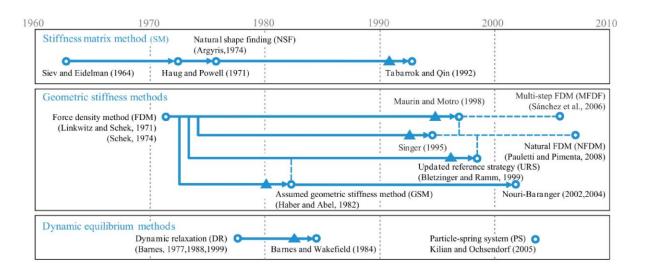






### Form finding of structures

With computational tools











### The variable shell thickness

The optimal floorslab has a variable height









### The variable shell thickness

The optimal floorslab has a variable height

Multiple loadcases are guiding not able to have a concurrent optimization process

SECTION III EVALUATION







### The variable shell thickness

The optimal floorslab has a variable height

Multiple loadcases are guiding not able to have a concurrent optimization process

SECTION III EVALUATION

Fabrication constraints

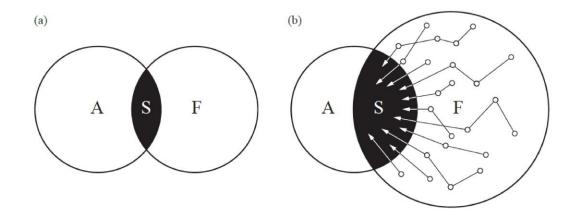
Cannot be intergrated directly in funicular methods







# Form-finding as a tool for shape optimization



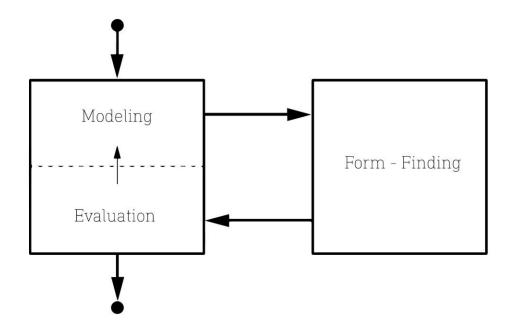








### Form-finding as a tool for shape optimization



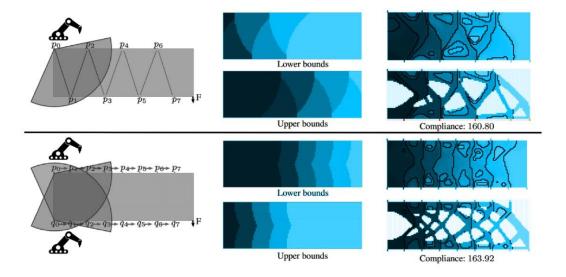




section II design



## Concurrent optimization process With computational tools











Concurrent optimization process
With computational tools

Why is there little research?

in concurrent optimization methods





SECTION II DESIGN



Concurrent optimization process
With computational tools

Why is there little research?

in concurrent optimization methods

No clear objective function
In multi-objective, fabrication-aware problems

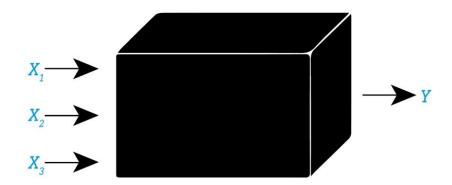




SECTION II DESIGN



# Concurrent optimization process Using derivative free optimization



SECTION III EVALUATION

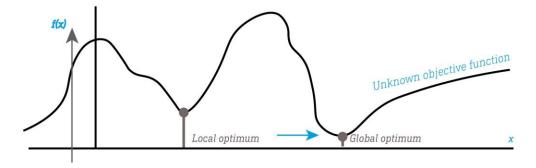
54







## Derivative free optimization to find the global optimum



SECTION III EVALUATION







Derivative free optimization to find the global optimum

Metaheuristic methods

Direct-search methods

Model-based methods

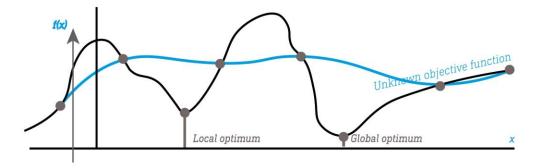
SECTION III EVALUATION







## Model-based optimization to find the global optimum



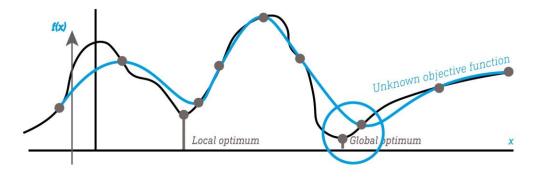




SECTION II DESIGN



# Concurrent optimization process Using derivative free optimization













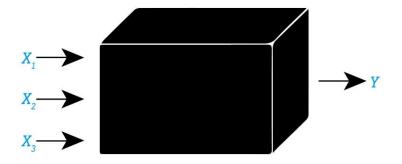




60

# Floor slab optimization Structural optimization (SO)

# Derivative-free optimization process using surrogate-model based optimization solvers



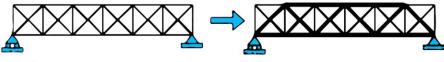




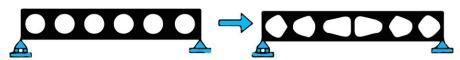


### Shape and size optimization

To find the structural form



Size optimization



Shape optimization

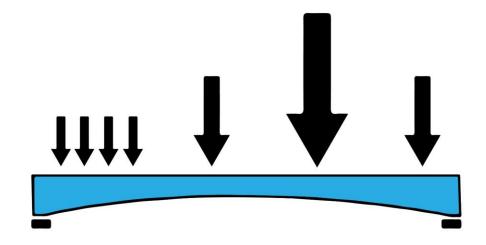








## Intergration of multiple loadcases in the optimization process







SECTION II DESIGN



### Fabrication constraints taken into account











Derivative-free optimization process using surrogate-model based optimization solvers

Shape and size optimization
To find the structural form

Intergration of multiple loadcases in the optimization process

Fabrication constraints







Structural optimization will likely be highly effective, in adressing the environmental impact of floor slabs







### Concrete manufacturing (CM)

Where are the emissions?
In concrete construction

What can we do? to reduce the emissions









# Concrete manufacturing (CM) Environmental impact of concrete

### 85% of the emissions

is related to the binder in prefabricated concrete





SECTION II DESIGN

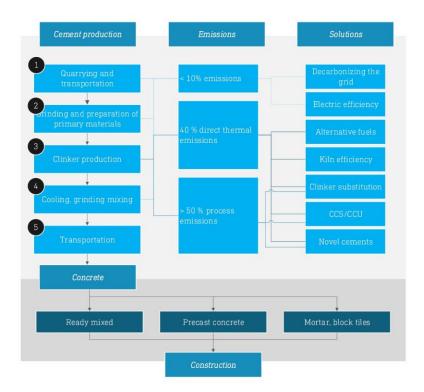


Source: (Kong, Kang, He, Li, & Wang, 2020)

# Concrete manufacturing (CM) Environmental impact of concrete

#### 85% of the emissions

is related to the binder in prefabricated concrete



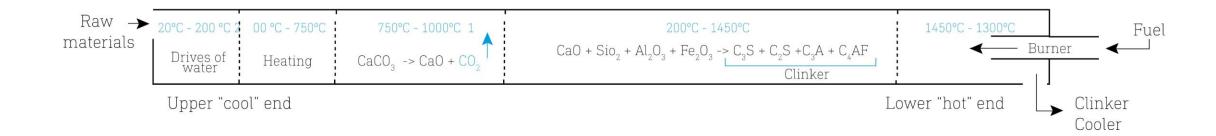








#### Concrete emissions: key findings

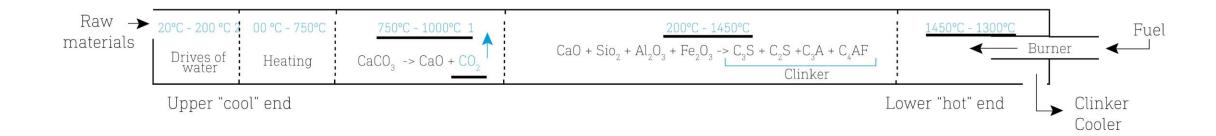








#### Concrete emissions: key findings



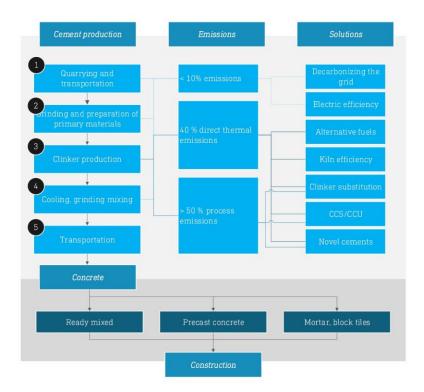




# Concrete manufacturing (CM) Environmental impact of concrete

#### 85% of the emissions

is related to the binder in prefabricated concrete









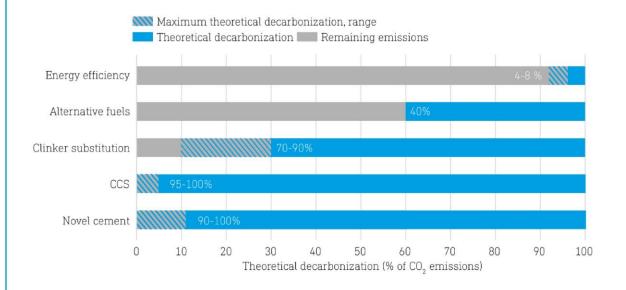


Source: (J. Lehne & F. Preston, 2018)

## Concrete manufacturing (CM) Reducing the environmental impact

### Reducing of the impact

What is the effectivity of the measures?







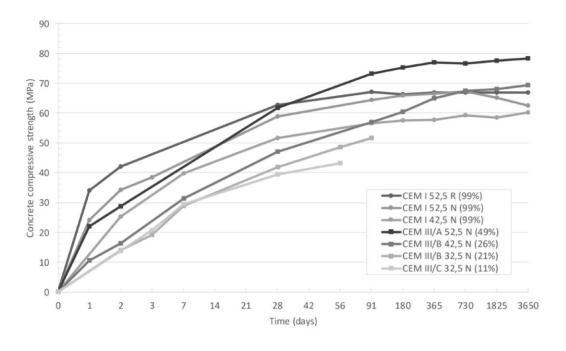




# Concrete manufacturing (CM) Reducing the environmental impact of the floorslab

### Use of clinker substitutes (SCMs)

in Portland clinker-based cement







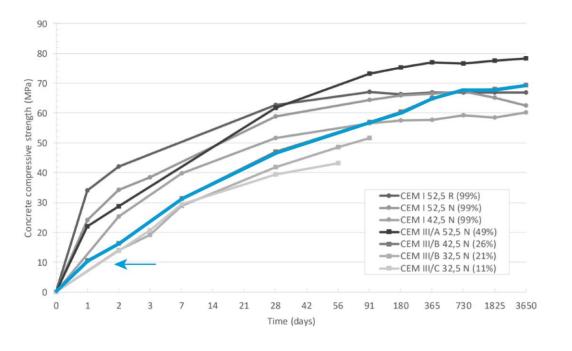




# Concrete manufacturing (CM) Reducing the environmental impact of the floorslab

### Use of clinker substitutes (SCMs)

in Portland clinker-based cement











## Concrete manufacturing (CM) Reducing the environmental impact of the floorslab

Use of clinker substitutes (SCMs) in Portland clinker-based cement

More efficient use of clinker by optimizing for lower strength concrete









# SECTION II HYPOTHESIS DRIVEN DESIGN

### Hypothesis

Fabrication-aware, structurally optimized floor slabs can significantly reduce the environmental impact of concrete construction.









### This adresses a current gap in literature

In a derivative-free optimization approach for concurrent structural design problems (e.g. taking into account fabrication constraints, and multiple loadcases)









#### Research through design

### Floor slab optimization

Reducing the environmental impact of concrete construction through fabrication-aware, structurally optimized floor slabs

## 1. Introduction of the flooring system Thin-shells, shell theory, and critical aspect

- 2. Boundary conditions loadcase, material intergration and assumptions
- 3. The optimization algorithm Insight on the optimization process
- 4. Resulting floorslabs
  The basis for the LCA analysis









Strength through geometry

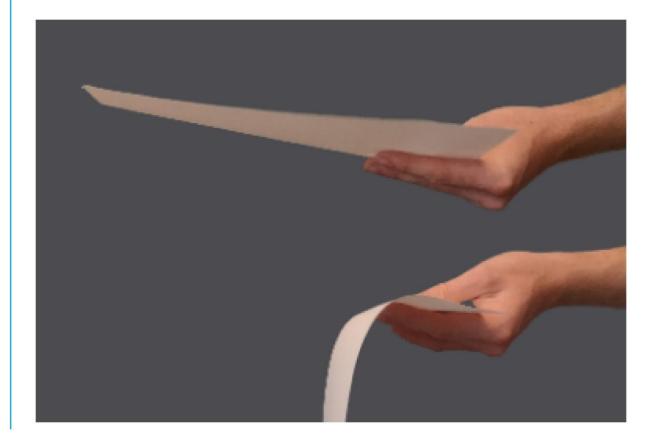






The concept

1. INTRODUCTION OF THE FLOORING SYSTEM Strength through geometry



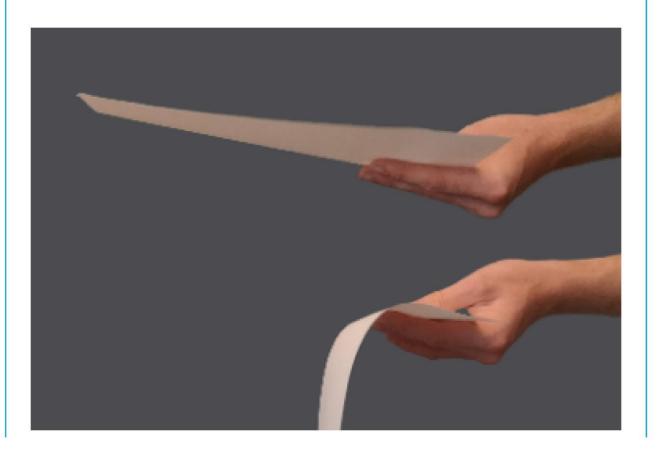


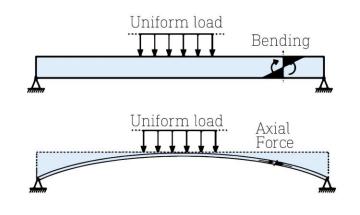


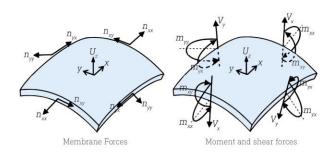




#### Strength through geometry





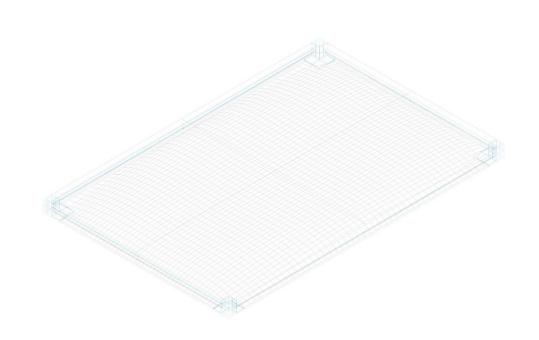


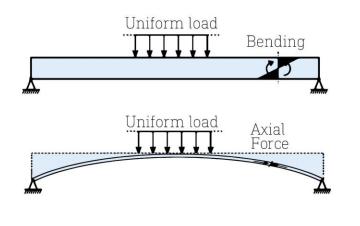


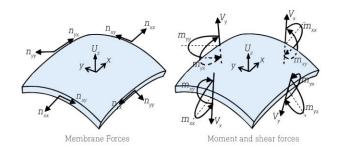












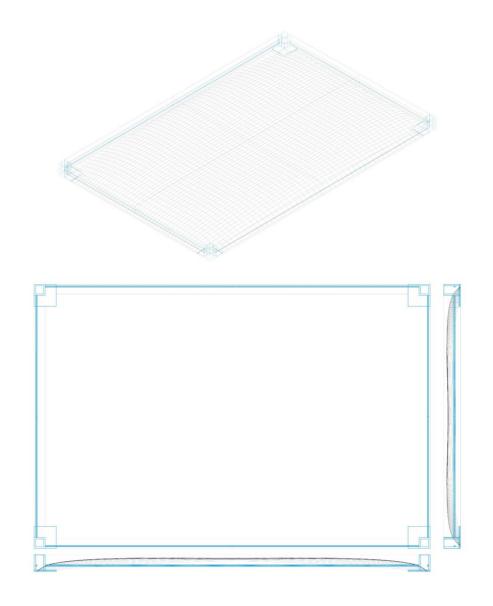


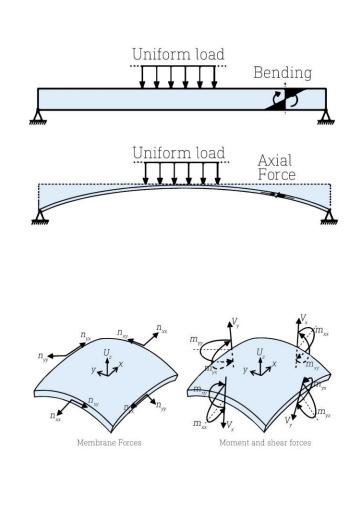




The concept

1. INTRODUCTION OF THE FLOORING SYSTEM



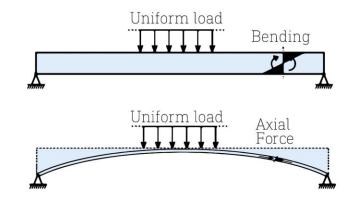


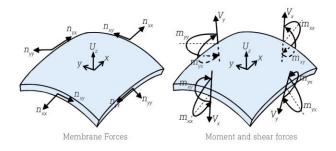






# Casting as the fabrication method Due to material related emissions





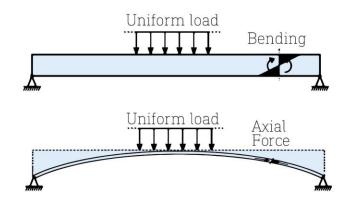


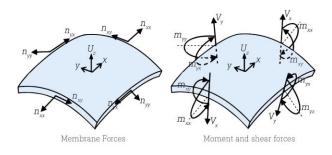




## Casting as the fabrication method Due to material related emissions

Simplicity over complexity in the fabrication process









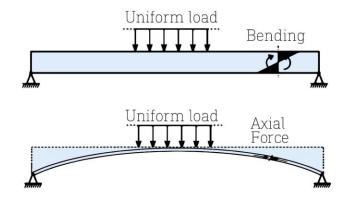


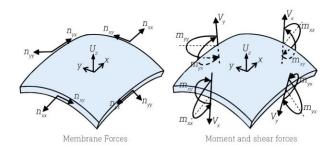


### Casting as the fabrication method Due to material related emissions

Simplicity over complexity in the fabrication process

Prefabrication and modularization
Reusability of the formwork, and further optimization











Casting as the fabrication method

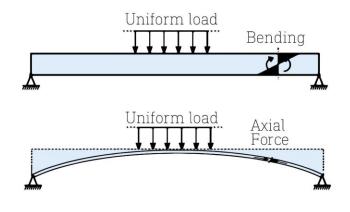
Due to material related emissions

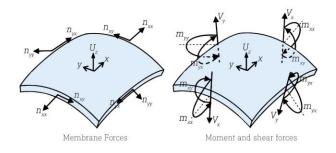
Simplicity over complexity in the fabrication process

Prefabrication and modularization
Reusability of the formwork, and further optimization

Conform the building regulation

To allow for a more direct application











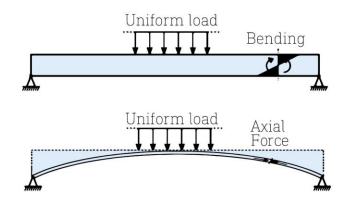
Casting as the fabrication method Due to material related emissions

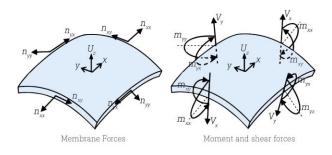
Simplicity over complexity in the fabrication process

Prefabrication and modularization Reusability of the formwork, and further optimization

Conform the building regulation To allow for a more direct application

Focus on the LCA in the hypothetical office building













The concept

1. INTRODUCTION OF THE FLOORING SYSTEM

### Punching shear Four support points

Fire safety Of the exposed steel

What will it look like? the flooring system

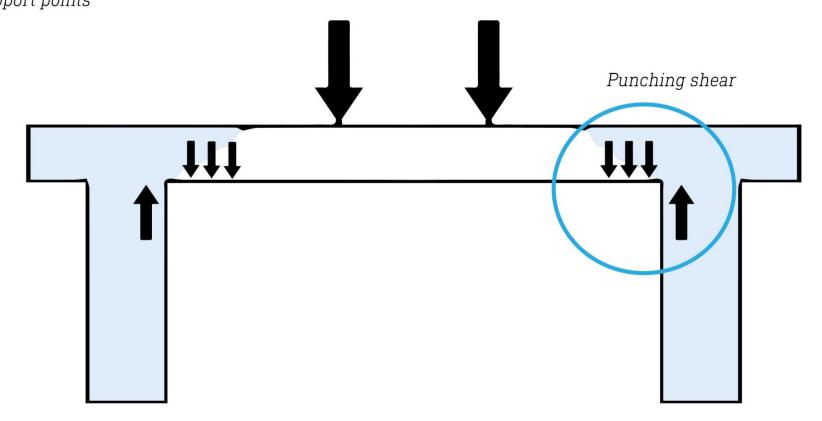








# Punching shear Four support points





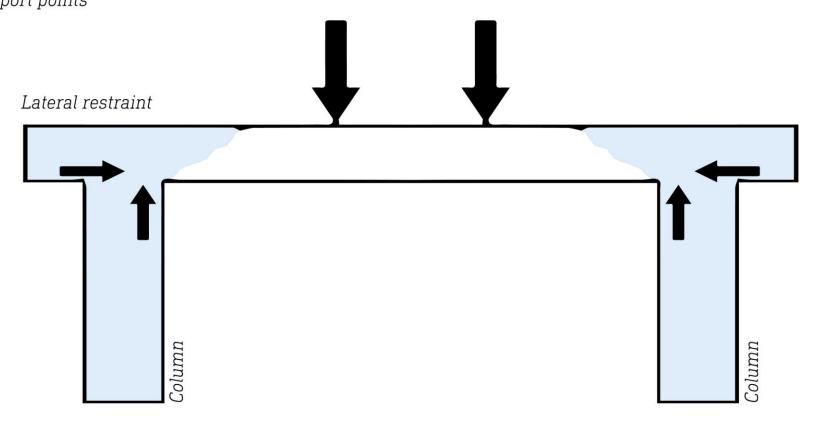






Source: (Wijte, 2019)

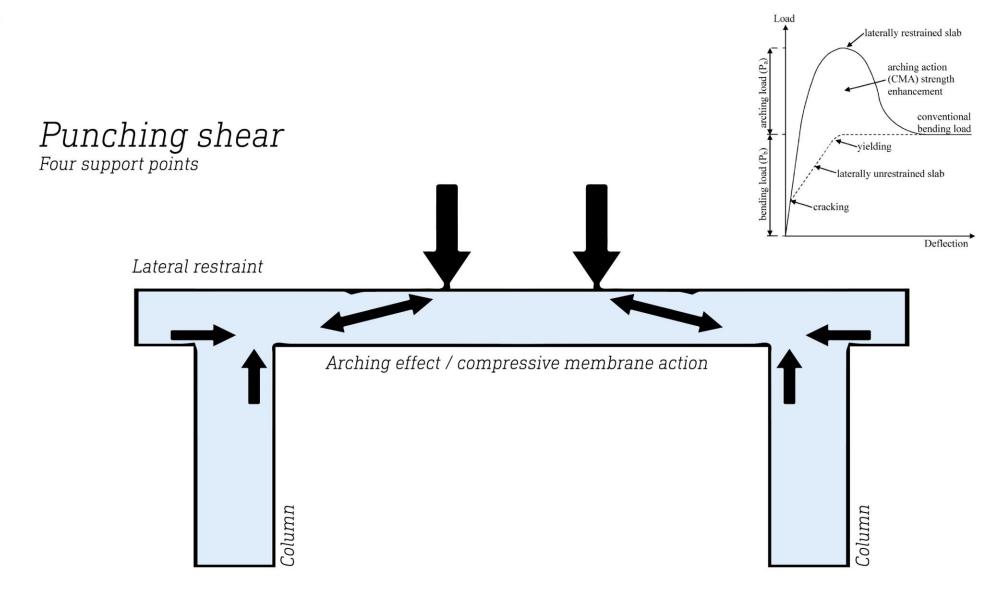
# Punching shear Four support points







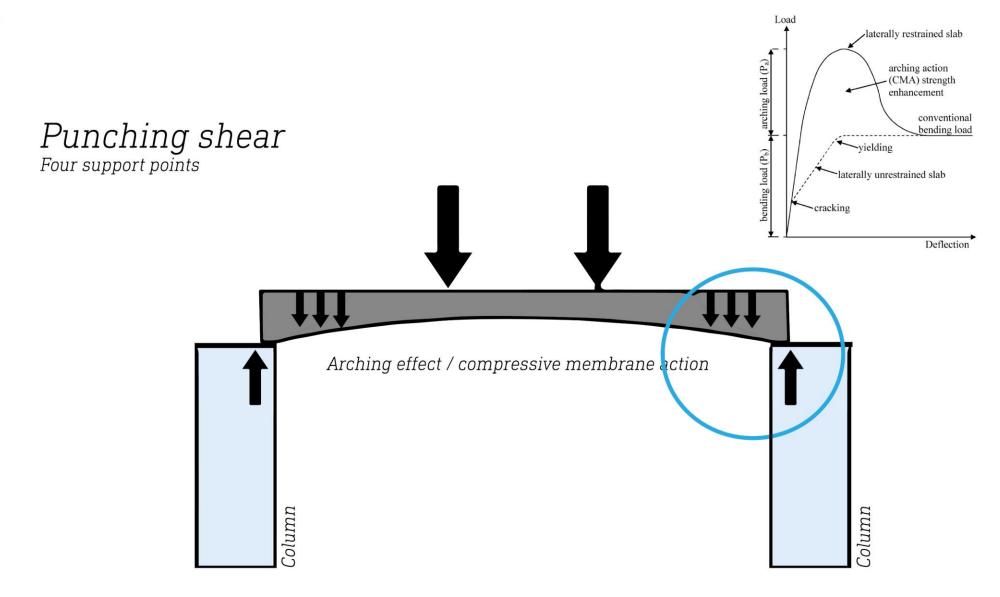








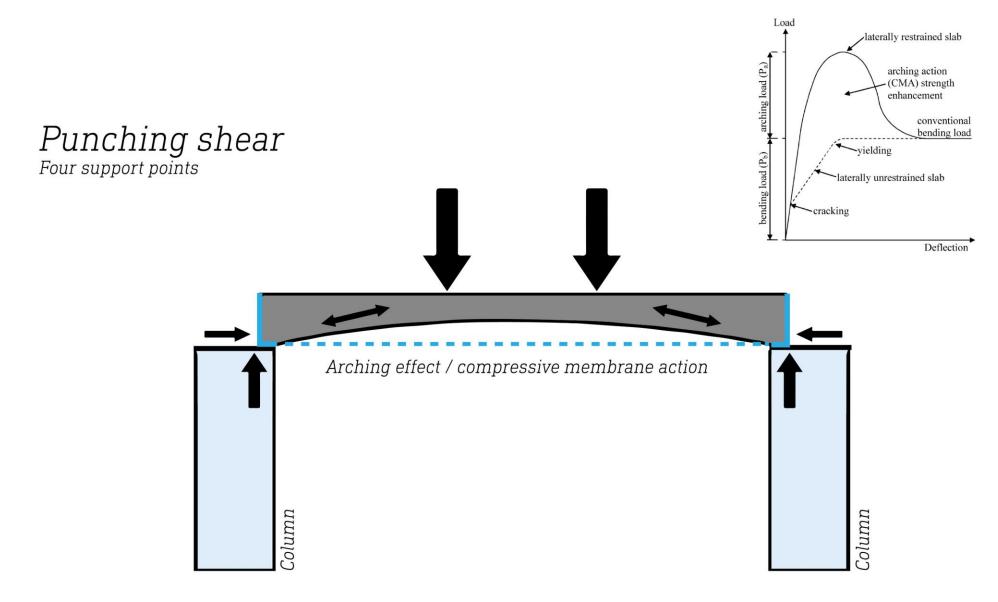








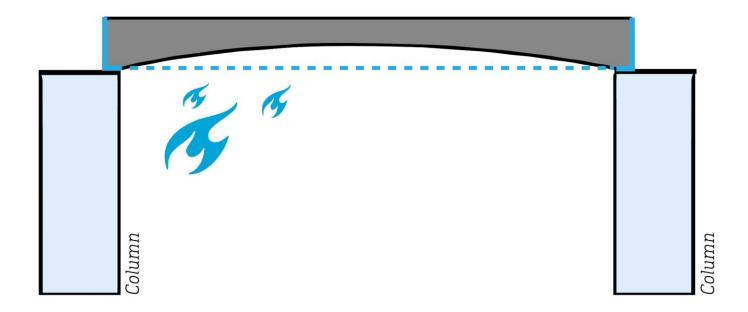








Fire safety
Of the exposed steel







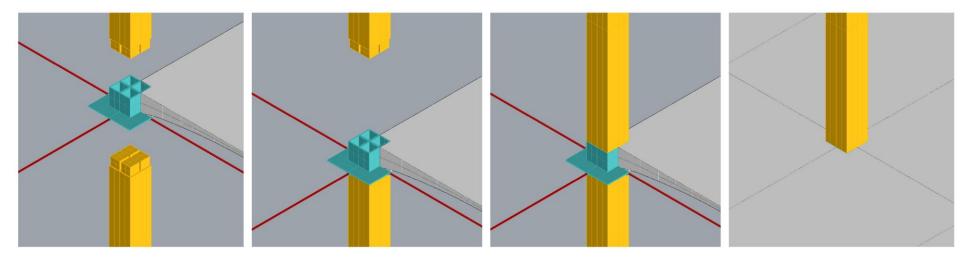




Source: (Rankin, et al. (1997)

# Fire safety Of the exposed steel

No exposed steel on the top side





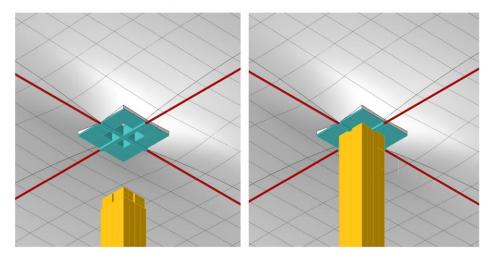






# Fire safety Of the exposed steel

#### Intumescent coating





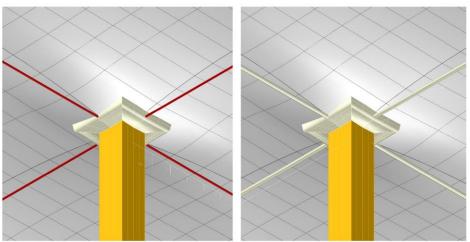




# Fire safety Of the exposed steel

Intumescent coating

#### Covering it with an insulating material











### What will it look like?

the flooring system

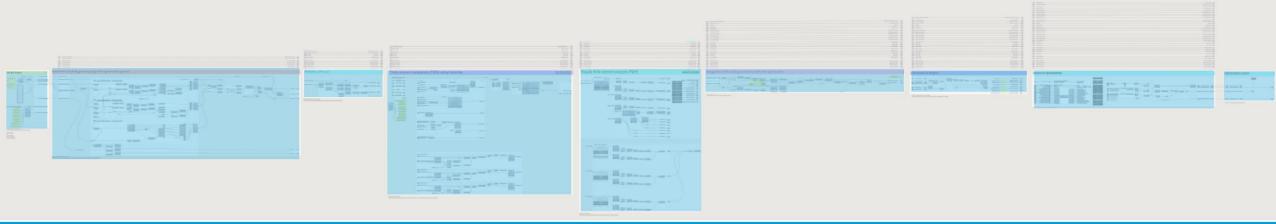






### Floor slab optimization

In a derivative-free optimization approach for concurrent structural design problems (e.g. taking into account fabrication constraints, and multiple loadcases)



SECTION II DESIGN

2. BOUNDARY **CONDITIONS** 

# Focus on office buildings as they are easier for transformation











#### The boundary conditions

1. INTRODUCTION OF THE FLOORING **SYSTEM** 

2. BOUNDARY **CONDITIONS** 

### Focus on office buildings as they are easier for transformation

Eurocode, loading conditions

- Total load of 5.37  $kN/m^2$  + self weight



- Offices CC2 2.5 kN/m<sup>2</sup>
- Additional loading CC2 1.2 kN/m<sup>2</sup>
- Safety factor permanent load 1.5
- Safety factor variable load 1.35
- Total load of  $5.37 \text{ kN/m}^2$  + self weight







#### The boundary conditions

1. INTRODUCTION OF THE FLOORING **SYSTEM** 

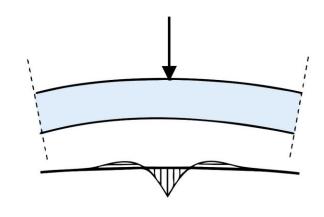
2. BOUNDARY **CONDITIONS** 

### Focus on office buildings as they are easier for transformation

Eurocode, loading conditions - Total load of 5.37  $kN/m^2$  + self weight

Intergration of critical point loads As they are guiding in thin shells





Incidental point load, might result in tension









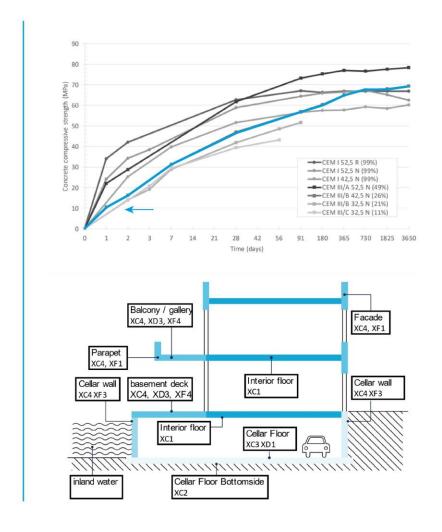
2. BOUNDARY CONDITIONS

## Focus on office buildings as they are easier for transformation

Eurocode, loading conditions
- Total load of 5.37 kN/m² + self weight

Intergration of critical point loads
As they are guiding in thin shells

Intergration of material in the optimization process









#### The boundary conditions

1. INTRODUCTION OF THE FLOORING SYSTEM

2. BOUNDARY **CONDITIONS** 

#### Focus on office buildings as they are easier for transformation

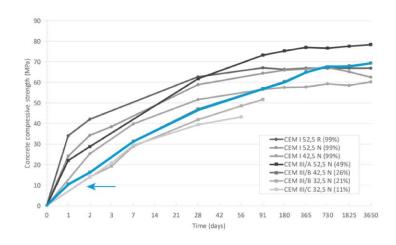
Eurocode, loading conditions

- Total load of 5.37 kN/m<sup>2</sup> + self weight

Intergration of critical point loads As they are guiding in thin shells

Intergration of material

in the optimization process



Strength class = C20/25

Exposure class = XC 1

Consistency class = C2, S2, F2

Maximal w/c factor = 0.65

Design w/c factor = 0.63

Minimal cement  $= 260 \, \text{kg/m}$ 

Cement types used = CEM III/B 42.5 N

Aggregate size = 4/16







2. BOUNDARY **CONDITIONS** 

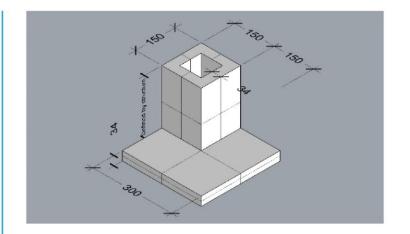
#### Focus on office buildings as they are easier for transformation

Eurocode, loading conditions - Total load of  $5.37 \text{ kN/m}^2$  + self weight

Intergration of critical point loads As they are guiding in thin shells

Intergration of material in the optimization process

Assumptions in the process uncracked concrete, linear finite element analysis, steel shoe to prevent localized edge effects











#### The boundary conditions

1. INTRODUCTION OF THE FLOORING SYSTEM

2. BOUNDARY CONDITIONS

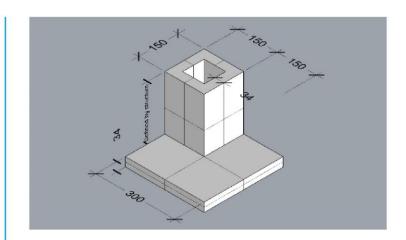
## Focus on office buildings as they are easier for transformation

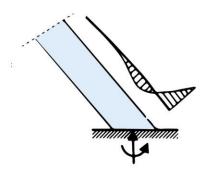
Eurocode, loading conditions
- Total load of 5.37 kN/m² + self weight

Intergration of critical point loads
As they are guiding in thin shells

Intergration of material in the optimization process

Assumptions in the process uncracked concrete, linear finite element analysis, steel shoe to prevent localized edge effects





SECTION III EVALUATION

Distributing the load by enclosing the concrete



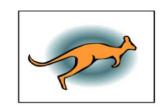




### Script in Rhino Grasshopper









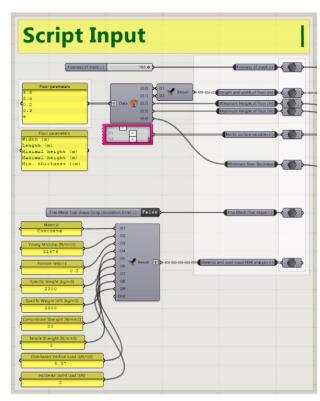


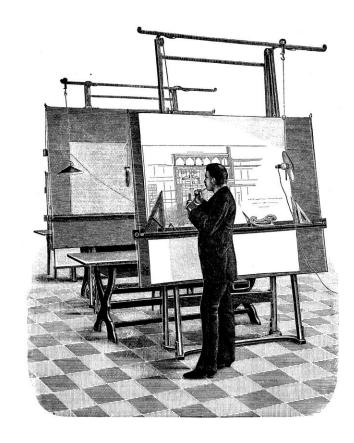




- 1. INTRODUCTION OF THE FLOORING **SYSTEM**
- 2. BOUNDARY **CONDITIONS**
- 3. OPTIMIZATION **SCRIPT**

# STEP 1 Definition of the input length, width, mesh size, height and material properties









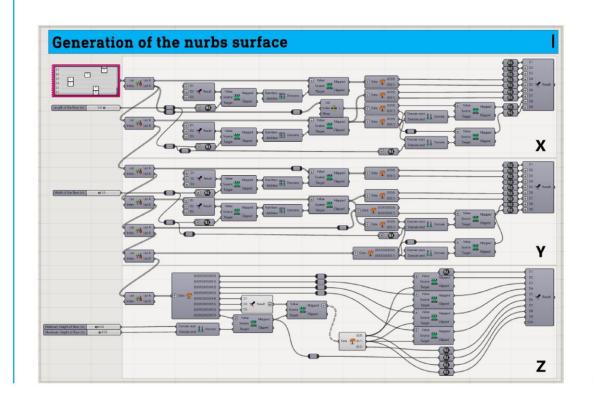


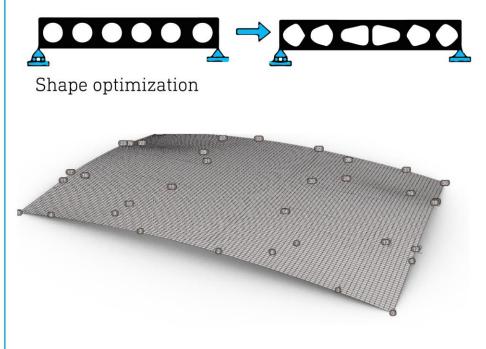


2. BOUNDARY **CONDITIONS** 

3. OPTIMIZATION **SCRIPT** 

# STEP 2 Shape optimization length, width, mesh size, height and material properties









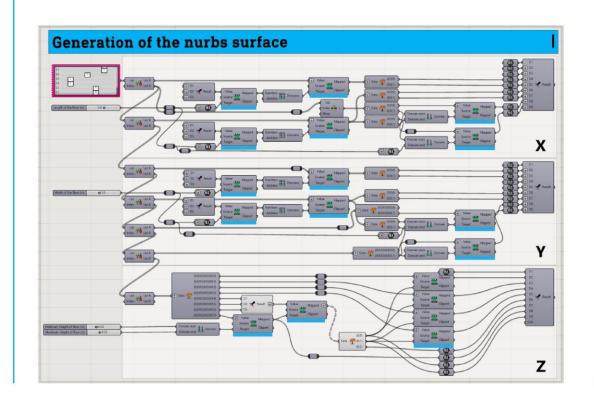


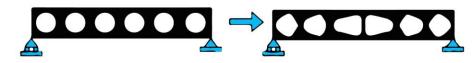




- 1. INTRODUCTION OF THE FLOORING **SYSTEM**
- 2. BOUNDARY **CONDITIONS**
- 3. OPTIMIZATION **SCRIPT**

# STEP 2 Shape optimization length, width, mesh size, height and material properties





Shape optimization



- Remapping of the variables, to influence the solution-space and thereby allow for faster convergence





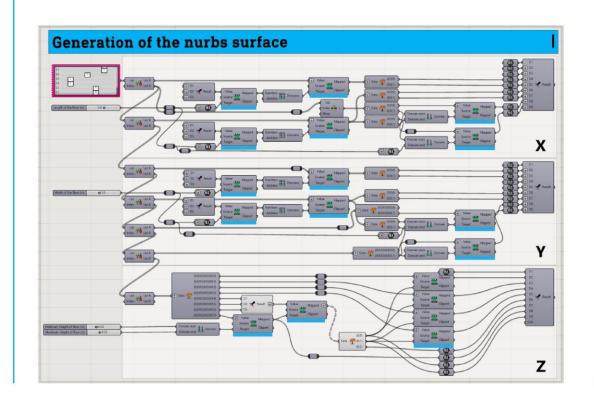


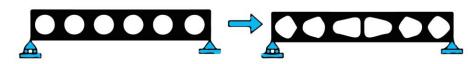


- 1. INTRODUCTION
  OF THE FLOORING
  SYSTEM
- 2. BOUNDARY CONDITIONS
- 3. OPTIMIZATION SCRIPT

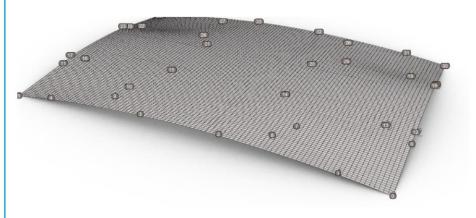
## STEP 2 Shape optimization

length, width, mesh size, height and material properties





Shape optimization



- Remapping of the variables, to influence the solution-space and thereby allow for faster convergence
- Quad-Mesh is automatically generated, and forms the input for step three







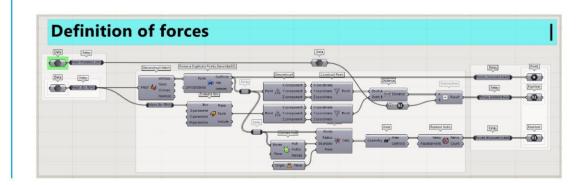


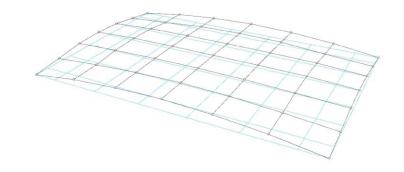
- 1. INTRODUCTION OF THE FLOORING **SYSTEM**
- 2. BOUNDARY **CONDITIONS**
- 3. OPTIMIZATION **SCRIPT**

## STEP 3 Intergration of self weight

Intergration of the weight added by the casting constraints

- Generation of the projected voronoi
- area of voronoi \* height difference \* SW of concrete in N
- Defines the added load on the structure











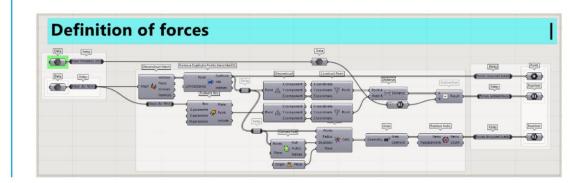


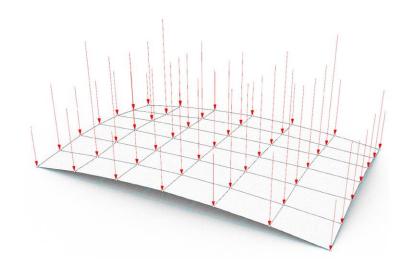
- 1. INTRODUCTION OF THE FLOORING SYSTEM
- 2. BOUNDARY CONDITIONS
- 3. OPTIMIZATION SCRIPT

## STEP 3 Intergration of self weight

Intergration of the weight added by the casting constraints

- Generation of the projected voronoi
- area of voronoi \* height difference \* SW of concrete in N
- Defines the added load on the structure









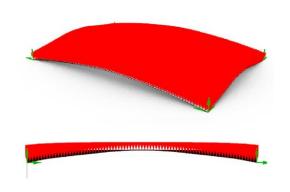


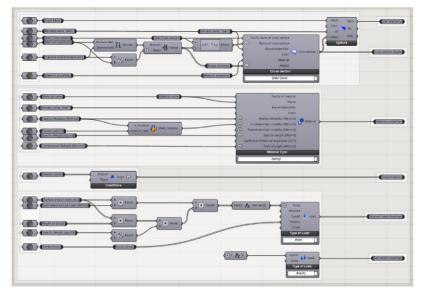
SECTION III EVALUATION

- 1. INTRODUCTION
  OF THE FLOORING
  SYSTEM
- 2. BOUNDARY CONDITIONS
- 3. OPTIMIZATION SCRIPT

## STEP 4 Finite element analysis Using karamba3D

- Generating the input in karamba3D, (e.g. support, load, variable shell thickness, material)
- Primary load-case (distributed Q-load)









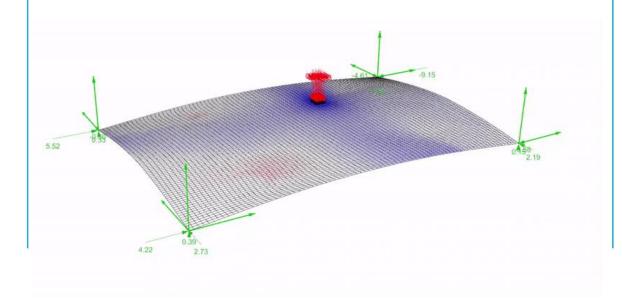


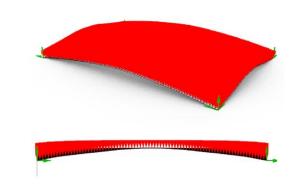
SECTION III EVALUATION

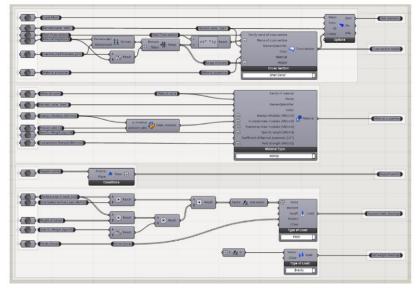
- 1. INTRODUCTION OF THE FLOORING **SYSTEM**
- 2. BOUNDARY **CONDITIONS**
- 3. OPTIMIZATION **SCRIPT**

### STEP 4 Finite element analysis Using karamba3D

- Generating the input in karamba3D, (e.g. support, load, variable shell thickness, material)
- Primary load-case (distributed Q-load)











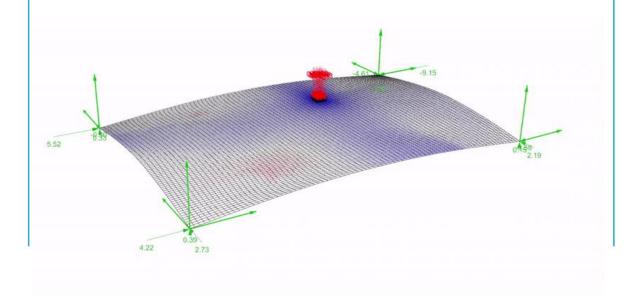


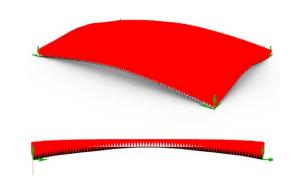
SECTION II DESIGN

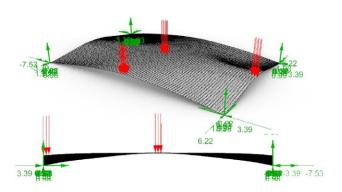
- 1. INTRODUCTION OF THE FLOORING **SYSTEM**
- 2. BOUNDARY **CONDITIONS**
- 3. OPTIMIZATION **SCRIPT**

### STEP 4 Finite element analysis Using karamba3D

- Generating the input in karamba3D, (e.g. support, load, variable shell thickness, material)
- Primary load-case (distributed Q-load)











SECTION II DESIGN



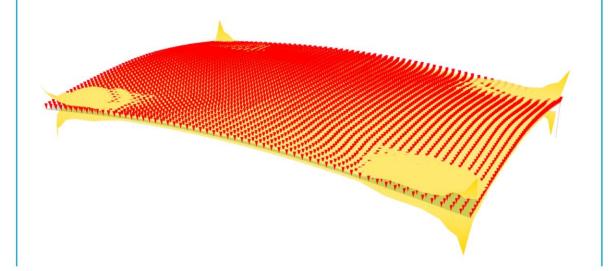
1. INTRODUCTION OF THE FLOORING **SYSTEM** 

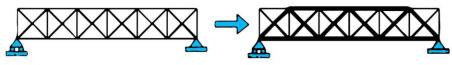
2. BOUNDARY CONDITIONS

3. OPTIMIZATION **SCRIPT** 

# STEP 5 Size optimization Based on the finite element results of the Q-load

- five optimization steps, to optimize the compression stress





Size optimization









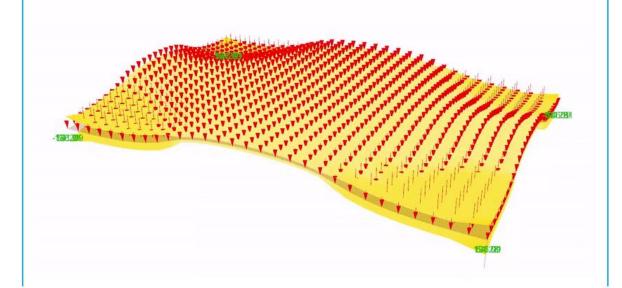
1. INTRODUCTION OF THE FLOORING **SYSTEM** 

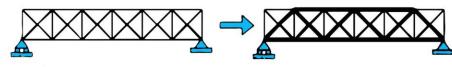
2. BOUNDARY **CONDITIONS** 

3. OPTIMIZATION **SCRIPT** 

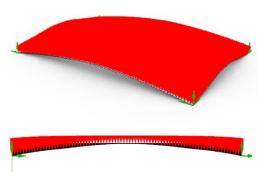
# STEP 5 Size optimization Based on the finite element results of the Q-load

- five optimization steps, to optimize the compression stress





Size optimization



The Q-load defines the variable thickness











1. INTRODUCTION OF THE FLOORING SYSTEM

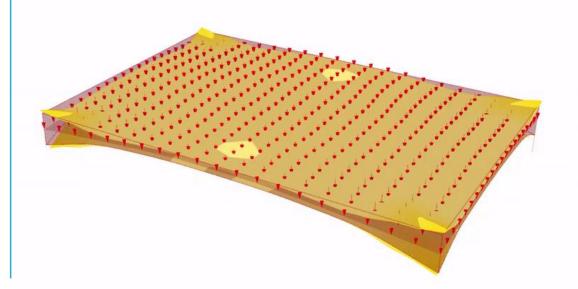
2. BOUNDARY CONDITIONS

3. OPTIMIZATION SCRIPT

### STEP 6 Fabrication-aware

rationalisation of the shell

- The variable mesh is converted to a nurbs surface, forming the basis of the final geometry.











1. INTRODUCTION OF THE FLOORING **SYSTEM** 

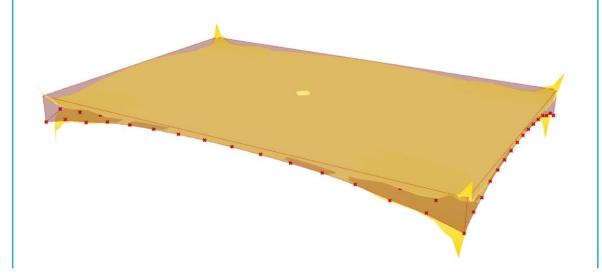
2. BOUNDARY CONDITIONS

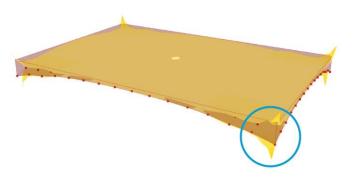
3. OPTIMIZATION **SCRIPT** 

### STEP 6 Fabrication-aware

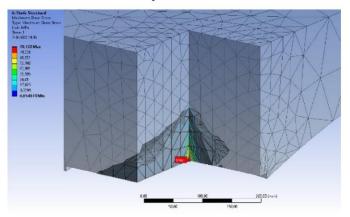
rationalisation of the shell

- The stress singularities are due to the linear model, Steel shoes will be used for the localized edge effects.





#### Solid FEM in Ansys





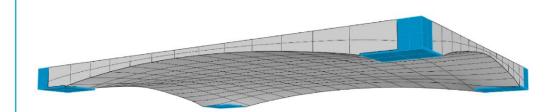




- 1. INTRODUCTION OF THE FLOORING **SYSTEM**
- 2. BOUNDARY **CONDITIONS**
- 3. OPTIMIZATION **SCRIPT**

### STEP 7 Generation of the results unity checks

- Performing the unity checks on the tensile, compression and deflection limits.









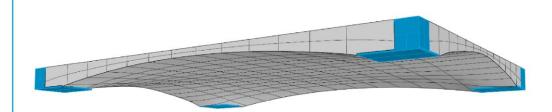


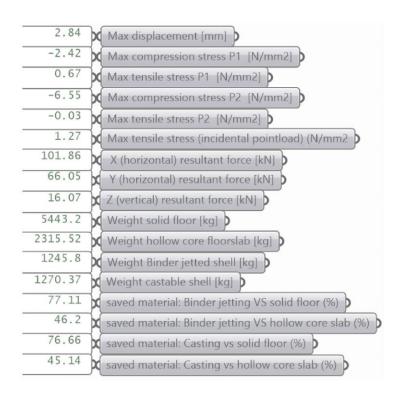
SECTION III EVALUATION

- 1. INTRODUCTION
  OF THE FLOORING
  SYSTEM
- 2. BOUNDARY CONDITIONS
- 3. OPTIMIZATION SCRIPT

## STEP 7 Generation of the results

- Performing the unity checks on the tensile, compression and deflection limits.
- Combining the results in the objective value









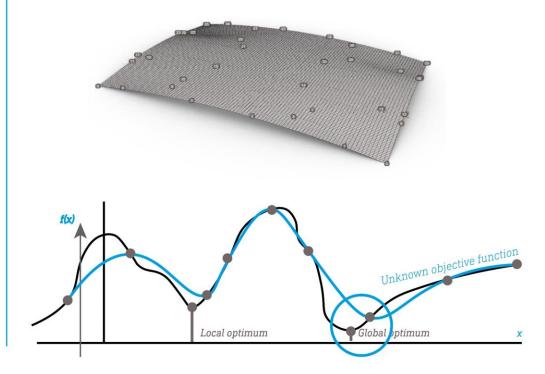


SECTION III EVALUATION

2. BOUNDARY **CONDITIONS** 

3. OPTIMIZATION **SCRIPT** 

### STEP 8 Model-based black-box optimization strategy







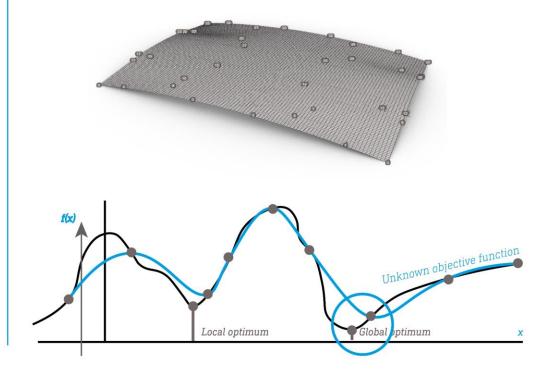
SECTION II DESIGN

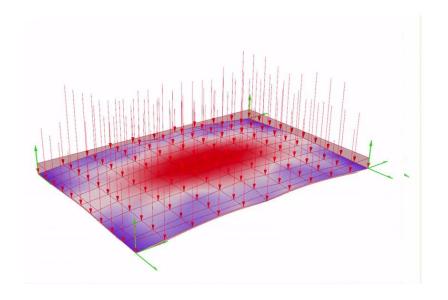


2. BOUNDARY **CONDITIONS** 

3. OPTIMIZATION **SCRIPT** 

### STEP 8 Model-based black-box optimization strategy











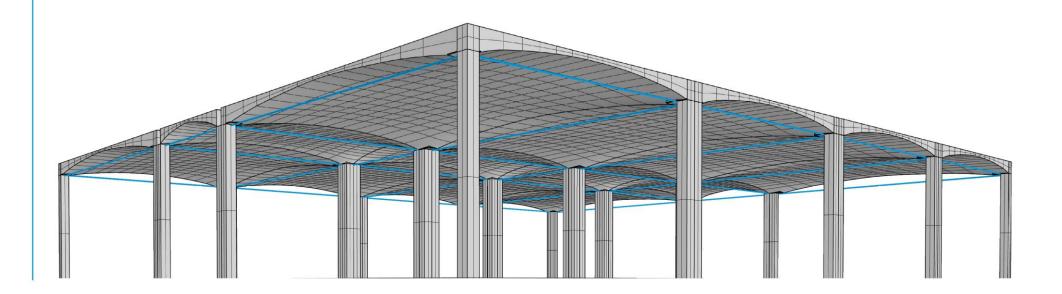
SECTION III EVALUATION

2. BOUNDARY **CONDITIONS** 

3. OPTIMIZATION **SCRIPT** 

4. RESULTING *FLOORSLABS* 

# The resulting floorslabs 3600 x 2400 mm and 3600 x 5400 mm



SECTION II DESIGN







The results

1. INTRODUCTION OF THE FLOORING **SYSTEM** 

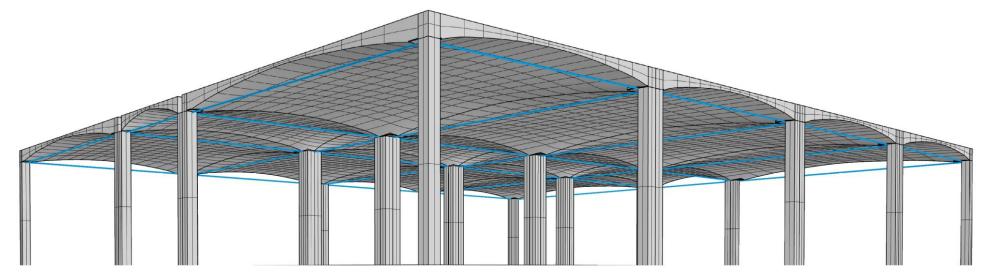
2. BOUNDARY **CONDITIONS** 

3. OPTIMIZATION **SCRIPT** 

4. RESULTING *FLOORSLABS* 

# The resulting floorslabs 3600 x 2400 mm and 3600 x 5400 mm





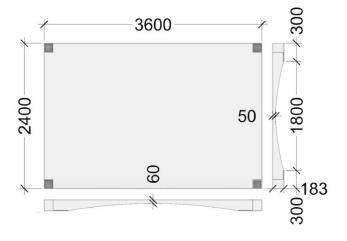








- 1. INTRODUCTION OF THE FLOORING **SYSTEM**
- 2. BOUNDARY **CONDITIONS**
- 3. OPTIMIZATION **SCRIPT**
- 4. RESULTING *FLOORSLABS*



Results	Description	Unity checks	Description	Description
Max compression stress P1 [N/mm2]	-2,91 N/mm2	Unity check	0.1455 [-]	Passed UC > 1
Max compression stress P2 [N/mm2]	-10,5 N/mm2	Unity check	0.525 [-]	Passed UC > 1
Max tensile stress P1 [N/mm2]	1.48 N/mm2	Unity check	0,99 [-]	Critical UC (Passed)
Max tensile stress P2 [N/mm2]	0.45 N/mm2	Unity check	0.3 [-]	Passed UC > 1
Max tensile stress LC 1 [N/mm2]	1,06 N/mm2	Unity check	0.71 [-]	Passed UC > 1
Max tensile stress LC 2 [N/mm2]	1,02 N/mm2	Unity check	0.68 [-]	Passed UC > 1
Max tensile stress LC 3 [N/mm2]	1,37 N/mm2	Unity check	0.91 [-]	Passed UC > 1
X (horizontal) resultant force [kN]	96,75 kN	Diameter steel wire	12 mm	DIN3064 6x36 warrington- seale+steelcore cable (eurocable)
Y (horizontal) resultant force [kN]	61,99 kN	Diameter steel wire	9 mm	DIN3064 6x36 warrington- seale+steelcore cable (eurocable)
Z (vertical) resultant force [kN]	60.96 kN	Vertical load Z [kN]	58,2 kN	
Weight castable shell [kg]	1182,91 kg	Volume	0,514 m <sup>3</sup>	
Reduction of weight vs hollowcore [%]	48,91%	Comparison floor	VBI 150mm	0,99 [-]
Reduction of weight vs solid floor [%]	70,24%	Comparison floor	200mm 2300kg concrete	

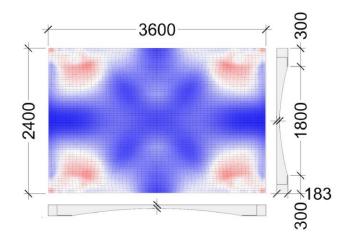








- 1. INTRODUCTION OF THE FLOORING **SYSTEM**
- 2. BOUNDARY **CONDITIONS**
- 3. OPTIMIZATION **SCRIPT**
- 4. RESULTING *FLOORSLABS*



3600 x 2400 mm

Results	Description	Unity checks	Description	Description
Max compression stress P1 [N/mm2]	-2,91 N/mm2	Unity check	0.1455 [-]	Passed UC > 1
Max compression stress P2 [N/mm2]	-10,5 N/mm2	Unity check	0.525 [-]	Passed UC > 1
Max tensile stress P1 [N/mm2]	1.48 N/mm2	Unity check	0,99 [-]	Critical UC (Passed)
Max tensile stress P2 [N/mm2]	0.45 N/mm2	Unity check	0.3 [-]	Passed UC > 1
Max tensile stress LC 1 [N/mm2]	1,06 N/mm2	Unity check	0.71 [-]	Passed UC > 1
Max tensile stress LC 2 [N/mm2]	1,02 N/mm2	Unity check	0.68 [-]	Passed UC > 1
Max tensile stress LC 3 [N/mm2]	1,37 N/mm2	Unity check	0.91 [-]	Passed UC > 1
X (horizontal) resultant force [kN]	96,75 kN	Diameter steel wire	12 mm	DIN3064 6x36 warrington- seale+steelcore cable (eurocable)
Y (horizontal) resultant force [kN]	61,99 kN	Diameter steel wire	9 mm	DIN3064 6x36 warrington- seale+steelcore cable (eurocable)
Z (vertical) resultant force [kN]	60.96 kN	Vertical load Z [kN]	58,2 kN	
Weight castable shell [kg]	1182,91 kg	Volume	0,514 m <sup>3</sup>	
Reduction of weight vs hollowcore [%]	48,91%	Comparison floor	VBI 150mm	0,99 [-]
Reduction of weight vs solid floor [%]	70,24%	Comparison floor	200mm 2300kg concrete	

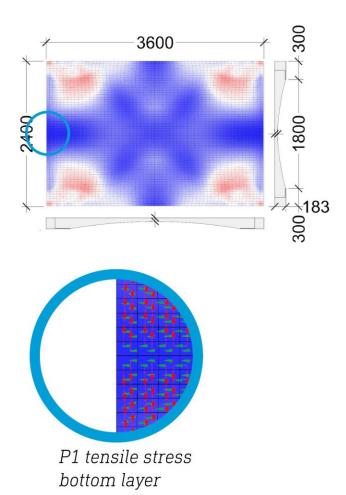








- 1. INTRODUCTION OF THE FLOORING **SYSTEM**
- 2. BOUNDARY **CONDITIONS**
- 3. OPTIMIZATION **SCRIPT**
- 4. RESULTING *FLOORSLABS*



### The resulting floorslabs 3600 x 2400 mm

Results	Description	Unity checks	Description	Description
Max compression stress P1 [N/mm2]	-2,91 N/mm2	Unity check	0.1455 [-]	Passed UC > 1
Max compression stress P2 [N/mm2]	-10,5 N/mm2	Unity check	0.525 [-]	Passed UC > 1
Max tensile stress P1 [N/mm2]	1.48 N/mm2	Unity check	0,99 [-]	Critical UC (Passed)
Max tensile stress P2 [N/mm2]	0.45 N/mm2	Unity check	0.3 [-]	Passed UC > 1
Max tensile stress LC 1 [N/mm2]	1,06 N/mm2	Unity check	0.71 [-]	Passed UC > 1
Max tensile stress LC 2 [N/mm2]	1,02 N/mm2	Unity check	0.68 [-]	Passed UC > 1
Max tensile stress LC 3 [N/mm2]	1,37 N/mm2	Unity check	0.91 [-]	Passed UC > 1
X (horizontal) resultant force [kN]	96,75 kN	Diameter steel wire	12 mm	DIN3064 6x36 warrington- seale+steelcore cable (eurocable)
Y (horizontal) resultant force [kN]	61,99 kN	Diameter steel wire	9 mm	DIN3064 6x36 warrington- seale+steelcore cable (eurocable)
Z (vertical) resultant force [kN]	60.96 kN	Vertical load Z [kN]	58,2 kN	
Weight castable shell [kg]	1182,91 kg	Volume	0,514 m <sup>3</sup>	
Reduction of weight vs hollowcore [%]	48,91%	Comparison floor	VBI 150mm	0,99 [-]
Reduction of weight vs solid floor [%]	70,24%	Comparison floor	200mm 2300kg concrete	

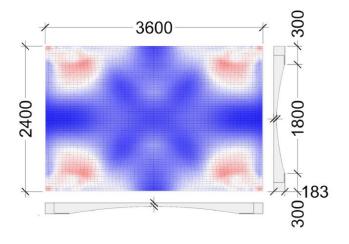








- 1. INTRODUCTION OF THE FLOORING **SYSTEM**
- 2. BOUNDARY **CONDITIONS**
- 3. OPTIMIZATION **SCRIPT**
- 4. RESULTING *FLOORSLABS*



### The resulting floorslabs 3600 x 2400 mm

Results	Description	Unity checks	Description	Description
Max compression stress P1 [N/mm2]	-2,91 N/mm2	Unity check	0.1455 [-]	Passed UC > 1
Max compression stress P2 [N/mm2]	-10,5 N/mm2	Unity check	0.525 [-]	Passed UC > 1
Max tensile stress P1 [N/mm2]	1.48 N/mm2	Unity check	0,99 [-]	Critical UC (Passed)
Max tensile stress P2 [N/mm2]	0.45 N/mm2	Unity check	0.3 [-]	Passed UC > 1
Max tensile stress LC 1 [N/mm2]	1,06 N/mm2	Unity check	0.71 [-]	Passed UC > 1
Max tensile stress LC 2 [N/mm2]	1,02 N/mm2	Unity check	0.68 [-]	Passed UC > 1
Max tensile stress LC 3 [N/mm2]	1,37 N/mm2	Unity check	0.91 [-]	Passed UC > 1
X (horizontal) resultant force [kN]	96,75 kN	Diameter steel wire	12 mm	DIN3064 6x36 warrington- seale+steelcore cable (eurocable)
Y (horizontal) resultant force [kN]	61,99 kN	Diameter steel wire	9 mm	DIN3064 6x36 warrington- seale+steelcore cable (eurocable)
Z (vertical) resultant force [kN]	60.96 kN	Vertical load Z [kN]	58,2 kN	
Weight castable shell [kg]	1182 91 kg	Volume	0,514 m <sup>3</sup>	
Reduction of weight vs hollowcore [%]	48,91%	Comparison floor	VBI 150mm	0,99 [-]
Reduction of weight vs solid floor [%]	70,24%	Comparison floor	200mm 2300kg concrete	

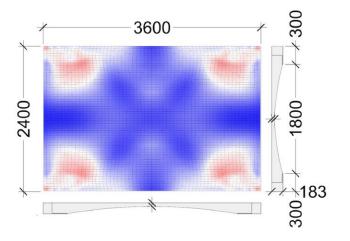


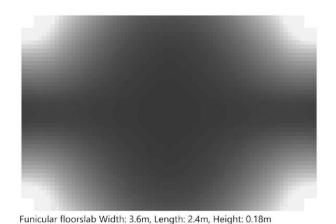






- 1. INTRODUCTION OF THE FLOORING **SYSTEM**
- 2. BOUNDARY **CONDITIONS**
- 3. OPTIMIZATION **SCRIPT**
- 4. RESULTING *FLOORSLABS*





### The resulting floorslabs 3600 x 2400 mm

Results	Description	Unity checks	Description	Description
Max compression stress P1 [N/mm2]	-2,91 N/mm2	Unity check	0.1455 [-]	Passed UC > 1
Max compression stress P2 [N/mm2]	-10,5 N/mm2	Unity check	0.525 [-]	Passed UC > 1
Max tensile stress P1 [N/mm2]	1.48 N/mm2	Unity check	0,99 [-]	Critical UC (Passed)
Max tensile stress P2 [N/mm2]	0.45 N/mm2	Unity check	0.3 [-]	Passed UC > 1
Max tensile stress LC 1 [N/mm2]	1,06 N/mm2	Unity check	0.71 [-]	Passed UC > 1
Max tensile stress LC 2 [N/mm2]	1,02 N/mm2	Unity check	0.68 [-]	Passed UC > 1
Max tensile stress LC 3 [N/mm2]	1,37 N/mm2	Unity check	0.91 [-]	Passed UC > 1
X (horizontal) resultant force [kN]	96,75 kN	Diameter steel wire	12 mm	DIN3064 6x36 warrington- seale+steelcore cable (eurocable)
Y (horizontal) resultant force [kN]	61,99 kN	Diameter steel wire	9 mm	DIN3064 6x36 warrington- seale+steelcore cable (eurocable)
Z (vertical) resultant force [kN]	60.96 kN	Vertical load Z [kN]	58,2 kN	
Weight castable shell [kg]	1182,91 kg	Volume	0,514 m <sup>3</sup>	
Reduction of weight vs hollowcore [%]	48,91%	Comparison floor	VBI 150mm	0,99 [-]
Reduction of weight vs solid floor [%]	70,24%	Comparison floor	200mm 2300kg concrete	

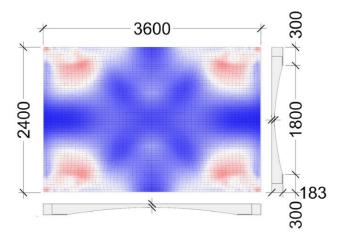


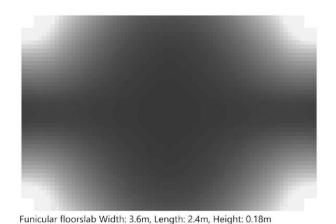






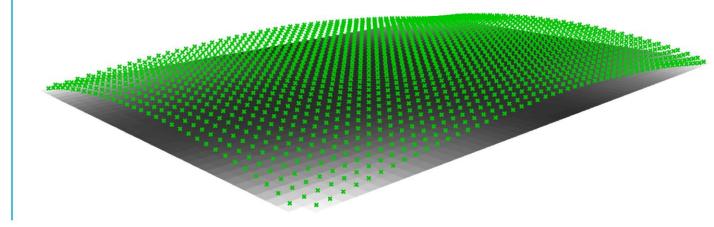
- 1. INTRODUCTION OF THE FLOORING SYSTEM
- 2. BOUNDARY CONDITIONS
- 3. OPTIMIZATION SCRIPT
- 4. RESULTING FLOORSLABS





3600 x 2400 mm

- Critical loadcase, P1 tensile stress due to distributed Q-load
- bitmap representation



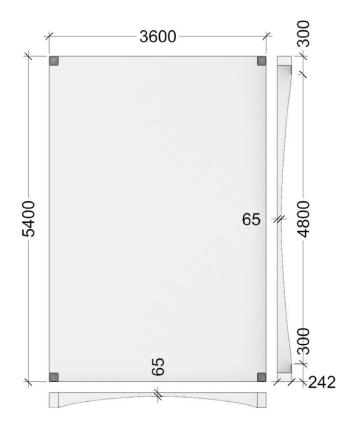








- 1. INTRODUCTION OF THE FLOORING SYSTEM
- 2. BOUNDARY CONDITIONS
- 3. OPTIMIZATION SCRIPT
- 4. RESULTING FLOORSLABS



Results	Description	Unity checks	Description	Description
Max compression stress P1 [N/mm2]	-4,14 N/mm2	Unity check	0.207 [-]	Passed UC > 1
Max compression stress P2 [N/mm2]	-16,7 N/mm2	Unity check	0.89 [-]	Passed UC > 1
Max tensile stress P1 [N/mm2]	1,47 N/mm2	Unity check	0.98 [-]	Critical UC
Max tensile stress P2 [N/mm2]	0,06 N/mm2	Unity check	0.04 [-]	Passed UC > 1
Max tensile stress LC 1 [N/mm2]	1,22 N/mm2	Unity check	0.81 [-]	Passed UC > 1
Max tensile stress LC 2 [N/mm2]	0,96 N/mm2	Unity check	0.64 [-]	Passed UC > 1
Max tensile stress LC 3 [N/mm2]	1,48 N/mm2	Unity check	0.99 [-]	Passed UC > 1
X (horizontal) resultant force [kN]	143,66 kN	Diameter steel wire	14 mm	DIN3064 6x36 warrington- seale+steelcore cable (eurocable)
Y (horizontal) resultant force [kN]	218,22 kN	Diameter steel wire	17 mm	DIN3064 6x36 warrington- seale+steelcore cable (eurocable)
Z (vertical) resultant force [kN]	36,25 kN	Total horizontal force	145 kN	
Weight castable shell [kg]	3313.61 kg	Volume	1.44 m³	
Reduction of weight vs. hollow-core [%]	36,4%	Comparison of floor	VBI 150mm	
Reduction of weight vs. solid floor [%]	69,12%	Comparison floor	240 mm 2300kg concrete	

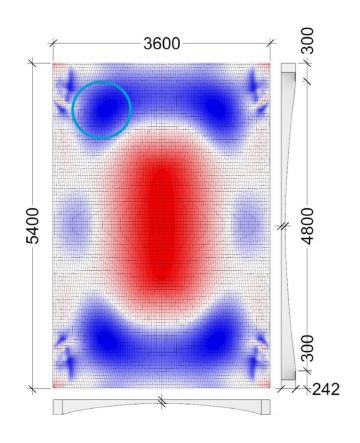








- 1. INTRODUCTION OF THE FLOORING SYSTEM
- 2. BOUNDARY CONDITIONS
- 3. OPTIMIZATION SCRIPT
- 4. RESULTING FLOORSLABS



3600 x 5400 mm

Results	Description	Unity checks	Description	Description
Max compression stress P1 [N/mm2]	-4,14 N/mm2	Unity check	0.207 [-]	Passed UC > 1
Max compression stress P2 [N/mm2]	-16,7 N/mm2	Unity check	0.89 [-]	Passed UC > 1
Max tensile stress P1 [N/mm2]	1,47 N/mm2	Unity check	0.98 [-]	Critical UC
Max tensile stress P2 [N/mm2]	0,06 N/mm2	Unity check	0.04 [-]	Passed UC > 1
Max tensile stress LC 1 [N/mm2]	1,22 N/mm2	Unity check	0.81 [-]	Passed UC > 1
Max tensile stress LC 2 [N/mm2]	0,96 N/mm2	Unity check	0.64 [-]	Passed UC > 1
Max tensile stress LC 3 [N/mm2]	1,48 N/mm2	Unity check	0.99 [-]	Passed UC > 1
X (horizontal) resultant force [kN]	143,66 kN	Diameter steel wire	14 mm	DIN3064 6x36 warrington- seale+steelcore cable (eurocable)
Y (horizontal) resultant force [kN]	218,22 kN	Diameter steel wire	17 mm	DIN3064 6x36 warrington- seale+steelcore cable (eurocable)
Z (vertical) resultant force [kN]	36,25 kN	Total horizontal force	145 kN	
Weight castable shell [kg]	3313,61 kg	Volume	1.44 m³	
Reduction of weight vs. hollow-core [%]	36,4%	Comparison of floor	VBI 150mm	
Reduction of weight vs. solid floor [%]	69,12%	Comparison floor	240 mm 2300kg concrete	



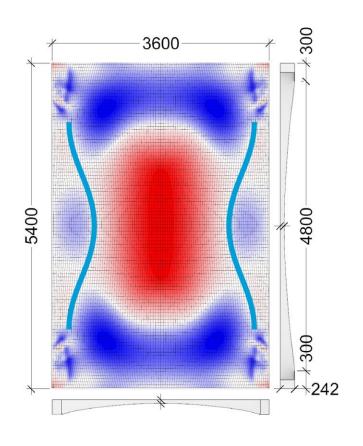






#### The results

- 1. INTRODUCTION OF THE FLOORING **SYSTEM**
- 2. BOUNDARY **CONDITIONS**
- 3. OPTIMIZATION **SCRIPT**
- 4. RESULTING *FLOORSLABS*



## The resulting floorslabs

3600 x 5400 mm

Results	Description	Unity checks	Description	Description
Max compression stress P1 [N/mm2]	-4,14 N/mm2	Unity check	0.207 [-]	Passed UC > 1
Max compression stress P2 [N/mm2]	-16,7 N/mm2	Unity check	0.89 [-]	Passed UC > 1
Max tensile stress P1 [N/mm2]	1,47 N/mm2	Unity check	0.98 [-]	Critical UC
Max tensile stress P2 [N/mm2]	0,06 N/mm2	Unity check	0.04 [-]	Passed UC > 1
Max tensile stress LC 1 [N/mm2]	1,22 N/mm2	Unity check	0.81 [-]	Passed UC > 1
Max tensile stress LC 2 [N/mm2]	0,96 N/mm2	Unity check	0.64 [-]	Passed UC > 1
Max tensile stress LC 3 [N/mm2]	1,48 N/mm2	Unity check	0.99 [-]	Passed UC > 1
X (horizontal) resultant force [kN]	143,66 kN	Diameter steel wire	14 mm	DIN3064 6x36 warrington- seale+steelcore cable (eurocable)
Y (horizontal) resultant force [kN]	218,22 kN	Diameter steel wire	17 mm	DIN3064 6x36 warrington- seale+steelcore cable (eurocable)
Z (vertical) resultant force [kN]	36,25 kN	Total horizontal force	145 kN	
Weight castable shell [kg]	3313,61 kg	Volume	1.44 m³	
Reduction of weight vs. hollow-core [%]	36,4%	Comparison of floor	VBI 150mm	
Reduction of weight vs. solid floor [%]	69,12%	Comparison floor	240 mm 2300kg concrete	



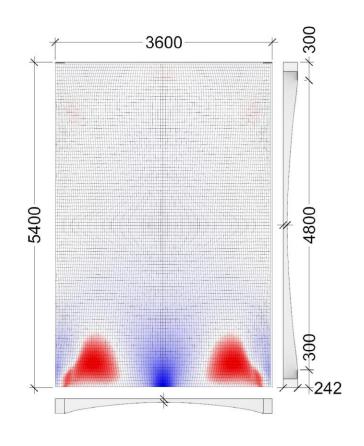






#### The results

- 1. INTRODUCTION OF THE FLOORING **SYSTEM**
- 2. BOUNDARY **CONDITIONS**
- 3. OPTIMIZATION **SCRIPT**
- 4. RESULTING *FLOORSLABS*



## The resulting floorslabs

3600 x 5400 mm

Results	Description	Unity checks	Description	Description
Max compression stress P1 [N/mm2]	-4,14 N/mm2	Unity check	0.207 [-]	Passed UC > 1
Max compression stress P2 [N/mm2]	-16,7 N/mm2	Unity check	0.89 [-]	Passed UC > 1
Max tensile stress P1 [N/mm2]	1,47 N/mm2	Unity check	0.98 [-]	Critical UC
Max tensile stress P2 [N/mm2]	0,06 N/mm2	Unity check	0.04 [-]	Passed UC > 1
Max tensile stress LC 1 [N/mm2]	1,22 N/mm2	Unity check	0.81 [-]	Passed UC > 1
Max tensile stress LC 2 [N/mm2]	0,96 N/mm2	Unity check	0.64 [-]	Passed UC > 1
Max tensile stress LC 3 [N/mm2]	1,48 N/mm2	Unity check	0.99 [-]	Passed UC > 1
X (horizontal) resultant force [kN]	143,66 kN	Diameter steel wire	14 mm	DIN3064 6x36 warrington- seale+steelcore cable (eurocable)
Y (horizontal) resultant force [kN]	218,22 kN	Diameter steel wire	17 mm	DIN3064 6x36 warrington- seale+steelcore cable (eurocable)
Z (vertical) resultant force [kN]	36,25 kN	Total horizontal force	145 kN	
Weight castable shell [kg]	3313,61 kg	Volume	1.44 m³	
Reduction of weight vs. hollow-core [%]	36,4%	Comparison of floor	VBI 150mm	
Reduction of weight vs. solid floor [%]	69,12%	Comparison floor	240 mm 2300kg concrete	

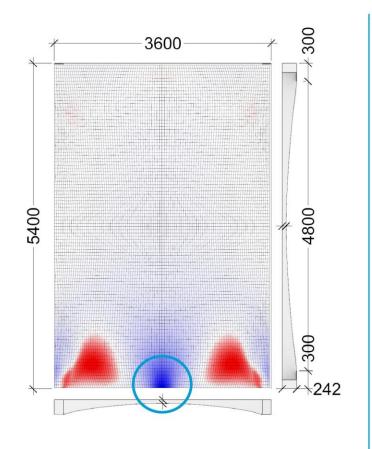




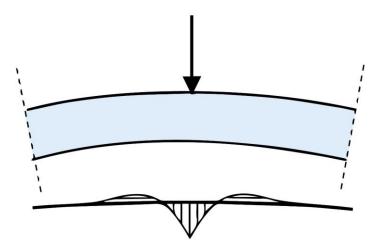




- 1. INTRODUCTION OF THE FLOORING **SYSTEM**
- 2. BOUNDARY **CONDITIONS**
- 3. OPTIMIZATION **SCRIPT**
- 4. RESULTING *FLOORSLABS*



### The resulting floorslabs 3600 x 5400 mm



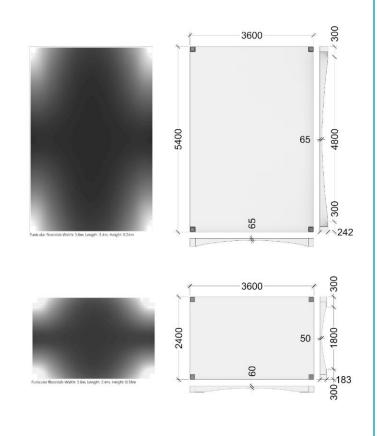
Incidental point load, might result in tension







- 1. INTRODUCTION OF THE FLOORING SYSTEM
- 2. BOUNDARY CONDITIONS
- 3. OPTIMIZATION SCRIPT
- 4. RESULTING FLOORSLABS



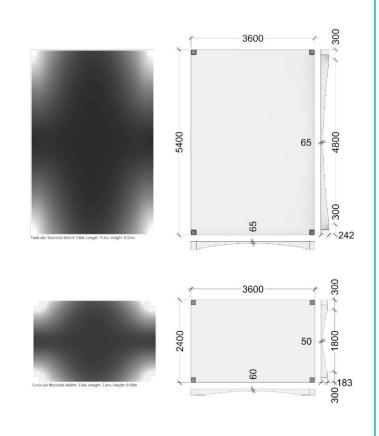
## Tensile stresses are guiding In thin-shell floorslabs







- 1. INTRODUCTION OF THE FLOORING SYSTEM
- 2. BOUNDARY CONDITIONS
- 3. OPTIMIZATION SCRIPT
- 4. RESULTING FLOORSLABS



## Tensile stresses are guiding In thin-shell floorslabs

Reduction of 69% of weight
While intergrating fabrication constraints

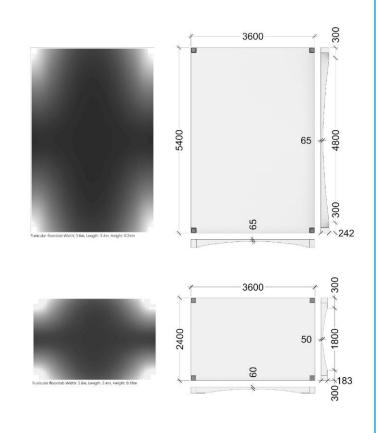
SECTION III EVALUATION







- 1. INTRODUCTION OF THE FLOORING **SYSTEM**
- 2. BOUNDARY **CONDITIONS**
- 3. OPTIMIZATION **SCRIPT**
- 4. RESULTING **FLOORSLABS**



### Tensile stresses are guiding In thin-shell floorslabs

Reduction of 69% of weight While intergrating fabrication constraints

Multiple loadcases are guiding in the optimization process





SECTION III
EVALUATION
OF THE HYPOTHESIS

### Hypothesis

Fabrication-aware, structurally optimized floor slabs can significantly reduce the environmental impact of concrete construction.





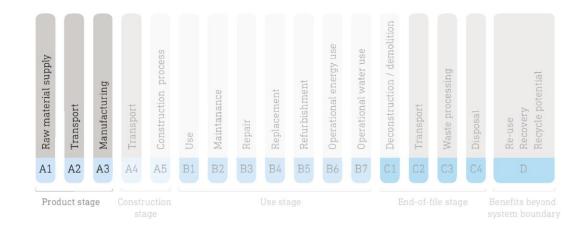




Reducing the environmental impact of concrete construction through fabrication-aware, structurally optimized floor slabs



### Life Cycle Assessment (LCA) Of the product stage



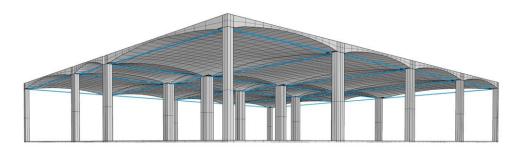
SECTION III EVALUATION





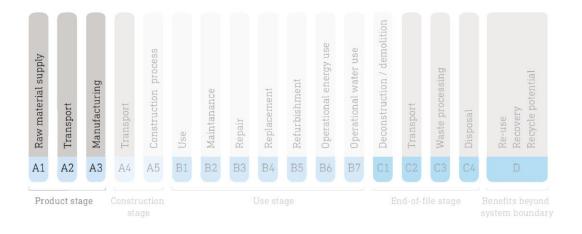


Reducing the environmental impact of concrete construction through fabrication-aware, structurally optimized floor slabs



### Life Cycle Assessment (LCA) Of the product stage

- The product stage, as it accounts for more than 80% of the embodied emissions



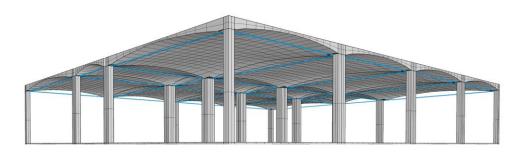








Reducing the environmental impact of concrete construction through fabrication-aware, structurally optimized floor slabs



### Life Cycle Assessment (LCA) Of the product stage

Virtual office building

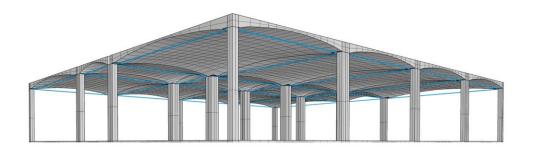






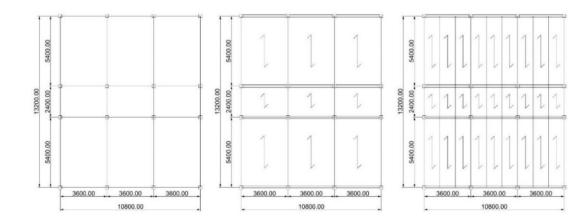


Reducing the environmental impact of concrete construction through fabrication-aware, structurally optimized floor slabs



### Life Cycle Assessment (LCA) Of the product stage

### Virtual office building









Reducing the environmental impact of concrete construction through fabrication-aware, structurally optimized floor slabs



Life Cycle Assessment (LCA) Of the product stage

Virtual office building

Ten flooring systems compared 5400 mm span flooring systems

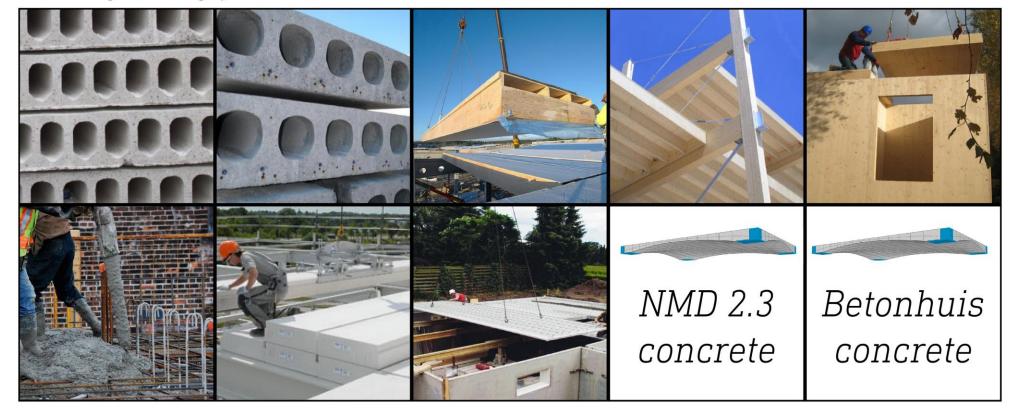








## Ten flooring systems 5400 mm span flooring systems



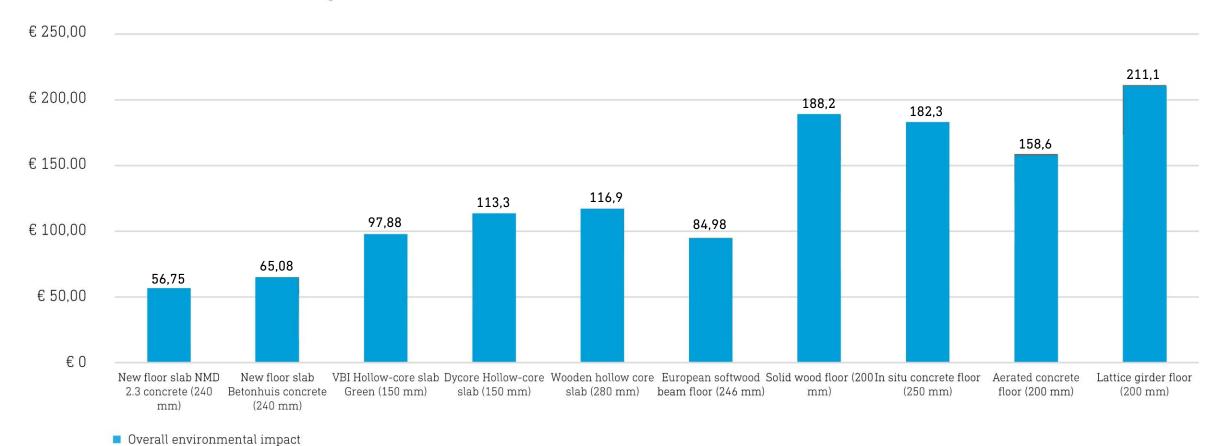








# Ten flooring systems Overall environmental impact in shadowcost (3600 mm x 5400 mm)



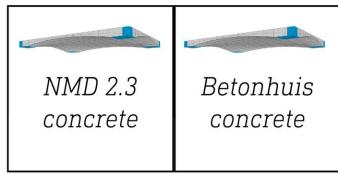


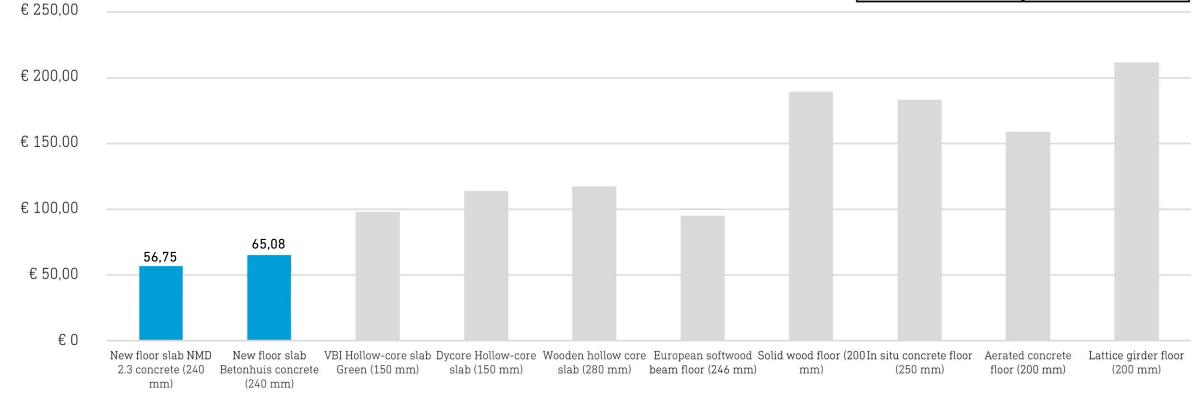






# Ten flooring systems Overall environmental impact in shadowcost (3600 mm x 5400 mm)





Overall environmental impact



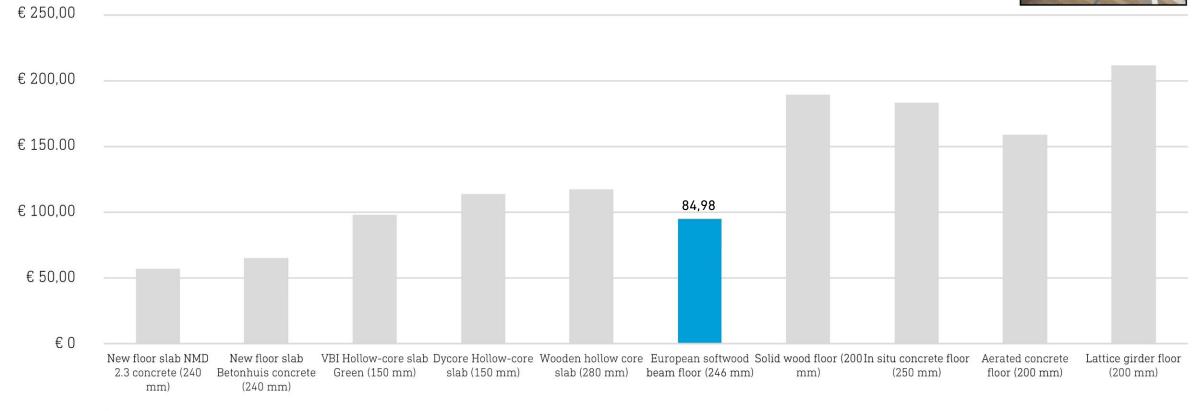






## Ten flooring systems Overall environmental impact in shadowcost (3600 mm x 5400 mm)





Overall environmental impact

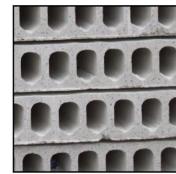


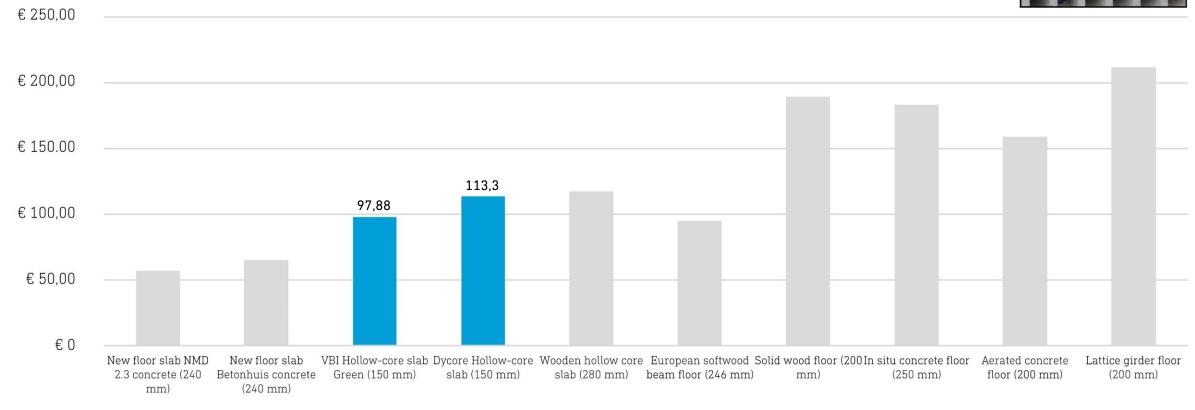






## Ten flooring systems Overall environmental impact in shadowcost (3600 mm x 5400 mm)





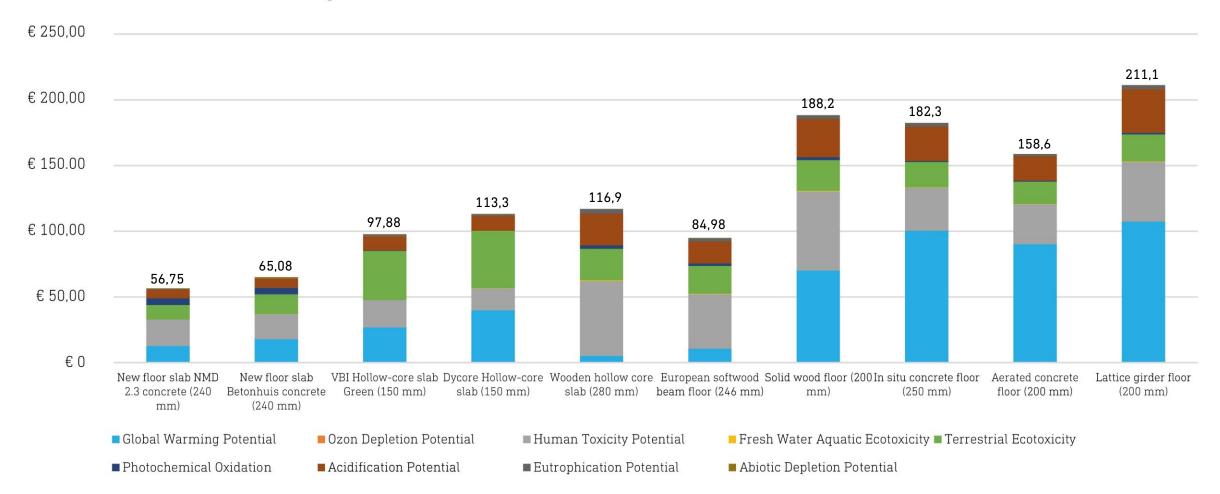
Overall environmental impact







### Ten flooring systems Overall environmental impact in shadowcost (3600 mm x 5400 mm)



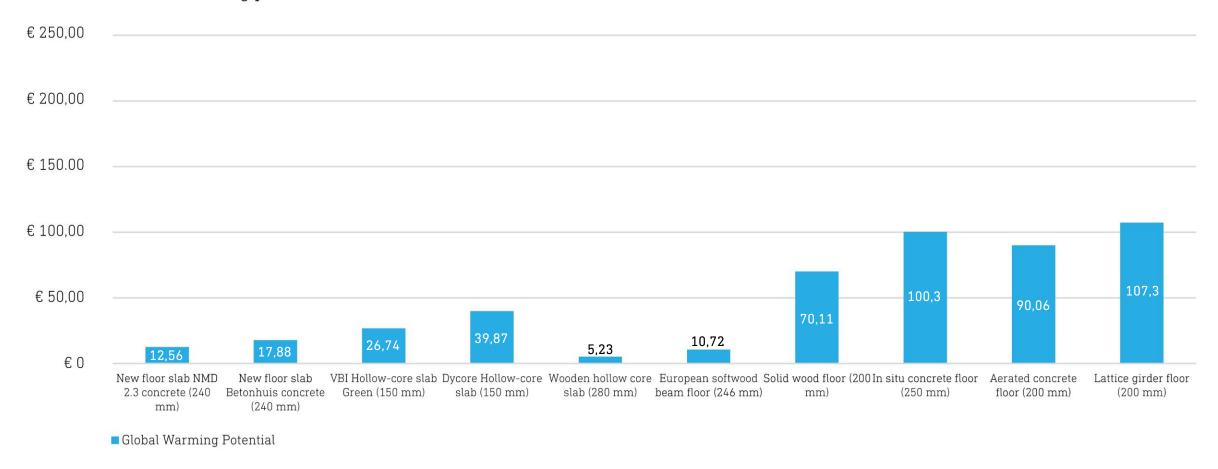








## Ten flooring systems Global warming potential in shadow cost (3600 mm x 5400 mm)















Summary Conclusion and Outlook



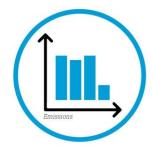






161

#### Main research question



Process-related material requirements



Reinforcement





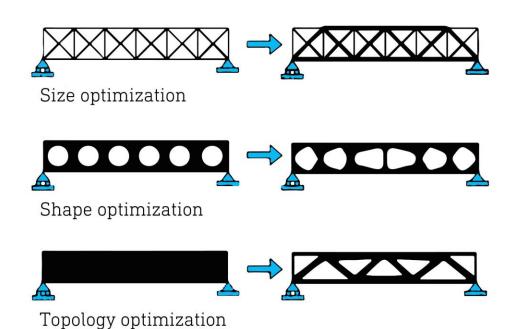
Life cycle cost









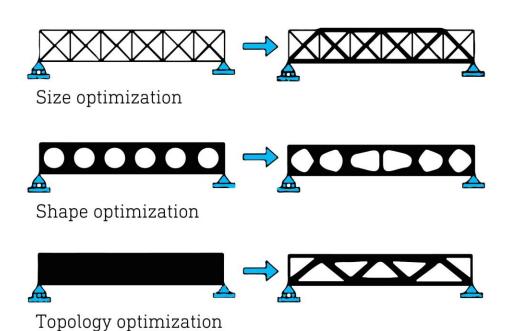


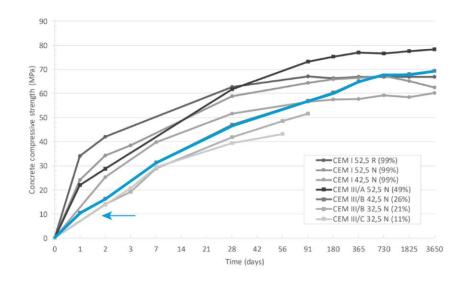




















In what manner can we use additive manufacturing and structural optimization in the building sector to address the environmental impact of concrete construction?

**85%** of the emissions is the binder











Fabrication-aware, structurally optimized floor slabs can significantly reduce the environmental impact of concrete construction.

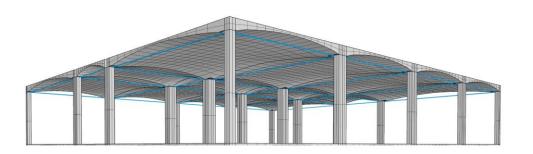








Reducing the environmental impact of concrete construction through fabrication-aware, structurally optimized floor slabs



#### Research through design

- A derivative free optimimization approach allows for the succesful intergration of fabrication constraints and multiple loadcases in the optimization process.

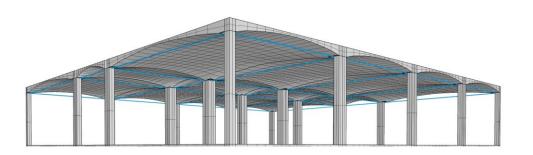








Reducing the environmental impact of concrete construction through fabrication-aware, structurally optimized floor slabs



#### Research through design

- A derivative free optimimization approach allows for the successful intergration of fabrication constraints and multiple loadcases in the optimization process.

This adresses a current gap in literature, on a derivative approach for concurrent structural design problems.

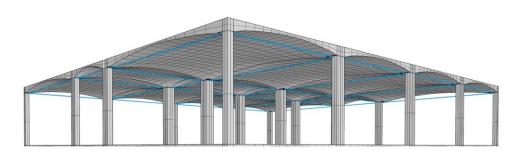






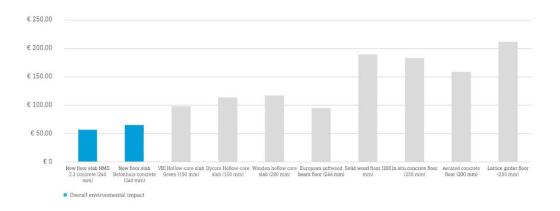


Reducing the environmental impact of concrete construction through fabrication-aware, structurally optimized floor slabs



#### Research through design

- Thin-shell flooring systems which utilize membrane action, result in a significant reduction in both carbon and environmental footprint.











"Although reinforced concrete has been used for over a hundred years and with increasing interest during the last decades, few of its properties and potentialities have been fully exploited so far. Apart from the unconquerable inertia of our own minds, which do not seem to be able to adapt freely any new ideas, the main cause of this delay is a trivial technicality: The need to prepare wooden frames." – Nervi, 1956









#### Designing sustainable by designing with less material,











# Designing sustainable by designing with less material, with a smaller impact,













173

# Designing sustainable by designing with less material, with a smaller impact, in an easy to construct way











174

### Designing sustainable by designing with less material, with a smaller impact, in an easy to construct way















### A step towards a more sustainable building sector













### Thanks for listening









