

## MAJOR DTNSRDC ORGANIZATIONAL COMPONENTS



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#### Abstract

In order to design and model some combat systems, it may be necessary to consider joint distribution of two or more natural environment parameters. This can be accomplished by simultaneous sampling of various natural environment parameters. A major part of the investigation reported herein is the development of wind generated significant wave height as a function of latitude for the Northern Hemisphere, however, a joint sampling of other surface and atmospheric parameters is also included.


## ADMINISTRATIVE INFORMATION

The work reported herein was carried out at the request of the Naval Sea Systems Command (NAVSEA) 61433 and authorized by Work Request Numbers WR 92590 and WR OGO91. It is identified by Work Unit Numbers 1568-817 and 1568-830 at the David W. Taylor Naval Ship Research and Development Center (DTNSRDC). The data presented herein was developed as long ago as 1976, and in keeping with the sponsor's wishes at the time that the work was initlated, metric units have not been used in this report.

## INTRODUCTION

The procedures used for modeling the effects of the natural environment on naval ship performance are outlined in another report* and Reference 1.** The "Sea Environment Manual for Ship Design" is a source document on seaway models where wind and wave statistics are developed for seakeeping analyses typical of concept and preliminary ship design investigations. Reference 1 is an extraction from the so-called Ship Designer's Atlas*** which provides a mesh of both threat and natural environments derived for a number of global "hot spots." It provides an overall climatology, with the emphasis on the worst season (month) for each hot spot, and is primarily aimed at the combat systems (weapons, sensors, etc.) designer.

[^0]A fundamental deficiency in existing ship design methodology is the lack of integration of realistic measures of ship performance into the decision making process. While the Ship Designer's Atlas is an attempt at overcoming this deficiency, it has several weaknesses which have not been satisfactorily addressed. The most important ones are:

1. Threat and natural environment parameters are not integrated into consistent data sets
2. Simultaneous sampling of natural environment parameters from each medium (atmosphere, surface, subsurface) is not addressed In order to address the first weakness, it is necessary to overcome the second, and it is this which is addressed in the current report.

Specifically, this report outlines the statistical results derived by simultaneous sampling of various natural environment parameter distributions taken from Reference 1 and from an expanded version which is in preparation. The physics of the marine environment as well as meteorological and oceanographic dynamics have been considered in the procedures developed. Global locations considered are sixteen in number, and are designated Points $A$ through $P$ which are identified in Table 1 and Figure 1.

## ENVIRONMENTAL PARAMETERS

Eight environment parameters have been considered for each location. They are winds, waves, fog, thunderstorms, icing (superstructure); pressure centers, refractivity, and air masses. Before discussing the results of this investigation, some comments regarding the quality of the data are in order. The data examined are for the worst month* at each location as presented in Reference 1 and its revision (now in preparation). Unfortunately, some parameters may not be well represented, especially at the extremes, due to the fact that data is developed from shipboard observations, and ships generally try to avoid areas of severe weather.

A description of the phenomena associated with the parameters analyzed (except winds and waves) is now given. Winds and waves are discussed in detail in a subsequent section of the report.

[^1]
## METEOROLOGICAL DAY

As indicated in Figure 2, from Reference 2, a meteorological day is divided into three periods:

1. Night - from 2 hours after sunset until 2 hours after sunrise
2. Afternoon - from 5 hours after sunrise until 1 hour before sunset
3. Transition - the two 3-hour periods between the night and afternoon period; also, if the sky is covered by opaque clouds at any time of the day, the period should be treated as a transition period

FOG
Fog is rare when the difference between aị and sea temperature is more than $5^{\circ} \mathrm{F}$. A high relative humidity is the major contributor to the formation of fog, since no condensation will occur unless the relative humidity is more than 90 percent, see References 3 and 4. A light wind causes a gentle mixing action which is generally favorable for a deeper and thicker layer of fog, and a very light wind usually generates a shallow layer only about 6 feet deep. In general, one would expect benign to moderate wave conditions under a layer of fog. Most fogs evaporate after sunrise.

## THUNDERSTORMS

Thunderstorms over the ocean are most common during the night and early morning. They frequently occur offshore in low pressure centers when the land and sea breezes are blowing toward the water, as indicated in Reference 3. The rapid change in wind direction and speed are the major characteristics prior to storm passage over the sea. Also, the wind speeds at the leading edge of the storm are far greater than those at the trailing edge: A particular sequence of pressure variations usually accompanies thunderstorms:

1. Pressure falls as the storm approaches
2. Pressure rises rapidly as the storm brings rain showers overhead
3. Rain ceases and pressure gradually returns to normal after the storm

Generally, thunderstorms provide high winds, severe wave conditions, and visibility is normally poor.

## ICING (SUPERSTRUCTURE)

The worst icing conditions are met with the combination of very low temperatures and strong winds. They frequently occur to the rear of a low pressure system on its poleward side. As indicated in Réference 1 , a potential for moderate icing exists when the air temperature is $28^{\circ} \mathrm{F}$ $\left(-2.2^{\circ} \mathrm{C}\right)$ or less and the wind speeds are 13 knots or greater. Moderate icing potential implies a buildup of less than one-tenth of an inch an hour. Severe icing of the ship is likely when the air temperature drops to $16^{\circ} \mathrm{F}\left(-8.9^{\circ} \mathrm{C}\right)$ or less and the wind speed is 30 knots or greater. Severe icing implies a buildup of one-tenth of an inch or more per hour.

## LOW PRESSURE CENTERS

The wind flow around a low pressure system is counterclockwise in the Northern Hemisphere. Low pressure systems are usually associated with severe storm characteristics such as hurricanes, tropical storms, and tornadoes. Other unfavorable conditions in low pressure systems are low clouds, poor visibility caused by precipitation and fog, severe wave conditions, and closely spaced isobars with strong and gusty winds; see References 3 and 5. Standard atmospheric pressure is about 1013 mb in the near surface ocean environment and, in general, is also taken as the boundary contour that separates high from low pressure system.

## HIGH PRESSURE CENTERS

The wind flow around a high pressure system is clockwise in the Northern Hemisphere. High pressure systems occur predominately over cold surfaces and are accompanied by few clouds. Other favorable conditions associated with high pressure centers are good daytime visibility, benign to moderate wind and wave conditions, and widely spaced isobars with light and calm winds.

## SUPER-REFRACTION OR DUCTING

As indicated in References 6 and 7, if the refractive index decreases with height at more than 0.000013 per 1000 feet, radar waves will be bent
closer to the earth's surface and the distance to the radar horizon will increase. This phenomenon is referred to as super-refraction or ducting. Ducts frequently occur offshore with high pressure systems during the transition from morning to afternoon and generally indicate a decrease of relative humidity with height. Ducts are also associated with warm sea or land breezes over a cold surface. Ducts are sometimes accompanied by strong winds and severe wave conditions:

## SUB-REFRACTION

If the refractive index decreases with height at less than 0.000013 per 1000 feet, radar waves will tend to lift further above the earth's surface and the radar horizon will be limited to a shorter range. This phenomenon is known as sub-refraction. Sub-refractions frequently occur simultaneously with sea or land breezes during the evening transition perlod. In general, sub-refraction is associated with an increase of relative humidity with height and with the occurrence of cold air over a warm surface.

## COLD FRONT

As indicated in References 3 and 4, a cold front is the leading edge of an advancing mass of cold air, and clouds are predominately cumuliform with good to excellent visibility. Cumuliform clouds are clouds with vertical development and generally have their bases below 6500 feet and their tops sometimes above 65,000 feet. Cold fronts frequently occur together with low pressure systems and hence with strong winds, high waves, and a line of thunderstorms developing along the surface front and may extend for hundreds of miles.

## WARM FRONT

A warm front is the trailing edge of a retreating mass of cold air with stratiform clouds. Warm fronts may be accompanied by fog and poor to fair visibility. Stratiform clouds are low clouds occurring from near the surface to about 6500 feet. Warm fronts also occur simultaneously in low pressure systems with light to calm winds.

## JOINT PARAMETER DATA

The surface natural environment data of the worst months for the 16 locations are presented in Tables 2 through 7. The alphabetic designation of locations within each table corresponds to that given in Reference 1 . All wind and wave data (except for locations C, D, E, F, H and I) are derived from the Twenty Year Hindcast Wind and Wave Climatology described in Reference 1 . In some cases, a particular phenomenon or parameter was not available for a given location. These cases are noted by a dashed line as they occur.

The first approach to simultaneous sampling of natural environment parameters is by selecting the most probable values of the weather features associated with each phenomenon. For example, Table 2 presents numerical values of the most probable weather features associated with fog. Values for air-sea temperature difference, air temperature, relative humidity, sun, meteorological period, wind direction, wind speed, significant wave height, and modal wave period for each of the 16 locations are provided. Thus, if the effects of fog are to be considered in a combat system design, Table 2 can be used to provide probable values of other environmental parameters. Similarly, Tables 3, 4, 5, 6, and 7 provide probable values for thunderstorms, icing, low and high pressure centers, refractivity, and cold and warm air masses, respectively.

## GEOGRAPHIC VARIATIONS OF WINDS AND WAVES

Ocean waves are generated by four major factors:

1. Wind blowing over the water surface
2. Surface pressure variations
3. Earthquakes
4. Sun and moon tidal attraction

Wind waves are probably the most important and fundamental phenomenon in the open sea. The second approach to simultaneous sampling of natural environment parameters is by using wind speed as a fixed parameter. The most probable values of wind generated wave height can be calculated as a function of latitude for each of the 16 ocean locations by using wind speed as the independent variable in linear regression. The results are shown in Figure 3, which permits the determination of significant wave
height for given values of wind speed and latitude in the Northern Hemisphere. The three sets of curves plotted on Figure 3 correspond to the open ocean area, the coastal area, and the boundary area between them. Coastal area is defined to be within 200 miles of the continent or 75 miles from an island; all other ocean areas are classified as open ocean. The boundary area is taken as a 50-mile wide zone between open ocean and coastal areas. A few aids useful in applying Figure 3 are now given. In general, it is assumed that a wind speed and direction is known.

The equation to find the great circle distance between two points on the earth's surface as indicated in Reference 8 is

$$
D=60 \cos ^{-1}\left[\sin L_{1} \sin L_{2}+\cos L_{1} \cos L_{2} \cos \left(\lambda_{2}-\lambda_{1}\right)\right]
$$

where $D$ is the distance in nautical miles, $L_{i}$ and $\lambda_{i}$ are longitude and latitude in degrees, respectively.

Wind speed should be considered the average value for at least one hour. When the change of wind direction is no greater than 15 degrees, it should be treated as a constant. If wind persists for more than 5. hours from the same general direction, Table 8 should be used to determine correction factors for significant wave heights produced by different wind speeds blowing for various lengths of time. If wind speed is less than 3 knots, wind generated wave height is negligible (e.g., $\leq 2$ feet).

Landlocked ocean areas (e.g., the Gulf of Mexico and the Mediterranean Sea) should be classified as boundary areas even though some regions are located more than 200 miles from the continent.

The highest wave heights are generated between about 58 and $62^{\circ} \mathrm{N}$; beyond that point, wind generated waves start declining with respect to latitude. This probably is due to the limited fetch and great possibility of land mass interference near the North Pole.

A sample application of Figure 3 is now given.
A 20-knot wind has been blowing for the last 10 hours from the same general direction at a region located near $50^{\circ} \mathrm{N}$ and $30^{\circ} \mathrm{W}$. What is the estimated significant wave height?

Since this region is located at more than 250 miles from the continent, it is classified as an open ocean area. By reading across the
intersection at $50^{\circ} \mathrm{N}$ in Figure 3 , the wind speed coefficient is 0.68 and the constant is 1.5 . Then

$$
\begin{aligned}
\left(\tilde{\zeta}_{w}\right)_{1 / 3} & =\text { wind speed (in knots) } \times \text { Coefficient + Constant } \\
\left(\tilde{\zeta}_{w}\right)_{1 / 3} & =20 \times(0.68)+1.5 \\
& =15.1 \mathrm{ft}
\end{aligned}
$$

As the wind has been blowing for 10 hours in the same general direction, a correction factor of 1.25 is taken from Table 8 adopted from Reference 5. Finally, the estimated significant wave height is

$$
\begin{aligned}
\left(\tilde{\zeta}_{w}\right)_{1 / 3} & =15.1 \times 1.25 \\
& =18.9 \mathrm{ft}
\end{aligned}
$$

In general, modal wave period is a function of wind speed and fetch. Attempts to correlate it with latitude have not been successful in this investigation. However, significant wave height and modal wave period by wind speed is presented in Table 9 for all 16 ocean locations. Table 10 provides a comparison of wind speed and significant wave height by wind direction. The primary objective of these tables is in ship design and engineering applications. However, in ship operations applications, Tables 9 and 10 could produce misleading results. For example, surface pressure variations and swells from distant storms are important factors in wave height forecasts that are excluded in this investigation due to lack of available data.

## CONCLUDING REMARKS

In summary, this report outlines the results of simultaneous sampling of various natural environment parameters in the Ship Designer's Atlas, see Reference 1. Eight environmental phenomena have been considered for each of 16 locations. They are winds, waves, fog, thunderstorms, icing (superstructure), pressure centers, refractivity, and air masses. The first approach applied to the development of consistent natural environment
parameter sets is that of selecting the most probable values for the weather features associated with each phenomenon as presented. These results are given in Tables 2 through 7. The second approach to simultaneous sampling of natural environment parameters is the development of wind generated wave height as a function of latitude and proximity to the coast for the Northern Hemisphere and is given in Figure 3.

It is considered that each approach provides additional guidance to the combat systems engineer. As the Navy further refines the emerging ship performance design practice, this guidance will become useful in systems integration analyses.

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Figure 2 - Meteorological Day (from Reference 3)


Figure 3 - Significant Wave Height by Wind Speed

TABLE 1 - OPERATIONAL AREA IDENTIFICATION

| Location 10 | Latitude, Longitude | Description | Area |
| :---: | :---: | :---: | :---: |
| A | $63^{\circ} \mathrm{N}, 2^{\circ} \mathrm{W}$ | Northern Northeast Atlantic (off Norway) | Boundary |
| B | $58^{\circ} \mathrm{N}, 12^{\circ} \mathrm{W}$ | Northern North Atlantic (off Scotland) | Boundary |
| C | $\begin{aligned} & 33^{\circ} 30^{\prime}-35^{\circ} 0^{\prime} N, \\ & 29^{\circ} 30^{\prime}-30^{\circ} 30^{\prime} E \end{aligned}$ | Eastern Mediterranean (off Cyprus) | Coastal |
| D | $39^{\circ} \mathrm{N}, 129^{\circ} \mathrm{E}$ | Japan Sea (off Korea) | Coastal |
| E | $12^{\circ} \mathrm{N}, 46^{\circ} 30^{\prime} \mathrm{E}$ | Gulf of Aden (off Saudi Arabia) | Coastal |
| F | $9^{\circ} 30^{\prime} \mathrm{N}, 16^{\circ} 0^{\prime} \mathrm{W}$ | Southeastern North Atlantic (off Guinea) | Coastal |
| G | $50^{\circ} \mathrm{N}, 180^{\circ} \mathrm{W}$ | North Pacific (off the Aleutians) | Open <br> Ocean |
| H | $\begin{aligned} & 20^{\circ} 45^{\prime}-21^{\circ} 50^{\prime} \mathrm{N}, \\ & 80^{\circ}-86^{\circ} \mathrm{W} \end{aligned}$ | ```Caribbean (off Cuba)``` | Coastal |
| 1 | $0^{\circ} \mathrm{N}, 106^{\circ} \mathrm{E}$ | Strait of Malacca (off Singapore) | Coastal |
| J | $34^{\circ} 12^{\prime} \mathrm{N}, 163^{\circ} 48^{\prime} \mathrm{E}$ | Western North Pacific (North of Wake Island) | Open Ocean |
| K | $50^{\circ} 54^{\prime} \mathrm{N}, 145^{\circ} 36{ }^{\prime} \mathrm{W}$ | Northeastern North Pacific (South of Gulf of Alaska) | 0pen Ocean |
| L | $24^{\circ} 48^{\prime} \mathrm{N}, 162^{\circ} 3^{\prime} \mathrm{W}$ | Mid-North Pacific <br> (Northwest of Hawailan Islands) | Open Ocean |
| M | $51^{\circ} 18^{\prime} \mathrm{N} ; 162^{\circ} 3^{\prime \prime} \mathrm{E}$ | Northern Northwest Pacific (Off Kamehatka Peninsula) | Open <br> Ocean |
| N | $52^{\circ} 48^{\prime} \mathrm{N}, 33^{\circ} 48^{\prime} \mathrm{W}$ | Mid-Northern North Atlantic | Open Ocean |
| 0 | $34^{\circ} 61 \mathrm{~N}, 52^{\circ} 54^{\prime} \mathrm{W}$ | Mid-North. Atlantic | Open Ocean |
| P | $39^{\circ} 54^{\prime} \mathrm{N}, 21^{\circ} 48^{\prime} \mathrm{W}$ | Mid-Eastern North Atlantic (East of Azores) | Open Ocean |

TABLE 2 - MOST PROBABLE WEATHER FEATURES OF FOG

| LOCATION | FOG | AIR-SEA TEMPERATURE DIFFERENCE | AIR TEMPERATURE | relative HUMIDITY | SUN | METEOROLOGICAL, PERIOD | WIND DIRECTION | WIND SPEED | Wave HE I GHT $\left(S_{W}\right) 1 / / 3$ | MODAL wave PERIOD |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| A | DEEP LAYER | $\therefore \leq 5^{\circ} \mathrm{F}$ | $\leq 40^{\circ} \mathrm{F}$ | $\begin{aligned} & \geq 90 \% \\ & \text { HIGH } \end{aligned}$ | $\begin{gathered} \text { NC } \\ \text { SUNSHINE } \end{gathered}$ | TRANSITION. | SOUTH OR SOUTHWEST | $\leq 8 \mathrm{KTS}$ | $\leq 6 \mathrm{ft}$ | $\leq 10 \mathrm{SEC}$ |
|  | SHALLOW LAYER |  |  |  |  |  |  | $\leq 5 \mathrm{KTS}$ | $\leq 5 \mathrm{ft}$ | $\leq 9 \mathrm{SEC}$ |
| 8 | DEEP LAYER | $\leq 6^{\circ} \mathrm{F}$ | $\leq 45^{\circ} \mathrm{F}$ | $\geq 90 \%$HIGH | NO SUNSHIHE | TRANSITIION | EAST ORSOUTH | $\leq 8 \mathrm{KTS}$ | $\leq 7 \mathrm{ft}$ | $\leq 10 \mathrm{SEC}$ |
|  | SHALLOW LAYER |  |  |  |  |  |  | $\leq 5 \mathrm{KTS}$ | $\leq 6 \mathrm{ft}$ | $\leq 9 \mathrm{SEC}$ |
| C | DEEP LAYER | $\leq 40 \mathrm{~F}$ | $\leq 58{ }^{\circ} \mathrm{F}$ | $\begin{aligned} & \geq 90 \% \\ & \text { HIGH } \end{aligned}$ | NO SUNSHINE | TRANSITION | SOUTH | $\leq 5 \mathrm{KTS}$ | $\leq 5 \mathrm{ft}$ | $\leq 6 \mathrm{SEC}$ |
|  | SHALLOW LAYER |  |  |  |  |  |  | $\leq 3 \mathrm{KTS}$ | $\leq 4 \mathrm{ft}$ | $\leq 5 \mathrm{SEC}$ |
| D | DEEP LAYER | $\leq 4^{0} \mathrm{~F}$ | $\leq 38^{\circ} \mathrm{F}$ | $\begin{aligned} & \geq 90 \% \\ & \mathrm{HIGH} \end{aligned}$ | $\begin{gathered} \text { NO } \\ \text { SUNSHINE } \end{gathered}$ | TRANSITION |  | $\leq 5 \mathrm{KTS}$ | $\leq 4 \mathrm{ft}$ | $\leq 6 \mathrm{SEC}$ |
|  | SHALLOW LAYER |  |  |  |  |  |  | $\leq 3 \mathrm{KTS}$ | $\leq 3 \mathrm{ft}$ | $\leq 5 \mathrm{SEC}$ |
| E | deEP LAYER | $\leq 60 \mathrm{~F}$ | $\leq 85{ }^{\circ} \mathrm{F}$ | $\geq 90 \%$ | $\begin{gathered} \text { ND } \\ \text { SUNSHINE } \end{gathered}$ | TRANSITION | NORTHEAST OR SDUTHEAST | $\leq 5 \mathrm{KTS}$ | $\leq 4 \mathrm{ft}$ | $\leq 6 \mathrm{SEC}$ |
|  | SHALLOW LAYER |  |  |  |  |  |  | $\leq 3 \mathrm{KTS}$ | $\leq 3 \mathrm{ft}$ | $\leq 5 \mathrm{SEC}$ |
| F | DEEP. LAYER | $\leq 2^{0} \mathrm{~F}$ | $\leq 78{ }^{\circ} \mathrm{F}$ | $\geq 90 \%$ | $\begin{aligned} & \text { NO } \\ & \text { SUNSHINE } \end{aligned}$ | TRANSITION | SOUTHWEST OR NORTHWEST | $\leq 4 \mathrm{KTS}$ | $\leq 4 \mathrm{ft}$ | $\leq 6 \mathrm{SEC}$ |
|  | SHALLOW LAYER |  |  |  |  |  |  | $\leq 2 \mathrm{KTS}$ | $\leq 3 \mathrm{ft}$ | $\leq 5 \mathrm{SEC}$ |
| G | DEEP LAYER | $\leq 40 \%$ | $\leq 35{ }^{\circ} \mathrm{F}$ | $\frac{290 \%}{\mathrm{HIGH}}$ | NO SUNSHINE | TRANSITION | - | $\leq 8 \mathrm{kTS}$ | $\leq 9 \mathrm{ft}$ | $\leq 12 \mathrm{SEC}$ |
|  | SHALLOW LAYER |  |  |  |  |  |  | $\leq 5 \mathrm{kTS}$ | $\leq 8 \mathrm{ft}$ | $\leq 11 \mathrm{SEC}$ |
| H | DEEP LAYER | $\leq 40 F$ | $\leq 75^{\circ} \mathrm{F}$ | $\begin{aligned} & \geq 90 \% \\ & \text { HI GH } \end{aligned}$ | NO SUNSHINE | TRANSITION | - | $\leq 6 \mathrm{KTS}$ | $\leq 4 \mathrm{ft}$ | $\leq 6 \mathrm{SEC}$ |
|  | $\begin{aligned} & \text { SHALLOW } \\ & \text { LAYER } \end{aligned}$ |  |  |  |  |  |  | $\leq 3 \mathrm{KTS}$ | $\leq 3 \mathrm{ft}$ | $\leq 5 \mathrm{SEC}$ |

TABLE 2 (Continued)

| LOCATION | FOG | AIR-SEA TEMPERATURE DIFFERNECE | AIR TEMPERATURE | RELATIVE huilidity | SUN | METEOROLOGICAL PERIOD | $\begin{aligned} & \text { WIND } \\ & \text { DIRECTION } \end{aligned}$ | WIND SPEED | WAVE HEI GHT $\left(\bar{\zeta}_{W}\right) 1 / 3$ | MODAL WAVE PERIOD |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| I | DEEP LAYER | $\leq 2^{\circ} \mathrm{F}$ | $\leq 80^{\circ} \mathrm{F}$ | $\begin{aligned} & \geq 90 \% \\ & \mathrm{HI} \mathrm{CH} \end{aligned}$ | NO <br> SUNSHINE | .TRANS ITIION | NORTH | $\leq 5 \mathrm{KTS}$ | $\leq 4 \mathrm{ft}$ | $\leq 6 \mathrm{SEC}$ |
|  | SHALLOW LAYER |  |  |  |  |  |  | $\leq 3 \mathrm{KTS}$ | $\leq 3 \mathrm{ft}$ | $\leq 5 \mathrm{SEC}$ |
| J | DEEP LAYER | $\leq 4^{\circ} \mathrm{F}$ | $\leq 55^{\circ} \mathrm{F}$ | $\begin{aligned} & \geq 90 \% \\ & \mathrm{HIGH} \end{aligned}$ | $\begin{gathered} \text { NO } \\ \text { SUNSHINE } \end{gathered}$ | TRANSITION |  | $\leq 8 . \mathrm{KTS}$ | $\leq 9 \mathrm{ft}$ | $\leq 13 \mathrm{SEC}$ |
|  | SHALLOW -LAYER |  |  |  |  |  |  | $\leq 5 . \mathrm{KTS}$ | $\leq 8 \mathrm{ft}$ | $\leq 12 \mathrm{SEC}$ |
| $K$ | deep layer | $\leq 4^{\circ} \mathrm{F}$ | $\underline{-42}{ }^{\circ} \mathrm{F}$ | $\begin{aligned} & \geq 90 \% \\ & \text { HIGH } \end{aligned}$ | NO SUNSHINE | TRANSITION |  | $\leq 8 \mathrm{KTS}$ | $\leq 9 \mathrm{ft}$ | $\leq 12 \mathrm{SEC}$ |
|  | SHALLOW LAYER |  |  |  |  |  |  | $\leq 5$ KTS | $\leq 8 \mathrm{ft}$ | $\leq 11 \mathrm{SEC}$ |
| I | deep layer | $\leq 4^{\circ} \mathrm{F}$ | $\leq 70^{\circ} \mathrm{F}$ | $\begin{aligned} & \geq 90 \% \\ & \text { HIGH } \end{aligned}$ | $\begin{aligned} & \therefore \text { NO } \\ & \text { SUNSHINE } \end{aligned}$ | TRANSITION | $\dot{-}$ | $\leq 6 \mathrm{KTS}$ | $\leq 6 \mathrm{ft}$ | $\leq 12 \mathrm{SEC}$ |
|  | LAYER |  |  |  |  |  |  | $\leq 3 \mathrm{kTS}$ | $\leq 5 \mathrm{ft}$ | $\leq 11 \mathrm{SEC}$ |
|  | deEp layer | $\leq 4^{\circ} \mathrm{F}$ | $\leq 23^{\circ} \mathrm{F}$ | $\geq 90 \%$ | $\begin{gathered} \text { NO } \\ \text { SUNSHINE } \end{gathered}$ | TRANSITION | - | $\leq 8 \mathrm{kTS}$ | $\leq 9 \mathrm{ft}$ | $\leq 13 \mathrm{SEC}$ |
|  | SHALLOW LAYER |  |  |  |  |  |  | $\leq 5 \mathrm{KTS}$ | $\leq 8 \mathrm{ft}$ | $\leq 12 \mathrm{SEC}$ |
|  | DEEP LAYER | $\leq 4^{\circ} \mathrm{F}$ | $\leq 40^{\circ} \mathrm{F}$ | $\begin{aligned} & \geq 90 \% \\ & \text { HIGH: } \end{aligned}$ | $\begin{aligned} & \text { NO } \\ & \text { SUNSHINE } \end{aligned}$ | TRANSIT ! ON | - | $\leq 8 \mathrm{KTS}$ | $\leq 11 \mathrm{ft}$ | $\leq 12 \mathrm{SEC}$ |
|  | SHALLOW LAYER |  |  |  |  |  |  | $\leq 5 \mathrm{KTS}$ | $\leq 10 . \mathrm{ft}$ | $\leq 11 \mathrm{SEC}$ |
| 0 | DEEP LAYER | $\leq 4^{\circ} \mathrm{F}$ | $\leq 63^{\circ} \mathrm{F}$ | $\geq 90 \%$ | NO SUNSHINE | TRANSITION | - | $\leq 6 \mathrm{KTS}$ | $\leq 6$ frt | $\leq 12 \mathrm{SEC}$ |
|  | SHALLOW LAY:ER |  |  |  |  |  |  | $\leq 3 \mathrm{KTS}$ | $\leq 5 \mathrm{ft}$ | $\leq 11$ SEC |
| 'P | DEEP LAYER | $\leq 4^{\circ} \mathrm{F}$ | $\leq 57^{\circ} \mathrm{F}$ | $\begin{aligned} & \geq 90 \% \\ & \mathrm{HIGH} \end{aligned}$ | NO SUNSHINE | TRANSITION | $-$ | $\leq 6 \mathrm{kTS}$ | $\leq 6 \mathrm{ft}$ | $\leq 12 \mathrm{SEC}$ |
|  | SHALLOW LAYER |  |  |  |  |  |  | $\leq 3 \mathrm{KTS}$ | $\leq 5 \mathrm{ft}$ | $\leq 11$ SEC |

TABLE 3 - MOST PROBABLE WEATHER FEATURES OF THUNDERSTORMS

| LOCATION | $\begin{aligned} & \text { METEOROLOGICAL } \\ & \text { PERIOO } \\ & \end{aligned}$ | PRECIPITATIOA |  | PRESSURECENTER | $\begin{gathered} \text { LIGHTNING } \\ \text { ANO } \\ \text { THUNDER } \end{gathered}$ | CEILINGANOVISIBILITY | PRESSURE VARIATIONS IN THESTORM |  |  | WIND OIRECTIONS IN THE STORH |  |  | WAVE HEI GHT$\left(\tilde{s}_{w}\right) 1 / 3$ | MOOAL WAVE PERIOO |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Liquio | Statio |  |  |  | BEFORE | OURING | AFter | BEFORE | OURING |  |  |  |
| A | NIGHT ANO EARLY MORNING | LIKELY ${ }_{\text {+ }}^{+}$ | CHANC: ${ }^{*}$ | LOW | Líkely | POOR OVERCAST $\leq 2$ N.M. | FALLING | RISING | GRAOUAL RETURN TO NORMAL | FROM LANO BLOWING TOWARO THE SEA | VARY UP TO $180^{\circ}$ | $1 \geq 27$ KTS | $\geq 14 \mathrm{ft}$ | $\geq 12 \mathrm{SEC}$ |
| B | $\begin{aligned} & \text { NIGHT } \\ & \text { ANO } \\ & \text { EARLY } \\ & \text { MORNING } \end{aligned}$ | Likely | CHANC: | LOW | LI KELY | POOR OVERCAST $\leq 2$ N.M. | FALLING | RISING | GRAOUAL RETURN TO NORMAL | FROM LAFIO BLOWING TOWARO THE SEA | VARY <br> UP TO <br> $180^{\circ}$ | $\geq 30 \mathrm{KTS}$ | $\geq 14 \mathrm{ft}$ | $\geq 12 \mathrm{SEC}$ |
| c | NIGHT ANO EARLY MORNING | L. CELY | CHANCE | LOW | L.I KELY | POOR OVERCAST $\leq 2 \mathrm{~N} . \mathrm{M}_{.}$ | FALLING | RISING | GRAOUAL RETURN TO NORMAL | FROM LANO BLOWING. TOWARO THE SEA | $\begin{aligned} & \text { - VARY } \\ & \text { UP TO } \\ & 180^{\circ} \end{aligned}$ | $\geq 25 \mathrm{KTS}$ | $\geq 10 \mathrm{ft}$ | $\geq 7 \mathrm{SEC}$ |
| D | $\begin{aligned} & \text { NIGHTT } \\ & \text { ANO } \\ & \text { EARLY } \\ & \text { MORNING } \end{aligned}$ | LIKELY | CHANCE | LOW | LI'KELY | POOR OVERCAST $\leq 2 \mathrm{~N} \cdot \mathrm{M}$ | EALLING | RISING | GRADUAL RETURN TO NORMAL | FROM LANO BLOWING TOWARO THE SEA | VARY <br> UP TO <br> $180^{\circ}$ | $\geq 25 \mathrm{KTS}$ | $\geq 10 \mathrm{ft}$ | $\geq$ 7. SEC |
| E | NIGHT ANO EARLY MORNING | LI KELY | CHANCE | LOW | LIKELY | POOR OVERCAST $\leq 2 \cdot N . M_{.}$ | FALLING | RISING | GRAOUAL RETURE TO NORMAL | FROM LANO BLOWING TOWARO THE SEA | VARY UP TO $180^{\circ}$ | $\geq 20 \mathrm{KTS}$ | $\geq 7 \mathrm{ft}$ | $\geq 6 \mathrm{SEC}$ |
| F | $\begin{aligned} & \text { NIGHT } \\ & \text { ANO } \\ & \text { EARLY } \\ & \text { MORNING } \end{aligned}$ | LILKELY | Chance | LOW | L.IKEL. ${ }^{\text {P }}$ | POOR OVERCAST $\leq 2$ N.M. | falling | RISING | GRAOUAL RETURN TO NORMAL | FROM LANO BLOWING TOWARO THE SEA | VARY UP TO $180^{\circ}$ | $\geq 15 \mathrm{KTS}$ | $\geq 6 \mathrm{ft}$ | $\geq 6 \mathrm{SEC}$ |
| G | NIGHT ANO EARLY MORNING | L-I KELY | CHANCE | LOW | LI KELY | POOR OVERCAST $\leq 2$ N.M. | FALLING. | RISING | GRAOUAL RETURN TO NORMAL | FROM LANO BLOWING TOWARO THE SEA | VARY UP TO $180^{\circ}$ | $\geq 30 \mathrm{KTS}$ | $\geq 17 \mathrm{ft}$ | $\geq 14 \mathrm{SEC}$ |
| H | $\begin{aligned} & \text { NIGHT } \\ & \text { ANO } \\ & \text { EARLY } \\ & \text { MORNING } \end{aligned}$ | LI KELY | CHANCE | LOW | LIKELY | POOR OVERCAST $\leq 2$ N.M. | FALLING | RISING | $\begin{aligned} & \text { GRADUAL } \\ & \text { RETURN TO } \\ & \text { NORMAL } \end{aligned}$ | FROM LANO BLOWING TOWARO THE SEA | VARY <br> UP TO $180^{\circ}$ | $\geq 20 \mathrm{KTS}$ | $\geq 7 \mathrm{ft}$ | $\geq 6 \mathrm{SEC}$ |

TABLE 3 (Continued)

| LOCATION | METEOROLOGICALPEROIO | PRECIPITATION |  | PRESSURE CENTER | $\begin{aligned} & \text { LIGHTNING } \\ & \text { ANO } \\ & \text { THUNOER } \end{aligned}$ | $\begin{gathered} \text { CEILING } \\ \text { AND } \\ \text { VISIBILITY } \end{gathered}$ | PRESSURE VARIATIONS <br> IN THE STORM |  |  | WINO OIRECTIONS IN' THE STORM |  |  | WAVE HEIGHT$\left(\tilde{\zeta}_{w}\right) 1 j_{3}$ | MOOAL WAVE PERIOO |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | LIQUID | STATI $¢$ |  |  |  | BEFORE | OURING | AFter | BEFORE | OURING |  |  |  |
| 1 | $\begin{aligned} & \text { NIGHT } \\ & \text { ANO } \\ & \text { EARLY } \\ & \text { MORNING } \end{aligned}$ | LIMELY | CHANCS | LOW | L'tkely | POOR OVERCAST $\leq 2 \mathrm{~N} \cdot \mathrm{M}_{0}$ | FALLING | RISING | GRAOUAL RETURN TO NORMAL | FROM LȦNO BLOWING TOWARD THE SEA | VARY UP TO $180^{\circ}$ | $\geq 20 \mathrm{KTS}$ | $\geq 5 \mathrm{ft}$ | $\geq 5 \mathrm{SEC}$ |
| J | $\begin{gathered} \text { NIGHT } \\ \text { ANO } \\ \text { EARLY } \\ \text { MORNING } \end{gathered}$ | LI IKELY | CHANC: | LOW. | LIKELY | POOR OVERCAST $\leq 2$ N.M. | FALLING | RISING | GRAOUAL RETURN TO NORMAL | FROM LAND BLOWING TOWARO THE SEA | VARY UP TO $180^{\circ}$ | $\geq 27$ KTS | $\geq 13 \mathrm{ft}$ | $\geq 13 \mathrm{SEC}$ |
| - K | NIGHT ANO EARLY MORNING | LIMKELY | CHANCE | LOW | LİEELY | POOR OVERCAST $\leq 2$ N.M. | FALLING | RISING | GRAOUAL RETURN Td NORMAL | FROM LANO BLOWING TOWARO the sea | VARY <br> UP TO $180^{\circ}$ | $\geq 30 \mathrm{KTS}$ | $\geq 15 \mathrm{ft}$ | $\geq 13 \mathrm{SEC}$ |
| L | $\begin{aligned} & \text { NIGHTT } \\ & \text { ANO } \\ & \text { EARLY } \\ & \text { MORNING } \end{aligned}$ | LI KELY | CHANCE | LOW | Likély | POOR. OVERCAST $\leq 2$ N.M. | FALLING | RISING | $\begin{aligned} & \text { GRAOUAL } \\ & \text { RETURN T } \\ & \text { NORMAL } \end{aligned}$ | FROM 'LANO BLOWING TOWARO THE SEA | VARY UP TO $180^{\circ}$ | $\geq 20 \mathrm{KTS}$ | $\geq 7 \mathrm{ft}$ | $\geq 11 \mathrm{SEC}$ |
| M | $\begin{aligned} & \text { NIGHT } \\ & \text { ANO } \\ & \text { EARLY } \\ & \text { MORNING } \end{aligned}$ | LUKELY | CHANCE | LOW | LIKELY | POOR OVERCAST $\leq 2$ N.M. | FALLING | RISING | $\begin{gathered} \text { GRAOUAL } \\ \text { RETURN TO } \\ \text { NORMAL } \end{gathered}$ | FROM LANO BLOWING TOWARO THE SEA | VARY UP TO $180^{\circ}$ | $\geq 30 \mathrm{KTS}$ | $\geq 16 \mathrm{ft}$ | $\geq 13 \mathrm{SEC}$ |
| N | NIGHT ANO <br> EÄRLY <br> MORNING | LIMELY | CHANCE | E LOW | LIKELY | PODR OVERCAST $\leq 2$ N.M. | FALLING | RISING | GRAOUAL RETURN TC nORMAL | FROM LAND BLOWING TOWARO THE SEA | VARY <br> UP TO <br> $180^{\circ}$ | $\geq 30 \mathrm{KTS}$ | $\geq 16$ ft | $\geq 13 \mathrm{SEC}$ |
| 0 | $\begin{aligned} & \text { NIGHT } \\ & \text { ANO } \\ & \text { EARLY } \\ & \text { MORNING } \end{aligned}$ | LIKELY | CHANCE | E LOW | LIKELY | POOR OVERCAST $\leq 2 \text { N.M. }$ | FALLING | RISING | GRAOUAL return td NORMAL | FROM LAND BLOWING TOWARO THE SEA | VARY UP TO $180^{\circ}$ | $\geq 25 \mathrm{KTS}$ | $\geq 12 \mathrm{ft}$ | $\geq 12 \mathrm{SEC}$ |
| P | - NุIGHT ANO EARLY MORNING | LIKELY | CHANCE | E LOW | LIKELY | POOR OVERCAST: $\leq 2 \mathrm{~N} \cdot \mathrm{M}_{.}$ | FALLING | RISING | $\begin{gathered} \text { GRAOUAL } \\ \text { RETURN TO } \\ \text { NORMAL } \end{gathered}$ | FROM LAND BLOWING TOWARO THE SEA | VARY UP TO $180^{\circ}$ | $\geq 25 \mathrm{KTS}$ | $\geq 13 \mathrm{ft}$ | $\geq 12 \mathrm{SEC}$ |

table 4 - most probable weather features of icing

| LOCATION | AIR TEMPERATURE | $\begin{gathered} \text { SEA } \\ \text { TEMPERATURE } \end{gathered}$ | WIND SPEED | PRESSURE |
| :---: | :---: | :---: | :---: | :---: |
| A | $\leq 30^{\circ} \mathrm{F}$ | $\leq 37^{\circ} \mathrm{F}$ | $\geq 25 \mathrm{KTS}$ | REAR OF A LOW PRESSURE SYSTEM ON ITS POLEWARD SIDE |
| B | $\leq 32^{\circ} \mathrm{F}$ | $\leq 40^{\circ} \mathrm{F}$ | $\geq 27 \mathrm{KTS}$ | RẸAR OF A LOW PRESSURE SYSTEM ON ITS POLEWARD SIDE |
| D | $\leq 28^{\circ} \mathrm{F}$ | $\leq 40^{\circ} \mathrm{F}$ | $\geq 20 \mathrm{KTS}$ | REAR OF A LOW PRESSURE SYSTEM ON ITS POLEWARD SIDE |
| G | $\leq 28^{\circ} \mathrm{F}$ | $\leq 37^{\circ} \mathrm{F}$ | $\geq 27 \mathrm{KTS}$ | REAR OF A LOW PRESSURE SYSTEM ON ITS POLEEWARD SIDE |
| $J$ | $\leq 32^{\circ} \mathrm{F}$ | $\leq 40^{\circ} \mathrm{F}$ | $\geq 25 \mathrm{KTS}$ | REAR OF A LOW PRESSURE SYSTEM ON ITS POLEWARD SIDE |
| K | $\leq 32^{\circ} \mathrm{F}$ | $\leq 40^{\circ} \mathrm{F}$ | $\geq 27 \mathrm{KTS}$ | REAR OF A LOW PRESSURE SYSTEM ON ITS POLEWARD SIDE |
| M | $\leq 28^{\circ} \mathrm{F}$ | $\leq 35^{\circ} \mathrm{F}$ | $\geq 28 \mathrm{KTS}$ | REAR OF A LOW PRESSURE SYSTEM ON ITS POLEWARD SIDE |
| $N$ | $\leq 28^{\circ} \mathrm{F}$ | $\leq 40^{\circ} \mathrm{F}$ | $\geq 30 \mathrm{KTS}$ | REAR OF A LOW PRESSURE SYSTEM ON ITS POLEWARD SIDE |
| 0 | $\leq 32^{\circ} \mathrm{F}$ | $\leq 40^{\circ} \mathrm{F}$ | $\geq 22 \mathrm{KTS}$ | RĖAR OF. A LOW PRESSURE SYSTEM ON ITS POLEWARD SIDE |

TABLE 5 - MOST PROBABLE WEATHER FEATURES OF PRESSURE CENTERS

| LOCATION | PRESSURE CENTER | SEA LEvEL PRESSURE | I SOBARS | STORM | $\begin{aligned} & \text { CLOUD } \\ & \text { COVER } \end{aligned}$ | TEMPERATURE | FOG | PRECIPITATION | VISIBILITY | $\left\lvert\, \begin{gathered} \text { WIND } \\ \text { DIRECTION } \end{gathered}\right.$ | WIND SPEED | WAVE HEIGHT $\left(\tilde{S}_{\mathrm{W}}\right) 1 / 3$ | MODAL WAVE PERTOD |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| A | LOW | $\leq 10.13 \mathrm{mb}$ | CLOSELY <br> SPACED | CHANCE | $.6-.9$ <br> BROKEN | < $40^{\circ} \mathrm{F}$ | CHANCE | CHANCE | < 4 N.M. | COUNTER CLOCKWISE | $\geq 25 \mathrm{KTS}$ | $\geq 15 \mathrm{ft}$ | $\geq 13 \mathrm{SEC}$ |
|  | HIGH | > 1013mb | WIDELY <br> SPACED | RARE | .1 .- .5 <br> SCATTERED  | $\frac{\geq 40^{\circ} \mathrm{F}}{<40^{\circ} \mathrm{F}}$ | $\qquad$ RARE | RARE** | $\geq 4$ N.M. | CLOCKWISE | $\leq 15 \mathrm{KTS}$ | $\leq 10 \mathrm{ft}$ | $\leq 11 \mathrm{SEC}$ |
| B | LOW | $\leq 1013 \mathrm{mb}$ | $\begin{aligned} & \text { CLOSELY } \\ & \text { SPACED } \end{aligned}$ | CHANCE | $.6-.9$ <br> BROKEN | $<45 \mathrm{~F}$ | CHANCE | CHANCE | $<5 \text { N.M. }$ | COUNTER CLOCKWISE | $\geq 27 \mathrm{KTS}$ | $\geq 15 \mathrm{ft}$ | $\geq 13$ SEC |
|  | HIGH | > 1013 mb | WIDELY SPACED | RARE | $\left\|\begin{array}{cc} .1-5 \\ \text { SCATTERED } \end{array}\right\|$ | $\frac{\geq 45^{\circ} \mathrm{F}}{<45^{\circ} \mathrm{F}}$ | CHANCE | 'RARE | $\geq 5 \mathrm{~N} . \mathrm{M}$. | CLOCKWISE | $\leq 17 \mathrm{KTS}$ | $\leq 10 \mathrm{ft}$ | $\leq 11 \mathrm{SEC}$ |
| : C | LOW | $\leq 1013 \mathrm{mb}$ | Closely SPACED | CHANCE | $.6-.9$ <br> BROKEN | $<60^{\circ} \mathrm{F}$ | CHANCE | CHANCE | $<6$ N.M. | COUNTER CLOCKWISE | $\geq 15 \mathrm{kTS}$ | $\geq 8 \mathrm{ft}$ | $\geq 6 \mathrm{SEC}$ |
|  | HIGH. | > 1013 mb | WIDELY <br> SPACED | RARE | $\left\lvert\, \begin{gathered} .1-.5 \\ \text { SCATTERED } \end{gathered}\right.$ | $\frac{\geq 60^{\circ} F}{<60^{\circ} F}$ | CHANCE <br> RARE | ,RARE | $\geq 6 \mathrm{~N} . \mathrm{M}$. | CLOCKWISE | $\leq 10 \mathrm{KTS}$ | $\leq 6 \mathrm{ft}$ | $\leq 5$ SEC |
| - D | LOW | $\leq 1013 \mathrm{mb}$ | CLOSELY <br> SPACED | CHANCE | $\begin{aligned} & .6-.9 \\ & \text { BROKEN } \end{aligned}$ | $<50^{\circ} \mathrm{F}$ | CHANCE | CHANCE | $<6$ N.M. | COUNTER CLOCKWISE | $\geq 20 \mathrm{KTS}$ | $\geq 9 \mathrm{ft}$ | $\geq 7 \mathrm{SEC}$ |
|  | HIGH | > 1013mb | WIDELY <br> SPACED | RARE | $\begin{gathered} .1-.5 \\ \text { SCATTERED } \end{gathered}$ | $\frac{\geq 50^{\circ} \mathrm{F}}{<50^{\circ} \mathrm{F}}$ | CHANCE <br> RARE | RARE | $\geq 6 \mathrm{~N} . \mathrm{M}$. | CLOCKWISE | $\leq 12 \mathrm{KTS}$ | $\leq 6 \mathrm{ft}$ | $\leq 5 \mathrm{SEC}$ |

* RARE - < $10 \%$ OF OCCURENCES
TABLE 5 (Continued)

| LOCATION | PRESSURE CENTER | SEA LEVEL PRESSURE | ISOBARS | STORM | $\begin{aligned} & \text { CLOUD } \\ & \text { COVER } \end{aligned}$ | TEMPERATURE | FOG | PRECIPITATION | VISIBILITY | WIND DIRECTION | $\begin{aligned} & \text { WINB } \\ & \text { SPEED } \end{aligned}$ | WAVE HEIGHT $\left(\tilde{S}_{\text {wis }}\right) 1 / 3$ | MODAL WAVE PERIOD |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| E | LOW | $\leq 1013 \mathrm{mb}$ | CLOSELY SPACED | CHANCE | $\begin{aligned} & .6-.9 \\ & \text { BPOKEN } \end{aligned}$ | $<85^{\circ} \mathrm{F}$ | CHANCE | CHANCE | $\leqslant 5$ N.M. | COUNTER CLOCKWISE | $\geq 17 \mathrm{KTS}$ | $\geq 6 \mathrm{ft}$ | $\geq 5 \mathrm{SEC}$ |
|  | HIGH | > 1013 mb | WIDELY SPACED | RARE | $\left\lvert\, \begin{array}{r} .1-.5 \\ \text { SCATTERED } \end{array}\right.$ | $\frac{\geq 85^{\circ} \mathrm{F}}{<85^{\circ} \mathrm{F}}$ | $\frac{\text { CHANCE }}{\text { RARE. }}$ | RARE | $\geq 5$ N.M. | CLOCKWISE | $\leq 8 \mathrm{KTS}$ | $\leq 4 \mathrm{ft}$ | $\leq 5 \mathrm{SEC}$ |
| $\mathbf{F}$ | LOW | $\leq 1013 \mathrm{mb}$ | ClOSELY <br> SPACED | CHANCE | $.6-.9$ <br> BROKEN | $<78^{\circ} \mathrm{F}$ | CHANCE | CHANCE | < 5 N.M. | $\left\|\begin{array}{c} \text { COUNTER } \\ \text { CLOCKW!SE } \end{array}\right\|$ | $\geq 10 \mathrm{KTS}$ | $\geq 5 \mathrm{ft}$ | $\geq 5 \mathrm{SEC}$ |
|  | HIGH | > 1013mb | WI DELY <br> SPACED | RARE | $\begin{gathered} .1-.5 \\ \text { SCATTERED } \end{gathered}$ | $\frac{\geq 78^{\circ} \mathrm{F}}{<78^{\circ} \mathrm{F}}$ | CHANCE <br> RARE | RARE | $\geq 5 \mathrm{~N} . \mathrm{M}$. | CLOCKWISE | $\leq 3 \mathrm{KTS}$ | $<2 \mathrm{ft}$ | < 5 SEC |
| $\therefore-G$ | LOW | $\leq 1013 \mathrm{mb}$ | CLOSELY <br> SPACED | CHANCE | $.6-.9$ <br> BROKEN | $<36{ }^{\circ} \mathrm{F}$ | CHANCE | CHANCE | < 4 N.M. | $\left\lvert\, \begin{gathered} \text { COUHTTER } \\ \text { CLOCKWISE } \end{gathered}\right.$ | $\geq 27 \mathrm{KTS}$ | $\geq 16 \mathrm{ft}$ | $\geq 14 . S E C$ |
|  | HIGH | > 1013 mb . | WI DELY <br> SPACED | ;RARE | $\begin{aligned} & .1-.5 \\ & \text { SCATTERED } \end{aligned}$ | $\geq 36^{\circ} \mathrm{F}$ $<36^{\circ} \mathrm{F}$ | CHANCE <br> RARE | RARE | $\geq 4$ N.M. | CLOCKWISE | $\leq 17 \mathrm{KTS}$ | $\leq 14 \mathrm{ft}$ | $\leq 13 \mathrm{SEC}$ |
| - H. | LOW | $\leq 1013 \mathrm{mb}$ | cLosely <br> SPACED: | CHANCE | $\text { . } 6-6$ <br> BROKEN | $<77^{\circ} \mathrm{F}$ | CHANCE | CHANCE | $<5$ N.M. | COUNTER CLOCKWISE | $\geq 18 \mathrm{KTS}$ | $\geq 7 \mathrm{ft}$ | $\geq 6 \mathrm{SEC}$ |
|  | High | > 1013 mb | WIDELY <br> SPACED | RARE | $\begin{array}{r} \because 1-.5 \\ \text { SCATTERE } \end{array}$ | $\geq 77^{\circ} \mathrm{F}$ $<77^{\circ} \mathrm{F}$ | Chance <br> RARE | RARE | $\geq 5$ N.M. | CLOCKWISE | $\leq 8 . \mathrm{kTS}$ | $\leq 4 \mathrm{ft}$ | $\leq 5 \mathrm{SEC}$ |

TABLE 5 (Conitinued)

| LLOCATION | PRESSURE CENTER | SEA LEvel PRESSURE | I SOBARS | STORM | $\begin{aligned} & \text { CLOUD } \\ & \text { COVER } \end{aligned}$ | TEMPERATURE | FOG | Precipitation | VISIBILITY | $\begin{array}{\|c\|} \text { WIND } \\ \text { DIRECTION } \end{array}$ | WIND SPEED | WAVE HEIGHT $\left(s_{w}\right) 1 / 3$ | MODAL WAVE PERIOD |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | LOW | $\leq 1013 \mathrm{mb}$ | CLOSELY <br> SPACED | CHANCE | $.6-.9$ BROKEN | $<80^{\circ} \mathrm{F}$ | CHANCE | CHANCE | < 5 N.M. | COUNTER CLOCKWISE | $\geq 15 \mathrm{KTS}$ | $\geq 4 \mathrm{ft}$ | $\geq 5 \mathrm{SEC}$ |
|  | HIGH | > 1013 mb | WIDELY <br> SPACED | RARE | $\left\lvert\, \begin{gathered} .1-.5 \\ \text { SCATTERED } \end{gathered}\right.$ | $\frac{\geq 80^{\circ} \mathrm{F}}{<80^{\circ} \mathrm{F}}$ | CHANCE <br> RARE | RARE | $\geq 5 \mathrm{~N} . \mathrm{M}$ | CLOCKWISE | $\leq 6 \mathrm{KTS}$ | $\leq 2 \mathrm{ft}$ | $\leq 4 \mathrm{SEC}$ |
| J | LOH | $\leq 1013 \mathrm{mb}$ | $\begin{aligned} & \text { CLOSELY } \\ & \text { SPACED } \end{aligned}$ | CHANCE | $.6-.9$ <br> BROKEN | $<57^{\circ} \mathrm{F}$ | CHANCE | CHANCE. | < 6 N.M. | COUNTER CLOCKWISE | $\geq 25 \mathrm{KTS}$ | $\geq 15 \mathrm{ft}$ | $\geq 14 \mathrm{SEC}$ |
|  | HIGH | > 1013 mb | WIDELY SPACED | RARE | $\begin{gathered} .1-.5 \\ \text { SCATTERED } \end{gathered}$ | $\geq 57^{\circ} \mathrm{F}$ | Chance |  | $\geq 6$ N.M. | CLOCEWISE | $\leq 15 \mathrm{KTS}$ | $\leq 12 \mathrm{ft}$ | $\leq 13 \mathrm{SEC}$ |
|  |  |  |  |  |  | $<57^{\circ} \mathrm{F}$ | RARE |  |  |  |  |  |  |
| K | LOW | $\leq 1013 \mathrm{mb}$ | CLOSELY <br> SPACED | CHANCE | $\begin{aligned} & .6-.9 \\ & \text { BROKEN } \end{aligned}$ | $<42^{\circ} \mathrm{F}$ | CHANCE | CHANCE | < 5 N.M. | COUNTER CLOCKWISE | $\geq 27 \mathrm{KTS}$ | $\geq 15 \mathrm{ft}$ | $\geq 13 \mathrm{SEC}$ |
|  | HIGH | > 1013mb | WIDELY <br> SPACED | RARE | $\begin{gathered} .1-.5 \\ \text { SCATTERED } \end{gathered}$ | $\frac{\geq 42^{\circ} \mathrm{F}}{<42^{\circ} \mathrm{F}}$ | CHANCE <br> RARE | RARE | $\geq 5$ H.M. | CLOCKWISE | $\leq 17 \mathrm{KTS}$ | $\leq 12 \mathrm{ft}$ | $\leq 12 \mathrm{SEC}$ |
| - L | LOW | $\leq 1013 \mathrm{mb}$ | CLOSELY SPACED | CHANCE | $\begin{aligned} & .6-.9 \\ & \text { BROKEN } \end{aligned}$ | $<72{ }^{\circ} \mathrm{F}$ | C.HANCE | CHANCE | $<6$ N.M. | COUNTER CLOCKWISE | $\geq 17 \mathrm{KTS}$ | $\geq 7 \mathrm{ft}$ | $\geq 12 \mathrm{SEC}$ |
|  | HIGH | $>1013 \mathrm{mb}$ | WIDELY SPACED | RARE | $\text { . } 1-.5$ <br> SCATTERED | $\geq 72^{\circ} \mathrm{F}$ <br> < $72^{\circ} \mathrm{F}$ | CHANCE | RARE | $\geq 6$ N.M. | CLOCKWISE | $\leq 8 \mathrm{kTS}$ | $\leq 6^{\prime \mathrm{ft}}$ | $\leq 12 \text { SEC }$ |

TABLE 5 (Continued)

| LOCATION | PRESSURE CENTER | SEA Leyel PRESSURE | ISOBARS | STORM | $\begin{aligned} & \text { CLOUD } \\ & \text { COVER } \end{aligned}$ | TEMPERATURE | F06 | PRECIPITATION | VISIBILITY | WIHD DI.RECTION | WIND SPEED | WAVE HE I GHT $\left(\tilde{r}_{W}\right) 1 / 3$ | MODAL WAVE <br> PERIOD |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| M | LOW | $\leq 1013 \mathrm{mb}$ | CLOSELY SPACED | CHANCE | $.6-.9$ <br> BROKEN | $<25^{\circ} \mathrm{F}$ | CHANCE | Chance | < 2 N.M. | $\begin{gathered} \text { COUNTER } \\ \text { CLOCKWISE } \end{gathered}$ | $\geq 28 \mathrm{KTS}$ | $\geq 16 \mathrm{ft}$ | $\geq 14 \mathrm{SEC}$ |
|  | - IMIGH | > 1013 mb | WIDELY | RARE | . 1 - . 5 | $\geq 25^{\circ} \mathrm{F}$ | CHANCE | RARE | $\geq 2$ N.M. | CLOCKWISE | $\leq 18 \mathrm{KTS}$ | $\leq 13 \mathrm{ft}$ | $\leq 13 \mathrm{SEC}$ |
|  |  |  |  |  |  | $<25^{\circ} \mathrm{F}$ | RARE |  |  |  |  |  |  |
| $N$ | LOW | $\leq 1013 \mathrm{mb}$ | $\begin{aligned} & \text { CLOSELY } \\ & \text { SPACED } \end{aligned}$ | CHANCE | $.6-.9$ <br> BROKEN | $<40^{\circ} \mathrm{F}$ | CHANCE | CHANCE | < 6 N.M. | $\left\|\begin{array}{c} \text { COUNTER } \\ \text { CLOCKWISE } \end{array}\right\|$ | $\geq 30 \mathrm{KTS}$ | $\geq 17 \mathrm{ft}$ | $\geq 13 \mathrm{SEC}$ |
|  | HIGH | > 10 f 3 mb | WI DELY | RARE | $\left\|\begin{array}{cc} .1-.5 \\ \text { SCATTERED } \end{array}\right\|$ | $\geq 40^{\circ} \mathrm{F}$ | CHANCE | RARE | $\geq 6 \mathrm{~N} . \mathrm{M}_{\text {. }}$ | CLOCLWIISE | $\leq 20 \mathrm{KTS}$ | $\leq 13 \mathrm{ft}$ | $<13$ SEC |
|  |  |  |  |  |  | $<40^{\circ} \mathrm{F}$ | RARE |  |  |  |  |  |  |
| 0 | LOW | $\leq 1013 \mathrm{mb}$ | $\begin{aligned} & \text { CLOSELYY } \\ & \text { SPACED } \end{aligned}$ | CHANCE | $.6-.9$ <br> BROKEN | $<64^{\circ} \mathrm{F}$ | CHANCE | CHANCE | < 7 N.M. | $\left\|\begin{array}{c} \text { COUNTTER } \\ \text { CLOCKWISE } \end{array}\right\|$ | $\geq 22 \mathrm{KTS}$ | $\geq 12 \mathrm{ft}$ | $\geq 12 \mathrm{SEC}$ |
|  | HiGH | > 1013mb | WIDELY. SPACED | 'RARE | $\begin{gathered} .1 \cdots .5 \\ \text { SCATTERED } \end{gathered}$ | $\geq 64^{\circ} \mathrm{F}$ | Chance | RARE | $\geq 7$ N.M. | CLOCKWISE | $\leq 12 \mathrm{KTS}$ | $\leq 10 \mathrm{ft}$ | < 12 SEC |
|  |  |  |  |  |  | $<64{ }^{\circ} \mathrm{F}$ | RARE |  |  |  |  |  |  |
|  | LOW | $\leq 1013 \mathrm{mb}$ | Closely <br> SPACED | CHANCE | $.6-.9$ <br> BROKEN | $<58^{\circ} \mathrm{F}$ | CHANCE | CHANCE | < 9 N.M. | COUNTER CLOCKWISE | $\geq 22 \mathrm{KTS}$ | $\geq 8 \mathrm{ft}$ | $\geq 12 \mathrm{SEC}$ |
|  | HIGH | > 1013 mb | WIDELY <br> SPACED | RARE | $\begin{array}{r} .1-.5 \\ \text { SCATTERED } \end{array}$ | $\begin{aligned} & \geq 58^{\circ} \mathrm{F} \\ & <58^{\circ} \mathrm{F} \end{aligned}$ | CHANCE <br> RARE | R4ise | $\geq 9$ N.M. | CLOCKWISE | $\leq 12 \mathrm{KTS}$ | $\leq 7 \mathrm{ft}$ | < 12 SEC |

TABLE 6 - MOST PROBABLE WEATHER FEATURES OF REFRACTIVITY

| LOCATION | REFRACTIVITY | METEOROLOG:I CAL PERIOD | RELATIVE HUMIDITY | PRESSURE CENTER | TEMPERATURE VARIATION | FOG | AREA. | $\begin{aligned} & \text { WIND } \\ & \text { DIRECTION } \end{aligned}$ | WIND SPEGED | WAVE HEIGHT $\left(\tilde{s}_{w}\right) 1 / 3$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| ALL | SuB REFRACTION | EVENING TRANSIT.ION | $\begin{aligned} & \text { INCREASING } \\ & \text { WITH } \\ & \text { HEIGHT } \end{aligned}$ | - | COLD AIR OVER WARM SURFACE | RARE |  | SEA OR LAND BREEZE | - | - | - |
| A | SUPER REFRACTION OR DUCT | MORIIING <br> TRANSITION TO AFTERNOON | $\begin{aligned} & \text { DECREASING } \\ & \text { WITH. } \\ & \text { HEIGHT } \end{aligned}$ | [HIGH | WARM AIR OVER COLD SURFACE | RARE | COAS TAL AREAS | $\begin{aligned} & \text { SEA OR } \\ & \text { LAND } \\ & \text { BREEEZE } \end{aligned}$ | $\geq 25 \mathrm{KTS}$ | $\geq 13 \mathrm{ft}$ | $\geq 11 \mathrm{SEC}$ |
| B | SUPER REFRACTION OR DUCT | MORNING TRANSITION TO AFTERNOON | $\begin{aligned} & \text { DECREASING } \\ & \text { WITH } \\ & \text { HEIGHT } \end{aligned}$ | HIGH : | WARM AIIR OVER COLD SURFACE | RARE | COASTAL AREAS | $\begin{aligned} & \text { SEA OR } \\ & \text { LAND } \\ & \text { BREEZE } \end{aligned}$ | $\geq 27 \mathrm{KTS}$ | $\geq 13 \mathrm{ft}$ | $\geq 11 \mathrm{SEC}$ |
| C | SUPER REFRACTION OR DUCT | MORNING TRANSITION TO AFTERNOON | $\begin{gathered} \text { DECREAS ING } \\ \text { WITH } \\ \text { HEIGHT } \end{gathered}$ | HIGH | WARM AIR OVER COLL SURFACE | RARE | CUASTAL AREAS | SEA OR LAND BREEZE | $\geq 15 \mathrm{KTS}$ | $\geq 8 \mathrm{ft}$ | $\geq 6 \mathrm{SEC}$ |
| D | SUPER REFRACTION OR DUCT | MORNIING TRANSITION TO AFTERNOON | $\begin{array}{\|l} \text { DECREASING } \\ \text { W.ITH } \\ \text { HEIGHT: } \end{array}$ | HIGH | WARM AIR OVER COLD SURFACE | RARE | COASTAL AREAS | $\begin{aligned} & \text { SEA OR } \\ & \text { LAND } \\ & \text { BREEZE } \end{aligned}$ | $\geq 20 \mathrm{KTS}$ | $\geq 9 \mathrm{ft}$ | $\geq 6 \mathrm{SEC}$ |
| E | SUPER REFRACTION OR DUCT | MORNING TRANSITION TO AFTERNOON | $\begin{aligned} & \text { DECREASING } \\ & \text { WITH } \\ & \text { HEIGHT } \end{aligned}$ | HIGH | WARM AIR OVER COLD SURFACE | RARE | COASTAL AREAS | $\begin{aligned} & \text { SEA OR } \\ & \text { LAND } \\ & \text { BREEZE } \end{aligned}$ | $\geq 17 \mathrm{KTS}$ | $\geq 6 \mathrm{ft}$ | $\geq 5 \mathrm{SEC}$ |
| F | SUPER REFRACTION OR DUCT | $\begin{gathered} \text { MORNING } \\ \text { TRANSITION } \\ \text { TO } \\ \text { AFTERNDON } \end{gathered}$ | $\begin{gathered} \text { DECREAS ING } \\ \text { WITH } \\ \text { HEIGHT } \end{gathered}$ | HIGH | WARM AIR OVER COLD SURFACE | RARE | COASTAL AREAS | $\begin{aligned} & \text { SEA OR } \\ & \text { LAND } \\ & \text { BREEZE } \end{aligned}$ | $\geq 12 \mathrm{KTS}$ | $\geq 6 \mathrm{ft}$ | $\geq 6 \mathrm{SEC}$ |
| G | SUPER REFRACTION OR DUCT | $\begin{gathered} \text { MORHING } \\ \text { TRANSITION } \\ \text { TO } \\ \text { AFTERNOON } \end{gathered}$ | $\begin{gathered} \text { DECREASING } \\ \text { WITH } \\ \text { HEIGHT } \end{gathered}$ | HIGH | WARM AIR OVER COLD SURFACE | RARE | COASTAL AREAS | SEA OR LAND BREEZE | $\geq 27 \mathrm{KTS}$ | $\geq 16 \mathrm{ft}$ | $\geq 14 \mathrm{SEC}$ |
| : H | SUPER REFRACTION OR DUCT | MORNING TRANSITITON AFTERNOON | $\begin{aligned} & \text { DECREASING } \\ & \text { WITH } \\ & \text { HEIGHT } \end{aligned}$ | HIGH | WARM AIR OVER COLO SURFACE | RARE | COASTAL AREAS | SEA OR LAND BREEZE | $\geq 18 \mathrm{KTS}$ | $\geq 7 \mathrm{ft}$ | $\geq 6 \mathrm{SEC}$ |

TABLE 6 (Continued)

| LOCATION | REFRACTIVITY | METEOROLOGICAL PERIOD | RELATiVE HUMIDITY | PRESSURE CENTER | TEMPERATURE VARIATION | FOG | AREA | WIND DIRECTION | WIND SPEED | WAVE HEIGHT $\left(c_{w}\right) 1 / 3$ | MODAL WAVE PERIOD |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| ALL | $\begin{gathered} \text { SUB } \\ \text { REFRACT.ION } \end{gathered}$ | EVENIHG TRANSITION | $\begin{aligned} & \text { INCREAS ING } \\ & \text { WITH } \\ & \text { HEIGHT } \end{aligned}$ | - | COLD AIR OVER WARY SURFACE | RARE | - | $\begin{aligned} & \text { SEA OR } \\ & \text { LAND } \\ & \text { BREEZE } \end{aligned}$ | - | - | - |
| I | SUPER REFACTION OR DUCT | $\begin{gathered} \text { MORNING } \\ \text { TRANSITION } \\ \text { TO } \\ \text { AFTERNOON } \end{gathered}$ | $\begin{aligned} & \text { DECREAS ING } \\ & \text { WITH } \\ & \text { HEIGHT } \end{aligned}$ | HIGH | WARM AIIR OVER COLD SURFACE | RARE | COASTAL AREAS | SEA OR LAND BREEZE | $\geq 15 \mathrm{KTS}$ | $\geq 4 \mathrm{ft}$ | $\geq 5 \mathrm{SEC}$ |
| J | SUPER REFACTION OR DUCT | MORNING TRANSIITION TO AFTERNOON | $\begin{aligned} & \text { DECREASING } \\ & \text { WITH } \\ & \text { HEIGHT } \end{aligned}$ | HIGH | WARM AIIR OVER COLD SURFACE | RARE | COASTAL AREAS | SEA OR LAND BREEZE | $\geq 25$ KTS | $\geq 12 \mathrm{ft}$ | $\geq 12 \mathrm{SEC}$ |
| K | SUPER REFACTION OR DUCT | MORNING TRANSITION TO AFTERNOON | $\begin{gathered} \text { DECREAS ING } \\ \text { WI TH } \\ \text { HEI GHT } \end{gathered}$ | HIGH | WARM AIR OVER COLD SURFACE | RARE | COASTAL AREAS | SEA OR LAND BREEZE | $\geq 27 \mathrm{KTS}$ | $\geq 14 \mathrm{ft}$ | $\geq 12 \mathrm{SEC}$ |
| L | $\begin{aligned} & \text { SUPER } \\ & \text { REFACTION } \\ & \text { OR DUCT } \end{aligned}$ | MORNING TRANSITION to. AFTERNOON | $\begin{aligned} & \text { DECREAS ING } \\ & \text { WI TH } \\ & \text { HEI GHT } \end{aligned}$ | HIGH | WARM AIR OVER COLD SURFACE | RARE | COASTAL AREAS | SEA OR LAND BREEZE | $\geq 17 \mathrm{KTS}$ | $\geq 6 \mathrm{ft}$ | $\geq 10 \mathrm{SEC}$ |
| M | SUPER REFACTION OR DUCT | MORNING TRANSITION TO AFTERNOON | $\begin{aligned} & \text { DECREASING } \\ & \text { WITH } \\ & \text { HEIGHT } \end{aligned}$ | HIGH | WARM AIR OVER COLD SURFACE | RARE | COASTAL AREAS | SEA OR LAND BREEZE | $\geq 27$ KTS | $\geq 15 \mathrm{ft}$ | $\geq 12 \mathrm{SEC}$ |
| .N | SUPER REFACTION OR DUCT | $\begin{gathered} \text { MORNING } \\ \text { TRANSITION } \\ \text { TO } \\ \text { AFTERNOON } \end{gathered}$ | $\begin{aligned} & \text { DECREASING } \\ & \text { WITH } \\ & \text { HEIGHT } \end{aligned}$ | HIGH | WARM AIR OVER COLD SURFACE | RARE | COASTAL AREAS | SEA OR LAND BREEZE | $\geq 27 \mathrm{KTS}$ | $\geq 15 \mathrm{ft}$ | $\geq 12 \mathrm{SEC}$ |
| 0 | SUPER REFACTION OR DUCT | MORNING TRANSITION T0 AFTERNOON | $\begin{aligned} & \text { DECREASING } \\ & \text { WITH } \\ & \text { HEIGHT } \end{aligned}$ | HICH | WARM AIIR OVER COL'D SURFACE | RARE | COASTAL AREAS | SEA OR LAND BREEZE | $\geq 22 \mathrm{KTS}$ | $\geq 11 \mathrm{ft}$ | $\geq 12 \mathrm{SEC}$ |
| P | SUPER REFACTION OR DUCT | $\begin{gathered} \text { MORNING } \\ \text { TRANSITION } \\ \text { TO } \\ \text { AFTERNOON } \end{gathered}$ | $\begin{aligned} & \text { DECREASING } \\ & \text { WITH } \\ & \text { HEIGHT } \end{aligned}$ | HIGH | WARM AIR OVER COLD SURFACE | RARE | COASTAL AREAS | SEA OR LAND BREEZE | $\geq 22 \mathrm{KTS}$ | $\geq 12 \mathrm{ft}$ | $\geq 12 \mathrm{SEC}$ |

TABLE 7 - MOST PROBABLE WEATHER FEATURES OF AIR MASSES

| LOCATION. | FRONT | THUNDERSTORM | relative HUMIDITY | visibility | PRESSURE CENTER | FOG | WIND SPEED | WAVE HEIGHT $\left(r_{w}\right) 1 / 3$ | MODAL WAVE PERIOD |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | COLD | - chance | $\leq 83 \%$ | > 6 N.M. | LOW | RARE | $\geq 25 \mathrm{KTS}$ | $\geq 15 \mathrm{ft}$ | $\geq 13 \mathrm{SEC}$ |
|  | WARM' | RARE | $\geq 88 \%$ | $\leq 6$ N.M. | LOW | Chance | $\leq 15 \mathrm{KTS}$ | $\leq 10 \mathrm{ft}$ | $\leq 11 \mathrm{SEC}$ |
|  | COLD | Chance | $\leq 75 \%$ | > $6 \mathrm{~N} . \mathrm{M}$. | LOW | RARE | $\geq 27 \mathrm{KTS}$ | $\geq 15 \mathrm{ft}$ | $\geq 13 \mathrm{SEC}$ |
|  | WARM | RARE | $\geq 82 \%$ | $\leq 6$ N.M. | LOW. | CHANCE | $\leq 17 \mathrm{KTS}$ | $\leq 10 \mathrm{ft}$ | $\leq 11 \mathrm{SEC}$ |
|  | COLD | CHANCE | $\leq 70 \%$ | > 7 N.M. | LOW | RARE | $\geq 15 \mathrm{KTS}$ | $\geq 7 \mathrm{ft}$ | $\geq 6 \mathrm{SEC}$ |
|  | WARM | RARE | $\geq 75 \%$ | $\leq 7$ M.M. | LOW | Chance. | $\leq 10 \mathrm{KTS}$ | $\leq 5 \mathrm{ft}$ | $\leq 5 \mathrm{SEC}$ |
|  | COLD | CHANCE | $\leq 65 \%$ | $\geqslant 6$ N.M. | LOW | rare | $\geq 20 \mathrm{kTS}$ | $\geq 9 \mathrm{ft}$ | $\geq 7 \mathrm{SEC}$ |
|  | WARM | RARE | $\geq 72 \%$ | $\leq 6$ N.M. | LOW | CHANCE | $\leq 12 \mathrm{KTS}$ | $\leq 6 \mathrm{ft}$ | $\leq 5 \mathrm{SEC}$ |

TABLE 7 (Cont inued)

| LOCATION | FRONT | THUNDERSTORM | RELATIVE HUMIDITY | VISIBILITY | PRESSURE CENTER | FOG | WIND SPEED | WAVE HE IGHT $\left(\bar{x}_{w}\right) 1 / 3$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| - E | COLD | CHANCE | $\leq 75 \%$ | > 6 N.M. | LOW | RARE | $\geq 17 \mathrm{krs}$ | $\geq 6 \mathrm{ft}$ | $\geq 5 \mathrm{SEC}$ |
|  | WARM | RARE | $\geq 80 \%$ | $\leq 6$ N.M. | LOW | CHANCE | $\leq 8 \mathrm{KTS}$ | $\leq 4 \mathrm{ft}$ | $<5$ SEC |
| ${ }^{\prime} \mathbf{F}$ | COLD | CHANCE | $\leq 83 \%$ | > 6 N.M | LOW | RARE | $\geq 10 \mathrm{KTS}$ | $\geq 5 \mathrm{ft}$ | $\geq 5 \mathrm{SEC}$ |
|  | WARM | RARE | $\geq 88 \%$ | $\leq 6$ N.M. | LOW | CHANCE | $\leq 3 \mathrm{KTS}$ | $<3 \mathrm{ft}$ | < 5 SEC |
| G | COLD | CHANCE | $\pm 82 \%$ | > 5 N.M. | LOW | RARE | $\geq 27 \mathrm{KTS}$ | $\geq 16 \mathrm{ft}$ | $\geq 14 \mathrm{SEC}$ |
|  | WARM | RARE | $\geq 88 \%$ | $\leq 5$ N.M. | LOW | CHANCE | $\leq 17 \mathrm{KTS}$ | $\leq 14 \mathrm{ft}$ | $\leq 13 \mathrm{SEC}$ |
| H | COLD | CHANCE | $\leq 73 \%$ | $>5$ N.M. | LOW | RARE | $\geq 18 \mathrm{krs}$ | $\geq 7 \mathrm{ft}$ | $\geq 6$ SEC |
|  | WARM | RARE | $\geq 78 \%$ | $\leq 5$ N.M. | LOW | CHANCE | $\leq 8 \mathrm{KTS}$ | $\leq 4 \mathrm{ft}$ | $\leq 5 \mathrm{SEC}$ |
|  |  |  |  |  |  |  |  |  |  |

TABLE 7 (Continued)
LOCATION
TABLE 7 (Continued)


TABLE 8 - CORRECTION FACTORS FOR SIGNIFICANT WAVE HEIGHTS PRODUCED BY DIFFERENT WIND SPEEDS BLOWING FOR VARIOUS LENGTHS OF TIME

|  | DURATION (HOURS) |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 5 | 10 | 15 | 20 | 30 | 40 | 50 |
| 10 | 1 | 1 | 1 | 1 | 1 | 1 | 1. |
| 15 | 1 | 1 | 1.2 | 1.2 | 1.2 | 1.2 | 1.2 |
| 20 | 1 | 1.25 | 1.4 | 1.4 | 1.5 | 1.5 | 1.5 |
| 30 | 1 | 1.3 | 1.4 | 1.5 | 1.6 | 1.6 | 1.6 |
| 40 | 1 | 1.3 | 1.4 | 1.6 | 1.7 | 1.7 | 1.7 |
| 50 | 1 | 1.3 | 1.5 | 1.6 | 1.7 | 1.8 | 1.8 |
| 60 | 1 | 1.4 | 1.5 | 1.7 | 1.8 | 1.8 | 2 |

TABLE 9 -. MOST PROBABLE SIGNIFICANT WAVE HEIGHT AND MODAL PERIOD BY WIND SPEED

|  | OCATION | A |  | B |  | c |  | D |  | $E$ |  | $F$ |  | G |  | H |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| WITHD SPEED (KTS) | MAX Wave HEIGHT (f.t) | $\left(\tilde{\tau}_{W}\right) 1 / 3$ <br> (ft) | $\begin{gathered} \text { MODAL } \\ \text { PERIOD } \\ \text { (SEC) } \end{gathered}$ | $\begin{aligned} & \left(\tilde{u}_{w}\right) 1 / 3 \\ & (f t) \end{aligned}$ | $\begin{array}{\|c} \text { MODAL } \\ \text { PERIOD } \\ \text { (SEC) } \end{array}$ | $\begin{aligned} & \left(\tilde{s}_{w}\right) 1 / 3 \\ & (f t) \end{aligned}$ | MODAL PERIOD (SEC) | $\begin{aligned} & \left(\tilde{r}_{w}\right) 1 / 3 \\ & (f t) \end{aligned}$ | MODAL PERIOD (SEC) | $\begin{aligned} & \left(\tilde{r}_{w}\right) 1 / 3 \\ & (f t) \end{aligned}$ | MODAL PERIOD (SEC) | $\begin{aligned} & \left(\tilde{\zeta}_{w}\right) 1 / 3 \\ & (f t) \end{aligned}$ | MODAL PERIOD (SEC) | $\begin{aligned} & \left(\tilde{c}_{w}\right) 1 / 3 \\ & \left(f_{t}\right) \end{aligned}$ | $\begin{array}{r} \text { MODAL } \\ \text { PER1OD } \\ \text { (SEC) } \end{array}$ | $\begin{gathered} \left(\tilde{\tau}_{w}\right) 1 / 3 \\ (f t) \end{gathered}$ | MODAL PERIOD (SEC) |
| 8 | 12 | 6 | 10 | 7 | 11 | 5 | 5.5 | 4 | 5. | 4 | 4.5 | 4 | 5 | 9 | 12 | 4 | 5 |
| 12 | 13 | 8 | 1.1 .5 | 9 | 12 | 6 | 6 | 6 | 5.5 | 5 | 5 | 5 | 6 | 11 | 14 | 5 | 5.5 |
| 16 | 14 | 10 | 12.5 | 10 | 12.5 | 9 | 6.5 | 8 | 6.5 | 6 | 5.5 | 6 | 7 | 13 | 14.5 | 6 | 6 |
| 19 | 15 | 12 | 13 | 11 | 12.5 | 10 | 7 | 9 | 7 | 8 | 5.5 | 6.5 | 8 | 15 | 15 | 8 | 6.5 |
| 27 | 20 | 17 | 14 | 16 | 13.5 | 11 | 8 | 12 | 8.5 | 9 | 6 | 7 | 8.5 | 19 | 15.5 | 10 | 7.5 |
| 31 | 25 | 19 | 14 | 18 | 14 | 13 | 8.5 | 14 | 9 | 9 | 6 | 8 | 9 | 21 | 16 | 11 | 8 |
| 35 | 30 | 22 | 14 | 20 | 14 | 15 | 8.5 | 15 | 9.5 | 10 | 7 | - | - | 23 | 16.5 | - | - |
| 39 | 36 | 24 | 14.5 | 23 | 14 | 16 | 9 | - | - | - | - | - | $\rightarrow$ | 26 | 17 | - | - |
| 43 | 39 | 28 | 15 | 28 | 15 | 1.7 | 9.5 . | - | - | - | - | - | - | 29 | 17 | - | - |
| 47 | 45 | 32 | 15.5 | 34 | 16 | - | - | - | - | - | - | - | - | 33 | 17.5 | - | - |
| 51 | 51 | 36 | 16 | 39 | 16.5 | - | - | - | - | - | - | - | - | 36 | 18 | - | - |

TABLE 9 - (Cont inued)

|  | CATION | I |  | J |  | $k$ |  | L |  | M |  | $N$ |  | 0 |  | P |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| WIND SPEED (KTS) | MAX WAVE HE'I GHT ( ft ) | $\begin{gathered} \left(\tilde{\zeta}_{w}\right) 1 / 3 \\ (f t) \end{gathered}$ |  | $\left(\tilde{\zeta}_{w}\right) 1 / 3$ <br> (f.t) | MODAL PERIOD (SEC) | $\left(\tilde{\zeta}_{w}\right) 1 / 3$ <br> (ft) | MODAL PERIOD (SEC) | $\begin{aligned} & \left(\Sigma_{w}\right) 1 / 3 \\ & (\mathrm{ft}) \end{aligned}$ | $\begin{gathered} \text { MODAL } \\ \text { PERIIOD } \\ \text { (SEC) } \end{gathered}$ | $\left(\dot{c}_{w}\right) 1 / 3$ <br> ( ft ) | $\begin{aligned} & \text { MODAL } \\ & \text { PERIOD } \\ & \text { (SEC) } \end{aligned}$ | $\begin{gathered} \left(\tilde{r}_{w}\right) 1 / 3 \\ (f t) \end{gathered}$ | $\begin{array}{\|c} \text { MODAL } \\ \text { PERIOD } \\ \text { (SEC) } \end{array}$ | $\left(\tilde{\zeta}_{w}\right) 1 / 3$ <br> (ft) | MODAL PERIOD (SEC) | $\begin{aligned} & \left(\bar{s}_{w}\right) 1 / 3 \\ & (f t) \end{aligned}$ | MODAL PERIOD (SEC) |
| 8 | 12 | 2 | 4.5 | 9 | 13 | 9 | 12.5 | 5 | 11.5 | 9 | 13 | 11 | 13 | 6 | 12 | 6 | 12 |
| 12 | 13 | 3 | 5 | 11 | 14 | 11 | 13 | 7 | 11.5 | 11 | 13.5 | 12 | 13.5 | 7 | 12 | 7 | 12 |
| 16 | 14 | 5 | 5.5 | 13 | 14.5 | 12 | 13.5 | 8 | 12 | 13 | 14 | 12 | 13.5 | 8 | 12.5 | 8 | 12.5 |
| 19 | 15 | 6 | 6 | 14 | 14.5 | 13 | 13.5 | 9 | 12 | 14 | 14 | 14 | 14 | 10 | 13 | 10 | 13 |
| 27 | 20 | 8 | 6.5 | 16 | 15 | 16 | 14.5 | 13 | 12.5 | 17 | 14.5 | 18 | 14.5 | 14 | 14 | 15 | 14 |
| 31 | 25 | - | - | 18 | 15 | 19 | 15 | 14 | 13 | 20 | 14.5 | 2.1 | 15 | 17 | 14 | 18 | 15 |
| 35 | 30 | - | - | 20 | 15.5 | 22 | 15 | 16 | . 13 | 22 | 15 | 23 | 15.5 | 19 | 14 | 21 | 15.5 |
| 39 | 36 | - | - | 22 | 16 | 26 | 1.5 .5 | 17 | 13 | 25 | 15.5 | 26 | 15.5 | 22 | 14.5 | 24 | 15.5 |
| 43 | 39 | - | - | 25 | 16.5 | 31 | 16.5 | 18 | 13.5 | 29 | 16 | 31 | 16.5 | 28 | 15 | 29 | 16 |
| 47 | 45 | - | - | 29 | 17 | 37 | 17 | - | - | 33 | 17 | 38 | 17 | 33 | 16 | - | - |
| 51 | 51 | - | - | 33 | 17.5 | 42 | 17.5 | - | - | 36 | 17.5 | 43 | 17.5 | 38 | 17 | - | - |

table 10 - most probable wind speed and significant wave height by wind direction

TABLE 10 - (Continued)

TABLE 10 －（Continued）

|  | 앙 | $m$ | N | $\cdots$ | $\underset{\sim}{\infty}$ | ニ | $\simeq$ | $n$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 宕 | $\infty$ | $N$ | の | m | N | $\pm$ | の | $\bullet$ |
|  | $\infty$ | $N$ | ก | $\stackrel{n}{ }$ | $\mathfrak{\sim}$ | $\underline{\sim}$ | $\cdots$ | N |
| 돌 | $\cdots$ | $\sim$ | 2 | $\pm$ | $\stackrel{\sim}{\sim}$ | $\because$ | $\pm$ | $n$ |
| 気 W 5 en | $\sim$ | $\sim$ | $\stackrel{\sim}{n}$ | $\underline{m}$ | 9 | m | m | $N$ |
| 宕 | $\bigcirc$ | $\sim$ | $\pm$ | m | －． | $\pm$ | m | N |
|  | 응 | m | $\simeq$ | $\simeq$ | ～ | $\pm$ | $=$ | $\cdots$ |
| $\begin{aligned} & \text { 들 } \\ & \text { 旁 } \end{aligned}$ | $=$ | $m$ | $\pm$ | m | $\stackrel{\sim}{\sim}$ | $\pm$ | m | $n$ |
| $\stackrel{\text { 증 }}{\frac{0}{2}}$ | 을范范 | $\stackrel{E}{m}_{v^{3}}^{4}$ |  | $\stackrel{m}{n}_{5_{3}^{3}}^{4}$ | 을 | $\stackrel{m}{2}_{v^{3}}^{4}$ | 을 品范 | ${\underset{N}{m}}_{N^{3}}^{4}$ |
| 즟 | ． |  |  |  |  |  |  |  |

TABLE 10 - (Continued)



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[^0]:    *Bales, S.L. and J.M. Voelker, "Sea Environment Manual for Ship Design," Report DTNSRDC/SPD-0720-01 (to be published in 1980).

    NAA complete listing of references is given on page 11.
    ***The Ship Designer's Atlas is being developed under the cognizance of the Naval Sea Systems Command (NAVSEA) for purposes of Combatant Capability Assessment (CCA).

[^1]:    Worst month is defined to be that in which the wind speeds and wave heights are statistically most severe.

